

27/8/48

THE MT. NASSAU (RATHBONES) LIMESTONE QUARRY

The Mt. Nassau Limestone Quarry is situated about half a mile south from the Lyell Highway and about 13 miles from Hobart. It is at present being operated by the estate of Mr. K. R. Rathbone for the production of quicklime which is burnt in kilns situated at the Main Highway.

In the year 1928 Mr. P.B. Nye, Government Geologist, reported on the property at Mt. Nassau, then referred to as Mr. Rathbone's property. Nye records the geological sequence and allots a thickness of approximately 200 feet to the Limestone beds which occur as the mid-section of the Permian strata. Nye states that "the stone is quarried and burnt for the production of quicklime", but has not given any analyses of samples of the stone.

Quarrying has been carried out on each side of Quarry Creek. From the excavations it is noted that the beds are dipping at a low angle towards the west of south west. The excavations have been carried forward until a maximum depth of about 45 feet has been reached.

On the eastern side of the creek an excavation has been made of a total length of approximately 1,200 feet with an average width of 60 feet. The maximum height of the quarry wall is 45 feet but the average depth of excavation would not exceed 16 feet. It is evident that the difficulty experienced in removing the spoil has been a controlling factor in closing this quarry for large quantities have been stocked within the limits of the excavation and access to the working faces without its removal would be difficult.

2.

Present quarrying operations are being carried out on the western side of the creek. The excavation here measures about 650 feet in length with an average width of about 45 feet. The maximum height of the quarry wall is 35 feet but the average height would not exceed 24 feet. As these workings are progressing in a westerly direction the floor is becoming lower and as the quarry advances increasing difficulty in the removal of water must be expected.

The limestone of the quarry is well bedded in tiers ranging in thickness from 9 inches to 27 inches. The tiers are separated from each other by bands of calcareous shales ranging to 27 inches in thickness. The present working face has a total height of 35 feet of which approximately 11 feet is represented by shaly bands which have to be excluded as spoil. After quarrying, the stone from the tiers is broken by spalling to a size for convenient loading by hand and at the same time a proportion of the stone is discarded as spoil in the belief that its quality is such as to prevent complete burning in the kilns.

It is doubtful, therefore, whether the present operations yield more than 25% of the stone excavated as a product for the kilns and it is obvious that the quarry now idle did not yield a high proportion when operating. As the amount of overburden in the present quarry is increasing with depth the position appears to be becoming uneconomic for a progressively lower proportion of the product will reach the kilns.

For the purpose of this examination all the tiers in the present quarry were sampled as also were the principal shaly bands. A number of the tiers in the idle quarry were also sampled. The product at

the kiln site was also sampled to determine the grade of the kiln feed. In all 39 samples were taken and when sampling in the quarry all the stone from the tiers was included in the sample and there was no discard as occurs in practice. The analyses of the 39 samples is included herewith, and for purposes of comparison a number of analyses of samples recorded in 1929 as from the same quarry is also attached. Samples 19 to 22 inclusive represent the analyses of the principal shaly bands.

(see pages 4,5, and 6.)

4.  
ANALYSES OF SAMPLES OF MT. NASSAU LIMESTONES

| PER CENT   |                  |                                |                                |      |     |               |
|------------|------------------|--------------------------------|--------------------------------|------|-----|---------------|
| Sample No. | SiO <sub>2</sub> | Fe <sub>2</sub> O <sub>3</sub> | Al <sub>2</sub> O <sub>3</sub> | CaO  | MgO | Ignition Loss |
| 1          | 19.9             | 0.9                            | 1.8                            | 42.0 | 0.7 | 33.5          |
| 2          | 21.7             | 0.9                            | 1.8                            | 41.2 | 0.6 | 32.8          |
| 3          | 19.1             | 0.2                            | 2.1                            | 42.8 | 0.4 | 34.2          |
| 4          | 21.5             | 0.8                            | 2.6                            | 40.4 | 0.8 | 32.9          |
| 5.         | 34.4             | 0.9                            | 3.1                            | 33.0 | 0.6 | 26.7          |
| 6          | 18.7             | 0.4                            | 1.5                            | 43.4 | 0.4 | 34.6          |
| 7          | 33.1             | 1.3                            | 2.5                            | 34.1 | 0.5 | 27.6          |
| 8          | 15.6             | 0.7                            | 1.3                            | 45.4 | 0.6 | 36.3          |
| 9          | 21.4             | 0.9                            | 2.5                            | 40.7 | 0.6 | 33.0          |
| 10         | 41.8             | 2.2                            | 5.8                            | 25.1 | 0.9 | 21.8          |
| 11         | 23.4             | 1.1                            | 2.8                            | 39.3 | 0.7 | 32.0          |
| 12         | 33.3             | 1.3                            | 2.9                            | 33.4 | 0.6 | 27.6          |
| 13         | 29.3             | 1.2                            | 3.7                            | 34.9 | 0.5 | 28.8          |
| 14         | 52.9             | 2.0                            | 7.2                            | 17.5 | 0.7 | 15.5          |
| 15         | 44.6             | 1.9                            | 4.7                            | 24.6 | 0.6 | 20.8          |
| 16         | 31.0             | 1.2                            | 4.2                            | 33.1 | 0.7 | 27.3          |
| 17         | 27.0             | 1.1                            | 3.5                            | 36.3 | 0.6 | 29.8          |

A composite made up from the above samples  
 showed the presence of P<sub>2</sub>O<sub>5</sub> : 0.1% and MnO : 0.02%

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ANALYSES OF SAMPLES OF MT. NASSAU LIMESTONES

| Sample No. | SiO <sub>2</sub> | Fe <sub>2</sub> O <sub>3</sub> | Al <sub>2</sub> O <sub>3</sub> | CaO   | MgO  | Ignition Loss |
|------------|------------------|--------------------------------|--------------------------------|-------|------|---------------|
| 18         | 43.2             | 2.0                            | 4.8                            | 24.3  | 0.6  | 20.9          |
| 19         | 53.8             | 3.1                            | 11.7                           | 10.7  | 1.2  | 12.5          |
| 20         | 54.2             | 2.8                            | 9.5                            | 13.1  | 1.2  | 13.0          |
| 21         | 59.5             | 3.6                            | 10.3                           | 8.9   | 1.2  | 10.4          |
| 22         | 50.2             | 3.4                            | 9.9                            | 15.0  | 1.1  | 14.9          |
| 23         | 25.3             | 1.0                            | 1.8                            | 38.7  | 0.7  | 31.3          |
| 24         | 17.6             | 0.6                            | 1.2                            | 44.1  | 0.5  | 35.5          |
| 25         | 30.4             | 0.9                            | 4.1                            | 33.0  | 0.8  | 27.1          |
| 26         | 28.4             | 0.9                            | 2.0                            | 36.6  | 0.7  | 29.8          |
| 27         | 22.6             | 2.0                            | 1.8                            | 40.0  | 0.7  | 32.5          |
| 28         | 24.3             | 0.9                            | 1.7                            | 39.0  | 0.6  | 31.8          |
| 29         | 30.0             | 1.0                            | 2.1                            | 35.5  | 0.6  | 28.9          |
| 30         | 29.5             | 1.0                            | 2.0                            | 36.0  | 0.6  | 29.2          |
| 31         | 41.2             | 1.7                            | 5.0                            | 25.5  | 1.0  | 22.2          |
| 32         | 16.9             | 0.6                            | 2.0                            | 43.0  | 0.9  | 35.1          |
| 33         | 30.0             | 1.3                            | 4.2                            | 33.0  | 0.9  | 27.9          |
| 34         | 26.0             | 1.4                            | 2.2                            | 37.2  | 0.8  | 30.7          |
| 35         | 42.6             | 1.6                            | 5.8                            | 24.8  | 1.0  | 21.3          |
| 36         | 29.2             | 1.1                            | 2.4                            | 35.9  | 0.6  | 29.9          |
| 37         | 31.3             | 1.1                            | 3.1                            | 34.2  | 0.7  | 28.5          |
| 38         | 26.50            | 1.14                           | 2.51                           | 36.80 | 0.70 | 30.40         |
| 39         | 24.88            | 1.00                           | 1.82                           | 38.80 | 0.66 | 31.72         |

ANALYSES OF MT. NASSAU LIMESTONES (1929)

| CaCO <sub>3</sub> | MgCO <sub>3</sub> | MgO  | SiO <sub>2</sub> | Fe <sub>2</sub> O <sub>3</sub> | Fe <sub>2</sub> O <sub>3</sub><br>Al <sub>2</sub> O <sub>3</sub> | Al <sub>2</sub> O <sub>3</sub> | P <sub>2</sub> O <sub>5</sub> | SO <sub>3</sub> | H <sub>2</sub> O | Ignition<br>Loss |
|-------------------|-------------------|------|------------------|--------------------------------|--|--------------------------------|-------------------------------|-----------------|------------------|------------------|
| 59.89             | -                 | 1.09 | 31.40            | -                              | 1.79   | 4.45                           | -                             | -               | -                | -                |
| 86.40             | -                 | 0.72 | 10.32            | -                              | 0.91   | 2.27                           | -                             | -               | -                | -                |
| 68.90             | -                 | 1.09 | 25.40            | -                              | 1.29   | 3.39                           | -                             | -               | -                | -                |
| 68.93             | -                 | 0.36 | 26.64            | -                              | 1.86   | 2.54                           | -                             | -               | -                | -                |
| 70.70             | -                 | 0.24 | 23.56            | -                              | 2.14   | 3.74                           | -                             | -               | -                | -                |
| 63.60             | -                 | 0.50 | 30.04            | -                              | 1.86   | 4.50                           | -                             | -               | -                | -                |
| 78.49             | -                 | 0.60 | 17.60            | -                              | 1.60   | 2.40                           | -                             | -               | -                | -                |
| 63.26             | -                 | 1.01 | 29.72            | -                              | 1.56   | 2.64                           | -                             | -               | -                | -                |
| 65.26             | -                 | 1.23 | 27.28            | -                              | 1.64   | 2.7                            | -                             | -               | -                | -                |

Reference to the Analysis shows that the Kiln feed (samples 38,39) have a Calcium Carbonate content of approximately 69%. This grade has been gained by selective methods which have resulted in the discard of a large proportion of the stone quarried. It will also be noticed that several of the tiers of stone have yielded an analyses of a higher grade than the Kiln feed.

The following table shows the analyses of the tiers in their essentials only, i.e., Silica, Lime and Loss on Ignition. The progressive average grade of stone for 9,11,13,15 etc. tiers has also been calculated and recorded.

The average grade of stone for the first (bottom) nine tiers contains 72% of CaO and Ignition Loss, recorded here as CaCO<sub>3</sub> as compared with 69% for the Kiln feed. Similarly for 11 tiers and 13 tiers the grade is 68.9% and 65.2% respectively. The two latter figures are in excess of sample 38 and only slightly less than those for sample 39 which are the individual analyses of the two samples of the Kiln feed.

(TABLE: See pages 8 and 8A).

The analyses show that it is only in the upper tiers that there is an appreciable falling off in grade and they suggest that for at least 13 tiers the entire product, after excluding the shaly bands, could be sent to the Kilns for burning and the resultant product be equal to that now being produced. An increase in production and a saving in manpower should result.

The upper tiers of stone may need selective treatment.

Compared with the product of other limestone

| Tier No. | Sample No. | Sample Thickness. | Band Thickness. | Total Thickness. | Total Thickness. Limestone | SiO <sub>2</sub> % | Av. SiO <sub>2</sub> % | CaO % | Av. CaO % | % Loss on Ignition | Average Loss on Ignition % | Average CaCO <sub>3</sub> % |
|----------|------------|-------------------|-----------------|------------------|----------------------------|--------------------|------------------------|-------|-----------|--------------------|----------------------------|-----------------------------|
| 1        | 1          | 21                | -               | 21               | -                          | 19.9               |                        | 42.0  |           | 33.5               |                            |                             |
| 2        | 2          | 21                | 4               | 46               | 42                         | 21.7               |                        | 41.2  |           | 32.8               |                            |                             |
| 3        | 3          | 11½               | 3               | 60½              | 53½                        | 19.1               |                        | 42.8  |           | 34.2               |                            |                             |
| 4        | 4          | 11                | 2               | 73½              | 64½                        | 21.5               |                        | 40.4  |           | 32.9               |                            |                             |
| 5        | 5          | 21                | 1               | 95½              | 85½                        | 34.4               |                        | 33.0  |           | 26.7               |                            |                             |
| 6        | 6          | 18                | 3               | 116½             | 103½                       | 18.7               |                        | 43.4  |           | 34.6               |                            |                             |
| 7        | 7          | 15                | 5½              | 137              | 118½                       | 33.1               |                        | 34.1  |           | 27.6               |                            |                             |
| 8        | 8          | 13                |                 | 150              | 131½                       | 15.6               |                        | 45.4  |           | 36.3               |                            |                             |
| 9        | 9          | 14                |                 | 164              | 145½                       | 21.4               | 23.3                   | 40.7  | 40.1      | 33.0               | 32.1                       | 72                          |
| 10       | 10         | 14                | 4               | 182              | 159½                       | 41.8               |                        | 25.1  |           | 21.8               |                            |                             |
| 11       | 11         | 11                | 4½              | 197½             | 170½                       | 23.4               | 24.8                   | 39.3  | 37.6      | 32.0               | 31.3                       | 68.9                        |
| 12       | 12         | 12                | 4               | 213½             | 182½                       | 33.3               |                        | 33.4  |           | 27.6               |                            |                             |
| 13       | 13         | 11                | 5               | 229½             | 193½                       | 29.3               | 25.6                   | 34.9  | 37.2      | 28.8               | 31.0                       | 68.2                        |
| 14       | 14         | 9                 | 7               | 245½             | 202½                       | 52.9               |                        | 17.5  |           | 15.5               |                            |                             |
| 15       | 15         | 15½               | 21              | 282              | 218                        | 44.6               | 28.1                   | 24.6  | 35.6      | 20.8               | 29.6                       | 65.2                        |
| 16       | 16         | 27                | 22              | 331              | 245                        | 31.0               | 24.2                   | 33.1  | 35.9      | 27.3               | 29.2                       | 65.1                        |
| 17       | 17         | 20                | 27              | 378              | 265                        | 27.0               | 28.2                   | 36.3  | 35.9      | 29.8               | 29.2                       | 65.1                        |
| 18       | 18         | 17                | 12              | 407              | 282                        | 43.2               | 28.8                   | 24.3  | 35.2      | 20.9               | 28.1                       | 63.3                        |

8A.

| Tier No. | Sample No.   | Sample Thickness. | Band Thickness. | Total Thickness.  | Total Thickness less Bands. | SiO <sub>2</sub> % | Av. SiO <sub>2</sub> 1. | Av. SiO <sub>2</sub> 2. | Av. SiO <sub>2</sub> 3. | CaO % | Av. CaO 1. | Av. CaO 2. | Av. CaO 3. | %Loss on Ignition | Av. L.O.I. 1. | Av. L.O.I. 2. | Av. L.O.I. 3. | Av. CaCO <sub>3</sub> % |
|----------|--------------|-------------------|-----------------|-------------------|-----------------------------|--------------------|-------------------------|-------------------------|-------------------------|-------|------------|------------|------------|-------------------|---------------|---------------|---------------|-------------------------|
| 1        | 27           | 19                |                 | 19                | 19                          | 22.6               |                         |                         |                         | 40.0  |            |            |            | 32.5              |               |               |               |                         |
| 2        | 23           | 19                | 6               | 44                | 38                          | 25.3               |                         |                         |                         | 38.7  |            |            |            | 31.3              |               |               |               |                         |
| 3        | 24           | 19                | 1 $\frac{1}{2}$ | 64 $\frac{1}{2}$  | 57                          | 17.6               |                         |                         |                         | 44.1  |            |            |            | 35.5              |               |               |               |                         |
| 4        | 25           | 4                 | 2               | 70 $\frac{1}{2}$  | 61                          | 30.4               |                         |                         |                         | 33.0  |            |            |            | 27.1              |               |               |               |                         |
| 5        | 26           | 21                | 1 $\frac{1}{2}$ | 93                | 82                          | 28.4               |                         |                         |                         | 36.6  |            |            |            | 29.8              |               |               |               |                         |
| 6        | 28           | 20                | 8               | 121               | 102                         | 24.3               |                         |                         |                         | 39.0  |            |            |            | 31.8              |               |               |               |                         |
| 7        | 29           | 18                | 5               | 144               | 120                         | 30.0               |                         |                         |                         | 35.5  |            |            |            | 28.9              |               |               |               |                         |
| 8        | 30           | 21                | 2               | 167               | 141                         | 29.5               |                         |                         |                         | 36.0  |            |            |            | 29.2              |               |               |               |                         |
| 9        | 31           | 9 $\frac{1}{2}$   | 3               | 179 $\frac{1}{2}$ | 150 $\frac{1}{2}$           | 41.2               | 22.2                    | 31.0                    | 26.6                    | 25.5  | 31.4       | 33.4       | 37.5       | 22.2              | 25.5          | 27.7          | 30.5          | 68                      |
| 10       | 32           | 6                 | 2               | 187 $\frac{1}{2}$ | 156 $\frac{1}{2}$           | 16.9               |                         |                         |                         | 43.0  |            |            |            | 35.1              |               |               |               |                         |
| 11       | 33           | 8                 | 3               | 198 $\frac{1}{2}$ | 164 $\frac{1}{2}$           | 30.0               | 21.8                    | 31.1                    | 26.4                    | 33.0  | 30.9       | 33.1       | 37.5       | 27.9              | 25.3          | 27.7          | 30.6          | 68                      |
| 12       | 37           | 16                | 8               | 222 $\frac{1}{2}$ | 180 $\frac{1}{2}$           | 31.3               |                         |                         |                         | 34.2  |            |            |            | 28.5              |               |               |               |                         |
| 13       | 36           | 22                | 15              | 259 $\frac{1}{2}$ | 202 $\frac{1}{2}$           | 29.2               | 21.0                    | 31.0                    | 27.0                    | 35.9  | 28.8       | 31.5       | 37.0       | 29.9              | 23.6          | 26.7          | 30.3          | 67.3                    |
| 14       | 34           | 18                | 16              | 293 $\frac{1}{2}$ | 220 $\frac{1}{2}$           | 26.0               |                         |                         |                         | 37.2  |            |            |            | 30.7              |               |               |               |                         |
| 15       | 35           | 13 $\frac{1}{2}$  | 8               | 315               | 234                         | 42.6               | 20.6                    | 34.6                    | 27.8                    | 24.8  | 26.9       | 30.1       | 36.2       | 21.3              | 22.1          | 25.7          | 29.8          | 66                      |
| 16       | 38           |                   |                 |                   |                             | 26.5               |                         |                         |                         | 36.8  |            |            |            | 30.4              |               |               |               |                         |
|          | 39           |                   |                 |                   |                             | 24.88              |                         |                         |                         | 38.8  |            |            |            | 31.7              |               |               |               |                         |
|          | Av. of 38&39 |                   |                 |                   |                             | 25.68              |                         |                         |                         | 37.8  |            |            |            | 31.1              |               |               |               | 68.9                    |

9.

quarries in Tasmania, where Calcium Carbonate content at times exceeds 90%, the Limestone of Mt. Nassau is a low grade one. As the depth of overburden is increasing rapidly, a progressively higher proportion of the stone quarried will be discarded, and the necessity for opening new quarry faces will have to be considered. Suitable sites are available in the district.

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27/8/48.