

OR-550

THYLACINE-2



**CORE LABORATORIES  
AUSTRALIA PTY LTD**

copy 1

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***Reservoir Fluid  
Analysis of  
Sub-Surface Samples from  
Thylacine - 2  
Otway Basin, Victoria***

Prepared for  
**Woodside Energy Limited**

February 2002

File: AFL 2001-045

Reservoir Fluid Laboratory  
Core Laboratories Australia Pty Ltd  
Perth  
Western Australia

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**CORE LABORATORIES  
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8 February, 2002

Woodside Energy Limited  
1 Adelaide Terrace  
Perth  
Western Australia, 6000

Attention: Mr Werner Ribul

**Subject: Reservoir Fluid Analysis**  
**Well: Thylacine-2**  
**Location: Otway Basin**  
**File: AFL 2001-045**

Dear Werner,

Four sub-surface MDT sample chambers, collected on the Thylacine-2 well, were shipped to our Perth laboratory for validity checks and use in a reservoir fluid analysis study. Presented in the following report are the results of these analyses.

Core Laboratories Australia Pty Ltd appreciates this opportunity to be of service to Woodside Energy Limited. Should you have any questions regarding this report, or if we may be of any further assistance, please feel free to contact me at your convenience.

Yours Faithfully,  
For **CORE LABORATORIES AUSTRALIA PTY LTD**

Kevin R. Daken  
Laboratory Supervisor

**Woodside Energy Limited**  
**Thylacine-2**  
AFL 2001-045

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## LABORATORY PROCEDURES

### Sample Receipt and Validation

Four MDT sample chambers, with reservoir gas samples, were received in our Perth laboratory for use in a compositional and PVT analysis study. As a preliminary quality check, the opening pressure of each sample was determined. The results, summarised on page 3, indicated that all samples were reasonably consistent and were used for compositional analysis.

### Compositional Analysis

The hydrocarbon compositions of the reservoir fluid samples were determined by flash/separation techniques where a reservoir fluid sub-sample was flashed and separated into liquid and gas phases. Flashed gas was analysed by gas chromatography using the GPA 2286 method and the flash liquid by temperature programmed capillary chromatography. These flash compositions were mathematically recombined to the measured flash gas-liquid ratio and an original reservoir fluid composition was calculated. The resulting reservoir fluid compositions are reported on pages 4 through 7. Samples in chambers SN-157 and SN-193 were selected for PVT analysis.

Note: Processing of the flashed liquid chromatograms revealed low level contamination from the synthetic oil based drilling fluid.

### Pressure Volume Relations

A known volume of the SN-193 reservoir fluid sample was charged to the large volume Sloane-type, high-pressure visual cell and thermally expanded to 114 °C. Once equilibrated in single phase, the fluid was subjected to the constant composition expansion procedure. During this procedure, a trace of liquid was observed at 3200 psig. During subsequent pressure stages, this liquid level remained very constant (indicating probable contamination from the drilling fluid) until 2200 psig where a significant increase in retrograde liquid volume indicated the dew point for the reservoir gas. The pressure volume relations and a retrograde liquid curve were then completed with the resulting volumetric data, pressure volume relation and retrograde liquid measurements presented on page 8. Graphical representations are depicted in figures A-1 through A-3.

An additional constant composition expansion procedure was performed on sample SN-157. A known volume of this reservoir fluid was charged to the Sloane-type cell and thermally expanded to 109 °C, equilibrated in single phase and subjected to the constant composition expansion procedure. Again, a trace of (contamination) liquid was observed from 3400 psig until 2800 psig where the significant increase in retrograde liquid volume indicated dew point for the reservoir gas. The pressure volume relations and a retrograde liquid curve were then completed and the resulting volumetric data, pressure volume relation and retrograde liquid measurements tabulated on page 9. Graphical representations are depicted in figures A-4 through A-6.

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## General Well Information

Company.....	Woodside Energy Limited
Well Name.....	Thylacine-2
API Well Number.....	Not Aplicable
File Number.....	AFL 2001-045
Date Sample Collected.....	10-Sep-01
Sample Type.....	Bottom-Hole
Geographical Location.....	Otway Basin
Field.....	Thylacine

## Well Description

Formation.....	*	
Pool (or Zone).....	*	
Date Completed.....	*	
Elevation.....	*	m
Producing Interval.....	*	m
Total Depth.....	*	m
Tubing Size.....	*	in
Tubing Depth.....	*	m
Casing Size.....	*	in
Casing Depth.....	*	m

## Pressure Survey Data

### Data from Original Discovery Well

Date .....	*	
Reservoir Pressure .....	*	psig
Gas / Oil Contact.....	*	m
Oil / Water Contact.....	*	m

### Data at Sample Collection

Date.....	10-Sep-01	
Reservoir Pressure.....	*	psig
Reservoir Temperature.....	*	°C
Pressure Tool.....	MDT	
Flowing Bottom-Hole Pressure.....	*	psig
Gas / Oil Contact.....	*	m
Oil / Water Contact.....	*	m

\* Data not forwarded to Core Laboratories.

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## Production Data

### Data from Original Discovery Well

Location.....	*		
Date.....	*		
Oil Gravity @ STP.....	*	°API	
Separator Pressure.....	*	psig	
Separator Temperature.....	*	°F	
Production Rates			
Gas.....	*	Mscf/D	
Liquid.....	*	STbb/D	
Gas/Liquid Ratio.....	*	scf/bbl	

### Data at Sample Collection

Sampling Date.....	*		
Production Rate.....	*	bbl/D	
Produced G.O.R. ....	*	scf/bbl	
Liquid Gravity at 60.0 °F.....	*	°API	
Productivity Index.....	*	bbl/D/psi at	°F
		and	bbl/D

### Sampling Information

Sample Collected at.....	*	m MDBRT
Status of Well.....	*	
Sampled By.....		Schlumberger
Type Sampler.....		MPSR
Cylinder Names/Numbers .....		SN-157 (2144.0 m MDBRT)
		SN-186 (2144.0 m MDBRT)
		SN-187 (2296.8 m MDBRT)
		SN-193 (2296.8 m MDBRT)

\* Data not forwarded to Core Laboratories.

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**PRELIMINARY QUALITY CHECKS**  
**of Gas Samples Received in Laboratory**

Cylinder Number	Sample Number	Depth (m) MDBRT	Reservoir Condition		Shipping Condition		Lab Opening Condition		Dew Point Pressure		Approximate Sample Volume (cc)
			psia	°C	psig	°C	psig	°C	psig	°C	
✓ SN-157(700cc)1		2144.0	3266	100.2	-	-	3020	17.6	2800	109	235
SN-186	2	2144.0	3266	100.2	-	-	2677	17.6	-	-	265
SN-187	3	2296.8	3399	109.5	-	-	3265	17.8	-	-	250
✓ SN-193	4	2296.8	3399	109.5	-	-	3195	17.8	2200	114	260

Note 1 : Reservoir conditions were obtained from Oilphase sample transfer data sheet.  
 Note 2 : Laboratory opening conditions were measured on the glycol (non-sample) end.  
 Note 3 : Reported dew point pressures were measured during PVT analyses.

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COMPOSITION OF RESERVOIR FLUID SAMPLE : SN-157

(by Flash/Extended Chromatography)

Component Name	Mol %	Wt %	Density (gm/cc)	MW
Hydrogen Sulfide	0.00	0.00	0.8006	34.08
Carbon Dioxide	8.22	16.99	0.8172	44.01
Nitrogen	1.39	1.83	0.8086	28.013
Methane	80.60	60.75	0.2997	16.043
Ethane	5.56	7.86	0.3562	30.07
Propane	2.09	4.32	0.5070	44.097
iso-Butane	0.41	1.12	0.5629	58.123
n-Butane	0.51	1.39	0.5840	58.123
iso-Pentane	0.21	0.71	0.6244	72.15
n-Pentane	0.15	0.51	0.6311	72.15
Hexanes	0.19	0.75	0.6850	84
Heptanes	0.26	1.19	0.7220	96
Octanes	0.22	1.11	0.7450	107
Nonanes	0.06	0.36	0.7640	121
Decanes	0.03	0.18	0.7780	134
Undecanes	0.02	0.14	0.7890	147
Dodecanes plus	0.08	0.79	0.8311	205
<b>Totals</b>	<b>100.00</b>	<b>100.00</b>		

Total Sample Properties

Molecular Weight ..... 21.28  
 Theoretical Liquid Density, gm/scc ..... 0.3721

CGR from Flash : 2.36 bbls/MMscf

Plus Fractions	Mol %	Wt %	Density	MW
Heptanes plus	0.67	3.77	0.7586	118
Dodecanes plus	0.08	0.79	0.8311	205

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COMPOSITION OF RESERVOIR FLUID SAMPLE : SN-186  
(by Flash/Extended Chromatography)

Component Name	Mol %	Wt %	Density (gm/cc)	MW
Hydrogen Sulfide	0.00	0.00	0.8006	34.08
Carbon Dioxide	8.21	16.95	0.8172	44.01
Nitrogen	1.38	1.81	0.8086	28.013
Methane	80.47	60.59	0.2997	16.043
Ethane	5.63	7.95	0.3562	30.07
Propane	2.17	4.48	0.5070	44.097
iso-Butane	0.42	1.14	0.5629	58.123
n-Butane	0.51	1.39	0.5840	58.123
iso-Pentane	0.21	0.71	0.6244	72.15
n-Pentane	0.15	0.51	0.6311	72.15
Hexanes	0.19	0.75	0.6850	84
Heptanes	0.25	1.15	0.7220	96
Octanes	0.21	1.06	0.7450	107
Nonanes	0.06	0.36	0.7640	121
Decanes	0.04	0.24	0.7780	134
Undecanes	0.02	0.14	0.7890	147
Dodecanes plus	0.08	0.77	0.8351	212
<b>Totals</b>	<b>100.00</b>	<b>100.00</b>		

Total Sample Properties

Molecular Weight ..... 21.31  
Theoretical Liquid Density, gm/scc ..... 0.3723

CGR from Flash : 2.35 bbls/MMscf

Plus Fractions	Mol %	Wt %	Density	MW
Heptanes plus	0.66	3.72	0.7608	120
Dodecanes plus	0.08	0.77	0.8351	212

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COMPOSITION OF RESERVOIR FLUID SAMPLE : SN-187

(by Flash/Extended Chromatography)

Component Name	Mol %	Wt %	Density (gm/cc)	MW
Hydrogen Sulfide	0.00	0.00	0.8006	34.08
Carbon Dioxide	8.54	18.42	0.8172	44.01
Nitrogen	1.29	1.77	0.8086	28.013
Methane	84.24	66.27	0.2997	16.043
Ethane	3.58	5.29	0.3562	30.07
Propane	1.01	2.18	0.5070	44.097
iso-Butane	0.17	0.48	0.5629	58.123
n-Butane	0.26	0.74	0.5840	58.123
iso-Pentane	0.10	0.35	0.6244	72.15
n-Pentane	0.07	0.25	0.6311	72.15
Hexanes	0.10	0.41	0.6850	84
Heptanes	0.19	0.91	0.7220	96
Octanes	0.21	1.10	0.7450	107
Nonanes	0.08	0.49	0.7640	121
Decanes	0.04	0.23	0.7780	134
Undecanes	0.03	0.19	0.7890	147
Dodecanes plus	0.09	0.92	0.8332	209

Total Sample Properties

Molecular Weight ..... 20.40  
 Theoretical Liquid Density, gm/scc ..... 0.3655

CGR from Flash : 2.38 bbls/MMscf

Plus Fractions	Mol %	Wt %	Density	MW
Heptanes plus	0.64	3.84	0.7656	123
Dodecanes plus	0.09	0.92	0.8332	209
Totals	100.00	100.00		

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COMPOSITION OF RESERVOIR FLUID SAMPLE : SN-193

(by Flash/Extended Chromatography)

Component Name	Mol %	Wt %	Density (gm/cc)	MW
Hydrogen Sulfide	0.00	0.00	0.8006	34.08
Carbon Dioxide	8.80	18.89	0.8172	44.01
Nitrogen	1.25	1.71	0.8086	28.013
Methane	83.90	65.62	0.2997	16.043
Ethane	3.64	5.35	0.3562	30.07
Propane	1.07	2.30	0.5070	44.097
iso-Butane	0.18	0.51	0.5629	58.123
n-Butane	0.26	0.74	0.5840	58.123
iso-Pentane	0.10	0.35	0.6244	72.15
n-Pentane	0.07	0.25	0.6311	72.15
Hexanes	0.11	0.45	0.6850	84
Heptanes	0.19	0.90	0.7220	96
Octanes	0.21	1.09	0.7450	107
Nonanes	0.08	0.49	0.7640	121
Decanes	0.03	0.23	0.7780	134
Undecanes	0.02	0.18	0.7890	147
Dodecanes plus	0.09	0.94	0.8346	211
Totals	100.00	100.00		

Total Sample Properties

Molecular Weight ..... 20.48  
 Theoretical Liquid Density, gm/scc ..... 0.3667

CGR from Flash : 2.36 bbls/MMscf

Plus Fractions	Mol %	Wt %	Density	MW
Heptanes plus	0.62	3.83	0.7654	123
Dodecanes plus	0.09	0.94	0.8346	211

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PRESSURE-VOLUME RELATIONS (Sample #4-MPSR-193)

(at 114 °C)

Pressure psig	Relative Volume (A)	Liquid Volume Percent (B)	Deviation Factor Z	Instantaneous Compressibility v/v/psi (C)
6000	0.4316		1.052	111.95 E -6
5500	0.4573		1.022	120.98 E -6
5000	0.4877		0.991	137.98 E -6
4500	0.5258		0.962	164.15 E -6
4000	0.5757		0.936	200.80 E -6
3600	0.6284		0.920	238.58 E -6
3384	0.6633		0.913	262.41 E -6
3200	0.6976		0.909	284.75 E -6
2800	0.7902		0.901	340.50 E -6
2600	0.8486		0.899	372.68 E -6
2400	0.9175		0.898	408.78 E -6
2300	0.9567		0.897	429.33 E -6
d»2200	1.0000	0.00	0.897	
2100	1.0475	0.00		
2000	1.1001	0.01		
1900	1.1586	0.01		
1800	1.2240	0.02		
1600	1.3802	0.02		
1408	1.5733	0.02		
1234	1.8011	0.02		
1074	2.0760	0.02		
895	2.4997	0.02		
763	2.9381	0.02		
589	3.8100	0.01		

(A) Relative Volume: V/Vsat or volume at indicated pressure per volume at saturation pressure.

(B) Percent of the total volume of gas and liquid at the indicated pressure and 114 °C.

(C) Where: Instantaneous Compressibility =  $-dV / dP$

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PRESSURE-VOLUME RELATIONS (Sample #1-MPSR-157)

(at 109 °C)

Pressure psig	Relative Volume (A)	Liquid Volume Percent (B)	Deviation Factor Z	Instantaneous Compressibility w/psi (C)
6000	0.5578		1.047	99.99 E -6
5500	0.5878		1.011	111.29 E -6
5000	0.6242		0.977	130.45 E -6
4500	0.6707		0.945	158.40 E -6
4000	0.7326		0.918	196.10 E -6
3600	0.7982		0.900	233.92 E -6
3400	0.8382		0.893	255.64 E -6
3251	0.8718		0.888	273.20 E -6
3000	0.9375		0.882	306.22 E -6
2900	0.9674		0.880	321.57 E -6
d>2800	1.0000	0.00	0.878	
2700	1.0354	0.01		
2600	1.0739	0.02		
2500	1.1157	0.03		
2400	1.1615	0.04		
2200	1.2667	0.05		
2000	1.3947	0.05		
1600	1.7530	0.06		
1200	2.3607	0.05		
950	3.0050	0.04		
795	3.6082	0.04		
677	4.2509	0.03		
593	4.8619	0.03		
522	5.5285	0.02		

(A) Relative Volume:  $V/V_{sat}$  or volume at indicated pressure per volume at saturation pressure.

(B) Percent of the total volume of gas and liquid at the indicated pressure and 109 °C.

(C) Where: Instantaneous Compressibility  $\approx -dV / dP$

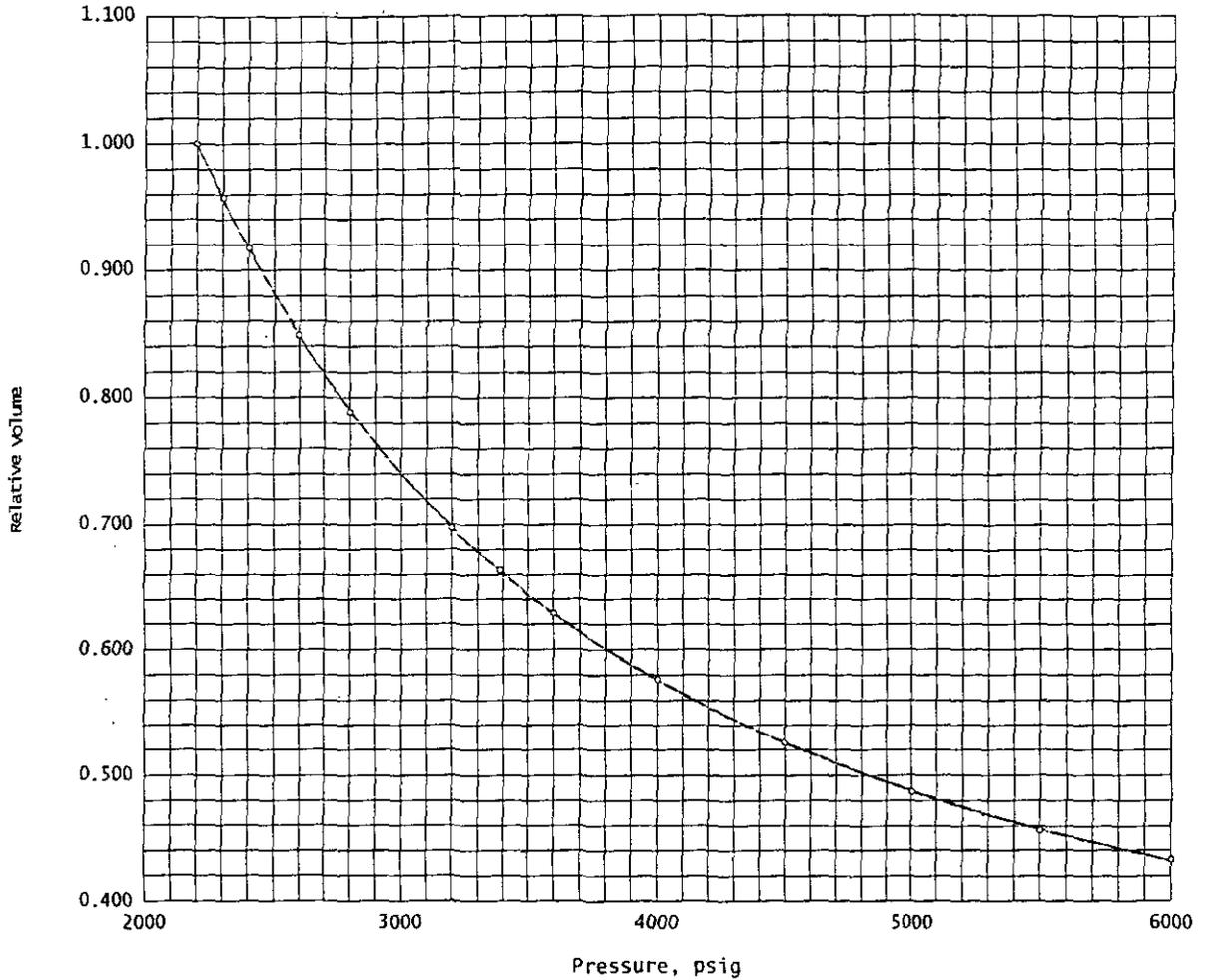
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RELATIVE VOLUME (MPSR-193)

( at 114 °C )



<p><b>Relative Volume Expression:</b></p> $y = a + b (Xd)^i + c (Xd)^j + d (\log(Xd))^k$	<p><b>LEGEND</b></p>								
<p>where:</p> <table> <tr> <td>a= -4.46569e+ 00</td> <td>i= 0.500</td> </tr> <tr> <td>b= 5.69123e+ 00</td> <td>j= 1.500</td> </tr> <tr> <td>c= -2.25537e- 01</td> <td>k= 0.998</td> </tr> <tr> <td>d= -7.98311e+ 00</td> <td></td> </tr> </table>	a= -4.46569e+ 00	i= 0.500	b= 5.69123e+ 00	j= 1.500	c= -2.25537e- 01	k= 0.998	d= -7.98311e+ 00		<p>○ Laboratory Data</p> <p>--- Confidence Limits</p> <p>— Analytical Expression</p> <p>Saturation Pressure: 2200 psig</p>
a= -4.46569e+ 00	i= 0.500								
b= 5.69123e+ 00	j= 1.500								
c= -2.25537e- 01	k= 0.998								
d= -7.98311e+ 00									
<p>Note: Xd (dimensionless 'X') = Pi / Psat, psig</p>									
<p>Confidence level: 99 %</p> <p>Confidence interval: +/- 0.00064</p> <p>'r squared': .999985</p>	<p><b>Pressure-Volume Relations</b></p> <p><b>Figure A-1</b></p>								

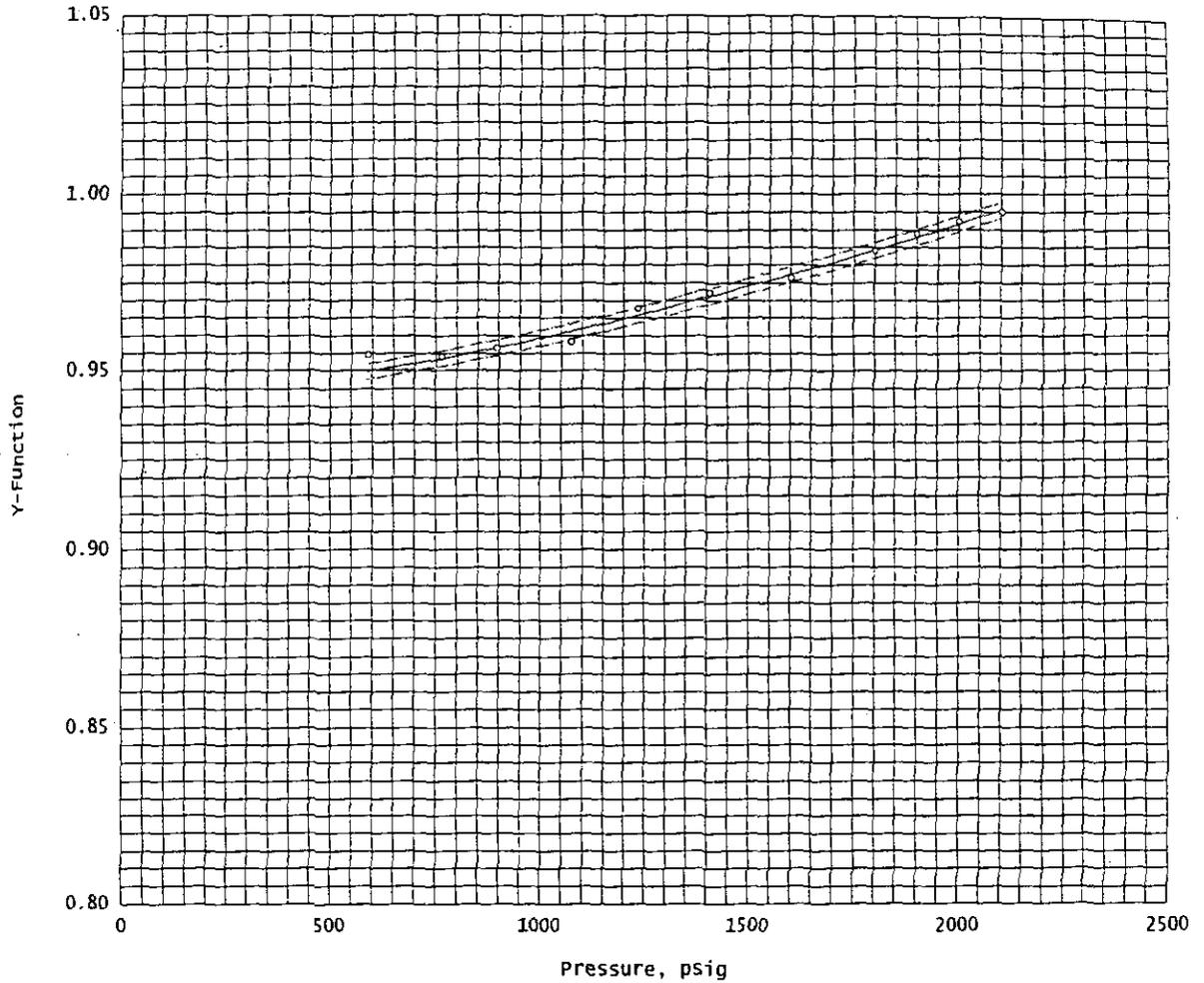
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Y-FUNCTION (MPSR-193)

( at 114 °C )



<p>Y-Function Expression:</p> $y = a + b (x_d)^{i_i}$	<p><b>LEGEND</b></p>
<p>where:</p> <p>a= 9.41935e- 01      i= 1.521</p> <p>b= 5.73156e- 02</p> <p>Note: <math>x_d</math> (dimensionless 'x') = <math>P_i / P_{sat}</math>, psig</p>	<p>○ Laboratory Data</p> <p>--- Confidence Limits</p> <p>— Analytical Expression</p> <p>Saturation Pressure: 2200 psig</p>
<p>Confidence level: 99 %</p> <p>Confidence interval: +/- 0</p> <p>'r squared': .984302</p>	<p><b>Pressure-Volume Relations</b></p> <p><b>Figure A-2</b></p>

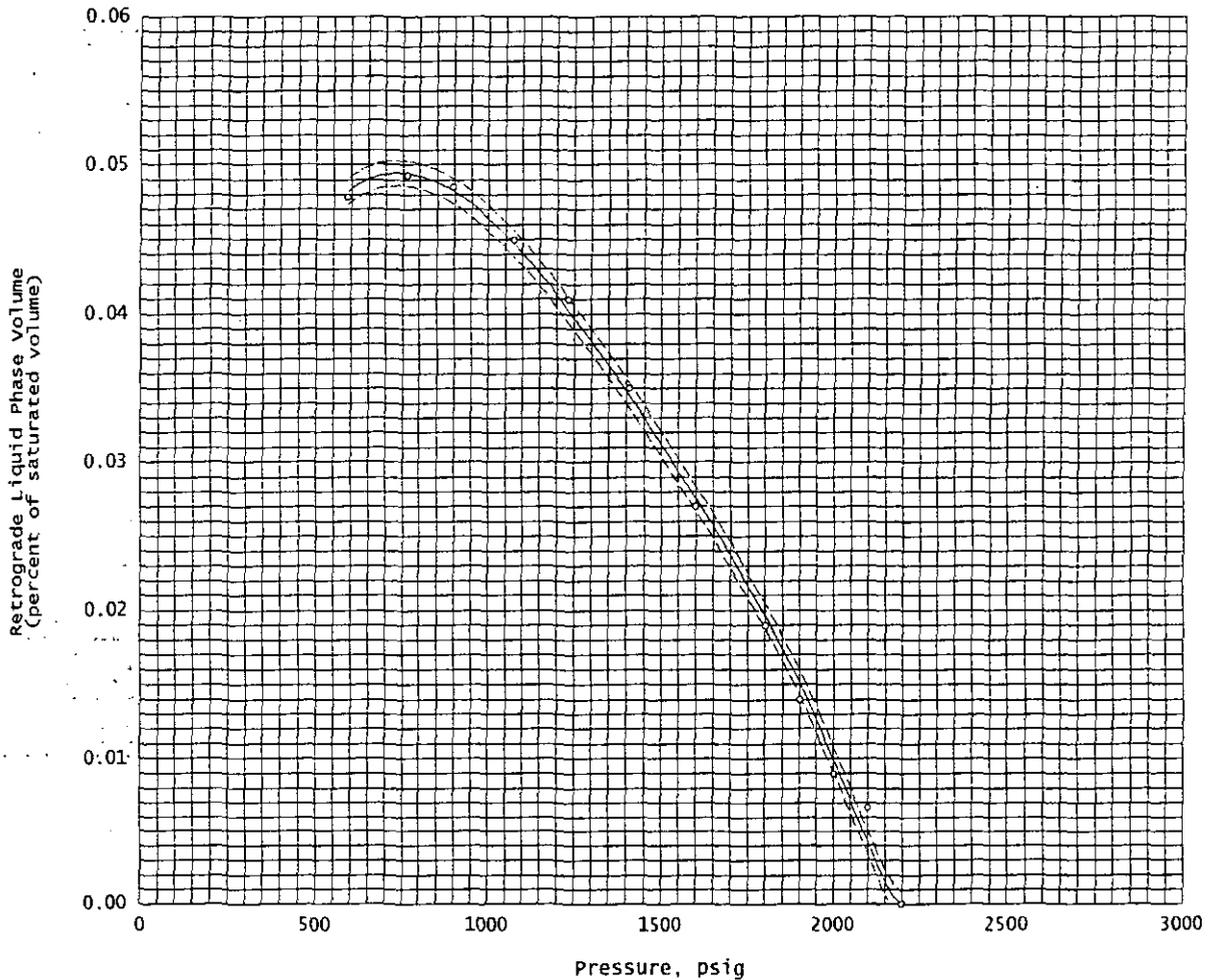
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LIQUID PHASE VOLUME (MPSR-193)

( at 114 °C )



<p>Retrograde Liquid Curve Expression:  <math>\sqrt{y} = a + b (Xd)^i + c (Xd)^j + d (10^4 Xd)^k</math></p>	<p><b>LEGEND</b></p>
<p>where:  <math>a = -4.07842e-02</math>                      <math>i = 0.800</math>  <math>b = -1.89514e+00</math>                      <math>j = 0.600</math>  <math>c = 2.02988e+00</math>                      <math>k = 7.000</math>  <math>d = -8.78110e-09</math></p> <p>Note: <math>X_d</math> (dimensionless 'X') = <math>P_i / P_{sat}</math>, psig</p>	<p>○ Laboratory Data          --- Confidence Limits          — Analytical Expression</p> <p>Saturation Pressure: 2200 psig</p>
<p>Confidence level:                      99 %          Confidence interval:                      +/- 0          'r squared':                      .99727</p>	<p><b>Pressure-Volume Relations</b>  <b>Figure A-3</b></p>

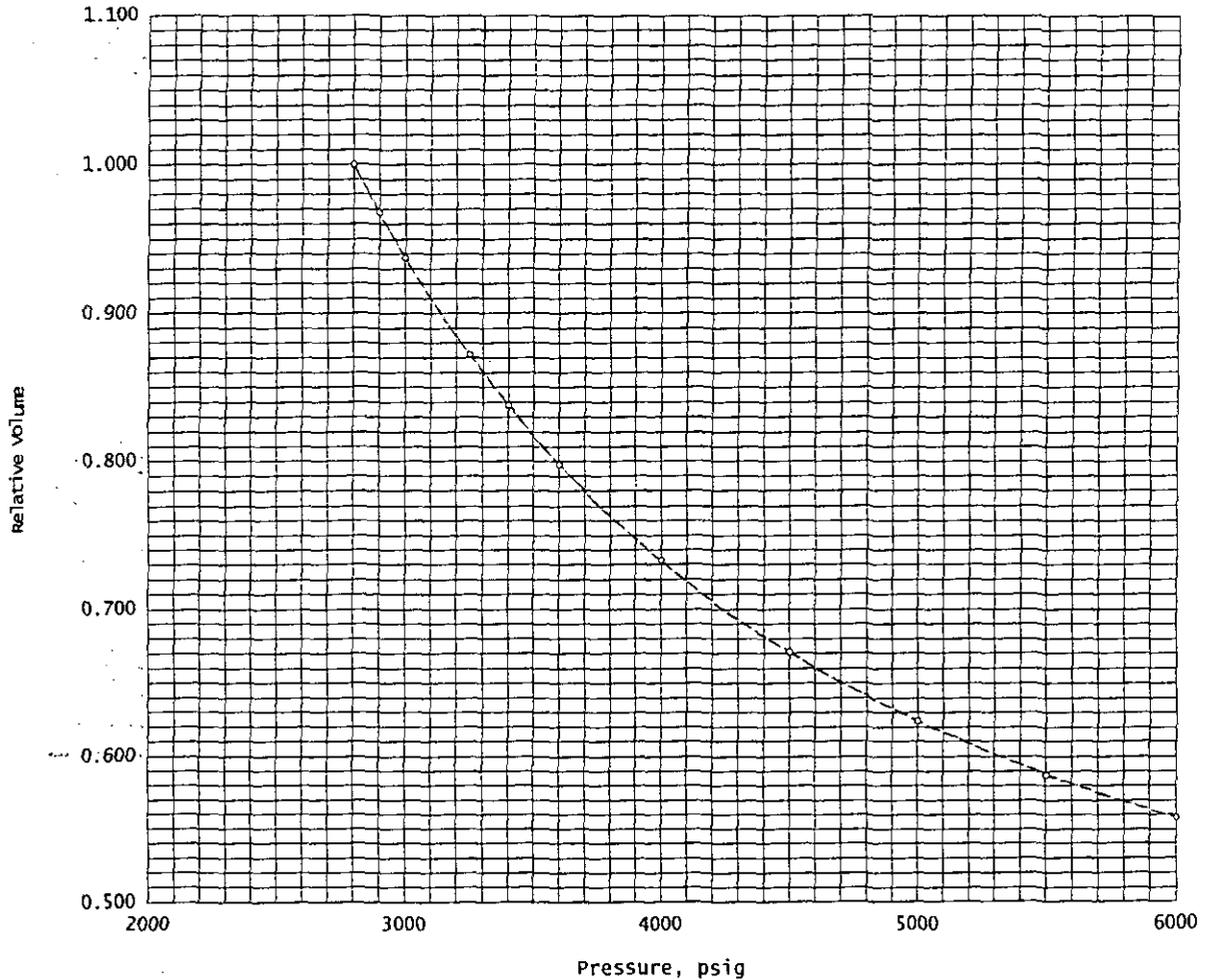
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RELATIVE VOLUME (MPSR-157)

( at 109 °C )



<p><b>Relative Volume Expression:</b></p> $y = a + b (Xd)^{Ai} + c (Xd)^{Aj} + d ( \log(Xd) )^{Ak}$	<p><b>LEGEND</b></p>								
<p>where:</p> <table> <tr> <td>a= -1.46681e+ 00</td> <td>i= 0.900</td> </tr> <tr> <td>b= 3.16542e+ 00</td> <td>j= 1.500</td> </tr> <tr> <td>c= -6.98579e- 01</td> <td>k= 0.996</td> </tr> <tr> <td>d= -6.22452e+ 00</td> <td></td> </tr> </table> <p>Note: Xd (dimensionless 'X') = Pi / Psat, psig</p>	a= -1.46681e+ 00	i= 0.900	b= 3.16542e+ 00	j= 1.500	c= -6.98579e- 01	k= 0.996	d= -6.22452e+ 00		<p>○ Laboratory Data</p> <p>--- Confidence Limits</p> <p>----- Analytical Expression</p> <p>Saturation Pressure: 2800 psig</p>
a= -1.46681e+ 00	i= 0.900								
b= 3.16542e+ 00	j= 1.500								
c= -6.98579e- 01	k= 0.996								
d= -6.22452e+ 00									
<table> <tr> <td>Confidence level:</td> <td>99 %</td> </tr> <tr> <td>Confidence interval:</td> <td>+/- 0.00029</td> </tr> <tr> <td>'r squared':</td> <td>.999996</td> </tr> </table>	Confidence level:	99 %	Confidence interval:	+/- 0.00029	'r squared':	.999996	<p><b>Pressure-Volume Relations</b></p> <p><b>Figure A-4</b></p>		
Confidence level:	99 %								
Confidence interval:	+/- 0.00029								
'r squared':	.999996								

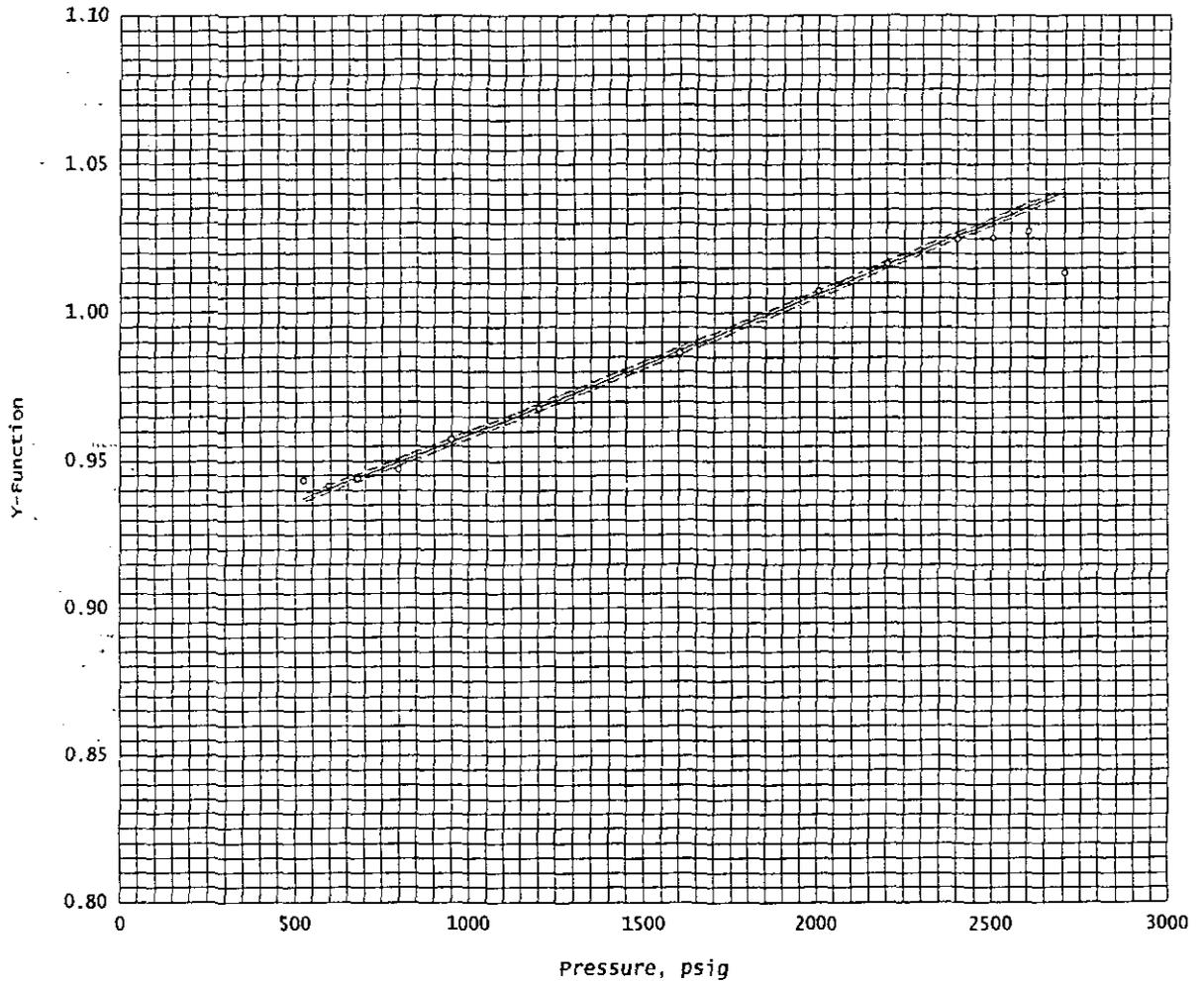
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Y-FUNCTION (MPSR-157)

( at 109 °C )



<p><b>Y-Function Expression:</b></p> $y = a + b (x_d)^{1.079}$	<p><b>LEGEND</b></p> <p>○ Laboratory Data</p> <p>--- Confidence Limits</p> <p>— Analytical Expression</p> <p>Saturation Pressure: 2800 psig</p>
<p>where:</p> <p>a= 9.16161e- 01      i= 1.079</p> <p>b= 1.29394e- 01</p> <p>Note: <math>x_d</math> (dimensionless 'x') = <math>P_i / P_{sat}</math>, psig</p>	
<p>Confidence level: 99 %</p> <p>Confidence interval: +/- 0</p> <p>'r squared': .998964</p>	<p><b>Pressure-Volume Relations</b></p> <p><b>Figure A-5</b></p>

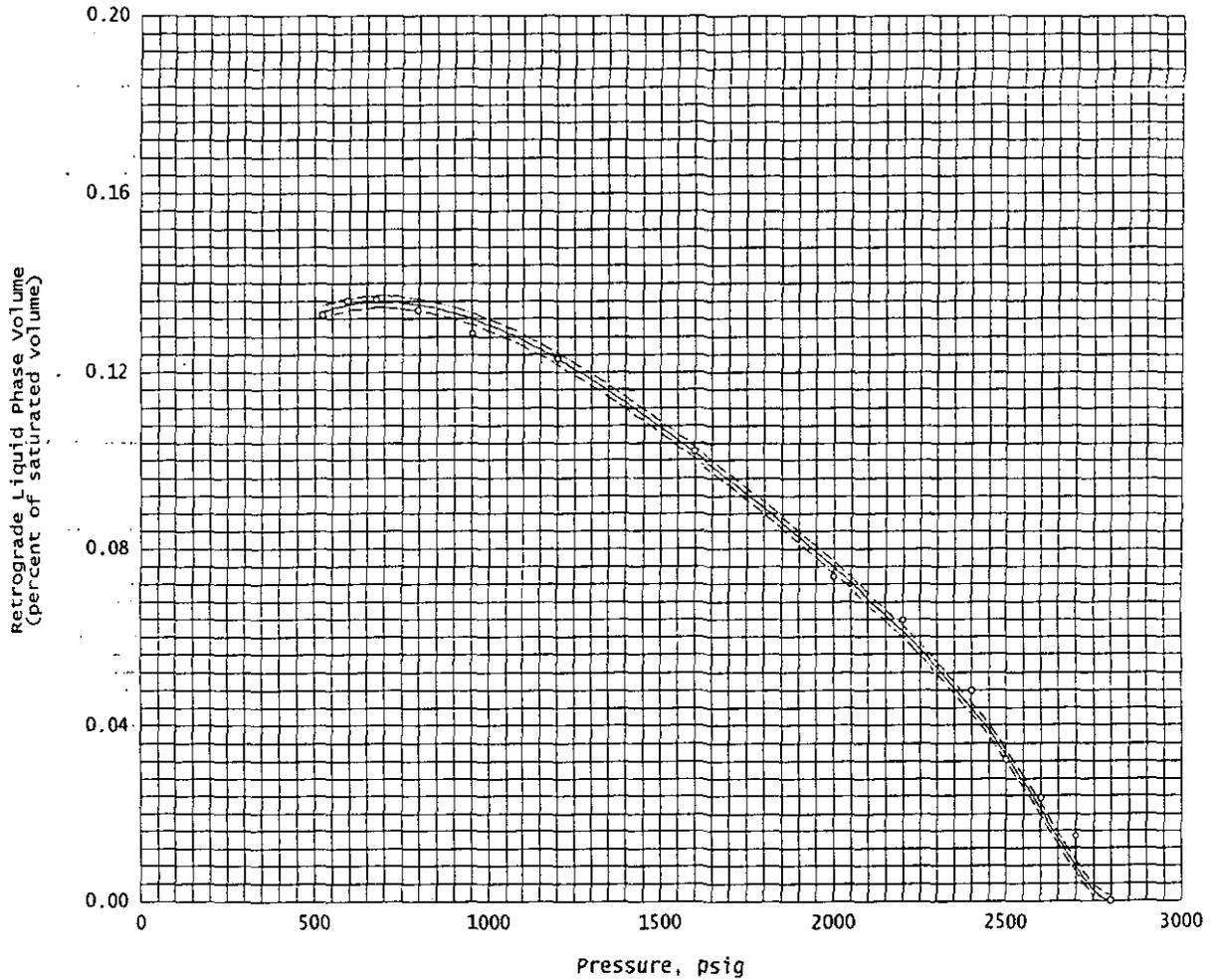
Woodside Energy Limited

Thylacine-2

AFL 2001-045

LIQUID PHASE VOLUME (MPSR-157)

(at 109 °C)



<p><b>Retrograde Liquid Curve Expression:</b>  <math>\text{sqrt } y = a + b (Xd)^i + c (Xd)^j + d (10^k Xd)^k</math></p>	<p><b>LEGEND</b></p>								
<p>where:</p> <table border="0"> <tr> <td>a= -2.05004e- 01</td> <td>i= 0.100</td> </tr> <tr> <td>b= 7.06621e- 01</td> <td>j= 1.500</td> </tr> <tr> <td>c= -3.33527e- 01</td> <td>k= 7.000</td> </tr> <tr> <td>d= -1.68373e- 08</td> <td></td> </tr> </table> <p>Note: Xd (dimensionless 'X') = Pi / Psat, psig</p>	a= -2.05004e- 01	i= 0.100	b= 7.06621e- 01	j= 1.500	c= -3.33527e- 01	k= 7.000	d= -1.68373e- 08		<p>○ Laboratory Data          - - - - - Confidence Limits          - - - - - Analytical Expression</p> <p>Saturation Pressure: 2800 psig</p>
a= -2.05004e- 01	i= 0.100								
b= 7.06621e- 01	j= 1.500								
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<table border="0"> <tr> <td>Confidence level:</td> <td>99 %</td> </tr> <tr> <td>Confidence interval:</td> <td>+/- 0</td> </tr> <tr> <td>'r squared':</td> <td>.999341</td> </tr> </table>	Confidence level:	99 %	Confidence interval:	+/- 0	'r squared':	.999341	<p><b>Pressure-Volume Relations</b>  <b>Figure A-6</b></p>		
Confidence level:	99 %								
Confidence interval:	+/- 0								
'r squared':	.999341								