

DOLPHIN GEOLOGICAL RESOURCE AND MINING RESERVE AS AT 1/1/1981

| OREBODY | AREA | MINING METHOD | PROVEN | | | | | | | | | | PROBABLE | | | | | | | | | | POSSIBLE | TOTAL PROVEN + PROBABLE | | | | | | | | | | | | | | | | | | |
|-------------|---------------------------|---------------|----------|---------------|------------|------------|---------------------|------------------|---------------------------|------------------|----------|------------------|----------|------------------|---------------|----------|---------------|------------|---------------------|---------|---------------------------|--------|----------|-------------------------|--------|------------------|--------|---------------------|--------|------------------|--------|------------------|--------|------------------|--------|------------------|--|--|--|--|--|--|
| | | | FACTORS | | | | GEOLOGICAL RESOURCE | | RESOURCE IN MAJOR PILLARS | | RESOURCE | | RESERVE | | FACTORS | | | | GEOLOGICAL RESOURCE | | RESOURCE IN MAJOR PILLARS | | | RESOURCE | | RESERVE | | GEOLOGICAL RESOURCE | | RESOURCE | | RESERVE | | | | | | | | | | |
| | | | PILLAR % | MINEABILITY % | RECOVERY % | DILUTION % | TONNES | %WO ₃ | TONNES | %WO ₃ | TONNES | %WO ₃ | TONNES | %WO ₃ | PROBABILITY % | PILLAR % | MINEABILITY % | RECOVERY % | DILUTION % | TONNES | %WO ₃ | TONNES | | %WO ₃ | TONNES | %WO ₃ | TONNES | %WO ₃ | TONNES | %WO ₃ | TONNES | %WO ₃ | TONNES | %WO ₃ | TONNES | %WO ₃ | | | | | | |
| SOUTHERN | 150-200 | CUT & FILL | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | pgH | | | | | | | | | | | | | 90 | 15 | 85 | 90 | 20 | pgH | | | | | | | | | | | | | | | | | | | | | |
| | | | U/C | | | | | | | | | | | | | | | | | U/C | 26,400 | 0.52 | | | 26,400 | 0.52 | 21,800 | 0.43 | 14,700 | | | | | | | | | | | | | |
| | | | L/C | | | | | | | | | | | | | | | | | L/C | | | | | | | | | | | | | | | | | | | | | | |
| | | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | | | | | | | | | | | | | | | | | | | | | | |
| 200-250 | POST PILLAR | pgH | | | | | | | | | | | | | 90 | 18.35 | 81.65 | 80 | 20 | pgH | | | | | | | | | | | | | | | | | | | | | | |
| | | U/C | | | | | | | | | | | | | | | | | U/C | 83,700 | 1.15 | | | 83,700 | 1.15 | | | 14,700 | | | | | | | | | | | | | | |
| | | L/C | | | | | | | | | | | | | | | | | L/C | 40,600 | 0.77 | | | 40,600 | 0.77 | | | 9,200 | | | | | | | | | | | | | | |
| | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | 124,300 | 1.03 | | | 124,300 | 1.03 | 87,700 | 0.88 | 23,900 | | | | | | | | | | | | | | |
| BELOW 250 | POST PILLAR | pgH | | | | | | | | | | | | | 90 | 18.35 | 81.65 | 80 | 20 | pgH | | | | | | | | | | | | | | | | | | | | | | |
| | | U/C | | | | | | | | | | | | | | | | | U/C | 79,500 | 1.15 | | | 79,500 | 1.15 | | | 92,400 | | | | | | | | | | | | | | |
| | | L/C | | | | | | | | | | | | | | | | | L/C | 9,700 | 0.77 | | | 9,700 | 0.77 | | | 56,000 | | | | | | | | | | | | | | |
| | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | 89,200 | 1.11 | | | 89,200 | 1.11 | 62,900 | 0.93 | 98,000 | | | | | | | | | | | | | | |
| TOTAL | | pgH | | | | | | | | | | | | | | | | | pgH | | | | | | | | | | | | | | | | | | | | | | | |
| | | U/C | | | | | | | | | | | | | | | | | U/C | | | | | | | | | | | | | | | | | | | | | | | |
| | | L/C | | | | | | | | | | | | | | | | | L/C | | | | | | | | | | | | | | | | | | | | | | | |
| | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | 239,900 | 1.00 | | | 239,900 | 1.00 | 172,400 | 0.83 | 176,200 | | | | | | | | | | | | | | |
| PIT DAG | 150-200 | OPEN STOPING | | | | | | | | | | | | | 90 | | 100 | 90 | 15 | | | | | | | | | | | | | | | | | | | | | | | |
| | | | pgH | 100 | 90 | 15 | | | | | | | | | | | | | pgH | | | | | | | | | | | | | | | | | | | | | | | |
| | | | U/C | | | | | | | | | | | | | | | | | U/C | 17,600 | 0.80 | | | 17,600 | 0.80 | 18,200 | 0.70 | | | 61,400 | 0.69 | 55,200 | 0.61 | | | | | | | | |
| | | | L/C | | | | | | | | | | | | | | | | | L/C | | | 2700 | 0.62 | 39,700 | 0.64 | 37,000 | 0.56 | | | | | | | | | | | | | | |
| | | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | 42,000 | 0.64 | 2700 | 0.62 | 39,700 | 0.64 | 37,000 | 0.56 | 61,400 | 0.69 | 55,200 | 0.61 | | | | | | | | | | |
| BELOW 200 | | pgH | | | | | | | | | | | | | | | | | pgH | | | | | | | | | | | | | | | | | | | | | | | |
| | | U/C | | | | | | | | | | | | | | | | | U/C | 1,700 | 0.80 | | | | | | | | | | | | | | | | | | | | | |
| | | L/C | | | | | | | | | | | | | | | | | L/C | REMNANT | | | | NIL | | | | | | | | | | | | | | | | | | |
| | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | 19,300 | 0.80 | | | | | | | | | | | | | | | | | | | | | |
| B LENS | WEDGE DECLINE CENTRAL PIT | pgH | | | | | | | | | | | | | 90 | 15 | 85 | 75 | 20 | pgH | 240,000 | 0.75 | 55,400 | 0.57 | ? | 0 | 89,500 | 0.72 | 20,000 | | | | | | | | | | | | | |
| | | U/C | | | | | | | | | | | | | | | | | U/C | 337,700 | 0.74 | | | 337,700 | 0.74 | 272,500 | 0.62 | 107,000 | | | | | | | | | | | | | | |
| | | L/C | | | | | | | | | | | | | | | | | L/C | 110,200 | 0.97 | 7,000 | 0.95 | | | 66,500 | 0.80 | 110,200 | | | | | | | | | | | | | | |
| | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | 460,900 | 0.94 | 62,400 | 0.95 | | | 550,000 | 0.85 | 9,000 | 0.94 | | | | | | | | | | | | | |
| SOUTHERN | TOTAL | pgH | | | | | | | | | | | | | | | | | pgH | 24,400 | 0.80 | | | | | 16,200 | 0.67 | | | | | | | | | | | | | | | |
| | | U/C | | | | | | | | | | | | | | | | | U/C | | | | | | | | | | | | | | | | | | | | | | | |
| | | L/C | | | | | | | | | | | | | | | | | L/C | | | | | | | | | | | | | | | | | | | | | | | |
| | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | 720,900 | 0.78 | 62,400 | 0.61 | 62,400 | 0.66 | 410,800 | 0.68 | 720,900 | 0.78 | 406,500 | 0.65 | | | | | | | | | | | |
| SUB-TOTAL : | | pgH | | | | | | | | | | | | | | | | | pgH | | | | | | | | | | | | | | | | | | | | | | | |
| | | U/C | | | | | | | | | | | | | | | | | U/C | | | | | | | | | | | | | | | | | | | | | | | |
| | | L/C | | | | | | | | | | | | | | | | | L/C | | | | | | | | | | | | | | | | | | | | | | | |
| | | TOTAL | | | | | | | | | | | | | | | | | TOTAL | | | | | | | | | | | | | | | | | | | | | | | |

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