

Frequently the wireline tools would stick causing invalid data to be recorded. These areas are easily recognised by the straight line characteristic nature of the curve.

There were tool problems with the ISF which were corrected by relogging. The first attempt with the RFT stuck. Additional pressure points were obtained by reducing the outside diameter of the tool.

Hydrocarbon fluid density could not be determined from the well logs because of the uncertainty of the water saturation of the flushed zone (SXO) and the low porosity of the rock.

Other log information used in processing the data:

Suite No. 2

Date of Logging	25 January, 1986
Run Number	2
Depth Logger	3003.5m.
Resistivity of the filtrate	.714 at 78 degrees F
Bottom hole temperature	204 degrees F.

Suite No. 3

Date of Logging	8 February, 1986
Run Number	3
Depth Logger	3649m.
Resistivity of the filtrate	.495 at 71 degrees F
Bottom hole temperature	288 degrees F

The temperature used to correct the formation fluid resistivities is the temperature obtained from the ISF log runs and not the projected static bottom hole temperature.

TECHNIQUE

The dual water method of analyzing shaly formations was used in processing this data. The basic Archie water saturation equation was modified to take into account the varying amounts of shale. The water saturation equation used in the interpretation is:

$$S_w = (R_{mix}/(R_t * \Phi^{**M}))^{**0.5}$$

$$R_{mix} = R_{wb} * R_{wf} / (V_{sh}(R_{wf} - R_{wb}) + R_{wb})$$