

TR19_84_90

9. Seismic survey at the Australian Commonwealth Carbide Company Works, Electrona.

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A seismic survey was undertaken for a feasibility study for new furnaces and buildings at the Electrona works at the request of K. Steinman of Crooks Michell Peacock Stewart Pty Ltd, engineers, architects and planners of Chatswood, New South Wales.

Seven spreads and two weathering spreads were fired at the proposed site. The location of these spreads is shown in Figure 20. The geophone spacing was 7.6 m for the first five spreads but it was reduced to 3 m for the remaining two spreads owing to the close proximity of the office building. The two weathering spreads were 15 m in length.

The carbide works are situated on a promontory north of Snug village. Triassic sandstone crops out along the foreshore and low cliffs north of the Snug Rivulet. Grey and brown clays were exposed in two exploration pits near the south-western corner fence of the works. Some very deeply weathered Triassic mudstone and, or, Tertiary clay is partly exposed in a disused clay pit at the western end of the low cliff line.

GEOPHYSICAL WORK

The seismic results are summarised in Table 1. The area is a particularly difficult one for seismic interpretation as there are large areas of fill (limestone, furnace slag, etc.) which may or may not overlie clay and sand. The clay and sand are probably derived from the very deep weathering and decomposition of the underlying sandstone and mudstone of Triassic age, although the possible presence of Tertiary clay and sand cannot be overlooked.

The clay and sand overlie deeply weathered Triassic sandstone and mudstone with a gradual transition to the unweathered parent rock. There is no precise boundary separating the various degrees of weathering in these sediments and consequently the interface between the seismic velocity layers is unlikely to coincide with weathering zones in the sandstone and mudstone. The slope of many of the interfaces leads to further imprecision in the calculation of seismic velocities and interface depths.

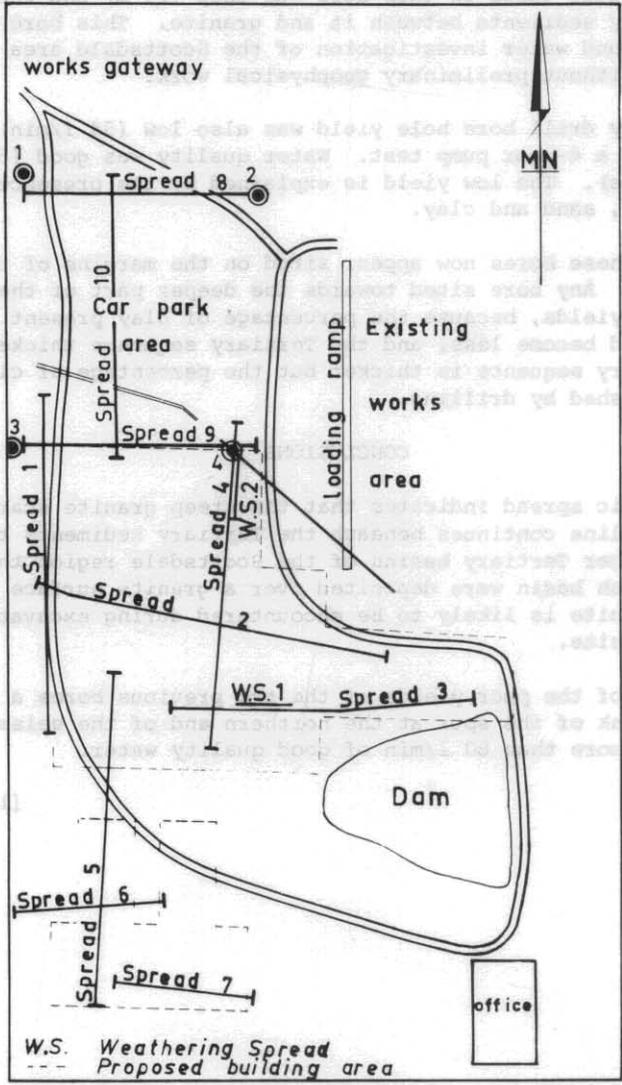
In the south-west corner of the site area the surface velocity layer (V_0) is the clay exposed in the two shallow clay pits. Its velocity (610 m/s) is the same as that recorded for the two weathering spreads which are located in areas of fill. Spread 1 was fired along the western boundary road of the works, and appears to be the only spread where the bedrock occurs at shallow depth. In all the other spreads the depth to bedrock is calculated as 10-18.3 m, where bedrock is defined as rock with a velocity of 1525 m/s or higher.

Even allowing for possible errors in the calculation of the seismic results there appears little doubt that much of the area is unsuitable for bearing heavy structures such as furnaces and will require further investigation.

CONCLUSIONS AND RECOMMENDATIONS

Even at this early stage of the feasibility study it appears that further drilling and geophysical investigation will be required for any site evaluation. It is recommended that two holes to a minimum depth of 15 m be drilled and cored. These holes should be located at the intersections of

The yield from the percussion bore was low, less than 7 litres being
 bailed from the bore. The water quality was high (78 ppm total dissolved
 solids). The water table in the bore was 1.5 m below the ground surface
 (12 m of water was bailed between 11 and 12 noon). This bore was sited fairly
 in the distance from the investigation of the dam. The bore was sited fairly
 in the distance from the investigation of the dam.



Positions of seismic spreads, Electrona; for seismic profiles see Figure 20 (in pocket).

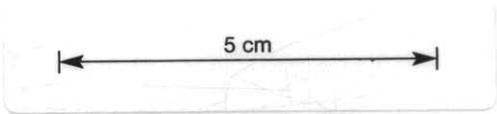


Table 1. SEISMIC RESULTS

Spread No.	Layer	Velocity (m/s)	Interface Depth (m)	Slope	Geological interpretation of the velocity layers	Remarks			
1	V ₀	610	$\frac{V_0}{V_1}$ 4.6-6.1	Nil	Fill and clay.				
	V ₁	1830					Weathered Triassic sediments.		
2	V ₀	610-915	$\frac{V_0}{V_1}$ 4.6-7.6	8-10° to E.	Clay and fill.	The slope of the interface down to the east and differing velocity layering at the ends of the spread is possibly due to the infilling of the natural gullying combined with deeper weathering at the lower levels of the valley.			
	West End V ₁	1525					$\frac{V_1}{V_2}$ 13.7-18.3	As above.	Weathered and decomposed Triassic sediments.
	V ₂	2135	Unweathered Triassic sediments.						
	East End V ₁	2135		$\frac{V_1}{V_2}$ 24.4-26.0	Slope to E not as apparent as at W end.		Unweathered but stained Triassic sediments.		
V ₂	3050	Consolidated Triassic sediments.							
3	V ₀	915	$\frac{V_0}{V_1}$ 10.6-14.0	Slight slope to E.	Clay and, or, fill.				
	V ₁	1525-1830					$\frac{V_1}{V_2}$ 28.9-30.5	No apparent slope.	Weathered Triassic sediments.
	V ₂	3660							
4	V ₀	610	$\frac{V_0}{V_1}$ 5.2-6.1	Nil	Fill	The level interfaces of this spread and depth to bedrock indicates a considerable amount of infilling.			
	V ₁	915-1220					$\frac{V_1}{V_2}$ 12.2-13.7	Clay and deeply weathered and decomposed Triassic sediments.	
	V ₂	1830-2135							Stained but unweathered Triassic sediments.

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Table 1. (continued)

Spread No.	Layer	Velocity (m/s)	Interface Depth (m)	Slope	Geological interpretation of the velocity layers	Remarks
5	V ₀	610	$\frac{V_0}{V_1}$	Slope to S.	Clay	Velocity interfaces are transitional.
	V ₁	1220-1525	$\frac{V_1}{V_2}$			
	V ₂	3050		12.2-13.7	No apparent slope on lower interface.	
6	V ₀	610	$\frac{V_0}{V_1}$	6° to W.	Clay.	Slope of the interface and absence of sharp velocity contrasts make depths only approximate.
	V ₁	915	$\frac{V_1}{V_2}$			
	V ₂	1830		10.4-11.3	Slight slope to W.	
7	V ₀	610	$\frac{V_0}{V_1}$	Slight slope to W.	Clay	Transitional V ₀ /V ₁ velocities.
	V ₁	1220	$\frac{V_1}{V_2}$			
	V ₂	2135		10.4-11.6	Sand and clay and, or, decomposed Triassic sediments. Unweathered Triassic sediments.	
Weathering Spread 1	V ₀	610				
	V ₁	915-1067				
2	V ₀	610				
	V ₁	915				

seismic lines 2 and 4, and 5 and 6. These drill holes would allow for the seismic velocity layering to be compared with lithology. The holes could then be used as a control for a resistivity survey. The clay and rock fill should give differing apparent resistivity and it may be possible to draw resistivity contours by the use of resistivity sounding and traversing. This would enable further information to be secured at little cost before undertaking extensive drilling for a detailed site feasibility study.

[4 October 1974]

APPENDIX 1

Second seismic survey.

At the request of the consulting engineers further seismic investigation was carried out at the Electrona works on 6-8 March. The investigation was made in the car park area, north of the area previously investigated.

GEOPHYSICAL WORK

Two E-W spreads (8 and 9) were to be fired between four proposed drill holes with a N-S cross spread (10). The geophone interval for all spreads was 6.1 m. The distance which shots could be extended from the geophone line was restricted and the amount of explosive which could be used was limited because of the amount of fly-rock occurring on firing. The fly-rock was mainly of limestone boulders which formed a thick surface layer to the car park. Even when the shot holes were 4 m deep and penetrated to the underlying clay the limestone boulders still flew to a distance of up to 30 m. Even using blast mats this survey was very difficult to execute because of danger to personnel and close proximity to buildings.

The results of these three further spreads are summarised in Table 2. As indicated in the previous survey no 'hard bed' was found close to the surface on which the blast furnaces could be sited. The seismic velocities and layering indicated that beneath the surface layer of fill was a thick layer of clay, sand and soft sandstone of Tertiary age overlying soft, deeply weathered, Triassic sandstone and mudstone. Bedrock of unweathered Triassic sandstone and mudstone with seismic velocities in excess of 3 000 m/s was not found, and must occur below depths of 16-21 m.

DRILLING

Subsequent drilling on the site by Davies and Moore, foundation investigation engineers, confirmed the seismic results. Eight holes were drilled using a Gemco auger and diamond rig and a Failing 800 rotary rig. The location of four of these is known to the writer who has seen briefly the core of some of them. The core from Bore 4, which was completed before the seismic work was finished was examined at greater length.

Bore 4 encountered a top layer, 3.5 m thick, consisting of fill, sand and sandy clay with one cemented band; a Permian mudstone boulder was also found. Soft Tertiary sand and sandstone continued to a depth of 14.3 m. No core was recovered between 14.3 and 14.9 m. Below 14.9 m to a depth of 20 m white graphitic and micaceous well bedded Triassic sandstone was encountered. The sandstone was soft, deeply weathered and stained, and had a bedding dip of 10°.

Bore 1 followed a similar sequence of fill, Tertiary sand and clay and white Triassic sandstone with similar depths as Bore 4.

In Bore 2 the Triassic sediments consisted of carbonaceous mudstone with minor sandstone (Cynet Coal Measures) and occurred between 18-21 m.

Bore 3 Tertiary sediments continued to 18 m and no Triassic sediments were encountered.

The only other core seen was from Bore 8A which was drilled to 7.3 m in Tertiary sand and clayey sandstone.

CONCLUSIONS

The drilling confirmed the presence of a Tertiary valley that traversed the Electrona works area. In this valley are Tertiary sand and clay which were probably overlain by basalt that has since been removed by erosion leaving only the silcrete boulders on the surface, one of which was encountered within one metre of the surface in Bore 8 causing the hole to be abandoned. This Tertiary valley was eroded into Triassic sandstone and mudstone which are soft and deeply weathered. This weathering probably occurred during Tertiary times.

[20 June 1975]

Bore	Interval (m)	Depth (m)	Notes
10 (B-8)	18.0-21.0	18.0	Triassic mudstone
	18.0-19.0	18.5	Triassic mudstone
	18.0-19.0	19.0	Triassic mudstone
	18.0-19.0	19.5	Triassic mudstone
8 (B-8)	7.0-7.3	7.15	Tertiary sandstone
	7.0-7.3	7.3	Tertiary sandstone
	7.0-7.3	7.45	Tertiary sandstone
	7.0-7.3	7.6	Tertiary sandstone

Table 2. RESULTS OF SECOND SEISMIC SURVEY

Spread No.	Length (m)	Velocity (m/s)	Interface Depth (m)	Slope	Geological interpretation of the velocity layers	Remarks	
8 (E-W)	116	<i>West End</i>					
		V ₀ 915					
		V ₁ 1525-2135	$\frac{V_0}{V_1}$	9.1-13.7	Upper layer thickens to W.	Fill and clay. Tertiary and soft, deeply weathered Triassic sediments.	No hard bedrock. No seismic velocities >3000 m/s detected in the spread. No bedrock anticipated before 16 m.
		<i>East End</i>					
9 (E-W)	128	V ₀ 1065					
		V ₁ 1525-1830	$\frac{V_0}{V_1}$	6.1-9.1	No slope	Fill and clay. Tertiary and soft, deeply weathered Triassic sediments.	With flyrock likely to fall on the existing works the eastern shot point was located in drill hole 2 at a depth of 5 m. This reduced the calculated thickness of the surface layer and the depth to the underlying layers. No bedrock anticipated at depths of <16-18 m.
		<i>East End</i>					
		V ₀ 1065					
V ₁ 1525-1830	$\frac{V_0}{V_1}$	6.8-8.5					
10 (N-S)	128	V ₀ 1065-1220					
		V ₁ 1830-2130	$\frac{V_0}{V_1}$	9.1-10.9	No slope.	Fill and clay. Tertiary and soft, deeply weathered Triassic sediments.	No bedrock detected. Depth to bedrock layer is probably more than 21 m.

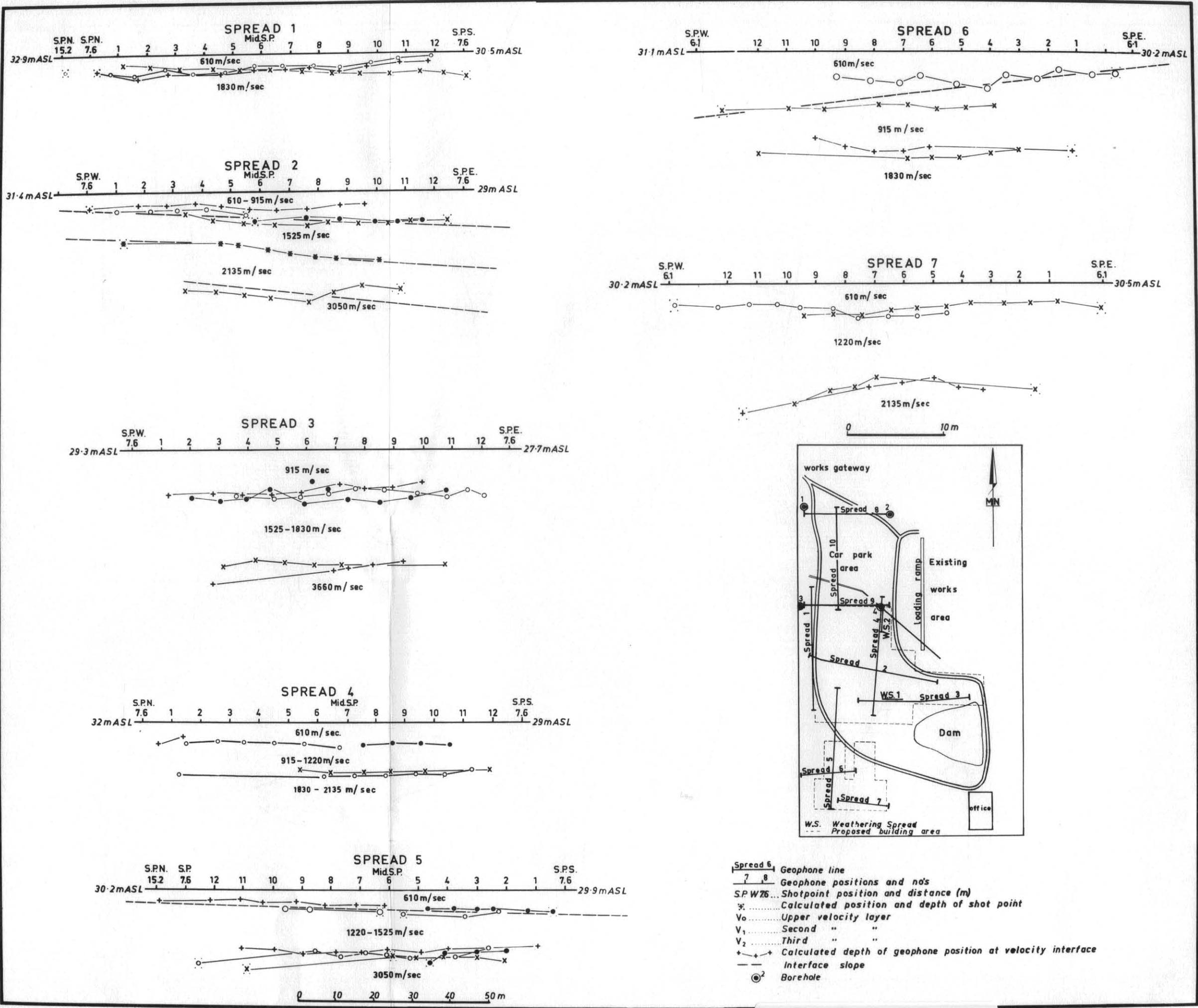


Figure 20. Electrona seismic survey.