* BIT # 8   SMITH F3J   BIT DIAMETER : 12.25 inch   NOZZ 13/13/13   HUD RHEOLOGICAL PARAMETERS : PV = 3 YP = 1 GEL = 1 *

466370

	TIME	MEASURED	DEPTHS VERTCL	LAGGED	ROP	WOB	RPM	TORQ	PRESS	FLOW IN	PIT VOL	DENSITY IN	DENSITY OUT	TEMP IN	TEMP OUT	RESIST IN	RESIST OUT	DCS	NORM	PF	ECD	FRAC	FEET	TIME	COST
	Hr:mn	feet	feet	feet	ft/h	klbs	rpm	ftlb	psi	gpm	bbls	ppg	ppg	degF	degF	ohmm	ohmm	unit			ppg	ppg	ppg	feet	Dthr	$
D	16:12	3965.6	3963.9	3928.0	29.8	30.0	104	1900	1862	493	364	8.6	8.6	56.0	63.7	.21	.21	1	1.40	1.05	8.6	8.6	14.0	1858.	20.17	54
D	16:18	3968.0	3766.9	3940.0	24.1	30.6	101	1800	1862	493	350	8.6	8.6	56.0	63.6	.21	.22	3	1.45	1.05	8.6	8.6	14.0	1861.	20.27	54
D	16:34	3970.5	3968.9	3945.0	15.5	30.4	106	1300	1843	487	269	8.6	8.6	55.8	62.6	.20	.22	3	1.54	1.05	8.6	8.6	14.0	1863.	20.39	54
D	16:41	3973.1	3970.9	3949.0	17.3	30.6	103	1300	1847	493	245	8.6	8.6	55.7	63.6	.20	.22	1	1.52	1.05	8.6	8.6	14.0	1865.	20.51	55
D	16:46	3975.6	3974.0	3950.0	29.7	33.0	109	1300	1847	483	297	8.6	8.6	55.6	63.9	.20	.23	1	1.40	1.05	8.6	8.6	14.0	1868.	20.59	55
D	16:51	3978.0	3976.9	3951.0	39.5	31.6	102	1300	1843	483	329	8.6	8.6	55.4	63.8	.20	.23	1	1.31	1.05	8.6	8.6	14.0	1871.	20.67	55
D	16:55	3980.5	3979.0	3952.0	47.2	30.4	107	1300	1852	488	339	8.6	8.6	55.4	63.8	.20	.23	1	1.27	1.05	8.6	8.6	14.0	1873.	20.73	55
D	16:58	3983.0	3981.9	3953.0	63.3	30.2	106	1300	1843	488	311	8.6	8.6	55.4	63.8	.20	.23	1	1.18	1.05	8.6	8.6	14.0	1876.	20.78	55
D	17: 2	3985.7	3983.9	3955.0	55.5	32.2	101	1300	1847	487	335	8.6	8.6	55.4	63.8	.20	.23	1	1.20	1.05	8.6	8.6	14.0	1878.	20.84	55
D	17: 5	3988.2	3987.1	3956.0	70.0	34.0	104	1300	1847	488	309	8.6	8.6	55.4	63.8	.20	.24	1	1.15	1.05	8.6	8.6	14.0	1881.	20.91	55
D	17: 8	3990.6	3989.1	3958.0	40.6	29.8	107	1400	1847	488	329	8.6	8.6	55.4	63.7	.20	.23	-0	1.31	1.05	8.6	8.6	14.0	1883.	20.95	55
D	17:12	3993.1	3990.9	3960.0	51.2	33.2	106	1400	1847	488	311	8.6	8.6	55.4	63.7	.20	.23	3	1.21	1.05	8.6	8.6	14.0	1885.	21.01	55
D	17:16	3995.5	3994.1	3962.0	32.7	29.4	101	1200	1843	491	337	8.6	8.6	55.4	63.6	.20	.24	4	1.36	1.05	8.6	8.6	14.0	1888.	21.08	55
D	17:21	3998.2	3996.0	3965.0	26.1	32.6	106	1300	1838	488	331	8.6	8.6	55.4	63.6	.20	.24	4	1.43	1.05	8.6	8.6	14.0	1890.	21.17	55
D	17:36	4000.8	3999.0	3969.0	24.6	34.5	97	1400	1700	473	249	8.6	8.6	55.4	62.6	.20	.26	5	1.49	1.05	8.6	8.6	14.0	1893.	21.20	55
D	17:39	4003.0	4001.9	3969.0	75.8	35.9	96	1400	1765	479	237	8.6	8.6	55.4	63.2	.20	.28	5	1.15	1.05	8.6	8.6	14.0	1896.	21.32	55
D	17:42	4005.6	4003.9	3970.0	56.2	37.5	96	1400	1760	473	243	8.6	8.6	55.4	63.3	.20	.29	5	1.24	1.05	8.6	8.6	14.0	1898.	21.37	55
D	17:46	4008.2	4007.1	3971.0	30.5	36.5	104	1400	1920	475	247	8.6	8.6	55.4	63.6	.20	.26	5	1.44	1.05	8.6	8.6	14.0	1901.	21.44	55
D	17:49	4010.5	4009.0	3972.0	60.6	37.3	98	1400	1755	478	251	8.6	8.6	55.4	63.5	.20	.25	4	1.21	1.05	8.6	8.6	14.0	1903.	21.48	55
D	17:52	4013.1	4012.0	3973.0	59.5	34.3	95	1300	1755	476	261	8.6	8.6	55.4	63.4	.20	.23	5	1.22	1.05	8.6	8.6	14.0	1906.	21.54	55
D	17:55	4015.6	4014.0	3974.0	56.4	35.7	95	1300	1751	478	279	8.6	8.6	55.4	63.4	.20	.24	5	1.24	1.05	8.6	8.6	14.0	1908.	21.58	55
D	17:56	4019.4	4017.5	3975.0	669.6	34.1	97	1300	1751	479	289	8.6	8.6	55.3	63.4	.20	.24	5	.49	1.05	8.6	8.6	14.0	1911.	21.61	55
D	18: 2	4020.6	4019.2	3978.0	97.7	32.1	39	1200	2007	512	315	8.6	8.6	55.3	63.4	.20	.23	5	1.06	1.05	8.6	8.6	14.0	1913.	21.64	55
D	18:10	4023.3	4021.9	3983.0	49.3	30.6	94	1700	1799	483	300	8.6	8.6	55.3	63.3	.20	.23	5	1.31	1.05	8.6	8.6	14.0	1916.	21.77	56
D	18:10	4025.6	4024.0	3983.0	96.0	35.1	97	1700	1799	488	300	8.6	8.6	55.3	63.3	.21	.23	5	1.05	1.05	8.6	8.6	14.0	1918.	21.78	56
D	18:11	4028.1	4027.0	3984.0	193.8	35.1	103	1800	1814	488	300	8.6	8.6	55.3	63.3	.21	.25	5	.07	1.05	8.6	8.6	14.0	1921.	21.79	56
D	18:12	4032.2	4030.4	3984.0	760.6	.0	2	0	1770	488	302	8.6	8.6	55.3	63.4	.21	.23	4	.44	1.05	8.6	8.6	14.0	1924.	21.80	55
D	20:18	4033.6	4031.9	4032.0	404.0	23.1	96	1300	1828	497	504	8.6	8.6	57.3	66.4	.20	.21	7	.57	1.05	8.6	8.6	14.0	1926.	21.81	55
D	20:19	4039.4	4037.5	4032.0	1166.0	29.0	103	1300	1843	498	502	8.6	8.6	57.3	66.0	.20	.21	7	.33	1.05	8.6	8.6	14.0	1931.	21.82	55
D	20:19	4044.5	4042.3	4032.0	819.4	21.5	104	1100	1843	498	502	8.6	8.6	57.3	65.9	.20	.21	7	.40	1.06	8.6	8.6	14.1	1936.	21.83	55
D	20:20	4048.3	4047.2	4032.0	487.0	15.0	103	1100	1843	498	502	8.6	8.6	57.3	65.0	.20	.21	7	.49	1.06	8.6	8.6	14.1	1941.	21.83	55
D	20:20	4052.1	4050.4	4032.0	624.3	7.1	107	1000	1847	497	504	8.6	8.6	57.3	65.5	.20	.21	7	.54	1.06	8.6	8.6	14.1	1945.	21.85	55
D	20:22	4053.1	4051.0	4032.0	274.5	.8	100	800	1830	493	506	8.6	8.6	57.3	65.5	.20	.21	5	.54	1.06	8.6	8.6	14.1	1945.	21.87	55
D	20:27	4055.5	4053.9	4032.0	42.9	13.0	100	1000	1852	503	510	8.6	8.6	57.2	65.6	.20	.21	5	.75	1.06	8.6	8.6	14.1	1948.	21.94	55
D	20:28	4060.3	4057.9	4032.0	802.2	10.7	100	1000	1852	478	512	8.6	8.6	57.2	65.7	.20	.21	5	.36	1.06	8.6	8.6	14.1	1952.	21.76	55
D	20:28	4063.1	4061.5	4032.0	701.6	6.9	105	900	1857	503	514	8.6	8.6	57.2	65.7	.20	.21	5	.34	1.06	8.6	8.6	14.1	1955.	21.96	55
D	20:41	4066.1	4064.1	4032.0	103.2	-.4	97	900	1920	508	546	8.6	8.6	57.3	65.5	.20	.21	4	.62	1.06	8.6	8.6	14.1	1958.	21.98	55
D	20:41	4068.4	4066.7	4032.0	620.1	1.6	99	1000	1925	508	540	8.6	8.6	57.2	65.5	.20	.21	4	.27	1.06	8.6	8.6	14.1	1961.	21.99	55
D	20:41	4072.6	4070.8	4032.0	795.9	9.5	96	1000	1823	508	544	8.6	8.6	57.2	65.1	.20	.21	4	.33	1.06	8.6	8.6	14.1	1965.	22.00	55
D	20:42	4076.5	4074.4	4032.0	1040.0	7.3	104	1000	1828	493	544	8.6	8.6	57.2	64.9	.20	.21	4	.46	1.06	8.6	8.6	14.1	1967.	22.00	55
D	20:42	4078.1	4076.9	4032.0	174.0	11.1	100	1000	1828	493	542	8.6	8.6	57.2	64.6	.20	.21	4	.68	1.06	8.6	8.6	14.1	1971.	22.01	55
D	20:44	4080.6	4079.5	4032.0	130.3	6.5	103	900	1823	493	542	8.6	8.6	57.3	64.1	.20	.21	4	.69	1.06	8.6	8.6	14.1	1973.	22.04	55
D	20:44	4083.3	4080.9	4032.0	338.4	3.8	96	900	1833	492	544	8.6	8.6	57.2	63.9	.20	.21	3	.42	1.06	8.6	8.6	14.1	1975.	22.04	54
D	20:44	4086.4	4085.0	4032.0	244.5	6.9	100	1000	1828	493	542	8.6	8.6	57.2	64.0	.20	.21	4	.55	1.06	8.6	8.6	14.1	1979.	22.05	54
D	20:45	4088.3	4086.2	4032.0	631.5	10.3	95	1100	1823	488	542	8.6	8.6	57.2	64.0	.20	.21	4	.38	1.06	8.6	8.6	14.1	1980.	22.05	54
D	20:45	4090.8	4089.1	4032.0	403.5	5.4	96	900	1833	493	540	8.6	8.6	57.2	64.0	.20	.21	3	.39	1.06	8.6	8.6	14.1	1983.	22.06	54
D	20:48	4093.3	4091.9	4032.0	511.3	.8	103	1000	1794	483	538	8.6	8.6	57.2	64.3	.20	.21	3	.20	1.06	8.6	8.6	14.1	1986.	22.07	54
D	20:58	4095.6	4094.3	4032.0	286.6	3.2	95	1000	1833	493	544	8.6	8.6	57.2	64.5	.20	.21	4	.40	1.06	8.6	8.6	14.1	1988.	22.08	54
D	20:59	4098.1	4097.0	4032.0	110.8	-1.0	97	900	1843	493	544	8.6	8.6	57.2	64.2	.20	.21	3	.55	1.06	8.6	8.6	14.1	1991.	22.10	54