



STONEHENGE METALS
LIMITED

Stonehenge Metals Limited

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Final Annual Report*
Cumberland Lake
EL31/2002

18 Dec 2007 to 18 Dec 2008 (due 18 Nov 2008)

*Licence expires 18 December 2008 an application for extension of term accompanies this report.

Compiled
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1 Introduction

This report details exploration activities by Stonehenge Metals Limited the 100% holder of EL 31/2002 "Cumberland Lake" during the period 18/12/2007 – 18/12/2008. The tenement is also commonly referred to as Federation, the Sweeney's deposit lies within the tenement. appendices

1.1 Location and access

EL31/2002 is located approximately twelve kilometres west of Zeehan on the west coast of Tasmania (Figure 1) and includes the manmade Lake Cumberland. The tenement is located approximately at Latitude: -41.907°, Longitude: 145.201°. All map co-ordinates in this report are relative to the GDA94 datum and located in UTM Zone 55 and use MGA co-ordinates except where stated (WGS84 also used).

EL 31/2002 initially covered an area of six square kilometres but was expanded to seven square kilometres in July 2007 to cover a 500m gap between the area being applied for by Stonehenge Metals Limited to the west due to the fact EL31/2002 is based on the GDA66 datum and the application area was based on the GDA94 datum.

Access to the area is from the southeast via the Trail Harbour Road. The existing tracks are cut into the granite and have a generally well-compacted surface in part suitable for 4WD vehicles, however the tracks over the steep escarpment in the east, south and west are difficult to traverse -- exacerbated by erosion and use by recreation vehicles. Foot access to and on the plateau area is generally good. Foot access to escarpment areas especially in the east are more difficult with heavily forested gullies and incised steep hill slopes. Elevations range from about 170m to 470m. The annual rainfall in the area is usually heavy – up to two and a half metres, with most falling in the winter months.

1.2 Tenure

EL 31/2002 was granted to Marshall Resources on December 18th, 2002. Marshall Resources was unable to raise capital for a comprehensive exploration program and invited McDermott Mining to joint venture the licence. A dealing was registered with Mineral Resources Tasmania, giving McDermott Mining 66% of the joint venture, and a program consisting of the following was drawn up for submission to Mineral Resources Tasmania. Marshall Resources subsequently withdrew from further active involvement in EL 31/2002.

The lease was transferred to Stonehenge Metals Limited in 2006 subject to Stonehenge's listing on the Australian Securities Exchange, which occurred on the 20th of December 2006. In January 2007, EL21/2002 was officially transferred from McDermott Mining to Stonehenge Metals Limited.

Stonehenge Metals Limited began active exploration of the tenement in January 2007. The tenement is currently held 100% by Stonehenge Metals Limited.

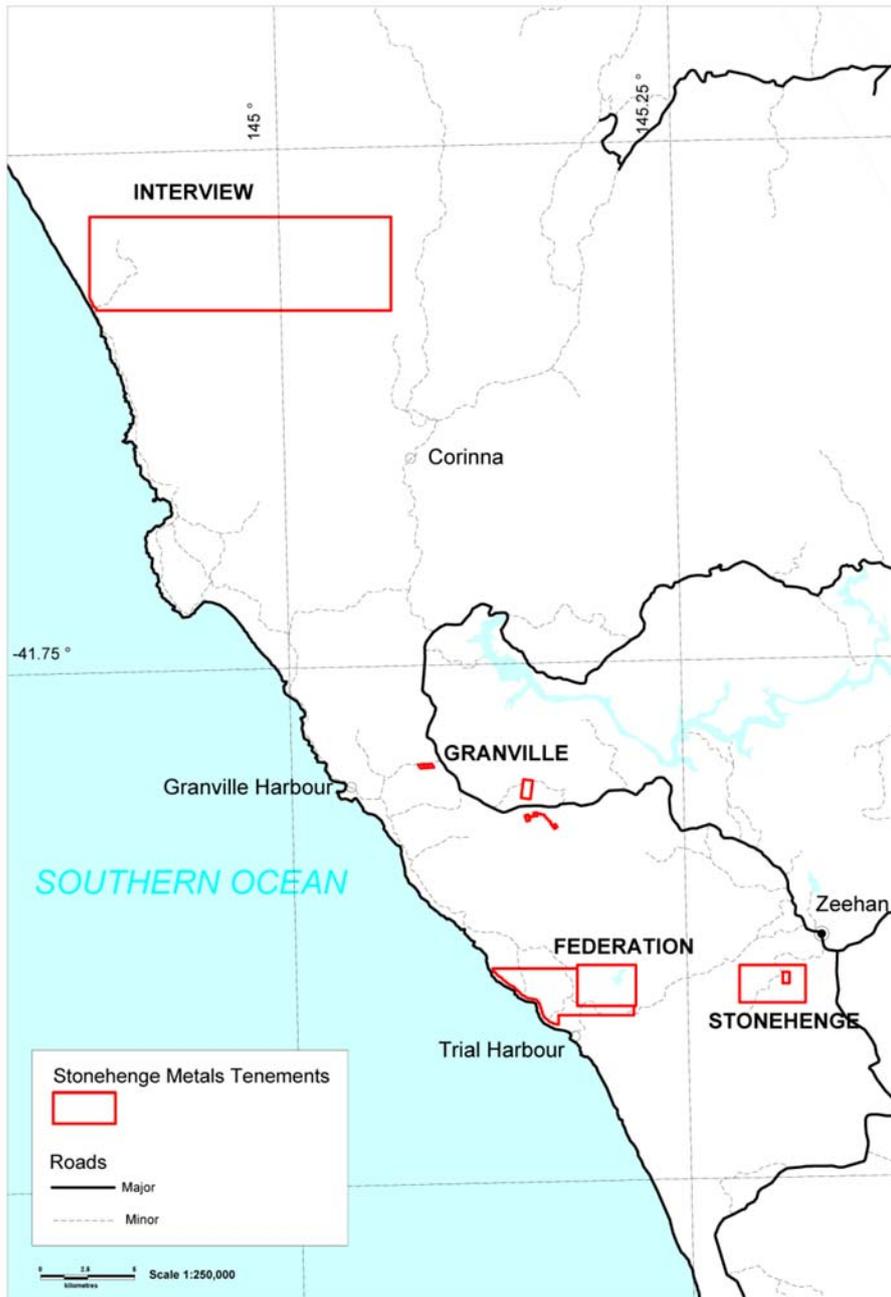


Figure 1. Map showing location of the Cumberland Lake/ Federation Exploration lease EL 31/2002.

2.1 Regional Geology

The main features of the regional geology are a large granite dome which intruded a sequence of Proterozoic sedimentary rocks (older than 600 Ma) during Late Devonian times (c.390 Ma ago). The granite is known as the Mt Heemskirk granite with the mountain of that name being located in the north east of the granite outcrop and rising to 742m. Mt Agnew, another significant topographic feature, is located in the south eastern area of the granite outcrop, rises to 848m, and lies 9km due west of the township of Zeehan.

The broad regional geology is presented in Figure 2 along with Stonehenge Metals tenements.

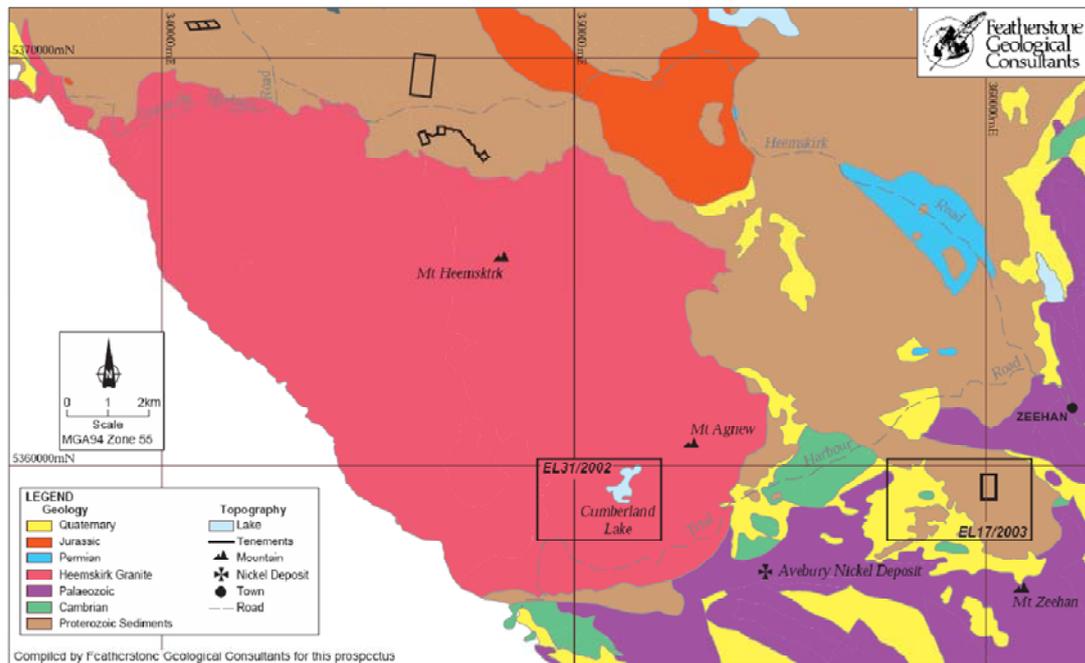


Figure 2. Regional Geology of the Zeehan Area, Stonehenge Metals tenements shown.

The granite is a coarse grained tourmaline rich muscovite granite. Its outcrop is roughly oval in shape, elongated E-W, with the western portions extending to the west under the sea. The outcrop is 10km north to south and the granite is not homogeneous with several different variations able to be mapped. The intrusion shows chilled margins within 2m to 3m of the contact where it is a fine grained, white, aplitic granite. The main body of the intrusion is formed of a red granite but in some areas a white granite is present and tin mineralisation may be associated with the white granite.

The Proterozoic rocks are mainly quartzite, micaceous quartzite, and black shale of the Oonah Formation. Carbonate rich beds are also present. These rocks have undergone medium grade regional metamorphism and may also have been subjected to contact metamorphic effects close to the granite where they were heated by the granite magma.

In the south east and the south rocks of Cambrian age are present and these are also intruded by the granite. These are mostly sedimentary but also include some

ultramafic bodies which are attracting attention as part of a new geological model for economic nickel deposits such as the Avebury deposit.

The late stages in the crystallisation of the granite resulted in the production of hot saline solutions containing various metallic elements. Stresses produced by the intrusion resulted in faults and fractures in the country rocks and also fractures in the granite itself in some places. The solutions carrying the metallic ions were able to enter some of the fissures and as the solutions travelled along them they began to cool and precipitate minerals which crystallised on the walls of the fissure and formed a vein. Such fissures are called lodes and such mineralisation is referred to as hydrothermal mineralisation. Since different metallic minerals crystallize at different temperatures those that crystallize at higher temperatures are deposited first and the others further along, or up, the lode. This results in a zonation of the mineralisation with high temperature minerals near the granite and lower temperature minerals further away.

2.2 Local Geology and exploration rationale

The tenement is entirely within a granite dome known as the Mt Heemskirk granite which has intruded a sequence of Proterozoic sedimentary rocks during the Late Devonian. The Heemskirk granite is a multiphase intrusion with tin mineralisation being related to the latest phase. The licence covers a number tin bearing lodes in an area known as the South Heemskirk Tin field.

A number of tin exploration targets occur within the granite near the southern contact. Historic mines here were mainly based on lode style mineralisation, however at Sweeney's the mineralisation is greisen tin-zinc style. A defined magnetic anomaly to the west of Sweeney's may be caused by another body of greisen mineralisation.

The focus of exploration is the Sweeney's tin-zinc prospect. During the late nineteen seventies a total of eighteen diamond drill holes were drilled into the Sweeney's mine. Although eight of these missed the target mineralisation, information from the remaining ten holes was used to assign a tonnage and grade estimate to the mineralisation of 500,000 tonnes at 0.6% tin. The tin mineralisation was open at depth and along (an interpreted SSE) strike. The most northerly adit contained 47 metres at 0.6% tin, 0.96% zinc and 7 g/t silver.

In April 2008, a JORC code compliant resource of **562,000t at 0.5% tin, 1.4% zinc and 36 g/t silver containing 2,869 tonnes of tin, 8,000 tonnes of zinc and 657,000 ounces of silver** was calculated on the Sweeney's deposit based on 17 diamond cored drill holes drilled in 1977 and 1978. See resource report in Appendices and also Section 5.2.1 of the report.

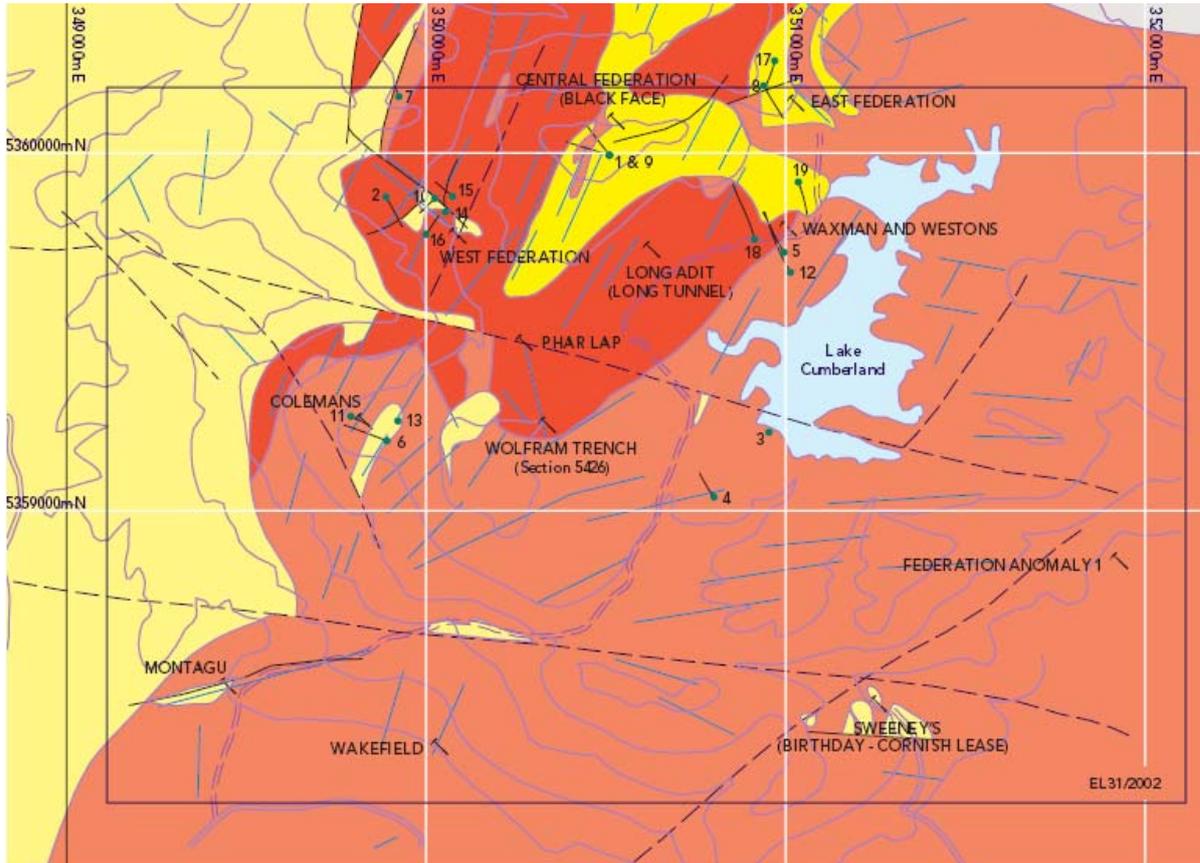


Figure 3. Prospect geology, historic working and drill-holes.

3 Previous Exploration

Historic compilation (modified) by Featherstone Geological Consultants for the Stonehenge Metals prospectus, principal consultant -- Dr A C Gifford.

3.1 South Heemskirk Tin field

Alluvial tin was discovered here by a surveyor in 1876 followed by primary mineralisation in lodes. By 1881 nine treatment plants had been erected comprising 80 heads of stamps with another four shortly afterwards. Unfortunately many of the prospects had not been developed to any extent and were unable to feed a regular supply of ore to a plant so production did not commence until 1884. In a number of cases the rich veins did not extend far along strike or down dip and in some others it was suspected that the presence of black tourmaline had led to an over estimation of grade.

In a few instances the ore contained a substantial amount of pyrite and the plants had not been designed to cope with pyrite. This resulted in many of the plants being unable to operate or only at reduced capacity. Since most of the money raised had been spent on plant and transporting it to the site there was little left to finance development of the mines. The Cumberland Mines were reputed to have produced a good amount of ore but no records of production are extant. The boom then turned to bust and no one would invest in South Heemskirk. The field was described as practically deserted in 1890.

3.2 The Federation Mine

In 1900 the Federation Tin Mining Co. NL was formed with a lease over the West Cumberland, Cumberland, and East Cumberland Mines. The West Cumberland lodes became the Western Workings with the Whip Shaft. About 600m NE the Cumberland lodes became the Central Workings with the Munro Shaft that was sunk from the top of a hill which was the highest point on the property. A single lode and minor workings 500m ENE of Munro Shaft formed the Eastern Workings. A sketch plan of the mines is shown in Figure 4. Levels at all workings at the mine were based on the depth below the collar of the Munro Shaft. Due to the topography of the area the lodes were often able to be accessed by means of adits driven from the sides of the hills which was a big advantage rather than having to sink shafts. Little work was then done except on the Tributors Workings.

Between 1920 and 1923 the Company explored and sampled the ore bodies despite limited capital. In 1926 Federation Tin Mines Ltd was floated in England. Work started the following year and about 80,000 pounds was spent on plant, a hydro electric scheme, and the construction of a self acting tramway from the Western Workings to a treatment plant 45m down the hill. A horse tramway was constructed from the Central workings to the Western Workings to connect up to the self acting tramway. Production commenced in 1928 but was suspended from 1929-1934 due to the low price of tin and lack of capital. Two boreholes drilled by the Government in 1938 proved disappointing and the Company went into liquidation shortly after.

From 1939-1942 a private operator extracted about 7.5t of concentrate, mainly from the Western Workings and from 1942-1953 about 7t of concentrate was produced from an area about 600m south of Munro Shaft. Total Production from the Federation Mine area is estimated at 327t of concentrate containing 197t of tin metal. Analysing some of the production records the estimated average grade of the ore was 1.34% Tin.

3.3 The Wakefield Mine

This is located about 1.7km just west of south of the Munro's Shaft at the Federation Mine. This was another of the mines which spent all their money on plant before developing the mine. Only one lode has been reported here striking N-S. An adit has been driven about 15m along the lode but is not accessible. No reported production.

3.4 The Montagu Mine

The old workings lie 1.6km SSW of the Munro's Shaft on the Federation Mine. It was the original Montagu Company which, in conjunction with the Cumberland Company constructed the Cumberland Dam with the object of supplying their mines with power and water. It is not stated when mining and treatment was started but in 1882 the mine flooded because the whim dewatering system could not cope with the inflow. At this stage the main shaft had been sunk to 36m with a crosscut at 30.5m and crossing lodes had been driven on; however the mine did not reopen. The Main Lode was up to 3.6m wide and contained rich shoots of cassiterite veining. It is reputed that 6 tonnes of cassiterite were produced from the Montagu lodes and 5t of alluvial cassiterite from alluvium in the Montagu Creek.

Subsequently a private miner worked the lodes at surface by underhand stoping to produce a small amount of concentrate. In 1943 another miner drove adits east and west from Montagu Creek and exposed several tin bearing lodes.

3.5 Colemans

This prospect lies about 1.4km south-west of the Munro's Shaft on the Federation Mine. The workings consist of two adits and several trenches. No recorded production. Renison held an option to purchase this prospect and drilled three holes on it, Fed-6, Fed-11, & Fed-13. Fed- 6 had a best intersection of 4m at 0.43% Tin but the other two holes did not intersect mineralisation. The option was allowed to lapse.

3.6 Sweeney's

This mine lies 1.5km south south-east of Munro's Shaft on the Federation Mine and is also known as Birthday or Cornish Lease. The mineralisation was unusual for the area in containing abundant black sphalerite with pyrite and small amounts of stibnite and chalcopyrite in a gangue of quartz, siderite, fluorite, and tourmaline. A 75m adit was driven into the hill and a crosscut at 30m intersected a thin vein of cassiterite with pyrite in sericitic kaolinised granite containing some mineralisation that is referred to as "greisen". In 1903-1904 about 13 tonnes of cassiterite was produced but it is believed that this was alluvial from Pykes Creek. The greisen mineralisation was later appraised by Renison Ltd. A number of outcrops of these bodies of greisen were located by soil sampling and geophysics.

3.7 Wolfram Trench

This prospect is on one of the few tungsten bearing lodes and was described by Waterhouse 1915. It is located about 750m due south of Munro's shaft and consists of trench up to 3m deep on a bearing of 328°. The trench exposes white quartz with a little green tourmaline and wolframite with minor cassiterite which appeared to be about 18m wide although the full width of the reef was not covered by the trench. The reef was judged to strike at 280° and dip south at 28° but the dip was uncertain.

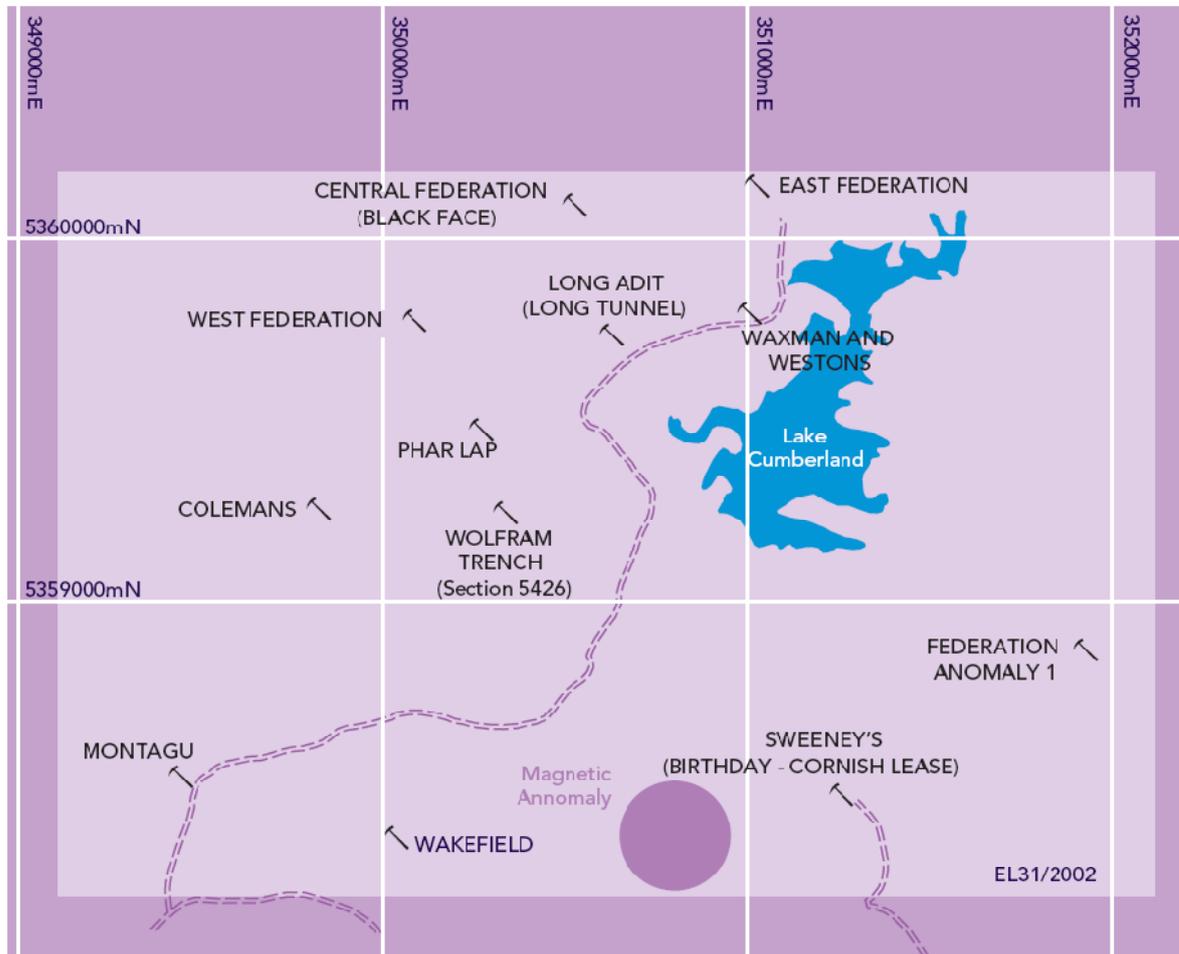


Figure 4. Location of historic workings and magnetic anomaly.

3.8 Modern Exploration

Renison Ltd (Renison) were granted EL11/1976 (26 km²) to look for large low grade tin deposits in the South Heemskirk Tin Field. In the first year of exploration interest was focussed on the Sweeney's Mine and sampling of the old adit (which terminated in mineralisation) gave 47m at 0.6% Tin, 0.96% zinc, & 7 g/t silver. Seventeen diamond cored holes were drilled during 1976 but the mine is located on a steep hillside and it was difficult to get the drill rig into position to drill optimally oriented holes. Results of the drilling are summarised below.

Hole No.	Intercept (m)	Tin Grade %	Zinc Grade %	Silver g/t	Comment
Swy 1-3	Failed to intersect main greisen zone				
Swy 4	51	0.50	2.7	14	
Swy 5	Drilled in margin of greisen				
Swy 6	Drilled below the greisen				
Swy 7	38	0.75	2.84	31	
Swy 8	32	0.41	1.03	23	
Swy 9	Drilled to the south of the greisen				
Swy 10	Drilled to the south of the greisen (intersected altered granite)				
Swy 11	23	1.17	1.7	121	Stannite & Topaz
Swy 12	In margin of greisen				
Swy 13	In margin of greisen				
Swy 14	23.6	0.27	0.52	42	In top of greisen
Swy 15	31.4	0.62	1.92	31	
Swy 16-17	Failed to intersect main greisen zone				

Table 1. Sweeney's Drilling

This drilling attempted to elucidate the shape of the mineralized zone however the topography in the area makes establishing suitable drill sites very difficult. This resulted in the holes being drilled in various directions, being collared at different heights, and is totally irregular so no survey data are presented in this report. The shape of this body of mineralisation is also irregular which resulted in a significant number of the holes (11 out of 17) failing to make satisfactory intersections. The results obtained do not define the shape of this zone of mineralisation. Various geophysical surveys were conducted to see if they could aid in defining the limits of the mineralisation but were of only limited value.

The assay results that have been obtained from the successful intersections were considered very encouraging. Since it was not known what the distribution of greisen zones was in the Heemskirk granite as a whole the EL was enlarged to 88 km² in July 1977 to cover the entire outcrop of the granite. Colour air photography and photo-geological interpretation were commenced over the whole tenement area. An access road to the Federation area was put in and gridding, mapping, and geochemical sampling of this area commenced.

During 1978-79 a further cored diamond hole was drilled at Sweeney's, (Swy 18. 249m), which failed to locate any mineralisation. Six cored diamond holes for 986m (Fed.1-6) were drilled on the Federation Plateau area mainly to follow up on the geophysical anomalies. Zones of alteration were intersected but only intercepts of low grade tin mineralisation of limited extent were found. The location of these drill holes is shown in Figure 3.

Hole FED001 was drilled into the Black Face Lode on the Federation Mine in a zone of intense alteration including complete tourmalinisation. Tin values were extremely low. Enquiries regarding the lack of tin mineralisation found that the lode is reputed to only carry tin in one section.

In 1979-80 six more cored diamond holes (FED007-012) for 978m were drilled in the Federation area. More zones of greisen were identified but tin grades were low and inconsistent. In July FED013 for 70m was drilled near Coleman's workings in order to make a decision on an option over this ground. Only red granite was encountered and it was recommended that the option not be exercised. Additional geophysical surveys were also being conducted to locate greisen zones and guide drilling.

In September 1996, Newnham reviewed the existing data for EL59/94 for the license holder David Lane. EL59/94 covered EL 31/2002 area in part. He recommended a number of items/areas for follow up which are summarised below.

Eastern Workings – possible extensions of the Zn rich alteration zone intersected in FED008 beneath the Eastern Workings have not been tested to the South towards Waxman's and Westons workings.

Waxman & Westons – a very large pyritic alteration zone exists in the vicinity of the Eastern Workings and Waxman & Westons. It has been tested by six cored holes which showed the zone to be very low in tin but containing significant zinc values in places. Possible extensions of these zinc intervals to the west are untested by drilling.

Sweeney's – drilling at Sweeney's has located two interconnected stanniferous polymetallic sulphide deposits one flat lying and one steeply dipping. Further drilling is required to more fully define potential tonnages and grades. Mineralogy is complex and further metallurgical work would be required to identify possible routes for upgrading the mineralisation into saleable concentrates.

Anomaly One – a tin-zinc-copper-silver zone of mineralisation in FED020 and a cassiterite zone in FED021 are considered worthy of further evaluation. This could best be done initially by drilling three close spaced cored holes adjacent to each intersection. This would establish the orientation of the mineralisation and provide a basis for further wide spaced drilling.

3.9 Work during current tenement.

Prior to Stonehenge Metals involvement, McDermott Mining restarted an exploration program consisting of the following:

- Repeat literature review of Report 18-1466 Federation Area E.L.11/76, Renison Exploration.
- Following visits to the area by mines inspector and forestry inspectors, a potential roadway deviating from the steep access road to Sweeney's was surveyed and flagged for future reference. Preliminary study of open cut areas above main adit at Sweeney's was conducted to determine the feasibility of open cut with a view to separating the high grade sphalerite from the high grade cassiterite and producing two concentrates or two high grade wet ores for sale to existing local companies.
- Sampling and assaying of the entire wall area of the number five open cut returned an average grade of 1.5% tin over thirty metres with the face averaging 3% tin across ten metres width. As well, the face gave assays of up to 23% zinc in sphalerite form. Test work performed at Amdel

Laboratories, South Australia, indicated the zinc could easily be removed from the gangue and concentrated using standard flotation treatment such as is used at Zinifex' Rosebery plant. The tin recovery presented a more difficult scenario as the majority of the cassiterite tended report to the sphalerite con. and with the research laboratory being the subject of a takeover, the final test results were lost. However, enough encouragement was given to pursue this avenue and further test work is expected will be conducted in the future. Discussions with Burnie Research Laboratories bide well for a comprehensive study of the Sweeney's ore being conducted in the near future.

- Further bulk sampling of the main adit at Sweeney's was carried out to determine the outline of the sphalerite zone. It appears the sphalerite is disseminated throughout the areas of cassiterite dissemination with the more enriched areas of mineralisation outlined in previous sampling hosting higher grades of both minerals although this may only be typical of the areas sampled. It was determined that there was not enough ore zone exposed either by excavation or drilling to determine whether this was typical of the total ore zone or simply an isolated occurrence.

In June 2006, the tenement, together with others operated by McDermott Mining, became the subject of an IPO and consulting geologist, Mr. Greg Lear was engaged to carry out field reconnaissance and submit his findings to the proposed IPO company, Stonehenge Metals. Featherstone Geological Consultants, headed by Dr. A.C.Gifford was engaged to report on the prospect for possible inclusion in the proposed IPO. A section of this report pertaining to this particular tenement is attached.

4 Exploration completed to November 2007

4.1 Regional exploration activities

A literature review and compilation of historic data by Featherstone Geological Consultants as background for an independent geological report for Stonehenge Metals prospectus to float on the Australian Securities Exchange. A field visit was completed after the acquisition of the tenement from McDermott Mining in January 2007. Compilation of a regional data set and geological model was started.

Two days of collating and converting historic drill-hole coordinates into digital format. One week of modelling and evaluation of the Sweeney's tin-zinc deposit and surrounds to allow for planning of drilling. An aeromagnetic and radiometric survey was completed over the tenement.

5 Exploration completed during the current reporting period

In summary the following work was completed during the reporting period:

- Geophysical survey (results received in report period).
- Continuation of review and compilation of historic data.
- A JORC code compliant Inferred resource of **562,000t at 0.5% tin, 1.4% zinc and 36 g/t silver containing 2,869 tonnes of tin, 8,000 tonnes of zinc and 657,000 ounces of silver** was calculated on the Sweeney's deposit based on 17 diamond cored drill holes drilled in 1977 and 1978.

- Field visit to Federation plateau and reconnaissance sampling.
- Existing track clearing to Anomaly One.
- Petrology was completed on one sample from the Sweeney's deposit.

5.1 Regional Exploration

5.1.1 Exploration activity map

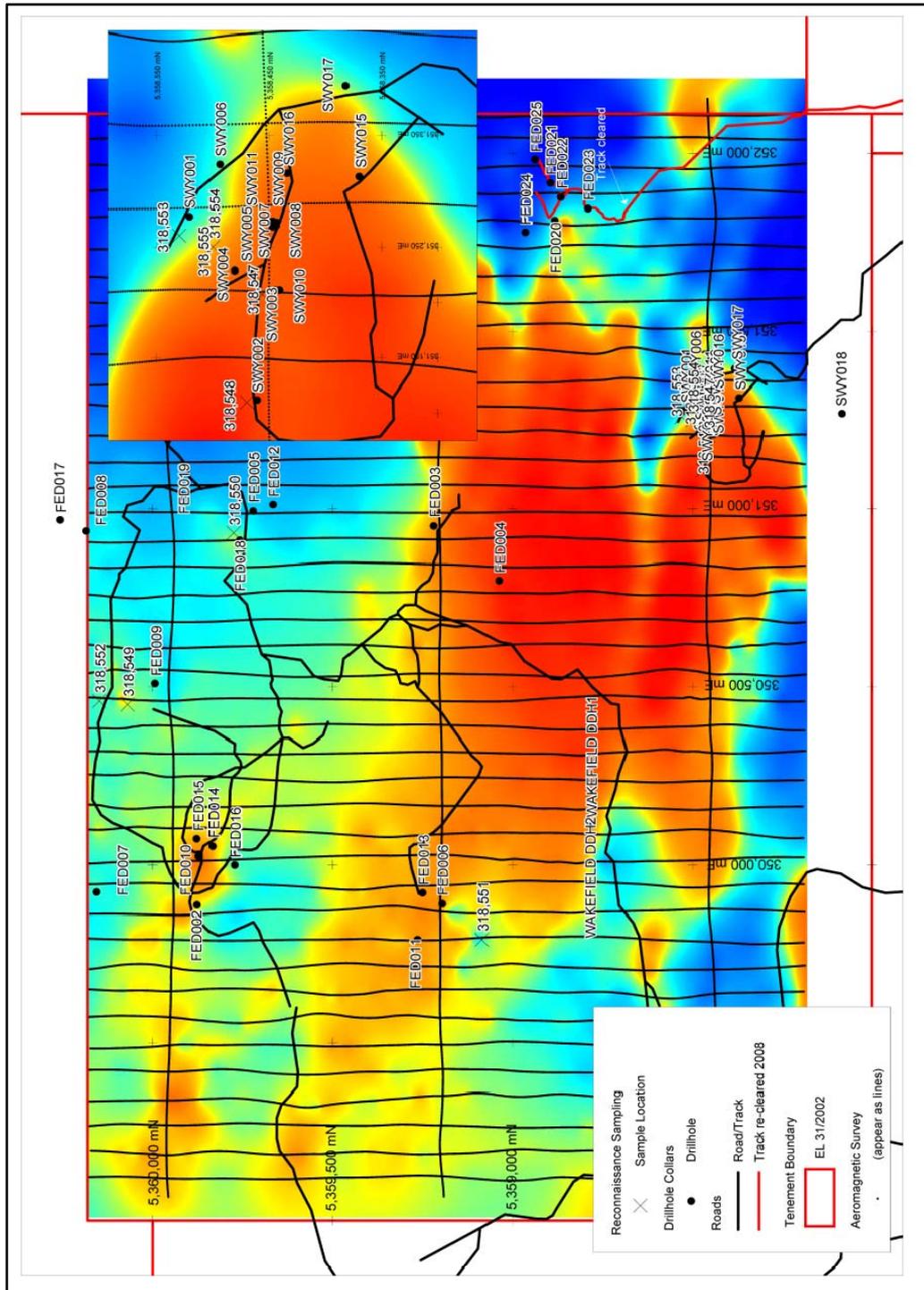


Figure 5. Exploration completed during 2008, with map insert of Sweeney's shown. Airborne geophysical survey lines (TMI image shown), reconnaissance sampling

(sample numbers shown), track cleared to Anomaly One (FED020) and previous drill holes digitised.

5.1.2 Literature review and compilation

Work continued on obtaining and reviewing historic work related to the licence area and converting this into digital format, see Appendices for drill hole digital data.

5.1.3 Geophysics

An airborne geophysical survey and digital terrain mapping was carried out over the entire lease area (at the time) by GPX Airborne Pty Ltd in June 2007. The data had been processed by August 2007, this included removal of diurnal variations in the magnetic field, subtraction of the earth's field (IGRF) from the recorded data, gridding and levelling. The survey collected Magnetic and Radiometric information, the data is included in the digital appendices, the full survey specifications are included in the ReadMe.txt file.

5.1.4 Geochemistry

A number of surface samples were collected during a field visit to the Federation Plateau in April 2008. They were assayed for copper, lead, zinc, silver tin, tungsten trioxide and bismuth at Burnie Research Lab (AMMTEC), Burnie. A summary of the significant results are shown in Table 2 and their location shown in Figure 5 and a summary of significant results in Figure 6. The full results are shown in Appendix 1.

Prospect	Zn %	Sn %	Pb ppm
Sweeney's adit floor sample	1.9%	0.9%	328
Sweeney's adit floor sample	-	0.7%	136
Central Federation float sample	0.2%	-	4769 (0.5%)
Central Federation Mine dump sample	1.3%	0.7%	342
Waxmans & Westons costean dump sample	-	0.6%	49
Colemans dump sample	-	0.2%	497

Table 2. Significant surface sample results from the Federation Plateau taken in April 2008.



Figure 6. Significant surface sample results from the Federation Plateau taken in April 2008 and Sweeney's resource.

5.2 Exploration at Sweeney's

A number of field visits were made to the Sweeney's deposit during the year to;

- Locate historic drill holes and obtain GPS co-ordinates, hole locations are shown in Appendices.
- Obtain samples for assaying to confirm mineralisation (included in section 5.1.4 Geochemistry – full results in appendices).
- Obtain samples for specific gravity (see resource report in appendices) and petrology (see appendices).
- Assess the viability of further sampling and drilling work.

5.2.1 Sweeney's Resource calculation

On the 21st of April 2008, Stonehenge Metals Limited announced to the Australian Securities Exchange an Inferred resource for the Sweeney's deposit of;

562,000t at 0.5% tin, 1.4% zinc and 36 g/t silver containing 2,869 tonnes of tin, 8,000 tonnes of zinc and 657,000 ounces of silver.

The following is from the announcement;

The Sweeney's resource has a number of positive attributes that bode well for its potential commercial development:

- Mineralisation starts at the surface and is open in all directions
- The bulk of the resource is shallow and is potentially amenable to open pit mining
- Potential to expand the resource and add additional resources from the adjacent Anomaly One deposit
- The deposit is located adjacent to a road and is within 10km of milling infrastructure

The company has initiated a preliminary scoping study to assess the potential commercial development of the project. Further work will focus on bulk sampling to test the metallurgical characteristics of the mineralisation and exploration modelling to determine trenching and drilling locations. Exploration will also commence on Anomaly One with the objective of identifying additional resources to complement the Sweeney's resource.

Resource Estimation Methodology:

The resource estimate is based on 17 diamond drill holes designed to intersect the mineralisation on a nominal 50m by 50m spacing. The deposit was been modelled in three dimensions using cross sectional interpretations of the geology and mineralisation. The deposit boundary was defined by a 0.2% Tin (Sn) cut-off grade which coincides with the geological boundary of the shear zone. Individual blocks were defined around drill hole intersections with block boundaries on and between cross sections were defined by the midpoints between adjacent holes and by geological constraints. Estimation methodologies included inverse distance squared and ordinary kriging. Based on statistical analysis, maximum sample assays were reduced to 3% Tin, 10% zinc and 160gpt silver (top cuts) and all grades were length weighted. Block densities were assigned based on sampling from Sweeney's underground adit and surface pits.

The full details of the resource calculation are in the resource report included in the appendices. See Figure 7 for drill hole locations and an outline of the deposit.



Figure 7. Plan of the resource outline and drill holes at Sweeney's.

6 Discussion, Conclusions and Further Work

It is suggested that the recommendations of Newnham 1996 summarised in Section 3.8 be followed. Therefore the following work for 2009 is recommended;

Exploration planed during 2009:

1. Prepare drill access to Sweeney's.
2. Drill a number of drill holes into the mineralisation at Sweeney's for metallurgical testing. Drilling proposed would total approximately 100m.
3. Conduct metallurgical testing of the material obtained.

This work would better determine the viability of pursuing further mineralisation at Sweeney's -- with the view of expanding the resource if the metallurgical test work is encouraging. It may also help determine the viability of other areas within the lease although there are indications that there is considerable variation in the mineralogy of the other deposits.

7 Environment

The historic track to Anomaly One was cleared, no rehabilitation required. All other work has been low impact to date. No rehabilitation or other non-exploration surveys carried out. It was noted that recreation vehicle access to the area had caused damage to a number of the tracks on the lease. No company vehicles accessed the plateau area.

8 Expenditure

The expenditure commitment for the report period is \$16,427 the amount spent at the time of the report was \$43,784.

December quarter 2007	\$25,950
March quarter 2008	\$14,435
June quarter 2008	\$20,669
September quarter 2008	\$4,520
December quarter 2008 to date	\$4,160
Total for year at time of report (March to December quarters)	\$43,784

9 References

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Appendix 1 – Surface Sampling

Sample No	Easting WGS_84_Zone_55	Northing WGS_84_Zone_55	Comment	Geology	Date	Sampled by	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Au ppm	Sn ppm	WO3 ppm	Bi ppm	SG units
318547	351207	5358456	Sweeney's	Granite, crushed sample from surface, slightly weathered.	April 2008	Mike Cowin, David Vaarwerk	4	27	24	1		110	190	12	
318548	351110	5358470	Sweeney's	Granite, rock chip sample from surface containing pyrite.	April 2008	Mike Cowin, David Vaarwerk	6	20	85	3		130	80	27	
318549	350450	5360070	Federation central	Gossan	April 2008	Mike Cowin, David Vaarwerk	667	4769	1580	8		260	40	46	
318550	350912	5359759	from near Fed018		April 2008	Mike Cowin, David Vaarwerk	33	49	102	1		6420	250	182	
318551	349790	5359085	Colemans	Altered black grey rock	April 2008	Mike Cowin, David Vaarwerk	41	497	69	1		2170	130	779	
318552	350460	5360150	Federation central		April 2008	Mike Cowin, David Vaarwerk	207	342	13200	6		7090	320	27	
318553	351260	5358530	Sweeney's adit, near entrance	Granite. Green alteration, sulphides	April 2008	Mike Cowin, David Vaarwerk	11	136	138	3		6530	350	37	
318554	351250	5358500	Sweeney's adit, from near end	Granite, sulphides. SG assay sample	April 2008	Mike Cowin, David Vaarwerk	287	328	19300	9		9460	560	40	
318555	351250	5358500	Sweeney's adit, from near end. G sample. Sample available.	Granite, sulphides. SG sample	April 2008	Mike Cowin, David Vaarwerk									3.15

Appendix 2 – Historic Drill hole details

Collars

DataSet	Hole_ID	Hole_Type	Max_Depth	Orig_East	Orig_North	Orig_RL	Lease_ID	Hole_Status	Prospect	Date_Completed	Date_Started	Data_Source	Historic_Hole_ID	Historic_Hole
Federation	FED001	DD	198	350509.43	5359993.81	512.37	EL31/2002	COMPLETE	Federation	12/01/1979		Renison Limited (Exploration)	FED001	TRUE
Federation	FED002	DD	138	349887.427	5359876.813	393.82	EL31/2002	COMPLETE	Federation	1/02/1979		Renison Limited (Exploration)	FED002	TRUE
Federation	FED003	DD	132	350952.445	5359218.808	410	EL31/2002	COMPLETE	Federation	20/02/1979		Renison Limited (Exploration)	FED003	TRUE
Federation	FED004	DD	131	350799.446	5359037.809	420.49	EL31/2002	COMPLETE	Federation	1/03/1979		Renison Limited (Exploration)	FED004	TRUE
Federation	FED005	DD	202	350994.438	5359721.808	417.31	EL31/2002	COMPLETE	Federation	14/03/1979		Renison Limited (Exploration)	FED005	TRUE
Federation	FED006	DD	187	349890.436	5359194.815	414.22	EL31/2002	COMPLETE	Federation	2/04/1979		Renison Limited (Exploration)	FED006	TRUE
Federation	FED007	DD	98	349923.423	5360157.812	371.87	EL31/2002	COMPLETE	Federation	14/01/1980		Renison Limited (Exploration)	FED007	TRUE
Federation	FED008	DD	152	350938.431	5360186.808	471.002	EL31/2002	COMPLETE	Federation	3/01/1980		Renison Limited (Exploration)	FED008	TRUE
Federation	FED009	DD	156	350509.43	5359993.81	512.296	EL31/2002	COMPLETE	Federation	28/01/1980		Renison Limited (Exploration)	FED009	TRUE
Federation	FED010	DD	139	350024.428	5359872.812	426.433	EL31/2002	COMPLETE	Federation	20/01/1980		Renison Limited (Exploration)	FED010	TRUE
Federation	FED011	DD	122	349790.434	5359263.815	415.388	EL31/2002	COMPLETE	Federation	11/02/1980		Renison Limited (Exploration)	FED011	TRUE
Federation	FED012	DD	311	351012.439	5359665.808	416.838	EL31/2002	COMPLETE	Federation	16/02/1980		Renison Limited (Exploration)	FED012	TRUE
Federation	FED013	DD	70	349921.436	5359249.815	425.55	EL31/2002	COMPLETE	Federation	11/07/1980		Renison Limited (Exploration)	FED013	TRUE
Federation	FED014	DD	105	350052.429	5359833.812	425.26	EL31/2002	COMPLETE	Federation	12/01/1981		Renison Limited (Exploration)	FED014	TRUE
Federation	FED015	DD	101	350073.428	5359877.812	437.56	EL31/2002	COMPLETE	Federation	21/01/1981		Renison Limited (Exploration)	FED015	TRUE
Federation	FED016	DD	110	349999.429	5359772.813	399.45	EL31/2002	COMPLETE	Federation	27/01/1981		Renison Limited (Exploration)	FED016	TRUE
Federation	FED017	DD	200	350969.43	5360256.807	485.95		COMPLETE	Federation	6/02/1981		Renison Limited (Exploration)	FED017	TRUE
Federation	FED018	DD	281	350912.437	5359758.808	415.55	EL31/2002	COMPLETE	Federation	17/02/1981		Renison Limited (Exploration)	FED018	TRUE
Federation	FED019	DD	197.3	351035.136	5359917.907	420.2	EL31/2002	COMPLETE	Federation	12/01/1982		Renison Limited (Exploration)	FED019	TRUE
Federation	FED020	DD	158	351811.458	5358882.803	320	EL31/2002	COMPLETE	Federation	21/01/1982		Renison Limited (Exploration)	FED020	TRUE
Federation	FED021	DD	117	351916.959	5358894.702	288.6	EL31/2002	COMPLETE	Federation	28/01/1982		Renison Limited (Exploration)	FED021	TRUE
Federation	FED022	DD	230	351876.959	5358865.903	313	EL31/2002	COMPLETE	Federation	5/02/1981		Renison Limited (Exploration)	FED022	TRUE
Federation	FED023	DD	233	351845.059	5358790.103	299.3	EL31/2002	COMPLETE	Federation	20/02/1982		Renison Limited (Exploration)	FED023	TRUE
Federation	FED024	DD	186	351778.456	5358964.803	348.1	EL31/2002	COMPLETE	Federation	4/02/1983		Goldfields Exploration Pty Ltd	FED024	TRUE
Federation	FED025	DD	198.2	351982.458	5358937.802	296	EL31/2002	COMPLETE	Federation	14/02/1983		Goldfields Exploration Pty Ltd	FED025	TRUE

Federation	FED026	DD	122.8	352622.461	5359287.798	407.6		COMPLETE	Federation	1/03/1983		Goldfields Exploration Pty Ltd	FED026	TRUE
Federation	SWY001	DD	149	351277	5358521	285.549	EL31/2002	COMPLETE	Sweeneys	8/06/1977	25/05/1977	Renison Ltd	SDD001	TRUE
Federation	SWY002	DD	101.5	351112	5358461	353.416	EL31/2002	COMPLETE	Sweeneys	14/06/1977	10/06/1977	Renison Ltd	SDD002	TRUE
Federation	SWY003	DD	152.5	351211	5358445	331.998	EL31/2002	COMPLETE	Sweeneys	23/06/1977	15/06/1977	Renison Ltd	SWY001	TRUE
Federation	SWY004	DD	101	351229	5358481	319.52	EL31/2002	COMPLETE	Sweeneys	29/06/1977	25/06/1977	Renison Ltd	SWY002	TRUE
Federation	SWY005	DD	80.4	351228	5358481	319.44	EL31/2002	COMPLETE	Sweeneys	1/07/1977	29/06/1977	Renison Ltd	SWY003	TRUE
Federation	SWY006	DD	155.2	351324	5358494	292.3	EL31/2002	COMPLETE	Sweeneys	15/07/1977	5/07/1977	Renison Ltd	SWY004	TRUE
Federation	SWY007	DD	95.5	351268	5358447	322.58	EL31/2002	COMPLETE	Sweeneys	20/07/1977	15/07/1977	Renison Ltd	SWY005	TRUE
Federation	SWY008	DD	137.3	351269	5358444	322.53	EL31/2002	COMPLETE	Sweeneys	27/07/1977	21/07/1977	Renison Ltd	SWY006	TRUE
Federation	SWY009	DD	102.5	351272	5358444	322.36	EL31/2002	COMPLETE	Sweeneys	4/08/1977	1/08/1977	Renison Ltd	SWY007	TRUE
Federation	SWY010	DD	92.4	351211	5358441	332.11	EL31/2002	COMPLETE	Sweeneys	9/08/1977	6/08/1977	Renison Ltd	SWY008	TRUE
Federation	SWY011	DD	134.3	351273	5358447	322.6	EL31/2002	COMPLETE	Sweeneys	17/08/1977	11/08/1977	Renison Ltd	SWY009	TRUE
Federation	SWY012	DD	191.5	351313	5358370	323.24	EL31/2002	COMPLETE	Sweeneys	1/09/1977	20/08/1977	Renison Ltd	SWY010	TRUE
Federation	SWY013	DD	140	351313	5358370	323.24	EL31/2002	COMPLETE	Sweeneys	12/09/1977	1/09/1977	Renison Ltd	SWY011	TRUE
Federation	SWY014	DD	191.5	351313	5358370	323.1	EL31/2002	COMPLETE	Sweeneys	21/09/1977	14/09/1977	Renison Ltd	SWY012	TRUE
Federation	SWY015	DD	254.5	351313	5358370	323.24	EL31/2002	COMPLETE	Sweeneys	10/10/1977		Renison Ltd	SWY013	TRUE
Federation	SWY016	DD	257.4	351316	5358434	313.13	EL31/2002	COMPLETE	Sweeneys	26/10/1977	12/10/1977	Renison Ltd	SWY014	TRUE
Federation	SWY017	DD	245.2	351395	5358382	296.17	EL31/2002	COMPLETE	Sweeneys	12/11/1977	28/10/1977	Renison Ltd	SWY015	TRUE
Federation	SWY018	DD	249.1	351269	5358084	270.622	EL31/2002	COMPLETE	Sweeneys	31/10/1978	29/10/1978	Renison Ltd	SWY016	TRUE
Federation	WAKEFIELD DDH1	DD	91	350111.443	5358782.814		EL31/2002	COMPLETE	Wakefield	18/11/1970		Pacific Copper Explorations Limited	WAKEFIELD DDH1	TRUE
Federation	WAKEFIELD DDH2	DD	122	350111.443	5358782.814		EL31/2002	COMPLETE	Wakefield	30/11/1970		Pacific Copper Explorations Limited	WAKEFIELD DDH2	TRUE

Appendix 2 continued

Assay results

Hole_ID	mFrom	mTo	SampleID	Zn_pct	Pb_pct	Ag_ppm	Sn_pct	Bi_pct	CaF2_pct	WO4_ppm
FED001	61.5	62.5	FED001-01	0.065	0.007	1	0.001	0.003		
FED001	62.5	63.5	FED001-02	0.065	0.007	1	0.001	0.003		
FED001	63.5	64.5	FED001-03	0.075	0.006	1	0.001	0.003		
FED001	64.5	65.5	FED001-04	0.16	0.01	1	0.001	0.003		
FED001	65.5	66.5	FED001-05	0.06	0.006	1	0.001	0.002		
FED001	66.5	67.5	FED001-06	0.1	0.014	1	0.001	0.003		
FED001	67.5	68.5	FED001-07	0.015	0.009	1	0.043	0.004		
FED001	68.5	69.5	FED001-08	0.065	0.023	2	0.087	0.002		
FED001	69.5	70.5	FED001-09	0.037	0.016	1	0.001	0.002		
FED001	70.5	71.5	FED001-10	0.11	0.06	11	0.002	0.003		
FED001	71.5	72.5	FED001-11	0.085	0.05	9	0.003	0.002		
FED001	72.5	73.5	FED001-12	0.015	0.005	1	0.024	0.002		
FED001	73.5	74.5	FED001-13	0.013	0.008	1	0.014	0.002		
FED001	74.5	75.5	FED001-14	0.012	0.016	1	0.003	0.002		
FED001	75.5	76.5	FED001-15	0.047	0.026	1	0.002	0.003		
FED001	76.5	77.5	FED001-16	0.065	0.032	3	0.001	0.001		
FED001	77.5	78.5	FED001-17	0.024	0.02	2	0.007	0.002		
FED001	78.5	79.5	FED001-18	0.015	0.16	1	0.001	0.003		
FED001	79.5	80.5	FED001-19	0.125	0.125	1	0.002	0.003		
FED001	80.5	81.5	FED001-20	0.11	0.095	1	0.001	0.003		
FED001	81.5	82.5	FED001-21	0.05	0.037	1	0.001	0.002		
FED001	82.5	83.5	FED001-22	0.06	0.048	1	0.002	0.001		
FED001	83.5	84.5	FED001-23	0.085	0.085	2	0.02	0.003		
FED001	84.5	85.5	FED001-24	0.11	0.026	2	0.002	0.002		
FED001	85.5	86.5	FED001-25	0.055	0.017	3	0.001	0.002		
FED001	86.5	87.5	FED001-26	0.14	0.026	3	0.002	0.003		
FED001	87.5	88.5	FED001-27	0.09	0.029	1	0.002	0.002		
FED001	88.5	89.5	FED001-28	0.095	0.038	3	0.002	0.002		
FED001	89.5	90.5	FED001-29	0.1	0.085	1	0.001	0.004		
FED001	90.5	91.5	FED001-30	0.1	0.075	1	0.003	0.003		
FED001	91.5	92.5	FED001-31	0.1	0.055	1	0.002	0.003		
FED001	92.5	93.5	FED001-32	0.35	0.02	1	0.003	0.003		
FED001	93.5	94.5	FED001-33	0.07	0.05	1	0.004	0.002		
FED001	94.5	95.5	FED001-	0.045	0.019	1	0.003	0.002		

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FED001	95.5	96.5	FED001-35	0.065	0.049	1	0.002	0.002
FED001	96.5	97.5	FED001-36	0.01	0.008	1	0.001	0.002
FED001	97.5	98.5	FED001-37	0.012	0.01	1	0.001	0.002
FED001	98.5	99.5	FED001-38	0.015	0.012	1	0.002	0.002
FED001	99.5	100.5	FED001-39	0.018	0.012	1	0.001	0.001
FED001	100.5	101.5	FED001-40	0.007	0.012	5	0.001	0.002
FED001	101.5	102.5	FED001-41	0.01	0.014	1	0.005	0.002
FED001	145.5	146.5	FED001-42	0.018	0.002	1	0.001	0.003
FED001	146.5	147.5	FED001-43	0.013	0.002	1	0.001	0.03
FED001	147.5	148.5	FED001-44	0.008	0.002	1	0.001	0.004
FED001	148.5	149.5	FED001-45	0.013	0.002	1	0.001	0.004
FED001	149.5	150.5	FED001-46	0.013	0.002	1	0.001	0.006
FED001	150.5	151.5	FED001-47	0.06	0.003	1	0.001	0.02
FED001	151.5	152.5	FED001-48	0.01	0.002	1	0.001	0.004
FED001	152.5	153.5	FED001-49	0.014	0.002	1	0.001	0.01
FED001	153.5	154.5	FED001-50	0.012	0.002	1	0.001	0.01
FED001	154.5	155.5	FED001-51	0.009	0.002	1	0.001	0.004
FED001	155.5	156.5	FED001-52	0.011	0.002	1	0.001	0.011
FED002	81	82	FED002-01	0.01	0.003	1	0.001	0.01
FED002	82	83	FED002-02	0.005	0.001	1	0.001	0.001
FED002	83	83.7	FED002-03	0.006	0.001	1	0.001	0.001
FED002	83.7	85	FED002-04	0.013	0.004	1	0.001	0.001
FED004	35.2	36.2	FED004-01				0.006	
FED004	36.2	37.2	FED004-02				0.004	
FED004	37.2	38.2	FED004-03				0.008	
FED004	38.2	39.2	FED004-04				0.008	
FED004	39.2	40.1	FED004-05				0.016	
FED004	54	55	FED004-06				0.001	
FED004	55	56	FED004-07				0.001	
FED004	56	57	FED004-08				0.001	
FED004	57	58	FED004-09				0.001	
FED004	58	59	FED004-10				0.001	
FED004	59	59.6	FED004-11				0.001	
FED004	69.3	69.85	FED004-12				0.002	
FED005	94	95	FED005-01	0.048	0.011	1	0.001	0.002
FED005	95	96	FED005-02	0.014	0.006	2	0.001	0.003
FED005	96	97	FED005-03	0.026	0.001	1	0.001	0.003

FED005	97	98	FED005-04	0.017	0.003	1	0.001	0.003
FED005	98	99	FED005-05	0.016	0.003	1	0.001	0.004
FED005	99	100	FED005-06	0.044	0.009	1	0.001	0.003
FED005	100	101	FED005-07	0.09	0.009	1	0.001	0.004
FED005	101	102	FED005-08	0.023	0.002	1	0.001	0.004
FED005	102	103	FED005-09	0.022	0.002	1	0.001	0.002
FED005	103	104	FED005-10	0.01	0.005	1	0.078	0.002
FED005	104	105	FED005-11	0.007	0.002	1	0.015	0.004
FED005	105	106	FED005-12	0.02	0.003	1	0.012	0.004
FED005	106	107	FED005-13	0.019	0.003	1	0.118	0.003
FED005	107	108	FED005-14	0.014	0.003	1	0.004	0.001
FED005	108	109	FED005-15	0.017	0.002	1	0.004	0.002
FED005	109	110	FED005-16	0.022	0.002	1	0.006	0.002
FED005	110	111	FED005-17	0.08	0.002	1	0.015	0.003
FED005	111	112	FED005-18	0.145	0.002	1	0.011	0.003
FED005	112	113	FED005-19	0.09	0.002	1	0.002	0.003
FED005	113	114	FED005-20	0.048	0.004	1	0.005	0.003
FED005	114	115	FED005-21	0.03	0.003	1	0.003	0.004
FED005	115	116	FED005-22	0.02	0.001	1	0.001	0.004
FED005	116	117	FED005-23	0.018	0.001	1	0.001	0.002
FED005	117	118	FED005-24	0.041	0.002	1	0.001	0.004
FED005	118	119	FED005-25	0.044	0.002	1	0.001	0.003
FED005	121	122	FED005-26	0.048	0.003	1	0.007	0.003
FED005	122	123	FED005-27	0.046	0.002	1	0.001	0.004
FED005	123	124	FED005-28	0.049	0.002	1	0.001	0.005
FED005	124	125	FED005-29	0.023	0.001	1	0.001	0.005
FED005	125	126	FED005-30	0.022	0.001	1	0.001	0.004
FED005	126	127	FED005-31	0.03	0.002	1	0.001	0.006
FED005	127	128	FED005-32	0.03	0.001	1	0.001	0.005
FED005	128	129	FED005-33	0.055	0.002	1	0.001	0.005
FED005	129	130	FED005-34	0.065	0.003	1	0.001	0.005
FED005	130	131	FED005-35	0.065	0.002	1	0.004	0.005
FED005	131	132	FED005-36	0.03	0.002	1	0.004	0.004
FED005	132	133	FED005-37	0.023	0.001	1	0.001	0.003
FED005	133	134	FED005-38	0.047	0.001	1	0.002	0.004
FED005	134	135	FED005-39	0.023	0.002	1	0.001	0.004
FED005	135	136	FED005-40	0.01	0.003	1	0.001	0.003
FED005	136	137	FED005-	0.013	0.002	1	0.001	0.002

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FED005	137	138	FED005-42	0.023	0.002	1	0.001	0.002
FED005	138	139	FED005-43	0.036	0.001	1	0.001	0.002
FED005	139	140	FED005-44	0.031	0.002	1	0.001	0.002
FED005	140	141	FED005-45	0.024	0.002	1	0.001	0.003
FED005	141	142	FED005-46	0.018	0.002	1	0.001	0.002
FED005	142	143	FED005-47	0.039	0.001	1	0.001	0.002
FED005	143	144	FED005-48	0.062	0.003	1	0.001	0.003
FED005	144	145	FED005-49	0.036	0.004	1	0.001	0.002
FED005	145	146	FED005-50	0.033	0.003	1	0.001	0.004
FED005	146	147	FED005-51	0.031	0.004	1	0.001	0.005
FED005	147	148	FED005-52	0.016	0.003	1	0.001	0.004
FED005	148	149	FED005-53	0.038	0.004	1	0.001	0.005
FED005	149	150	FED005-54	0.033	0.003	1	0.001	0.005
FED005	150	151	FED005-55	0.024	0.002	1	0.001	0.004
FED005	151	152	FED005-56	0.019	0.002	1	0.001	0.004
FED005	152	153	FED005-57	0.06	0.003	1	0.001	0.004
FED005	153	154	FED005-58	0.14	0.003	1	0.001	0.004
FED005	154	155	FED005-59	0.05	0.002	1	0.001	0.005
FED005	155	156	FED005-60	0.05	0.007	1	0.001	0.006
FED005	156	157	FED005-61	0.013	0.002	1	0.001	0.006
FED005	157	158	FED005-62	0.02	0.003	1	0.001	0.005
FED005	158	159	FED005-63	0.055	0.006	1	0.001	0.006
FED005	159	160	FED005-64	0.015	0.001	1	0.001	0.006
FED005	160	161	FED005-65	0.05	0.003	1	0.001	0.003
FED005	161	162	FED005-66	0.05	0.002	1	0.001	0.002
FED005	162	163	FED005-67	0.03	0.002	1	0.001	0.001
FED006	20	21	FED006-01				0.052	
FED006	21	22	FED006-02				0.006	
FED006	22	23	FED006-03				0.011	
FED006	23	24	FED006-04				0.102	
FED006	24	25	FED006-05				0.005	
FED006	25	26	FED006-06				0.003	
FED006	26	27	FED006-07				0.007	
FED006	27	28	FED006-08				0.005	
FED006	28	29	FED006-09				0.002	
FED006	29	30	FED006-10				0.002	
FED006	30	31	FED006-11				0.003	

FED006	31	32	FED006-12						0.026	
FED006	32	33	FED006-13						0.001	
FED006	33	34	FED006-14						0.001	
FED006	34	35	FED006-15						0.001	
FED006	35	36	FED006-16						0.001	
FED006	36	37	FED006-17						0.001	
FED006	37	38	FED006-18						0.001	
FED006	38	39	FED006-19						0.001	
FED006	39	40	FED006-20						0.001	
FED006	40	41	FED006-21						0.02	
FED007	6	7	FED007-01	0.03	0.01	1	0.005	0.002		600
FED007	7	8	FED007-02	0.02	0.01	1	0.002	0.002		600
FED007	8	9	FED007-03	0.03	0.01	1	0.001	0.004		600
FED007	9	10	FED007-04	0.01	0.01	1	0.001	0.006		600
FED007	10	11	FED007-05	0.01	0.01	1	0.001	0.002		700
FED007	11	12	FED007-06	0.01	0.01	1	0.001	0.002		700
FED007	12	13	FED007-07	0.01	0.01	1	0.001	0.001		700
FED007	13	14	FED007-08	0.02	0.01	1	0.001	0.001		800
FED007	14	15	FED007-09	0.02	0.01	1	0.001	0.001		700
FED007	15	16	FED007-10	0.03	0.01	1	0.001	0.001		700
FED007	16	17	FED007-11	0.02	0.01	1	0.001	0.002		700
FED007	17	18	FED007-12	0.03	0.01	2	0.001	0.002		700
FED007	18	19	FED007-13	0.03	0.01	1	0.001	0.001		600
FED007	19	20	FED007-14	0.03	0.01	1	0.001	0.001		700
FED007	20	21	FED007-15	0.02	0.01	2	0.001	0.002		800
FED007	21	22	FED007-16	0.01	0.01	2	0.001	0.001		800
FED007	22	23	FED007-17	0.02	0.01	2	0.001	0.001		700
FED007	23	24	FED007-18	0.04	0.01	1	0.001	0.002		700
FED007	24	25	FED007-19	0.07	0.01	2	0.001	0.002		800
FED007	25	26	FED007-20	0.05	0.01	2	0.001	0.003		800
FED007	26	27	FED007-21	0.04	0.01	3	0.001	0.002		800
FED007	27	28	FED007-22	0.03	0.01	4	0.001	0.003		900
FED007	28	29	FED007-23	0.04	0.01	2	0.001	0.002		800
FED007	29	30	FED007-24	0.03	0.01	1	0.001	0.002		800
FED007	30	31	FED007-25	0.05	0.01	1	0.001	0.002		800
FED007	31	32	FED007-26	0.04	0.01	2	0.001	0.002		300
FED007	32	33	FED007-27	0.04	0.01	2	0.001	0.01		400
FED007	33	34	FED007-	0.03	0.01	2	0.001	0.007		600

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FED007	34	35	FED007-29	0.02	0.01	1	0.001	0.002	300
FED007	35	36	FED007-30	0.03	0.01	1	0.001	0.004	300
FED007	36	37	FED007-31	0.03	0.01	1	0.001	0.005	400
FED007	37	38	FED007-32	0.02	0.01	2	0.001	0.005	300
FED007	38	39	FED007-33	0.02	0.01	2	0.001	0.002	200
FED007	39	40	FED007-34	0.03	0.01	2	0.001	0.003	400
FED007	40	41	FED007-35	0.04	0.01	1	0.003	0.005	500
FED007	41	42	FED007-36	0.06	0.01	1	0.004	0.003	400
FED007	42	43	FED007-37	0.06	0.01	1	0.002	0.004	400
FED007	43	44	FED007-38	0.05	0.01	1	0.001	0.004	300
FED007	44	45	FED007-39	0.07	0.01	1	0.001	0.002	200
FED007	45	46	FED007-40	0.07	0.01	1	0.001	0.004	300
FED007	46	47	FED007-41	0.07	0.01	2	0.001	0.005	200
FED007	47	48	FED007-42	0.05	0.01	1	0.001	0.002	300
FED007	48	49	FED007-43	0.05	0.01	1	0.002	0.003	300
FED007	49	50	FED007-44	0.06	0.01	1	0.01	0.003	300
FED007	50	51	FED007-45	0.05	0.01	1	0.027	0.004	200
FED007	51	52	FED007-46	0.05	0.01	2	0.007	0.004	200
FED007	52	53	FED007-47				0.01		
FED007	53	54	FED007-48				0.01		
FED007	54	55	FED007-49				0.01		
FED007	55	56	FED007-50				0.01		
FED007	56	57	FED007-51				0.01		
FED007	57	58	FED007-52				0.01		
FED007	58	58.7	FED007-53				0.01		
FED007	58.7	59.8	FED007-54	0.01	0.01	2	0.013	0.004	100
FED007	59.8	60.3	FED007-55	0.01	0.01	2	0.083	0.003	300
FED007	60.3	61.3	FED007-56	0.03	0.03	1	0.018	0.004	200
FED007	61.3	62.5	FED007-57	0.01	0.01	1	0.002	0.003	100
FED008	35.7	36.7	FED008-01	0.19	0.01	1	0.002	0.002	200
FED008	36.7	37.7	FED008-02	0.12	0.01	1	0.002	0.003	200
FED008	37.7	38.7	FED008-03	0.28	0.01	1	0.001	0.002	200
FED008	38.7	39.7	FED008-04	0.03	0.01	1	0.001	0.001	100
FED008	39.7	40.7	FED008-05	0.04	0.02	1	0.001	0.002	200
FED008	40.7	41.7	FED008-06	0.01	0.05	1	0.001	0.002	200
FED008	41.7	42.7	FED008-07	0.02	0.05	1	0.001	0.002	200
FED008	42.7	43.7	FED008-08	0.02	0.01	1	0.001	0.002	200

FED008	43.7	44.7	FED008-09	0.09	0.01	1	0.001	0.002	200
FED008	44.7	45.7	FED008-10	0.05	0.01	1	0.001	0.003	200
FED008	45.7	46.7	FED008-11	0.17	0.02	2	0.001	0.004	200
FED008	46.7	47.7	FED008-12	0.08	0.01	2	0.001	0.003	200
FED008	47.7	48.7	FED008-13	0.16	0.02	1	0.001	0.004	100
FED008	48.7	49.7	FED008-14	0.26	0.01	2	0.001	0.002	200
FED008	49.7	50.7	FED008-15	0.09	0.01	2	0.001	0.003	200
FED008	50.7	51.7	FED008-16	0.08	0.01	1	0.001	0.005	300
FED008	51.7	52.7	FED008-17	0.07	0.01	1	0.001	0.005	400
FED008	52.7	53.7	FED008-18	0.37	0.01	2	0.001	0.005	300
FED008	53.7	54.7	FED008-19	0.18	0.02	2	0.003	0.005	300
FED008	54.7	55.7	FED008-20	0.11	0.01	1	0.002	0.002	300
FED008	55.7	56.7	FED008-21	0.03	0.01	2	0.001	0.002	200
FED008	56.7	57.7	FED008-22	0.12	0.01	1	0.001	0.006	300
FED008	57.7	58.7	FED008-23	1.11	0.01	2	0.001	0.006	400
FED008	58.7	59.7	FED008-24	0.19	0.01	3	0.005	0.006	200
FED008	59.7	60.7	FED008-25	0.14	0.01	1	0.001	0.003	200
FED008	60.7	61.7	FED008-26	3.05	0.02	4	0.012	0.006	600
FED008	61.7	62.7	FED008-27	0.87	0.01	2	0.018	0.004	300
FED008	62.7	63.7	FED008-28	0.94	0.01	1	0.004	0.004	300
FED008	63.7	64.7	FED008-29	1.77	0.02	4	0.006	0.006	400
FED008	64.7	65.7	FED008-30	0.49	0.01	2	0.009	0.005	400
FED008	65.7	66.7	FED008-31	0.07	0.01	1	0.012	0.004	400
FED008	66.7	67.7	FED008-32	0.35	0.02	3	0.02	0.007	500
FED008	67.7	68.7	FED008-33	1.47	0.02	7	0.003	0.016	400
FED008	68.7	69.7	FED008-34	1.26	0.02	3	0.004	0.007	400
FED008	69.7	70.7	FED008-35	0.59	0.02	7	0.002	0.014	600
FED008	70.7	71.7	FED008-36	0.18	0.01	2	0.007	0.003	600
FED008	71.7	72.7	FED008-37	0.05	0.01	3	0.002	0.003	300
FED008	72.7	73.7	FED008-38	0.08	0.01	1	0.002	0.003	400
FED008	73.7	74.7	FED008-39	0.08	0.02	3	0.004	0.054	400
FED008	74.7	75.7	FED008-40	0.24	0.01	1	0.001	0.003	200
FED008	75.7	76.7	FED008-41	0.07	0.01	1	0.001	0.003	300
FED008	76.7	77.7	FED008-42	0.06	0.01	1	0.001	0.003	300
FED008	77.7	78.7	FED008-43	0.07	0.01	1	0.001	0.004	300
FED008	78.7	79.7	FED008-44	0.06	0.01	2	0.001	0.008	400
FED008	79.7	80.7	FED008-45	0.08	0.01	1	0.001	0.003	300
FED008	80.7	81.7	FED008-	0.04	0.01	1	0.001	0.003	300

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FED008	81.7	82.7	FED008-47	0.08	0.01	3	0.001	0.006	400
FED008	82.7	83.7	FED008-48	0.09	0.02	4	0.001	0.014	500
FED008	83.7	84.7	FED008-49	0.04	0.01	2	0.001	0.002	300
FED008	84.7	85.7	FED008-50	0.04	0.01	1	0.001	0.002	300
FED008	85.7	86.7	FED008-51	0.04	0.01	1	0.001	0.002	100
FED008	86.7	87.7	FED008-52	0.04	0.01	1	0.001	0.001	100
FED008	87.7	88.7	FED008-53	0.1	0.01	1	0.001	0.003	100
FED008	88.7	89.7	FED008-54	0.04	0.01	1	0.001	0.002	100
FED008	89.7	90.7	FED008-55	0.12	0.07	1	0.001	0.001	100
FED008	90.7	91.7	FED008-56	0.04	0.03	1	0.001	0.001	100
FED008	91.7	92.7	FED008-57	0.04	0.01	1	0.001	0.004	100
FED008	92.7	93.7	FED008-58	0.04	0.01	1	0.001	0.004	100
FED008	93.7	94.7	FED008-59	0.19	0.01	1	0.001	0.007	400
FED008	94.7	95.7	FED008-60	0.12	0.01	2	0.001	0.004	200
FED008	95.7	96.7	FED008-61	0.04	0.01	1	0.001	0.002	100
FED008	96.7	97.7	FED008-62	0.03	0.01	1	0.001	0.002	100
FED008	97.7	98.7	FED008-63	0.04	0.01	1	0.001	0.003	100
FED008	98.7	99.7	FED008-64	0.05	0.01	1	0.001	0.003	200
FED008	99.7	100.8	FED008-65	0.05	0.01	1	0.001	0.002	100
FED008	132.6	133.6	FED008-66	0.04	0.01	1	0.001	0.002	100
FED008	133.6	134.6	FED008-67	0.05	0.01	1	0.001	0.003	100
FED008	134.6	135.6	FED008-68	0.05	0.01	1	0.001	0.003	100
FED008	135.6	136.6	FED008-69	0.07	0.01	1	0.001	0.002	100
FED008	136.6	137.6	FED008-70	0.06	0.01	1	0.001	0.002	100
FED008	137.6	138.6	FED008-71	0.0175	0.004	1	0.00015	0.0025	100
FED008	138.6	140.6	FED008-72	0.0475	0.012	1	0.00005	0.0035	40
FED008	140.6	141.6	FED008-73	0.0375	0.01	1	0.00005	0.0025	40
FED008	141.6	142.6	FED008-74	0.014	0.005	1	0.0005	0.0025	20
FED008	142.6	143.6	FED008-75	0.0145	0.004	1	0.00005	0.003	30
FED008	143.6	145	FED008-76	0.0495	0.009	1	0.00005	0.0025	40
FED009	39	40	FED009-001	0.03	0.02	2	0.002	0.004	200
FED009	40	41	FED009-002	0.04	0.03	2	0.044	0.004	300
FED009	41	42	FED009-003	0.08	0.11	5	0.001	0.002	300
FED009	42	43	FED009-004	0.03	0.06	3	0.01	0.004	300
FED009	43	44	FED009-005	0.04	0.1	2	0.002	0.004	3300

FED009	44	45	FED009-006	0.07	0.15	6	0.001	0.003	300
FED009	45	46	FED009-007	0.07	0.03	1	0.001	0.002	300
FED009	46	47	FED009-008	0.07	0.04	2	0.001	0.003	300
FED009	47	48	FED009-009	0.07	0.02	2	0.001	0.002	300
FED009	48	49	FED009-010	0.03	0.03	3	0.001	0.003	200
FED009	49	50	FED009-011	0.02	0.04	2	0.002	0.002	200
FED009	50	51	FED009-012	0.02	0.05	2	0.001	0.004	200
FED009	51	52	FED009-013	0.04	0.09	2	0.012	0.004	300
FED009	52	53	FED009-014	0.04	0.03	1	0.001	0.003	300
FED009	53	54	FED009-015	0.12	0.16	8	0.029	0.004	300
FED009	54	55	FED009-016	0.01	0.32	2	0.006	0.004	
FED009	55	56	FED009-017	0.01	0.03	1	0.005	0.001	
FED009	56	57	FED009-018	0.01	0.02	1	0.006	0.033	
FED009	57	58	FED009-019	0.02	0.03	1	0.004	0.003	
FED009	58	59	FED009-020	0.02	0.04	2	0.001	0.005	
FED009	59	60	FED009-021	0.01	0.02	1	0.001	0.003	
FED009	60	61	FED009-022	0.02	0.01	1	0.001	0.003	
FED009	61	62	FED009-023	0.33	0.02	1	0.001	0.006	
FED009	62	63	FED009-024	0.07	0.01	1	0.001	0.004	
FED009	63	64	FED009-025	0.01	0.01	1	0.002	0.003	
FED009	64	65	FED009-026	0.001	0.01	1	0.001	0.023	
FED009	65	66	FED009-027				0.01		
FED009	66	67	FED009-028				0.01		
FED009	67	68	FED009-029				0.01		
FED009	68	69	FED009-030				0.011		
FED009	69	70	FED009-031				0.011		
FED009	70	71	FED009-032				0.024		
FED009	71	72	FED009-033				0.01		
FED009	72	73	FED009-034				0.01		
FED009	73	74	FED009-035				0.01		
FED009	74	75	FED009-036				0.011		

FED009	75	76	FED009-037						0.01	
FED009	76	77	FED009-038						0.01	
FED009	77	78	FED009-039						0.01	
FED009	78	79	FED009-040						0.01	
FED009	79	80	FED009-041						0.01	
FED009	80	81	FED009-042						0.01	
FED009	81	82	FED009-043						0.02	
FED009	82	83	FED009-044						0.01	
FED009	83	84	FED009-045						0.01	
FED009	84	85	FED009-046						0.01	
FED009	85	86	FED009-047						0.01	
FED009	86	87	FED009-048						0.01	
FED009	87	88	FED009-049						0.01	
FED009	88	89	FED009-050						0.014	
FED009	89	90	FED009-051						0.01	
FED009	90	91	FED009-052						0.01	
FED009	91	92	FED009-053						0.01	
FED009	92	93	FED009-054						0.013	
FED009	93	94	FED009-055						0.013	
FED009	94	95	FED009-056						0.015	
FED009	95	96	FED009-057						0.01	
FED009	96.6	97.6	FED009-058	0.02	0.01	1	0.009	0.002		200
FED009	97.6	98.6	FED009-059	0.02	0.01	2	0.009	0.003		200
FED009	98.6	99.6	FED009-060	0.04	0.01	2	0.004	0.002		200
FED009	99.6	100.6	FED009-061	0.04	0.01	1	0.003	0.002		200
FED009	100.6	101.6	FED009-062	0.05	0.01	1	0.003	0.002		200
FED009	101.6	102.6	FED009-063	0.05	0.01	1	0.004	0.001		200
FED009	102.6	103.6	FED009-064	0.05	0.01	1	0.005	0.002		200
FED009	103.6	104.6	FED009-065	0.06	0.01	1	0.003	0.002		200
FED009	104.6	105.6	FED009-066	0.04	0.01	1	0.004	0.002		200
FED009	105.6	106.6	FED009-067	0.09	0.01	1	0.002	0.003		200

FED009	106.6	107.6	FED009-068	0.04	0.01	1	0.003	0.002	200
FED009	107.6	108.6	FED009-069	0.06	0.01	1	0.002	0.002	200
FED009	108.6	109.6	FED009-070	0.04	0.01	1	0.002	0.003	200
FED009	109.6	110.6	FED009-071	0.01	0.01	1	0.002	0.003	200
FED009	110.6	111.6	FED009-072	0.04	0.01	1	0.002	0.002	200
FED009	111.6	112.6	FED009-073	0.04	0.01	1	0.005	0.006	200
FED009	112.6	113.6	FED009-074	0.02	0.01	1	0.003	0.006	200
FED009	113.6	114.6	FED009-075	0.02	0.01	1	0.004	0.003	200
FED009	114.6	115.6	FED009-076	0.02	0.01	1	0.001	0.002	200
FED009	115.6	116.6	FED009-077	0.05	0.01	1	0.001	0.002	200
FED009	116.6	117.6	FED009-078	0.04	0.01	1	0.001	0.002	200
FED009	117.6	118.6	FED009-079	0.04	0.01	1	0.001	0.001	200
FED009	118.6	119.6	FED009-080	0.04	0.01	1	0.001	0.002	200
FED009	119.6	120.6	FED009-081	0.06	0.01	1	0.001	0.003	200
FED009	120.6	121.6	FED009-082	0.04	0.01	1	0.002	0.001	200
FED009	121.6	122.6	FED009-083	0.01	0.01	1	0.003	0.005	200
FED009	122.6	123.6	FED009-084	0.01	0.01	1	0.004	0.006	200
FED009	123.6	124.6	FED009-085	0.01	0.01	1	0.003	0.004	200
FED009	130.8	131.8	FED009-086	0.04	0.01	1	0.001	0.002	100
FED009	131.8	132.8	FED009-087	0.02	0.01	1	0.001	0.002	100
FED009	132.8	133.8	FED009-088	0.02	0.01	1	0.001	0.002	100
FED009	133.8	134.8	FED009-089	0.02	0.01	1	0.001	0.002	100
FED009	134.8	135.8	FED009-090	0.08	0.07	1	0.001	0.003	200
FED009	135.8	136.8	FED009-091	0.01	0.01	1	0.001	0.002	100
FED009	136.8	137.8	FED009-092	0.02	0.01	1	0.001	0.002	100
FED009	137.8	138.8	FED009-093	0.02	0.01	1	0.001	0.002	100
FED009	138.8	139.8	FED009-094	0.01	0.01	1	0.002	0.003	100
FED009	139.8	140.8	FED009-095	0.01	0.01	1	0.002	0.003	100
FED009	140.8	141.8	FED009-096	0.02	0.01	1	0.001	0.002	100
FED009	141.8	142.8	FED009-097	0.02	0.01	1	0.001	0.002	100
FED009	142.8	143.8	FED009-098	0.04	0.01	1	0.001	0.002	100

FED009	143.8	144.8	FED009-099	0.06	0.01	1	0.001	0.004	100
FED009	144.8	145.8	FED009-100	0.03	0.01	1	0.001	0.004	100
FED009	145.8	146.8	FED009-101	0.06	0.04	1	0.001	0.023	200
FED009	146.8	147.8	FED009-102	0.02	0.01	1	0.001	0.001	100
FED010	5	8	FED010-001	0.01	0.01	5	0.005	0.004	400
FED010	8	9	FED010-002	0.01	0.01	3	0.001	0.004	400
FED010	9	10	FED010-003	0.01	0.01	1	0.001	0.007	400
FED010	10	11	FED010-004	0.01	0.01	1	0.001	0.007	400
FED010	11	12	FED010-005	0.22	0.01	10	0.006	0.004	500
FED010	12	13	FED010-006	0.01	0.01	3	0.002	0.004	500
FED010	13	14	FED010-007	0.01	0.01	1	0.001	0.003	400
FED010	14	15	FED010-008	0.18	0.03	6	0.191	0.003	600
FED010	15	16	FED010-009	0.01	0.01	1	0.002	0.003	400
FED010	16	17	FED010-010	0.01	0.01	1	0.002	0.006	500
FED010	17	18	FED010-011	0.01	0.01	2	0.002	0.003	400
FED010	18	19	FED010-012	0.01	0.01	3	0.174	0.008	700
FED010	19	22.7	FED010-013	0.02	0.01	1	0.005	0.007	500
FED010	22.7	23.9	FED010-014	0.01	0.01	1	0.001	0.004	500
FED010	29	32	FED010-015	0.33	0.01	11	0.012	0.008	700
FED010	32	33	FED010-016	0.67	0.07	9	0.022	0.007	1300
FED010	33	34	FED010-017	1.43	0.07	5	0.001	0.006	1000
FED010	34	35	FED010-018	0.6	0.05	8	0.002	0.007	1000
FED010	35	36	FED010-019	0.78	0.11	13	0.001	0.006	900
FED010	36	37	FED010-020	0.47	0.09	12	0.001	0.006	900
FED010	37	38	FED010-021	0.3	0.03	5	0.001	0.003	800
FED010	38	39	FED010-022	0.1	0.01	2	0.006	0.003	800
FED010	39	40	FED010-023	0.13	0.01	2	0.001	0.003	1000
FED010	40	41	FED010-024	0.17	0.03	2	0.016	0.003	600
FED010	41	42.4	FED010-025	0.05	0.01	3	0.001	0.001	500
FED010	56.9	60.9	FED010-026	0.08	0.01	2	0.001	0.009	500
FED010	60.9	61.7	FED010-027	0.05	0.01	2	0.001	0.003	500

FED012	6.5	7.5	FED010-028	0.01	0.01	3	0.003	0.008	100
FED012	7.5	8.5	FED010-029	0.01	0.01	1	0.004	0.009	100
FED012	10	11	FED010-030	0.01	0.01	1	0.007	0.011	100
FED012	11	12	FED010-031	0.03	0.01	1	0.002	0.013	100
FED012	33	34	FED010-032	0.03	0.01	2	0.001	0.003	100
FED012	51	52	FED010-033	0.03	0.01	1	0.003	0.003	100
FED012	52	53	FED010-034	0.04	0.01	2	0.003	0.005	100
FED012	53	54	FED010-035	0.04	0.01	1	0.002	0.007	100
FED012	69	70	FED010-036	0.02	0.01	2	0.001	0.002	100
FED012	70	70.6	FED010-037	0.01	0.01	2	0.001	0.003	100
FED012	74	75	FED010-038	0.01	0.01	2	0.003	0.004	100
FED012	112.5	113.5	FED010-039	0.02	0.01	2	0.003	0.005	100
FED012	113.5	115	FED010-040	0.02	0.01	2	0.001	0.004	10
FED012	119.5	120.5	FED010-041	0.01	0.01	2	0.002	0.006	100
FED012	120.5	122	FED010-042	0.02	0.01	3	0.002	0.005	100
FED012	124	125	FED010-043	0.01	0.01	1	0.002	0.003	100
FED012	125	126	FED010-044	0.02	0.01	2	0.002	0.003	100
FED012	126	127	FED010-045	0.01	0.01	2	0.001	0.002	100
FED012	127	128	FED010-046	0.01	0.01	1	0.001	0.003	100
FED012	128	129	FED010-047	0.01	0.01	1	0.002	0.002	100
FED012	129	130	FED010-048	0.01	0.01	1	0.001	0.002	100
FED012	130	131	FED010-049	0.01	0.01	1	0.002	0.004	100
FED012	131	132	FED010-050	0.01	0.01	1	0.002	0.004	100
FED012	132	133	FED010-051	0.01	0.01	1	0.001	0.002	100
FED012	133	134	FED010-052	0.01	0.01	1	0.002	0.008	100
FED012	134	135	FED010-053	0.01	0.01	1	0.003	0.003	100
FED012	135	136	FED010-054	0.01	0.01	1	0.003	0.011	100
FED012	136	137	FED010-055	0.01	0.01	1	0.003	0.003	100
FED012	137	138	FED010-056	0.01	0.01	2	0.003	0.003	100
FED012	138	139	FED010-057	0.01	0.01	2	0.002	0.003	100
FED012	139	140	FED010-058	0.01	0.01	1	0.001	0.001	100

FED012	140	141	FED010-059	0.01	0.01	2	0.002	0.002	100
FED012	141	142	FED010-060	0.01	0.01	2	0.001	0.001	100
FED012	142	143	FED010-061	0.01	0.01	1	0.001	0.002	100
FED012	143	144	FED010-062	0.01	0.01	1	0.001	0.002	100
FED012	144	145	FED010-063	0.01	0.01	1	0.001	0.002	100
FED012	145	146	FED010-064	0.01	0.01	1	0.001	0.002	100
FED012	146	147	FED010-065	0.01	0.01	1	0.001	0.003	100
FED012	147	148	FED010-066	0.01	0.01	1	0.001	0.001	100
FED012	148	149	FED010-067	0.01	0.01	1	0.001	0.001	100
FED012	149	150	FED010-068	0.01	0.01	2	0.002	0.002	100
FED012	150	151	FED010-069	0.01	0.01	1	0.001	0.002	100
FED012	151	152	FED010-070	0.01	0.01	1	0.001	0.003	100
FED012	152	153	FED010-071	0.01	0.01	1	0.002	0.002	100
FED012	153	154	FED010-072	0.01	0.01	1	0.001	0.002	100
FED012	154	155	FED010-073	0.02	0.01	1	0.001	0.002	100
FED012	155	156	FED010-074	0.01	0.01	1	0.001	0.002	100
FED012	156	157	FED010-075	0.01	0.01	1	0.001	0.002	100
FED012	157	158	FED010-076	0.02	0.01	1	0.001	0.003	100
FED012	158	159	FED010-077	0.01	0.01	1	0.001	0.002	100
FED012	159	160	FED010-078	0.01	0.01	1	0.002	0.004	100
FED012	160	161	FED010-079	0.01	0.01	1	0.001	0.003	100
FED012	161	162	FED010-080	0.01	0.01	1	0.001	0.002	100
FED012	162	163	FED010-081	0.01	0.01	1	0.001	0.002	100
FED012	163	164	FED010-082	0.1	0.01	1	0.001	0.003	100
FED012	164	165	FED010-083	0.01	0.01	1	0.001	0.003	100
FED012	165	166	FED010-084	0.03	0.01	2	0.001	0.003	100
FED012	166	167	FED010-085	0.02	0.01	2	0.001	0.002	100
FED012	167	168	FED010-086	0.01	0.01	1	0.001	0.002	100
FED012	168	169	FED010-087	0.01	0.01	1	0.001	0.004	100
FED012	169	170	FED010-088	0.01	0.01	1	0.001	0.003	100
FED012	170	171	FED010-089	0.01	0.01	1	0.001	0.002	100

FED012	171	172	FED010-090	0.01	0.01	1	0.001	0.005	100
FED012	172	173	FED010-091	0.01	0.01	2	0.001	0.005	100
FED012	173	174	FED010-092	0.01	0.01	3	0.002	0.099	100
FED012	174	175	FED010-093	0.01	0.01	3	0.001	0.114	100
FED012	175	176	FED010-094	0.01	0.01	1	0.001	0.136	100
FED012	176	177	FED010-095	0.01	0.01	1	0.001	0.234	100
FED012	177	178	FED010-096	0.01	0.01	1	0.001	0.19	100
FED012	178	179	FED010-097	0.01	0.01	1	0.003	0.011	100
FED012	179	180	FED010-098	0.01	0.01	2	0.028	0.064	100
FED012	180	181	FED010-099	0.01	0.01	1	0.001	0.172	2300
FED012	181	182	FED010-100	0.01	0.01	1	0.009	0.005	100
FED012	182	183	FED010-101	0.01	0.01	1	0.002	0.008	100
FED012	183	184	FED010-102	0.01	0.01	1	0.006	0.006	100
FED012	184	185	FED010-103	0.01	0.01	1	0.002	0.009	100
FED012	206	207	FED010-104	0.02	0.01	1	0.002	0.004	100
FED012	207	208	FED010-105	0.03	0.01	1	0.001	0.005	100
FED012	208	209	FED010-106	0.02	0.01	1	0.001	0.005	100
FED012	209	210	FED010-107	0.02	0.01	1	0.001	0.004	100
FED012	210	211	FED010-108	0.01	0.01	1	0.002	0.005	100
FED012	211	212	FED010-109	0.01	0.01	1	0.001	0.005	100
FED012	212	213	FED010-110	0.02	0.01	1	0.001	0.006	100
FED012	213	214	FED010-111	0.03	0.01	1	0.001	0.008	100
FED012	214	215	FED010-112	0.03	0.01	1	0.001	0.004	100
FED012	215	216	FED010-113	0.04	0.01	2	0.001	0.009	400
FED012	216	217	FED010-114	0.03	0.01	2	0.005	0.064	200
FED012	217	218	FED010-115	0.03	0.01	1	0.011	0.014	400
FED012	218	219	FED010-116	0.04	0.01	1	0.021	0.009	500
FED012	219	220	FED010-117	0.03	0.01	1	0.041	0.01	400
FED012	220	221	FED010-118	0.03	0.01	1	0.02	0.002	500
FED012	221	222	FED010-119	0.01	0.01	1	0.008	0.004	700
FED012	222	223	FED010-120	0.01	0.01	2	0.026	0.005	200

FED012	223	224	FED010-121	0.02	0.01	1	0.019	0.002	200
FED012	224	225	FED010-122	0.04	0.01	1	0.011	0.004	200
FED012	225	226	FED010-123	0.04	0.01	1	0.036	0.004	200
FED012	226	227	FED010-124	0.03	0.01	1	0.014	0.002	100
FED012	227	228	FED010-125	0.02	0.01	1	0.001	0.002	100
FED012	228	229	FED010-126	0.03	0.01	1	0.001	0.002	100
FED012	229	230	FED010-127	0.03	0.01	1	0.003	0.003	100
FED012	230	231	FED010-128	0.05	0.01	1	0.001	0.003	100
FED012	231	232	FED010-129	0.05	0.01	1	0.001	0.002	100
FED012	232	233	FED010-130	0.03	0.01	1	0.002	0.001	100
FED012	233	234	FED010-131	0.05	0.01	2	0.001	0.035	200
FED012	234	235	FED010-132	0.06	0.01	1	0.001	0.003	200
FED012	235	236	FED010-133	0.02	0.01	1	0.002	0.005	200
FED012	236	237	FED010-134	0.02	0.01	1	0.001	0.002	100
FED012	237	238	FED010-135	0.02	0.01	1	0.001	0.013	100
FED012	238	239	FED010-136	0.01	0.01	1	0.001	0.003	100
FED012	239	240	FED010-137	0.02	0.01	1	0.001	0.115	100
FED012	240	241	FED010-138	0.02	0.01	1	0.001	0.034	100
FED012	241	242	FED010-139	0.02	0.01	1	0.001	0.002	100
FED012	242	243	FED010-140	0.03	0.01	1	0.001	0.002	100
FED012	243	244	FED010-141	0.04	0.01	1	0.001	0.002	200
FED012	244	245	FED010-142	0.05	0.01	2	0.001	0.015	200
FED012	245	246	FED010-143	0.05	0.01	2	0.001	0.011	200
FED012	246	247	FED010-144	0.04	0.01	3	0.001	0.008	100
FED012	247	248	FED010-145	0.04	0.01	1	0.001	0.005	100
FED012	248	249	FED010-146	0.04	0.01	3	0.001	0.006	200
FED012	249	250	FED010-147	0.08	0.01	1	0.001	0.015	100
FED012	250	251	FED010-148	0.01	0.01	2	0.001	0.008	100
FED012	251	252	FED010-149	0.08	0.01	2	0.001	0.006	100
FED012	252	253	FED010-150	0.05	0.01	2	0.001	0.044	100
FED012	253	254	FED010-151	0.04	0.02	2	0.001	0.008	100

FED012	254	255	FED010-152	0.03	0.09	3	0.001	0.411	100
FED012	255	256	FED010-153	0.05	0.01	2	0.001	0.005	200
FED012	256	257	FED010-154	0.03	0.01	2	0.001	0.002	100
FED012	257	258	FED010-155	0.02	0.01	1	0.001	0.002	100
FED012	258	259	FED010-156	0.02	0.01	1	0.001	0.002	100
FED012	259	260	FED010-157	0.02	0.01	2	0.001	0.001	100
FED012	260	261	FED010-158	0.02	0.01	2	0.001	0.002	100
FED012	261	262	FED010-159	0.02	0.01	3	0.001	0.001	100
FED012	262	263	FED010-160	0.01	0.01	2	0.001	0.002	100
FED012	263	266	FED010-161	0.06	0.01	2	0.001	0.002	100
FED012	266	267	FED010-162	0.07	0.01	2	0.001	0.002	200
FED012	267	268	FED010-163	0.07	0.01	2	0.001	0.002	200
FED012	268	269	FED010-164	0.09	0.01	2	0.001	0.001	200
FED012	269	270	FED010-165	0.06	0.01	2	0.001	0.001	200
FED012	270	271	FED010-166	0.03	0.01	1	0.001	0.001	100
FED012	271	272	FED010-167	0.07	0.01	2	0.001	0.001	100
FED012	272	273	FED010-168	0.06	0.01	2	0.001	0.001	100
FED012	273	274	FED010-169	0.09	0.01	3	0.001	0.001	100
FED012	274	275	FED010-170	0.05	0.01	1	0.001	0.003	100
FED012	275	276	FED010-171	0.02	0.01	1	0.001	0.002	100
FED012	276	277	FED010-172	0.02	0.01	1	0.001	0.002	100
FED012	277	278	FED010-173	0.02	0.01	1	0.001	0.002	100
FED012	278	279	FED010-174	0.01	0.01	1	0.001	0.003	100
FED012	279	280	FED010-175	0.02	0.01	1	0.001	0.002	100
FED012	280	281	FED010-176	0.03	0.01	1	0.001	0.002	100
FED012	281	282	FED010-177	0.07	0.01	2	0.001	0.002	100
FED012	282	283	FED010-178	0.06	0.01	2	0.001	0.002	100
FED012	283	284	FED010-179	0.05	0.01	1	0.001	0.001	100
FED012	284	285	FED010-180	0.04	0.01	1	0.001	0.002	100
FED012	302.8	303.8	FED010-181	0.01	0.01	1	0.001	0.004	100
FED012	303.8	304.8	FED010-182	0.01	0.01	1	0.001	0.001	100

FED012	304.8	305.8	FED010-183	0.01	0.01	1	0.001	0.003	100
FED012	305.8	307.2	FED010-184	0.01	0.01	1	0.001	0.003	100
FED012	308.6	309.6	FED010-185	0.02	0.01	1	0.001	0.002	100
FED012	309.6	310.2	FED010-186	0.01	0.01	1	0.001	0.002	100
FED013	29	30	FED013-01				0.01		
FED013	30	31	FED013-02				0.01		
FED013	31	32	FED013-03				0.01		
FED013	32	33	FED013-04				0.01		
FED013	33	34	FED013-05				0.01		
FED013	34	35	FED013-06				0.01		
FED013	35	36	FED013-07				0.01		
FED013	36	37	FED013-08				0.01		
FED013	37	38	FED013-09				0.01		
FED013	52.8	53	FED013-10				0.01		
FED013	53	54	FED013-11				0.01		
FED013	54	55	FED013-12				0.01		
FED013	55	56	FED013-13				0.011		
FED013	63.6	64.6	FED013-14				0.01		
FED013	64.6	65.4	FED013-15				0.01		
FED014	62	63	FED014-01	0.01	0.01	7	0.003	0.003	200
FED014	63	64	FED014-02	0.01	0.01	1	0.001	0.002	200
FED014	64	65	FED014-03	0.01	0.01	1	0.002	0.003	200
FED014	65	66	FED014-04	0.01	0.01	2	0.005	0.006	400
FED014	66	67	FED014-05	0.01	0.01	7	0.005	0.006	300
FED014	67	68	FED014-06	0.01	0.01	2	0.004	0.006	400
FED014	68	69	FED014-07	0.01	0.01	10	0.016	0.012	400
FED014	69	70	FED014-08	0.01	0.01	2	0.006	0.004	500
FED014	70	71	FED014-09	0.01	0.01	2	0.003	0.006	300
FED014	71	72	FED014-10	0.01	0.01	1	0.003	0.022	200
FED014	72	73	FED014-11	0.01	0.01	1	0.001	0.015	500
FED014	73	74	FED014-12	0.01	0.01	1	0.001	0.002	200
FED014	74	75	FED014-13	0.01	0.01	1	0.001	0.002	200
FED014	75	76	FED014-14	0.01	0.01	1	0.001	0.001	200
FED014	76	77	FED014-15	0.01	0.01	1	0.001	0.001	200
FED014	77	78	FED014-16	0.01	0.01	1	0.001	0.001	200
FED014	78	79	FED014-17	0.01	0.01	1	0.001	0.001	300
FED014	79	80	FED014-18	0.01	0.01	1	0.001	0.001	300

FED014	80	81	FED014-19	0.01	0.01	1	0.001	0.001	300
FED014	81	82	FED014-20	0.01	0.01	1	0.001	0.001	500
FED015	50.7	51.7	FED015-01	0.01	0.02	1	0.001	0.02	200
FED015	51.7	52.9	FED015-02	0.01	0.01	1	0.001	0.034	300
FED015	62.3	63.2	FED015-03	0.01	0.01	1	0.001	0.052	200
FED015	70.3	71.3	FED015-04	0.01	0.01	1	0.002	0.002	200
FED015	71.3	72.3	FED015-05	0.05	0.01	1	0.004	0.001	200
FED015	72.3	73.7	FED015-06	0.01	0.01	1	0.001	0.005	200
FED016	48.1	49.1	FED016-01			2	0.001	0.001	200
FED016	49.1	50.1	FED016-02			1	0.001	0.001	300
FED016	50.1	51.3	FED016-03			1	0.001	0.002	200
FED016	57.9	58.8	FED016-04			1	0.001	0.009	200
FED017	43	44	FED017-01			1	0.0003	0.003	100
FED017	44	45	FED017-02			2	0.0002	0.001	100
FED017	140	141.5	FED017-03			1	0.0001	0.002	100
FED017	141.5	142.5	FED017-04			1	0.0001	0.002	100
FED017	142.5	143.5	FED017-05			1	0.0001	0.002	100
FED017	143.5	144.7	FED017-06			2	0.0001	0.001	100
FED018	14	17	FED018-001			1	0.0016	0.002	200
FED018	17	18.5	FED018-002			1	0.0019	0.003	200
FED018	18.5	20	FED018-003			1	0.0001	0.003	200
FED018	20	21.4	FED018-004			1	0.0024	0.002	200
FED018	21.4	22.8	FED018-005			1	0.0014	0.002	200
FED018	22.8	24	FED018-006			1	0.0001	0.002	200
FED018	24	25	FED018-007			1	0.0001	0.002	200
FED018	25	26	FED018-008			1	0.0001	0.001	200
FED018	26	27	FED018-009			1	0.0001	0.002	200
FED018	27	28	FED018-010			1	0.0001	0.002	200
FED018	28	29	FED018-011			1	0.0001	0.002	200
FED018	29	30	FED018-012			1	0.0001	0.001	200
FED018	30	31	FED018-013			1	0.0001	0.001	200
FED018	31	32	FED018-014			1	0.0021	0.002	100
FED018	32	33	FED018-015			1	0.0001	0.002	100
FED018	33	34	FED018-016			1	0.0001	0.002	100

FED018	34	35	FED018-017	1	0.0003	0.002	100
FED018	35	36	FED018-018	1	0.0016	0.003	100
FED018	36	37	FED018-019	1	0.0005	0.004	100
FED018	37	38	FED018-020	1	0.0002	0.004	100
FED018	38	39	FED018-021	1	0.0001	0.004	100
FED018	39	40	FED018-022	1	0.0003	0.004	100
FED018	40	41	FED018-023	1	0.0004	0.005	100
FED018	41	42	FED018-024	1	0.0001	0.004	100
FED018	42	43	FED018-025	1	0.0004	0.015	100
FED018	43	44	FED018-026	1	0.0006	0.051	100
FED018	44	45	FED018-027	1	0.0012	0.004	100
FED018	45	46	FED018-028	3	0.0011	0.029	100
FED018	46	47	FED018-029	1	0.0041	0.015	100
FED018	47	48	FED018-030	1	0.0057	0.008	100
FED018	48	49	FED018-031	1	0.0018	0.023	100
FED018	49	50	FED018-032	1	0.0025	0.015	100
FED018	50	51	FED018-033	1	0.0015	0.098	100
FED018	51	52	FED018-034	1	0.0006	0.004	100
FED018	52	53	FED018-035	2	0.007	0.04	100
FED018	53	54	FED018-036	1	0.0013	0.054	100
FED018	54	55	FED018-037	3	0.004	0.001	100
FED018	55	56	FED018-038	1	0.0015	0.006	100
FED018	56	57	FED018-039	1	0.0007	0.003	100
FED018	57	58	FED018-040	1	0.0003	0.002	100
FED018	58	59	FED018-041	1	0.0006	0.002	100
FED018	59	60	FED018-042	1	0.0002	0.002	100
FED018	60	61	FED018-043	1	0.0002	0.001	100
FED018	61	62	FED018-044	1	0.0007	0.002	100
FED018	62	65	FED018-045	1	0.0008	0.002	100
FED018	65	66	FED018-046	1	0.0002	0.002	100
FED018	66	67	FED018-047	1	0.0001	0.002	100

FED018	67	68	FED018-048		1	0.0003	0.002	100
FED018	68	69	FED018-049		1	0.0001	0.001	100
FED018	69	70	FED018-050		1	0.0001	0.001	100
FED018	95	96	FED018-051	0.09	1	0.0001	0.001	100
FED018	96	97	FED018-052	0.09	1	0.0001	0.001	100
FED018	100	101	FED018-053	0.06	1	0.0001	0.001	100
FED018	103	104.8	FED018-054	0.07	2	0.0001	0.001	100
FED018	104.8	105	FED018-055	0.05	1	0.0001	0.001	100
FED018	119.6	120.6	FED018-056	0.02	2	0.0007	0.001	100
FED018	120.6	121.6	FED018-057	0.01	1	0.0006	0.001	100
FED018	121.6	122.5	FED018-058	0.02	2	0.0007	0.001	100
FED018	123.8	124.4	FED018-059	0.02	1	0.0151	0.001	100
FED018	127.9	128.9	FED018-060	0.03	1	0.0148	0.001	100
FED018	128.9	129.9	FED018-061	0.03	1	0.0023	0.002	100
FED018	129.9	130.9	FED018-062	0.03	1	0.0023	0.001	100
FED018	130.9	131.9	FED018-063	0.01	1	0.0033	0.002	100
FED018	131.9	132.9	FED018-064	0.01	1	0.0025	0.002	100
FED018	132.9	133.9	FED018-065	0.01	1	0.0052	0.002	100
FED018	133.9	134.9	FED018-066	0.03	1	0.0031	0.001	100
FED018	134.9	135.9	FED018-067	0.01	1	0.0032	0.001	100
FED018	135.9	136.9	FED018-068	0.02	1	0.0008	0.001	100
FED018	136.9	137.9	FED018-069	0.01	1	0.0029	0.001	100
FED018	137.9	138.9	FED018-070	0.01	1	0.0091	0.001	100
FED018	138.9	139.9	FED018-071	0.03	1	0.002	0.001	100
FED018	139.9	140.9	FED018-072	0.03	1	0.0029	0.001	100
FED018	140.9	141.9	FED018-073	0.02	1	0.0019	0.001	100
FED018	141.9	142.9	FED018-074	0.01	1	0.0044	0.002	100
FED018	142.9	143.9	FED018-075	0.02	1	0.0048	0.002	100
FED018	143.9	144.9	FED018-076	0.01	1	0.0047	0.002	100
FED018	144.9	145.9	FED018-077	0.1	1	0.0011	0.002	100
FED018	145.9	146.9	FED018-078	0.01	1	0.0022	0.001	100

FED018	146.9	147.9	FED018-079	0.01	1	0.0018	0.002	100
FED018	147.9	148.9	FED018-080	0.01	1	0.0047	0.001	100
FED018	148.9	149.9	FED018-081	0.05	1	0.0048	0.004	100
FED018	149.9	150.9	FED018-082	0.08	1	0.0025	0.004	100
FED018	150.9	151.9	FED018-083	0.03	1	0.0012	0.002	100
FED018	151.9	152.9	FED018-084	0.03	1	0.0005	0.002	100
FED018	152.9	153.9	FED018-085	0.01	1	0.0001	0.001	100
FED018	153.9	154.9	FED018-086	0.03	2	0.0006	0.001	100
FED018	154.9	155.9	FED018-087	0.13	1	0.0003	0.004	100
FED018	155.9	156.9	FED018-088	0.12	1	0.0011	0.002	100
FED018	156.9	157.9	FED018-089	0.01	1	0.0001	0.002	100
FED018	157.9	158.9	FED018-090	0.2	1	0.0021	0.002	100
FED018	158.9	159.9	FED018-091	0.1	1	0.0003	0.002	100
FED018	159.9	160.9	FED018-092	0.2	1	0.0007	0.002	100
FED018	160.9	161.9	FED018-093	0.2	1	0.0011	0.001	100
FED018	161.9	162.9	FED018-094	0.43	1	0.0031	0.001	100
FED018	162.9	163.9	FED018-095	0.14	1	0.0003	0.001	100
FED018	163.9	164.9	FED018-096	0.1	1	0.0005	0.001	100
FED018	164.9	165.9	FED018-097	0.06	1	0.00018	0.001	100
FED018	165.9	166.9	FED018-098	0.004	1	0.0003	0.001	100
FED018	166.9	167.9	FED018-099	0.005	1	0.0011	0.002	100
FED018	167.9	168.9	FED018-100	0.012	1	0.0013	0.002	100
FED018	168.9	169.9	FED018-101	0.05	1	0.0011	0.002	100
FED018	169.9	170.9	FED018-102	0.15	1	0.0011	0.001	100
FED018	170.9	171.9	FED018-103	0.28	1	0.0004	0.001	100
FED018	171.9	172.9	FED018-104	0.05	1	0.0014	0.001	100
FED018	172.9	173.9	FED018-105	0.01	1	0.0001	0.001	100
FED018	173.9	174.9	FED018-106	0.07	2	0.0009	0.002	100
FED018	174.9	175.9	FED018-107	0.06	1	0.002	0.005	100
FED018	175.9	176.9	FED018-108	0.05	1	0.0011	0.001	100
FED018	176.9	177.9	FED018-109	0.05	1	0.0005	0.007	100

FED018	177.9	178.9	FED018-110	0.08		1	0.0001	0.001	100
FED018	178.9	179.9	FED018-111	0.04		1	0.0001	0.001	100
FED018	179.9	180.9	FED018-112	0.06		1	0.0005	0.002	100
FED018	180.9	181.9	FED018-113	0.05		2	0.0001	0.002	100
FED018	181.9	182.9	FED018-114	0.03		1	0.0015	0.003	100
FED018	182.9	183.9	FED018-115	0.09		1	0.0002	0.001	100
FED018	183.9	184.9	FED018-116	0.07		1	0.0009	0.002	100
FED018	184.9	185.9	FED018-117	0.02		1	0.0004	0.002	100
FED018	185.9	186.9	FED018-118	0.03		1	0.0002	0.001	100
FED018	186.9	187.9	FED018-119	0.02		1	0.001	0.001	100
FED018	187.9	188.9	FED018-120	0.02		1	0.0001	0.001	100
FED018	188.9	189.9	FED018-121	0.02		1	0.0001	0.001	100
FED018	189.9	190.9	FED018-122	0.02		1	0.001	0.002	100
FED018	190.9	192	FED018-123	0.02		1	0.0011	0.004	100
FED018	215	216	FED018-124	0.01		2	0.0017	0.003	100
FED018	216	217	FED018-125	0.01		2	0.0027	0.002	100
FED018	242.6	243.6	FED018-126	0.01		1	0.0043	0.012	100
FED018	243.6	244.6	FED018-127	0.01		1	0.0115	0.126	100
FED018	244.6	245.6	FED018-128	0.01		1	0.0125	0.036	100
FED018	245.6	246.8	FED018-129	0.01		1	0.0266	0.003	100
FED019	159.4	160.4	FED019-01	0.01	0.01		0.001	0.004	
FED019	160.4	161.4	FED019-02	0.01	0.01		0.001	0.003	
FED019	161.4	162.4	FED019-03	0.02	0.01		0.001	0.005	
FED019	162.4	163.4	FED019-04	0.01	0.01		0.004	0.004	
FED019	163.4	164.4	FED019-05	0.01	0.01		0.002	0.003	
FED019	164.4	165.4	FED019-06	0.01	0.01		0.004	0.004	
FED019	165.4	166.4	FED019-07	0.02	0.01		0.001	0.003	
FED019	166.4	167.4	FED019-08	0.01	0.01		0.002	0.006	
FED019	167.4	168.4	FED019-09	0.01	0.01		0.003	0.001	
FED019	168.4	169.4	FED019-10	0.01	0.01		0.002	0.001	
FED019	169.4	170.4	FED019-11	0.01	0.01		0.001	0.002	
FED020	0	3	FED020-01	0.03			0.001		
FED020	3	15	FED020-02	0.09			0.006		

FED020	15	17	FED020-03	0.03	0.001
FED020	17	18	FED020-04	0.03	0.001
FED020	18	19	FED020-05	0.06	0.001
FED020	19	20	FED020-06	0.18	0.002
FED020	20	21	FED020-07	0.77	0.003
FED020	21	22	FED020-08	0.48	0.002
FED020	22	23	FED020-09	0.06	0.001
FED020	23	24	FED020-10	0.12	0.001
FED020	24	25	FED020-11	0.09	0.001
FED020	25	26	FED020-12	0.2	0.001
FED020	26	27	FED020-13	0.18	0.006
FED020	27	28	FED020-14	0.67	0.003
FED020	28	29	FED020-15	0.1	0.001
FED020	29	30	FED020-16	0.21	0.008
FED020	30	31	FED020-17	6.56	0.059
FED020	31	32	FED020-18	4.94	0.039
FED020	32	33	FED020-19	0.15	0.004
FED020	33	34	FED020-20	2.61	0.21
FED020	34	35	FED020-21	2.48	0.16
FED020	35	36	FED020-22	1.41	0.058
FED020	36	37	FED020-23	5.67	0.029
FED020	37	38	FED020-24	0.9	0.014
FED020	38	39	FED020-25	0.28	0.005
FED020	39	40	FED020-26	0.03	0.003
FED020	40	41	FED020-27	0.06	0.005
FED020	41	42	FED020-28	0.06	0.002
FED020	42	43	FED020-29	0.04	0.002
FED020	43	44	FED020-30	0.03	0.002
FED020	44	45	FED020-31	0.06	0.021
FED020	45	46	FED020-32	0.08	0.017
FED020	46	47	FED020-33	0.41	0.035
FED020	47	48	FED020-34	0.83	0.003
FED020	48	49	FED020-35	0.08	0.003
FED020	49	50	FED020-36	0.19	0.003
FED020	50	51	FED020-37	0.6	0.004
FED020	51	52	FED020-38	0.28	0.004
FED020	52	53	FED020-39	0.28	0.004
FED020	53	54	FED020-40	0.35	0.003

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FED020	54	55	FED020-41	0.47
			FED020-42	0.011
FED020	55	56	FED020-43	0.49
			FED020-44	0.005
FED020	56	57	FED020-45	0.43
			FED020-46	0.006
FED020	57	58	FED020-47	0.22
			FED020-48	0.003
FED020	58	59	FED020-49	0.15
			FED020-50	0.004
FED020	59	60	FED020-51	0.31
			FED020-52	0.002
FED020	60	61	FED020-53	0.02
			FED020-54	0.003
FED020	61	62	FED020-55	0.02
			FED020-56	0.008
FED020	62	63	FED020-57	0.02
			FED020-58	0.002
FED020	63	64	FED020-59	0.15
			FED020-60	0.033
FED020	64	65	FED020-61	2.14
			FED020-62	0.108
FED020	65	66	FED020-63	0.19
			FED020-64	0.071
FED020	66	67	FED020-65	0.06
			FED020-66	0.019
FED020	67	68	FED020-67	0.11
			FED020-68	0.004
FED020	68	69	FED020-69	0.11
			FED020-70	0.002
FED020	69	70	FED020-71	0.01
			FED020-72	0.002
FED020	70	71	FED020-73	0.02
			FED020-74	0.029
FED020	71	72	FED020-75	0.01
			FED020-76	0.001
FED020	72	73	FED020-77	0.01
			FED020-78	0.004
FED020	73	74	FED020-79	0.01
			FED020-80	0.002
FED020	74	75	FED020-81	0.02
			FED020-82	0.013
FED020	75	76	FED020-83	0.01
			FED020-84	0.001
FED020	76	77	FED020-85	0.02
			FED020-86	0.001
FED020	77	78	FED020-87	0.01
			FED020-88	0.007
FED020	78	79	FED020-89	0.04
			FED020-90	0.001
FED020	79	80	FED020-91	0.04
			FED020-92	0.001
FED020	80	81	FED020-93	0.02
			FED020-94	0.001
FED020	81	82	FED020-95	0.01
			FED020-96	0.003
FED020	82	83	FED020-97	0.01
			FED020-98	0.014
FED020	83	84	FED020-99	0.01
			FED020-01	0.052
FED020	84	85	FED020-02	0.03
			FED020-03	0.001
FED020	85	86	FED020-04	0.02
			FED020-05	0.001
FED020	86	87	FED020-06	0.02
			FED020-07	0.002
FED020	87	88	FED020-08	0.02
			FED020-09	0.002
FED020	88	89	FED020-10	0.01
			FED020-11	0.092
FED020	89	90	FED020-12	0.01
			FED020-13	0.013
FED021	30	31	FED021-01	0.02
			FED021-02	0.001
FED021	31	32	FED021-03	0.08
			FED021-04	0.001

FED021	32	33	FED021-03	0.11	0.001
FED021	33	34	FED021-04	0.06	0.007
FED021	34	35	FED021-05	0.07	0.034
FED021	35	36	FED021-06	0.04	0.029
FED021	36	37	FED021-07	0.01	0.011
FED021	37	38	FED021-08	0.04	0.025
FED021	38	39	FED021-09	0.02	0.028
FED021	39	40	FED021-10	0.02	0.02
FED021	40	41	FED021-11	0.01	0.037
FED021	41	42	FED021-12	0.01	0.206
FED021	42	43	FED021-13	0.01	0.065
FED021	43	44	FED021-14	0.01	0.098
FED021	44	45	FED021-15	0.01	0.031
FED021	45	46	FED021-16	0.01	0.034
FED021	46	47	FED021-17	0.01	0.087
FED021	47	48	FED021-18	0.01	0.052
FED021	48	49	FED021-19	0.01	0.083
FED021	49	50	FED021-20	0.01	0.025
FED021	50	51	FED021-21	0.01	0.003
FED021	51	52	FED021-22	0.01	0.001
FED021	52	53	FED021-23	0.01	0.001
FED021	53	54	FED021-24	0.01	0.001
FED021	54	55	FED021-25	0.01	0.001
FED021	55	56	FED021-26	0.01	0.001
FED021	56	57	FED021-27	0.01	0.001
FED021	57	58	FED021-28	0.01	0.001
FED021	58	59	FED021-29	0.01	0.001
FED021	59	60	FED021-30	0.01	0.001
FED021	60	61	FED021-31	0.01	0.001
FED021	61	62	FED021-32	0.01	0.001
FED021	62	63	FED021-33	0.01	0.042
FED021	63	64	FED021-34	0.01	0.032
FED021	64	65	FED021-35	0.01	0.019
FED021	65	66	FED021-36	0.01	0.001
FED021	66	67	FED021-37	0.01	0.001
FED021	67	68	FED021-38	0.01	0.001
FED021	68	69	FED021-39	0.01	0.017
FED021	69	70	FED021-40	0.01	0.005

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FED021	70	71	FED021-41	0.01			0.001
FED021	71	72	FED021-42	0.01			0.001
FED022	134	135	FED022-01	0.02			0.004
FED022	135	136	FED022-02	0.01			0.001
FED022	136	137	FED022-03	0.01			0.001
FED022	137	138	FED022-04	0.01			0.001
FED023	92	93	FED023-01	0.02			0.001
FED023	93	94	FED023-02	0.02			0.001
FED023	94	95	FED023-03	0.02			0.001
FED023	95	96	FED023-04	0.03			0.001
FED023	96	97	FED023-05	0.04			0.001
FED023	97	98	FED023-06	0.02			0.001
FED023	98	99	FED023-07	0.02			0.001
FED023	99	100	FED023-08	0.02			0.002
FED023	100	101	FED023-09	0.02			0.001
FED023	101	102	FED023-10	0.02			0.001
FED023	102	103	FED023-11	0.03			0.002
FED023	103	104	FED023-12	0.02			0.001
FED023	104	105	FED023-13	0.02			0.001
FED023	105	106	FED023-14	0.02			0.002
FED023	106	107	FED023-15	0.02			0.001
FED023	107	108	FED023-16	0.02			0.002
FED023	108	109	FED023-17	0.001			0.001
FED023	109	110	FED023-18	0.01			0.001
FED023	110	111	FED023-19	0.02			0.001
FED023	111	112	FED023-20	0.03			0.007
FED023	112	113	FED023-21	0.02			0.001
FED024	3	4	FED024-001	3.21	0.01	3	0.005
FED024	4	5	FED024-002	2.03	0.01	3	0.013
FED024	5	6	FED024-003	0.14	0.01	1	0.012
FED024	6	7	FED024-004	0.02	0.01	1	0.001
FED024	7	8	FED024-005	0.01	0.01	1	0.002
FED024	8	9	FED024-006	0.01	0.01	1	0.003
FED024	9	10	FED024-007	0.03	0.01	1	0.003
FED024	10	11	FED024-008	0.03	0.01	2	0.001

FED024	11	12	FED024-009	0.01	0.01	2	0.001
FED024	12	13	FED024-010	0.03	0.01	1	0.004
FED024	13	14	FED024-011	0.05	0.01	2	0.007
FED024	14	15	FED024-012	0.02	0.01	2	0.002
FED024	15	16	FED024-013	0.03	0.01	1	0.004
FED024	16	17	FED024-014	0.03	0.01	1	0.005
FED024	17	18	FED024-015	0.11	0.01	1	0.001
FED024	18	19	FED024-016	0.06	0.01	1	0.001
FED024	19	20	FED024-017	0.13	0.01	1	0.001
FED024	20	21	FED024-018	0.06	0.01	1	0.007
FED024	21	22	FED024-019	0.01	0.01	1	0.02
FED024	22	23	FED024-020	0.01	0.01	1	0.03
FED024	23	24	FED024-021	0.08	0.01	1	0.001
FED024	29	30	FED024-022	0.09	0.01	1	0.001
FED024	30	31	FED024-023	0.06	0.01	1	0.001
FED024	31	32	FED024-024	0.01	0.01	1	0.002
FED024	32	33	FED024-025	0.01	0.01	1	0.001
FED024	33	34	FED024-026	0.01	0.01	1	0.005
FED024	34	35	FED024-027	0.01	0.01	1	0.001
FED024	35	36	FED024-028	0.01	0.01	1	0.001
FED024	36	37	FED024-029	0.02	0.01	1	0.002
FED024	37	38	FED024-030	0.03	0.01	1	0.019
FED024	38	39	FED024-031	0.03	0.01	1	0.002
FED024	39	40	FED024-032	0.03	0.01	1	0.004
FED024	40	41	FED024-033	0.03	0.01	1	0.001
FED024	41	42	FED024-034	0.03	0.01	1	0.001
FED024	42	43	FED024-035	0.06	0.01	1	0.001
FED024	43	44	FED024-036	0.05	0.01	1	0.001
FED024	44	45	FED024-037	0.03	0.01	1	0.001
FED024	45	46	FED024-038	0.01	0.01	1	0.001
FED024	46	47	FED024-039	0.04	0.01	1	0.001

FED024	47	48	FED024-040	0.02	0.01	1	0.008
FED024	48	49	FED024-041	0.05	0.01	1	0.001
FED024	50	51	FED024-042	0.05		1	0.001
FED024	51	52	FED024-043	0.02		1	0.001
FED024	52	53	FED024-044	0.02		1	0.001
FED024	53	54	FED024-045	0.003		1	0.001
FED024	54	55	FED024-046	0.01		1	0.001
FED024	55	56	FED024-047	0.04		1	0.016
FED024	56	57	FED024-048	0.03		1	0.052
FED024	57	58	FED024-049	0.02		1	0.001
FED024	58	59	FED024-050	0.04		1	0.007
FED024	59	60	FED024-051	0.04		1	0.003
FED024	60	61	FED024-052	0.03		1	0.001
FED024	61	62	FED024-053	0.02		1	0.001
FED024	62	63	FED024-054	0.03		1	0.001
FED024	63	64	FED024-055	0.03		1	0.001
FED024	64	65	FED024-056	0.03		1	0.001
FED024	65	66	FED024-057	0.04		1	0.001
FED024	66	67	FED024-058	0.12		1	0.001
FED024	67	68	FED024-059	0.09		1	0.002
FED024	68	69	FED024-060	0.02		1	0.001
FED024	69	70	FED024-061	0.01		1	0.001
FED024	70	71	FED024-062	0.03		1	0.001
FED024	71	72	FED024-063	0.02		1	0.001
FED024	72	73	FED024-064	0.01		1	0.001
FED024	73	74	FED024-065	0.01		1	0.001
FED024	74	75	FED024-066	0.01		1	0.001
FED024	75	76	FED024-067	0.01		1	0.001
FED024	76	77	FED024-068	0.02		1	0.001
FED024	77	78	FED024-069	0.02		1	0.001
FED024	78	79	FED024-070	0.35	0.01	1	0.005

FED024	79	80	FED024-071	1	0.01	1	0.06
FED024	80	81	FED024-072	1.81	0.02	1	0.084
FED024	81	82	FED024-073	0.51	0.05	1	0.008
FED024	82	83	FED024-074	0.25	0.02	1	0.043
FED024	83	84	FED024-075	0.04	0.01	1	0.044
FED024	84	85	FED024-076	0.02	0.3	5	0.125
FED024	85	86	FED024-077	0.02	0.07	1	0.08
FED024	86	87	FED024-078	0.08	0.08	1	0.002
FED024	87	88	FED024-079	0.05	0.03	1	0.003
FED024	88	89	FED024-080	0.06	0.01	1	0.001
FED024	89	90	FED024-081	0.03	0.02	1	0.142
FED024	90	91	FED024-082	0.07	0.01	1	0.001
FED024	91	92	FED024-083	0.02		1	0.001
FED024	92	93	FED024-084	0.04		1	0.218
FED024	93	94	FED024-085	0.05		1	0.005
FED024	94	95	FED024-086	0.02		1	0.001
FED024	95	96	FED024-087	0.04		1	0.001
FED024	96	97	FED024-088	0.03		1	0.001
FED024	97	98	FED024-089	0.02		1	0.001
FED024	98	99	FED024-090	0.01		1	0.055
FED024	99	100	FED024-091	0.01		1	0.047
FED024	100	101	FED024-092	0.01		1	0.094
FED024	101	102	FED024-093	0.01	0.03	1	0.26
FED024	102	103	FED024-094	0.01	0.01	1	0.006
FED024	103	104	FED024-095	0.01	0.01	1	0.013
FED024	104	105	FED024-096	0.01	0.01	1	0.002
FED024	105	106	FED024-097	0.01	0.01	1	0.002
FED024	106	107	FED024-098	0.01	0.01	1	0.025
FED024	107	108	FED024-099	0.01	0.01	1	0.005
FED024	108	109	FED024-100	0.07	0.01	1	0.029
FED024	109	110	FED024-101	0.05	0.01	1	0.003

FED024	110	111	FED024-102	0.01	0.01	1	0.006	
FED024	111	112	FED024-103	0.01	0.01	1	0.003	
FED024	112	113	FED024-104	0.01	0.01	1	0.001	
FED024	113	114	FED024-105	0.01	0.01	1	0.001	
FED024	114	115	FED024-106	0.01	0.01	1	0.002	
FED024	115	116	FED024-107	0.07	0.01	1	0.001	
FED026	4.8	5.8	FED026-01	0.97	0.14	3	0.001	0.001
FED026	5.8	6.8	FED026-02	0.34	0.09	2	0.001	0.001
FED026	6.8	7.8	FED026-03	0.23	0.11	1	0.001	0.001
FED026	7.8	8.8	FED026-04	0.18	0.13	1	0.001	0.001
FED026	8.8	9.8	FED026-05	0.22	0.14	4	0.001	0.002
FED026	9.8	10.8	FED026-06	0.38	0.04	6	0.001	0.004
FED026	10.8	11.8	FED026-07	0.09	0.04	2	0.001	0.002
FED026	11.8	12.8	FED026-08	0.04	0.01	1	0.001	0.001
FED026	12.8	13.8	FED026-09	0.1	0.36	7	0.001	0.003
FED026	13.8	14.8	FED026-10	0.47	0.05	5	0.001	0.001
FED026	14.8	15.8	FED026-11	1.36	0.1	8	0.001	0.001
FED026	15.8	16.8	FED026-12	0.18	0.06	3	0.001	0.003
FED026	16.8	17.8	FED026-13	0.13	0.04	2	0.001	0.003
FED026	17.8	18.8	FED026-14	0.05	0.02	1	0.001	0.001
FED026	18.8	19.8	FED026-15	0.03	0.01	2	0.001	0.001
FED026	19.8	20.8	FED026-16	0.04	0.02	1	0.001	0.001
FED026	20.8	21.8	FED026-17	0.8	0.06	1	0.001	0.001
FED026	21.8	22.8	FED026-18	0.39	0.09	2	0.001	0.001
FED026	22.8	23.8	FED026-19	0.36	0.09	8	0.001	0.004
FED026	23.8	24.8	FED026-20	1	0.22	7	0.003	0.004
FED026	24.8	25.8	FED026-21	0.21	0.07	2	0.001	0.001
FED026	25.8	26.8	FED026-22	0.15	0.04	2	0.001	0.002
FED026	26.8	27.8	FED026-23	0.04	0.02	1	0.001	0.0015
FED026	27.8	28.8	FED026-24	0.03	0.01	1	0.001	0.001
FED026	28.8	29.8	FED026-25	0.05	0.03	1	0.001	0.001
FED026	29.8	30.8	FED026-26	0.14	0.1	1	0.001	0.001
FED026	30.8	31.8	FED026-27	0.12	0.07	1	0.001	0.001
FED026	31.8	32.8	FED026-28	0.12	0.13	2	0.001	0.0005
FED026	32.8	33.7	FED026-29	2.25	0.26	8	0.004	0.001
FED026	33.7	34.7	FED026-30	2.73	1.08	137	0.035	0.0165

FED026	34.7	35.7	FED026-31	6.42	1.67	530	0.062	0.013
FED026	35.7	36.7	FED026-32	2.21	0.29	9	0.002	0.001
FED026	36.7	37.7	FED026-33	1.03	0.27	7	0.001	0.001
FED026	37.7	38.7	FED026-34	2.66	0.37	5	0.001	0.001
FED026	38.7	39.7	FED026-35	5.21	0.29	8	0.007	0.0015
FED026	39.7	40.7	FED026-36	4.96	0.27	8	0.004	0.003
FED026	40.7	41.7	FED026-37	2.07	0.27	6	0.002	0.003
FED026	41.7	42.7	FED026-38	1.42	0.32	4	0.007	0.003
FED026	42.7	43.7	FED026-39	1.7	0.53	6	0.025	0.0025
FED026	43.7	44.7	FED026-40	1.86	0.32	5	0.027	0.002
FED026	44.7	45.7	FED026-41	2.03	0.51	8	0.014	0.003
FED026	45.7	46.7	FED026-42	1.02	0.52	6	0.009	0.0035
FED026	46.7	47.7	FED026-43	0.62	0.09	4	0.005	0.0025
FED026	47.7	48.7	FED026-44	0.7	0.49	5	0.011	0.0035
FED026	48.7	49.7	FED026-45	0.91	0.33	5	0.007	0.0025
FED026	49.7	50.7	FED026-46	0.29	0.14	4	0.006	0.0025
FED026	50.7	51.7	FED026-47	0.19	0.05	3	0.008	0.002
FED026	51.7	52.7	FED026-48	0.25	0.07	3	0.01	0.0015
FED026	52.7	53.7	FED026-49	0.55	0.12	3	0.001	0.002
FED026	53.7	54.7	FED026-50	1.75	0.15	10	0.003	0.004
FED026	54.7	55.7	FED026-51	1.04	0.09	12	0.233	0.0055
FED026	55.7	56.7	FED026-52	0.27	0.02	4	0.015	0.0035
FED026	56.7	57.7	FED026-53	0.07	0.01	3	0.029	0.0035
FED026	57.7	58.7	FED026-54	0.08	0.01	1	0.007	0.002
FED026	58.7	59.7	FED026-55	0.2	0.03	1	0.008	0.002
FED026	59.7	60.7	FED026-56	0.29	0.12	2	0.007	0.0025
FED026	60.7	61.7	FED026-57	0.95	0.26	3	0.005	0.0025
FED026	61.7	62.7	FED026-58	0.87	0.03	3	0.012	0.0025
FED026	62.7	63.7	FED026-59	1.71	0.02	3	0.008	0.002
FED026	63.7	64.7	FED026-60	0.53	0.01	2	0.003	0.002
FED026	64.7	65.7	FED026-61	0.39	0.01	2	0.005	0.0015
FED026	65.7	66.7	FED026-62	0.34	0.24	6	0.015	0.0025
FED026	66.7	67.7	FED026-63	0.28	0.03	2	0.003	0.001
FED026	67.7	68.7	FED026-64	0.1	0.03	2	0.014	0.0025
FED026	90.5	91.5	FED026-65	0.03	0.01	1	0.012	0.002
FED026	91.5	92.5	FED026-66	0.04	0.01	1	0.01	0.0025
FED026	92.5	93.5	FED026-67	0.02	0.01	2	0.003	0.0025
FED026	94.5	95.5	FED026-	0.02	0.01	1	0.003	0.002

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FED026	95.5	96.5	FED026-69	0.03	0.01	1	0.001	0.002
FED026	96.5	97.5	FED026-70	0.04	0.01	2	0.001	0.004
FED026	97.5	98.5	FED026-71	0.14	0.01	2	0.02	0.003
FED026	98.5	99.5	FED026-72	0.02	0.01	2	0.004	0.004
FED026	99.5	100.5	FED026-73	0.02	0.01	2	0.001	0.002
SWY001	2	3	SWY001-01	0.031	0.004	1	0.1	0.003
SWY001	3	4.8	SWY001-02	0.014	0.002	-1	0.05	0.001
SWY001	4.8	6	SWY001-03	0.008	0.003	-1	0.05	-0.001
SWY001	6	7	SWY001-04	0.013	0.003	-1	0.05	-0.001
SWY001	7	8	SWY001-05	0.007	0.001	-1	0.06	0.001
SWY001	8	9.5	SWY001-06	0.013	0.002	-1	0.05	0.001
SWY001	9.5	10.5	SWY001-07	0.04	0.002	-1	0.06	0.002
SWY001	10.5	12	SWY001-08	0.013	0.001	-1	0.05	0.001
SWY001	12	13	SWY001-09	0.103	0.001	-1	0.05	-0.001
SWY001	13	14	SWY001-10	0.047	0.001	1	0.05	-0.001
SWY001	14	15	SWY001-11	0.032	0.001	-1	0.06	-0.001
SWY001	15	16	SWY001-12	0.022	0.003	-1	0.05	-0.001
SWY001	16	17	SWY001-13	0.037	0.001	-1	0.05	-0.001
SWY001	17	18	SWY001-14	0.029	0.002	-1	0.05	0.001
SWY001	18	19	SWY001-15	0.023	0.002	-1	0.05	0.003
SWY001	19	20	SWY001-16	0.021	0.002	-1	0.07	0.001
SWY001	20	21.2	SWY001-17	0.01	0.002	-1	0.07	0.001
SWY001	21.2	22.2	SWY001-18	0.026	0.003	-1	0.05	0.001
SWY001	22.2	23.8	SWY001-19	0.022	0.003	-1	0.05	0.001
SWY001	23.8	25	SWY001-20	0.01	0.002	-1	0.05	0.001
SWY001	25	26	SWY001-21	0.01	0.001	-1	0.05	0.001
SWY001	26	27	SWY001-22	0.015	0.002	-1	0.05	0.001
SWY001	27	28.2	SWY001-23	0.1	0.001	-1	0.05	0.001
SWY001	28.2	29	SWY001-24	0.018	0.003	-1	0.05	0.001
SWY001	29	30.3	SWY001-25	0.013	0.002	1	0.05	0.001
SWY001	30.3	31	SWY001-26	0.009	0.001	-1	0.05	0.001

SWY001	31	32	SWY001-27	0.01	0.001	-1	0.05	0.001
SWY001	32	33	SWY001-28	0.007	0.001	-1	0.05	0.001
SWY001	33	34	SWY001-29	0.007	0.001	-1	0.05	-0.001
SWY001	34	35	SWY001-30	0.009	0.001	-1	0.05	0.001
SWY001	35	36	SWY001-31	0.023	0.002	-1	0.8	0.001
SWY001	36	37	SWY001-32	0.009	0.001	-1	0.05	0.001
SWY001	37	38	SWY001-33	0.008	0.001	-1	0.07	0.001
SWY001	38	39	SWY001-34	0.015	0.002	-1	0.05	0.001
SWY001	39	40	SWY001-35	0.015	0.002	-1	0.07	-0.001
SWY001	40	41	SWY001-36	0.01	0.001	-1	0.05	-0.001
SWY001	41	42	SWY001-37	0.006	0.001	-1	0.05	0.001
SWY001	42	43	SWY001-38	0.011	0.001	-1	0.05	-0.001
SWY001	43	44	SWY001-39	0.008	0.003	-1	0.05	0.001
SWY001	44	45	SWY001-40	0.009	0.003	-1	0.05	0.001
SWY001	45	46	SWY001-41	0.011	0.003	-1	0.05	-0.001
SWY001	46	47	SWY001-42	0.008	0.001	-1	0.05	-0.001
SWY001	47	48	SWY001-43	0.005	0.001	-1	0.05	-0.001
SWY002	0	8.5	SWY002-01	0.006	-0.001	-1	0.07	0.001
SWY002	36	37	SWY002-02				0.05	
SWY002	37	38	SWY002-03				0.05	
SWY002	38	39	SWY002-04				0.03	
SWY002	39	40	SWY002-05				0.07	
SWY002	40	41	SWY002-06				0.04	
SWY002	41	42	SWY002-07				0.05	
SWY002	42	43	SWY002-08				0.05	
SWY002	43	44	SWY002-09				0.06	
SWY002	44	45	SWY002-10				0.05	
SWY002	45	46.2	SWY002-11				0.06	
SWY002	46.2	47.2	SWY002-12				0.04	
SWY002	47.2	48.6	SWY002-13				0.06	
SWY002	48.6	50	SWY002-14				0.06	

SWY002	50	51	SWY002-15				0.06		
SWY003	63.5	64.5	SWY003-01	0.021	0.003	2	0.06	0.001	-0.1
SWY003	64.5	65.5	SWY003-02	0.009	0.001	1	0.01	-0.001	-0.1
SWY003	65.5	66.5	SWY003-03	0.008	0.002	1	0.02	-0.001	-0.1
SWY003	66.5	67.5	SWY003-04	0.058	0.009	2	0.05	0.001	-0.1
SWY003	67.5	68.5	SWY003-05	0.046	0.008	-1	0.01	-0.001	-0.1
SWY003	68.5	69.5	SWY003-06	0.022	0.005	1	0.014	0.002	-0.1
SWY003	69.5	70.5	SWY003-07	0.01	0.002	-1	0.01	-0.001	-0.1
SWY003	70.5	71.5	SWY003-08	0.01	0.003	1	0.06	0.002	-0.1
SWY003	71.5	72.5	SWY003-09	0.011	0.003	1	0.05	0.002	-0.1
SWY003	72.5	73.5	SWY003-10	0.021	0.002	1	0.01	-0.001	-0.1
SWY003	73.5	74.5	SWY003-11	0.01	0.009	2	0.01	-0.001	-0.1
SWY003	74.5	75.5	SWY003-12	0.074	0.003	1	0.01	-0.001	-0.1
SWY003	75.5	76.5	SWY003-13	0.015	0.002	-1	0.05	-0.001	-0.1
SWY003	76.5	77.7	SWY003-14	0.007	0.003	1	0.06	-0.001	-0.1
SWY003	77.7	78.7	SWY003-15	0.003	0.002	1	0.04	-0.001	-0.1
SWY003	78.7	79.7	SWY003-16	0.004	0.001	-1	0.01	-0.001	-0.1
SWY003	79.7	80.7	SWY003-17	0.004	0.001	1	0.01	-0.001	-0.1
SWY003	80.7	81.6	SWY003-18	0.003	0.001	-1	0.05	-0.001	-0.1
SWY003	81.6	82	SWY003-19	0.003	0.003	1	0.04	-0.001	-0.1
SWY003	82	83	SWY003-20	0.005	0.001	-1	0.01	-0.001	-0.1
SWY004	0	4	SWY004-01	0.18	0.007	4	0.1	0.001	-0.5
SWY004	4	5	SWY004-02	0.4	0.037	3	0.31	0.004	0.54
SWY004	5	6	SWY004-03	0.18	0.018	1	0.03	0.001	-0.5
SWY004	6	7	SWY004-04	0.25	0.015	2	0.04	0.001	-0.5
SWY004	7	8	SWY004-05	1.5	0.054	8	0.29	0.002	-0.5
SWY004	8	9	SWY004-06	2.3	0.134	18	0.8	0.002	-0.5
SWY004	9	10	SWY004-07	0.88	0.021	3	0.68	0.002	-0.5
SWY004	10	11	SWY004-08	0.57	0.016	1	0.15	0.001	-0.5
SWY004	11	12	SWY004-09	2.9	0.027	12	1.43	0.001	0.68
SWY004	12	13	SWY004-10	0.09	0.004	1	0.01	0.002	0.97

SWY004	13	14	SWY004-11	0.25	0.011	1	0.04	0.001	-0.5
SWY004	14	15	SWY004-12	0.87	0.055	4	0.42	0.002	1.4
SWY004	15	16	SWY004-13	3.2	0.4	15	0.53	0.003	0.84
SWY004	16	17	SWY004-14	7	0.68	21	1.61	0.01	1.2
SWY004	17	18	SWY004-15	9.3	0.72	23	0.48	0.01	2
SWY004	18	19	SWY004-16	6.2	0.125	14	0.28	0.002	2.8
SWY004	19	20	SWY004-17	1.9	0.45	10	0.45	0.003	2
SWY004	20	21	SWY004-18	0.28	0.009	6	0.56	0.003	-0.5
SWY004	21	22	SWY004-19	1.2	0.33	10	0.39	0.004	1.2
SWY004	22	23	SWY004-20	1.7	0.33	13	0.18	0.004	2.6
SWY004	23	24	SWY004-21	5.1	1.63	45	0.12	0.003	1.7
SWY004	24	25	SWY004-22	6.7	0.62	45	0.26	0.004	5.6
SWY004	25	26	SWY004-23	24.5	5.96	120	0.2	0.004	9
SWY004	26	27	SWY004-24	7.7	1.09	57	0.23	0.011	6.4
SWY004	27	28	SWY004-25	1.05	0.57	15	0.19	0.004	1.9
SWY004	28	29	SWY004-26	3.7	0.05	20	0.19	0.004	0.76
SWY004	29	30	SWY004-27	1.4	0.05	11	0.17	0.003	-0.5
SWY004	30	31	SWY004-28	2.2	0.055	14	0.11	0.004	2.4
SWY004	31	32	SWY004-29	5.2	0.073	16	0.27	0.002	4.8
SWY004	32	33	SWY004-30	5.5	0.29	12	0.27	0.001	2
SWY004	33	34	SWY004-31	1.5	0.151	8	0.17	0.002	0.5
SWY004	34	35	SWY004-32	0.28	0.117	2	0.04	0.001	0.5
SWY004	35	36	SWY004-33	0.28	0.035	1	0.07	0.001	0.5
SWY004	36	37	SWY004-34	0.43	0.006	3	0.22	0.002	0.5
SWY004	37	38	SWY004-35	0.23	0.018	5	0.26	0.004	0.5
SWY004	38	39	SWY004-36	3.2	0.087	12	0.42	0.004	0.5
SWY004	39	40	SWY004-37	0.8	0.057	9	0.45	0.003	0.5
SWY004	40	41	SWY004-38	8.2	1.13	36	5.35	0.017	2.1
SWY004	41	42	SWY004-39	6.5	0.032	23	0.38	0.004	0.95
SWY004	42	43	SWY004-40	1.6	0.099	14	0.23	0.003	1.3
SWY004	43	44	SWY004-41	0.7	0.082	7	0.3	0.004	2.5

SWY004	44	45	SWY004-42	5.2	0.37	13	0.62	0.005	2.3
SWY004	45	46	SWY004-43	2.8	0.42	10	0.34	0.004	1.8
SWY004	46	47	SWY004-44	1.1	0.3	11	0.27	0.005	2.6
SWY004	47	48	SWY004-45	1.8	0.25	11	0.75	0.004	1.9
SWY004	48	49	SWY004-46	1.3	0.055	5	0.57	0.004	-0.5
SWY004	49	50	SWY004-47	0.5	0.032	11	0.6	0.004	-0.5
SWY004	50	51	SWY004-48	5.1	0.5	16	0.38	0.003	-0.5
SWY004	51	52	SWY004-49	2.8	0.055	11	0.74	0.004	-0.5
SWY004	52	53	SWY004-50	0.3	0.018	3	0.5	0.004	-0.5
SWY004	53	54	SWY004-51	0.7	0.044	8	0.35	0.003	0.55
SWY004	54	55	SWY004-52	3.3	0.37	10	1.04	0.004	1.6
SWY004	55	56	SWY004-53	2.3	0.11	10	0.47	0.003	1.5
SWY004	56	57	SWY004-54	1.7	0.92	31	0.46	0.005	1
SWY004	57	58	SWY004-55	1.4	0.22	3	0.17	0.001	-0.5
SWY004	58	59	SWY004-56	0.25	0.007	2	0.04	0.001	-0.5
SWY005	0	4	SWY005-01	0.018	0.008	4	0.01	0.001	-0.1
SWY005	4	5	SWY005-02	0.028	0.002	2	0.01	0.002	-0.1
SWY005	5	6	SWY005-03	0.021	0.002	2	0.01	0.002	-0.1
SWY005	6	7	SWY005-04	0.067	0.003	2	-0.01	0.002	-0.1
SWY005	7	8	SWY005-05	0.036	0.002	2	-0.01	0.002	-0.1
SWY005	8	9	SWY005-06	0.041	0.008	1	0.02	0.002	-0.1
SWY005	9	10	SWY005-07	0.17	0.066	2	0.02	0.001	-0.1
SWY005	10	11	SWY005-08	0.395	0.035	2	0.01	0.002	-0.1
SWY005	11	12	SWY005-09	0.058	0.016	1	0.01	0.002	-0.1
SWY005	12	13	SWY005-10	0.03	0.016	2	0.01	0.002	-0.1
SWY005	13	14	SWY005-11	0.028	0.007	-1	0.01	0.002	-0.1
SWY005	14	15	SWY005-12	0.031	0.042	2	-0.01	0.001	-0.1
SWY005	15	16.2	SWY005-13	0.015	0.005	-1	0.01	0.001	-0.1
SWY005	16.2	17.2	SWY005-14	0.053	0.003	-1	0.01	0.002	-0.1
SWY005	17.2	18.2	SWY005-15	0.04	0.006	1	0.01	0.002	-0.1
SWY005	18.2	19.2	SWY005-16	0.008	0.006	1	0.01	-0.001	-0.1

SWY005	19.2	20.2	SWY005-17	0.012	0.005	1	0.01	-0.001	0.1
SWY005	20.2	21.2	SWY005-18	0.014	0.006	1	0.01	0.001	-0.1
SWY005	21.2	21.7	SWY005-19	0.023	0.009	-1	0.01	0.001	-0.1
SWY005	21.7	22.3	SWY005-20	0.02	0.013	1	-0.01	0.001	0.1
SWY005	22.3	23.3	SWY005-21	0.018	0.007	1	0.01	0.001	0.11
SWY005	23.3	24.3	SWY005-22	0.013	0.001	-1	0.01	0.001	-0.1
SWY006	20	21	SWY006-01				0.52		
SWY006	21	22	SWY006-02				0.06		
SWY006	22	23	SWY006-03				0.11		
SWY006	23	24	SWY006-04				1.02		
SWY006	24	25	SWY006-05				0.05		
SWY006	25	26	SWY006-06				0.03		
SWY006	26	27	SWY006-07				0.07		
SWY006	27	28	SWY006-08				0.05		
SWY006	28	29	SWY006-09				0.02		
SWY006	29	30	SWY006-10				0.02		
SWY006	30	31	SWY006-11				0.03		
SWY006	31	32	SWY006-12				0.26		
SWY006	32	33	SWY006-13				0.01		
SWY006	33	34	SWY006-14				0.01		
SWY006	34	35	SWY006-15				0.01		
SWY006	35	36	SWY006-16				0.01		
SWY006	36	37	SWY006-17				0.01		
SWY006	37	38	SWY006-18				0.01		
SWY006	38	39	SWY006-19				0.01		
SWY006	39	40	SWY006-20				0.01		
SWY006	40	41	SWY006-21				0.02		
SWY007	8.5	9.5	SWY007-01	0.025	0.001	1	0.01	-0.001	
SWY007	9.5	10.5	SWY007-02	0.033	0.1	2	0.02	-0.001	
SWY007	10.5	11.5	SWY007-03	0.08	0.004	1	0.02	-0.001	
SWY007	11.5	12.5	SWY007-04	0.9	0.016	5	0.07	-0.001	

SWY007	12.5	13.5	SWY007-05	9	0.73	200	1.05	0.017
SWY007	13.5	14.5	SWY007-06	0.07	0.009	12	0.71	0.001
SWY007	14.5	15.5	SWY007-07	0.17	0.006	8	0.68	0.001
SWY007	15.5	16.5	SWY007-08	0.25	0.005	9	1.32	0.001
SWY007	16.5	17.5	SWY007-09	0.2	0.013	65	3.03	0.005
SWY007	17.5	18.5	SWY007-10	0.2	0.007	10	1.24	-0.001
SWY007	18.5	19.5	SWY007-11	0.12	0.016	9	0.67	0.003
SWY007	19.5	20.5	SWY007-12	0.32	0.022	8	0.77	0.003
SWY007	20.5	21.5	SWY007-13	1.12	0.138	12	1.87	-0.001
SWY007	21.5	22.5	SWY007-14	18.8	1.44	130	1.13	0.01
SWY007	22.5	23.5	SWY007-15	10.6	1.54	160	1.12	0.019
SWY007	23.5	24.5	SWY007-16	3.35	0.78	160	1.03	0.013
SWY007	24.5	25.5	SWY007-17	3.2	0.53	23	0.76	0.004
SWY007	25.5	26.5	SWY007-18	1.42	0.22	20	0.96	-0.001
SWY007	26.5	27.5	SWY007-19	1.35	0.29	13	0.58	-0.001
SWY007	27.5	28.5	SWY007-20	11.2	0.92	65	0.42	0.003
SWY007	28.5	29.5	SWY007-21	8.5	0.4	50	0.32	0.004
SWY007	29.5	30.5	SWY007-22	9.2	0.095	55	0.28	0.005
SWY007	30.5	31.5	SWY007-23	8.1	0.043	18	0.23	0.002
SWY007	31.5	32.5	SWY007-24	1.42	0.026	10	0.78	0.003
SWY007	32.5	33.5	SWY007-25	1.6	0.0381	21	0.9	0.003
SWY007	33.5	34.5	SWY007-26	0.85	0.04	8	0.29	0.001
SWY007	34.5	35.5	SWY007-27	0.5	0.013	3	0.2	0.005
SWY007	35.5	36.5	SWY007-28	0.113	0.008	1	0.18	0.005
SWY007	36.5	37.5	SWY007-29	0.044	0.008	2	0.23	0.004
SWY007	37.5	38.5	SWY007-30	0.024	0.007	1	0.23	0.005
SWY007	38.5	39.5	SWY007-31	0.1	0.008	1	0.35	0.008
SWY007	39.5	40.5	SWY007-32	0.067	0.01	1	0.21	0.007
SWY007	40.5	41.5	SWY007-33	0.196	0.01	2	0.25	0.004
SWY007	41.5	42.5	SWY007-34	1.1	0.025	4	0.59	0.005
SWY007	42.5	43.5	SWY007-35	1.1	0.046	5	0.91	0.004

SWY007	43.5	44.5	SWY007-36	3.2	0.057	13	1.03	0.004	
SWY007	44.5	45.5	SWY007-37	1.5	0.019	13	2.31	0.004	
SWY007	45.5	46.5	SWY007-38	0.7	0.011	4	0.44	0.004	
SWY007	46.5	47.5	SWY007-39	1.4	0.015	4	0.34	0.003	
SWY007	47.5	48.5	SWY007-40	1.6	0.02	6	0.41	0.004	
SWY007	48.5	49.5	SWY007-41	3.9	0.64	21	0.28	0.005	
SWY007	49.5	50.5	SWY007-42	2.6	0.011	15	0.29	0.002	
SWY007	50.5	51.5	SWY007-43	0.051	0.005	2	0.02	0.001	
SWY007	51.5	52.5	SWY007-44	0.061	0.01	1	0.02	-0.001	
SWY007	52.5	53.5	SWY007-45	0.106	0.005	1	0.02	-0.001	
SWY008	8	9	SWY008-01	0.033	0.001	10	0.01	0.001	-0.1
SWY008	9	10	SWY008-02	0.041	0.002	7	0.01	0.002	-0.1
SWY008	10	11	SWY008-03	0.049	0.001	7	0.01	0.003	-0.1
SWY008	11	12	SWY008-04	0.1	0.001	6	0.01	0.003	-0.1
SWY008	12	13	SWY008-05	0.04	0.002	5	0.01	0.003	-0.1
SWY008	13	14	SWY008-06	0.053	0.002	3	0.01	0.001	-0.1
SWY008	14	15	SWY008-07	5	0.012	13	0.04	0.002	-0.1
SWY008	15	16	SWY008-08	2	0.004	14	0.04	0.001	-0.1
SWY008	16	17	SWY008-09	0.3	0.003	3	0.02	0.002	-0.1
SWY008	17	18	SWY008-10	7.9	0.03	20	0.15	0.002	-0.1
SWY008	18	19	SWY008-11	0.3	0.003	2	0.04	0.001	-0.1
SWY008	19	20	SWY008-12	2.4	0.063	9	0.38	0.001	0.1
SWY008	20	21	SWY008-13	0.2	0.017	1	0.02	0.001	-0.1
SWY008	21	22	SWY008-14	0.6	0.011	3	0.4	0.001	0.15
SWY008	22	23	SWY008-15	2.1	0.079	13	0.34	0.003	0.9
SWY008	23	24	SWY008-16	0.7	0.034	9	0.42	0.003	0.52
SWY008	24	25	SWY008-17	0.6	0.006	3	0.17	0.001	-0.1
SWY008	25	26	SWY008-18	0.4	0.006	3	0.27	0.002	0.12
SWY008	26	27	SWY008-19	3	0.008	44	0.77	0.007	0.17
SWY008	27	28	SWY008-20	0.8	0.002	3	0.08	0.002	0.12
SWY008	28	29	SWY008-21	0.4	0.004	3	0.23	0.002	0.52

SWY008	29	30	SWY008-22	0.3	0.002	10	0.33	0.003	0.38
SWY008	30	31	SWY008-23	0.6	0.004	5	0.38	0.003	0.12
SWY008	31	32	SWY008-24	0.3	0.006	4	0.25	0.002	-0.1
SWY008	32	33	SWY008-25	0.3	0.004	3	0.28	0.003	-0.1
SWY008	33	34	SWY008-26	0.9	0.034	2	0.03	0.003	0.4
SWY008	34	35	SWY008-27	0.75	0.038	2	0.7	0.003	-0.1
SWY008	35	36	SWY008-28	0.008	0.002	2	0.28	0.002	0.1
SWY008	36	37	SWY008-29	0.3	0.005	3	0.04	0.003	0.2
SWY008	37	38	SWY008-30	0.8	0.006	4	0.46	0.003	0.34
SWY008	38	39	SWY008-31	0.8	0.011	8	0.36	0.004	0.4
SWY008	39	40	SWY008-32	0.6	0.046	4	0.27	0.003	0.45
SWY008	40	41	SWY008-33	0.6	0.17	9	0.29	0.003	
SWY008	41	42	SWY008-34	0.58	0.16	7	0.3	0.002	
SWY008	42	43	SWY008-35	0.8	0.135	29	0.36	0.004	
SWY008	43	44	SWY008-36	1.2	0.09	26	0.24	0.005	
SWY008	44	45	SWY008-37	0.4	0.017	37	0.27	0.005	
SWY008	45	46	SWY008-38	0.6	0.02	118	1.17	0.023	
SWY008	46	47	SWY008-39	0.084	0.027	12	0.84	0.044	
SWY008	47	48	SWY008-40	0.046	0.014	13	0.33	0.002	
SWY008	48	49	SWY008-41	0.2	0.062	14	0.72	0.003	
SWY008	49	50	SWY008-42	0.2	0.077	10	0.86	0.004	
SWY008	50	51	SWY008-43	3.8	0.011	123	0.62	0.015	
SWY008	51	52	SWY008-44	8.2	0.013	128	0.68	0.012	
SWY008	52	53	SWY008-45	1.4	0.011	47	0.35	0.002	
SWY008	53	54	SWY008-46	0.9	0.013	6	0.04	0.003	
SWY008	54	55	SWY008-47	0.082	0.004	-1	0.02	0.001	
SWY008	55	56	SWY008-48	0.103	0.013	-1	0.01	0.001	
SWY008	56	57	SWY008-49	0.053	0.004	-1	0.02	0.001	
SWY008	57	58	SWY008-50	0.016	0.004	1	0.03	0.001	
SWY010	62	62.2	SWY010-01				0.06		
SWY010	62.2	62.4	SWY010-02				0.13		

SWY010	62.4	62.8	SWY010-03					
SWY010	62.8	63	SWY010-04				0.04	
SWY010	63	63.2	SWY010-05				0.05	
SWY010	63.2	63.4	SWY010-06				0	
SWY010	63.4	63.6	SWY010-07				0.04	
SWY010	63.6	63.8	SWY010-08				0.06	
SWY011	66.3	67.3	SWY011-01	0.005	0.004	2	0.02	0.001
SWY011	67.3	68.3	SWY011-02	1.397	0.108	149	1.5	0.018
SWY011	68.3	69.3	SWY011-03	0.073	0.015	5	0.02	0.002
SWY011	69.3	70.3	SWY011-04	1.103	0.094	13	0.09	0.005
SWY011	70.3	71.3	SWY011-05	0.083	0.157	17	0.33	0.005
SWY011	71.3	72.3	SWY011-06	1.765	0.028	65	0.7	0.009
SWY011	72.3	73.3	SWY011-07	4.926	0.038	79	0.78	0.022
SWY011	73.3	74.3	SWY011-08	2.353	0.149	185	1.2	0.02
SWY011	74.3	75.3	SWY011-09	0.809	0.085	77	2.8	0.03
SWY011	75.3	76.3	SWY011-10	0.515	0.019	104	1.05	0.07
SWY011	76.3	77.3	SWY011-11	1.176	0.263	154	1.65	0.056
SWY011	77.3	78.3	SWY011-12	0.1	0.005	2	0.3	0.002
SWY011	78.3	79.3	SWY011-13	0.956	0.039	146	1.65	0.047
SWY011	79.3	80.3	SWY011-14	0.441	0.023	11	0.35	0.018
SWY011	80.3	81.3	SWY011-15	0.882	0.033	62	0.7	0.042
SWY011	81.3	82.3	SWY011-16	0.588	0.066	192	2.35	0.064
SWY011	82.3	83.3	SWY011-17	0.038	0.036	128	1.1	0.06
SWY011	83.3	84.3	SWY011-18	0.95	0.048	110	1.25	0.035
SWY011	84.3	85.3	SWY011-19	0.956	0.107	145	1.15	0.033
SWY011	85.3	86.3	SWY011-20	0.08	0.035	50	2.35	0.02
SWY011	86.3	87.3	SWY011-21	2.868	0.582	203	1.1	0.021
SWY011	87.3	88.3	SWY011-22	4.706	2.773	227	1	0.026
SWY011	88.3	89.3	SWY011-23	3.088	0.126	182	1.25	0.052
SWY011	89.3	90.3	SWY011-24	1.691	0.179	139	0.7	0.038
SWY011	90.3	91.3	SWY011-25	1.176	0.155	157	0.82	0.022

SWY011	91.3	92.3	SWY011-26	0.441	0.124	115	1	0.05
SWY011	92.3	93.3	SWY011-27	6.324	0.04	109	0.78	0.045
SWY011	93.3	94.3	SWY011-28	1.985	0.163	144	1.15	0.07
SWY011	94.3	95.3	SWY011-29	0.035	0.005	1	0.01	0.001
SWY012	119	120	SWY012-01				0.09	
SWY012	120	121	SWY012-02				0.09	
SWY012	121	122	SWY012-03				0.12	
SWY014	104.7	105.7	SWY014-01	0.17	0.007	2	0.03	0.001
SWY014	105.7	106.9	SWY014-02	1.4	0.43	101	0.25	0.018
SWY014	106.9	107.9	SWY014-03	0.25	0.004	3	0.07	0.003
SWY014	107.9	108.9	SWY014-04	0.33	0.004	1	0.03	0.001
SWY014	108.9	109.9	SWY014-05	0.17	0.003	4	0.03	0.003
SWY014	109.9	110.9	SWY014-06	0.25	0.002	10	0.14	0.004
SWY014	110.9	111.9	SWY014-07	0.17	0.001	2	0.03	0.002
SWY014	111.9	113	SWY014-08	1.6	0.078	92	0.66	0.022
SWY014	113	114	SWY014-09	0.043	0.111	61	0.3	0.014
SWY014	114	115	SWY014-10	0.045	0.056	64	0.48	0.016
SWY014	115	116	SWY014-11	0.5	0.048	97	0.72	0.032
SWY014	116	117	SWY014-12	0.25	0.13	27	0.17	0.014
SWY014	117	118.2	SWY014-13	0.75	0.45	31	0.03	0.017
SWY014	118.2	119	SWY014-14	2.2	0.66	41	0.19	0.015
SWY014	119	120	SWY014-15	0.011	0.2	20	0.11	0.007
SWY014	120	121	SWY014-16	0.33	0.015	15	0.07	0.005
SWY014	121	121.9	SWY014-17	2.3	0.32	23	0.1	0.006
SWY014	121.9	123	SWY014-18	1.2	0.34	120	0.74	0.016
SWY014	123	124	SWY014-19	0.5	0.069	122	0.7	0.011
SWY014	124	125	SWY014-20	0.67	0.21	85	0.21	0.014
SWY014	125	126	SWY014-21	0.5	0.39	25	0.04	0.013
SWY014	126	127	SWY014-22	0.42	0.22	27	0.12	0.014
SWY014	127	128	SWY014-23	0.58	0.56	44	0.64	0.019
SWY014	128	129	SWY014-24	0.013	0.005	6	0.06	0.003

SWY014	129	130	SWY014-25	0.026	0.003	16	0.25	0.012
SWY014	130	131	SWY014-26	0.013	0.006	6	0.08	0.003
SWY014	131	132	SWY014-27	0.009	0.003	10	0.1	0.004
SWY014	132	133	SWY014-28	0.028	0.089	24	0.12	0.014
SWY014	133	134	SWY014-29	0.01	0.004	9	0.11	0.007
SWY014	134	135.5	SWY014-30	0.015	0.008	8	0.14	0.008
SWY014	135.5	136.5	SWY014-31	0.022	0.002	2	0.004	0.001
SWY014	136.5	137.5	SWY014-32	0.056	0.011	1	0.02	0.001
SWY014	137.5	138.5	SWY014-33	0.25	0.001	1	0.03	0.001
SWY014	138.5	139.5	SWY014-34	0.011	0.001	1	0.03	0.002
SWY014	140.5	141.5	SWY014-35				0.11	
SWY014	141.5	142.5	SWY014-36				0.16	
SWY014	142.5	143.5	SWY014-37				0.1	
SWY014	143.5	144.5	SWY014-38				0.11	
SWY014	144.5	145.5	SWY014-39				0.07	
SWY014	145.5	146.5	SWY014-40				0.09	
SWY014	146.5	147.5	SWY014-41				0.07	
SWY014	147.5	148.5	SWY014-42				0.11	
SWY014	148.5	149.5	SWY014-43				0.06	
SWY014	149.5	150.5	SWY014-44				0.07	
SWY014	150.5	151.5	SWY014-45				0.05	
SWY014	151.5	152.5	SWY014-46				0.1	
SWY014	152.5	153.5	SWY014-47				0.12	
SWY014	153.5	154.5	SWY014-48				0.07	
SWY015	206.3	207.3	SWY015-01	0.014	0.013	2	-0.01	0.001
SWY015	207.3	208.3	SWY015-02	0.005	0.003	2	0.02	0.001
SWY015	208.3	209.3	SWY015-03	0.007	0.004	1	0.01	-0.001
SWY015	209.3	210.3	SWY015-04	0.007	0.004	1	0.02	0.007
SWY015	210.3	211.3	SWY015-05	0.39	0.53	47	0.34	0.01
SWY015	211.3	212.3	SWY015-06	0.32	0.54	50	0.23	0.018
SWY015	212.3	213.3	SWY015-07	2.1	1.1	10	0.14	0.004

SWY015	213.3	214.3	SWY015-08	0.11	0.87	48	0.56	0.007
SWY015	214.3	215.3	SWY015-09	0.3	1.2	93	0.48	0.011
SWY015	215.3	216.3	SWY015-10	1.2	1.4	68	0.29	0.007
SWY015	216.3	217.3	SWY015-11	1.1	1.2	85	0.8	0.009
SWY015	217.3	218.3	SWY015-12	0.84	0.77	73	0.6	0.005
SWY015	218.3	219.3	SWY015-13	0.37	0.44	48	0.24	0.003
SWY015	219.3	220.3	SWY015-14	0.041	0.013	2	0.01	0.001
SWY015	220.3	221.7	SWY015-15	0.021	0.022	1	0.02	-0.001
SWY015	221.7	222.7	SWY015-16	0.49	0.27	39	2.4	0.003
SWY015	222.7	223.7	SWY015-17	0.4	0.41	29	2.15	0.005
SWY015	223.7	224.7	SWY015-18	0.008	0.004	1	0.02	0.001
SWY015	224.7	225.7	SWY015-19	0.73	0.84	24	0.34	0.006
SWY015	225.7	226.7	SWY015-20	0.52	0.64	35	0.2	0.007
SWY015	226.7	227.7	SWY015-21	0.56	0.67	44	0.7	0.013
SWY015	227.7	228.7	SWY015-22	0.62	0.45	21	1.25	0.003
SWY015	228.7	229.7	SWY015-23	2.7	0.76	40	0.58	0.01
SWY015	229.7	230.7	SWY015-24	2.4	2.2	39	1.4	0.019
SWY015	230.7	231.7	SWY015-25	2.3	2	22	0.27	0.003
SWY015	231.7	232.7	SWY015-26	1.5	1.5	18	0.25	0.005
SWY015	232.7	233.7	SWY015-27	2.7	0.87	15	0.9	0.005
SWY015	233.7	234.7	SWY015-28	5.3	0.93	41	0.5	0.011
SWY015	234.7	235.7	SWY015-29	0.22	0.91	17	0.37	0.009
SWY015	235.7	236.7	SWY015-30	0.14	0.75	14	0.36	0.013
SWY015	236.7	237.7	SWY015-31	0.073	0.031	9	0.18	0.004
SWY015	237.7	238.7	SWY015-32	0.18	0.36	6	0.72	0.004
SWY015	238.7	239.7	SWY015-33	0.011	0.083	7	2.1	0.007
SWY015	239.7	240.7	SWY015-34	0.056	0.23	12	0.76	0.011
SWY015	240.7	241.7	SWY015-35	0.084	0.72	19	0.18	0.007
SWY015	241.7	242.7	SWY015-36	0.024	0.018	2	0.03	0.002
SWY015	242.7	243.7	SWY015-37	0.008	0.006	2	0.01	0.002
SWY015	243.7	244.7	SWY015-38	0.014	0.007	2	0.01	0.001

SWY015	244.7	245.7	SWY015-39	-0.1	0.01	2	0.074
SWY018	177.5	178.5	SWY018-01	-0.1			
SWY018	178.5	179.5	SWY018-02	-0.1			

Downhole Surveys

Hole_ID	Depth	Dip	Orig_Grid_ID	Orig_Azimuth
FED001	0	-50	GDA94_55	287
FED001	93	-51	GDA94_55	287
FED001	142	-51	GDA94_55	287.5
FED001	193	-52	GDA94_55	289
FED002	0	-45	GDA94_55	151
FED002	40	-47.5	GDA94_55	151
FED002	90	-46.5	GDA94_55	152
FED002	137.5	-46	GDA94_55	153
FED003	0	-89.5	GDA94_55	232
FED003	40	-90	GDA94_55	232
FED003	90	-89.75	GDA94_55	48
FED003	130	-89.75	GDA94_55	321
FED004	0	-54	GDA94_55	325
FED004	7	-54.5	GDA94_55	325
FED004	71	-54.5	GDA94_55	330
FED004	130	-54	GDA94_55	330.5
FED005	0	-46.5	GDA94_55	331
FED005	28	-50	GDA94_55	331
FED005	67	-51	GDA94_55	331
FED005	111	-52	GDA94_55	332
FED005	156	-53	GDA94_55	332.5
FED005	186	-53	GDA94_55	332
FED006	0	-45.75	GDA94_55	303
FED006	45	-47	GDA94_55	303
FED006	93	-47.5	GDA94_55	302.5
FED006	141	-47.5	GDA94_55	302
FED006	186	-46.5	GDA94_55	300.5
FED007	0	-70	GDA94_55	340
FED007	35	-71	GDA94_55	340
FED007	65	-71	GDA94_55	340
FED007	95	-71	GDA94_55	340
FED008	0	-45	GDA94_55	150
FED008	35	-46	GDA94_55	150
FED008	93	-47	GDA94_55	148
FED008	150	-48	GDA94_55	149
FED009	0	-50	GDA94_55	320
FED009	53	-48	GDA94_55	322
FED009	98	-49	GDA94_55	323
FED009	155	-48	GDA94_55	324
FED010	0	-63	GDA94_55	225
FED010	35	-65	GDA94_55	226
FED010	97	-65.5	GDA94_55	226
FED010	139	-66	GDA94_55	228

FED011	0	-66	GDA94_55	118
FED011	15	-66	GDA94_55	117
FED011	60	-65	GDA94_55	116
FED011	115	-64	GDA94_55	113
FED012	0	-52	GDA94_55	350
FED012	41	-53.8	GDA94_55	351
FED012	71	-54.2	GDA94_55	352
FED012	122	-54.2	GDA94_55	336
FED012	173	-54	GDA94_55	339
FED012	218	-53.5	GDA94_55	340
FED012	263	-54.5	GDA94_55	341
FED012	308	-55	GDA94_55	342
FED013	0	-90	GDA94_55	204
FED013	68	-89.5	GDA94_55	204
FED014	0	-90	GDA94_55	359
FED014	50	-88.5	GDA94_55	359
FED014	102	-88	GDA94_55	350
FED015	0	-55	GDA94_55	310
FED015	50	-56.8	GDA94_55	310
FED015	98	-56	GDA94_55	310
FED016	12	-56	GDA94_55	33
FED016	56	-56	GDA94_55	33.5
FED016	108	-55	GDA94_55	35
FED017	0	-70	GDA94_55	195
FED017	21	-69	GDA94_55	195.2
FED017	52	-68.5	GDA94_55	196.7
FED017	101	-68	GDA94_55	200.2
FED017	152	-67.5	GDA94_55	202.2
FED017	200	-66.5	GDA94_55	206.2
FED018	0	-50	GDA94_55	346.1
FED018	30	-52.5	GDA94_55	343.6
FED018	64	-53	GDA94_55	340.8
FED018	119	-55	GDA94_55	336.2
FED018	158	-55	GDA94_55	336.2
FED018	198	-56	GDA94_55	336.2
FED018	236	-56	GDA94_55	337.2
FED018	275	-56	GDA94_55	338.2
FED019	0	-60	GDA94_55	161
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FED019	118	-59.5	GDA94_55	167
FED019	157	-59	GDA94_55	169
FED019	157.3	-59	GDA94_55	171
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FED020	0	-47	GDA94_55	26
FED021	0	-53.7	GDA94_55	323

FED021	48	-53.7	GDA94_55	323
FED021	66	-53	GDA94_55	325
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FED021	117	-53	GDA94_55	325
FED022	0	-74	GDA94_55	9
FED022	53	-74	GDA94_55	11
FED022	74	-74	GDA94_55	13
FED022	113	-74	GDA94_55	14
FED022	152	-74	GDA94_55	18
FED022	193	-74	GDA94_55	21
FED022	230	-74	GDA94_55	26
FED023	0	-41	GDA94_55	36
FED023	37	-41	GDA94_55	39
FED023	76	-40	GDA94_55	42
FED023	115	-40	GDA94_55	45
FED023	154	-39.5	GDA94_55	46
FED023	193	-39	GDA94_55	49
FED023	232	-38.5	GDA94_55	52
FED024	0	-53	GDA94_55	119
FED024	31	-52.5	GDA94_55	121
FED024	61	-53.5	GDA94_55	121
FED024	94	-54	GDA94_55	121
FED024	124	-55	GDA94_55	123
FED024	154	-55	GDA94_55	122
FED024	184	-55	GDA94_55	123
FED025	0	-46	GDA94_55	257
FED025	37	-48	GDA94_55	258
FED025	76	-28	GDA94_55	260
FED025	115	-28	GDA94_55	261
FED025	154	-47.5	GDA94_55	263
FED025	196	-46	GDA94_55	264
FED026	0	-45	GDA94_55	299
FED026	29.8	-45.5	GDA94_55	297
FED026	59.8	-46.5	GDA94_55	298
FED026	89.8	-46.5	GDA94_55	299
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SWY001	95	-41	GDA94_55	222
SWY001	149	-38	GDA94_55	224
SWY002	0	-89.45	GDA94_55	12
SWY002	101	-89.15	GDA94_55	83
SWY003	0	-45	GDA94_55	352
SWY003	50	-45	GDA94_55	354
SWY003	100	-44.5	GDA94_55	356
SWY003	152	-42.5	GDA94_55	360

SWY004	0	-45.75	GDA94_55	109
SWY004	50	-46.5	GDA94_55	114
SWY004	101	-44.75	GDA94_55	119.5
SWY005	0	-81	GDA94_55	112
SWY005	80.4	-77	GDA94_55	119
SWY006	0	-45	GDA94_55	246
SWY006	50	-45	GDA94_55	246
SWY006	101	-43.5	GDA94_55	246
SWY006	155.2	-39	GDA94_55	247
SWY007	0	-70	GDA94_55	337
SWY007	17	-70.5	GDA94_55	335
SWY007	40	-70.5	GDA94_55	333
SWY007	65	-70	GDA94_55	334
SWY007	90	-70	GDA94_55	334
SWY008	0	-60	GDA94_55	245
SWY008	24	-60	GDA94_55	245
SWY008	49	-60	GDA94_55	245
SWY008	74	-59.75	GDA94_55	246
SWY008	101	-59.25	GDA94_55	247.5
SWY008	137.3	-59.25	GDA94_55	247.5
SWY009	0	-60	GDA94_55	102
SWY009	26	-60.5	GDA94_55	102
SWY009	51	-58.5	GDA94_55	104
SWY009	76	-57.75	GDA94_55	102
SWY009	102.3	-56.25	GDA94_55	102.5
SWY010	0	-60	GDA94_55	142
SWY010	17	-59.5	GDA94_55	147
SWY010	50	-58	GDA94_55	151
SWY010	92	-55	GDA94_55	148
SWY011	0	-60	GDA94_55	192
SWY011	100	-60.25	GDA94_55	199
SWY011	134.3	-58.25	GDA94_55	197
SWY012	0	-80	GDA94_55	265
SWY012	40	-80.25	GDA94_55	265
SWY012	76	-81	GDA94_55	275
SWY012	104	-80.75	GDA94_55	271
SWY012	148	-80.5	GDA94_55	277
SWY012	191.5	-79	GDA94_55	273
SWY013	0	-63	GDA94_55	272
SWY013	50	-63	GDA94_55	267
SWY013	101	-61.5	GDA94_55	266
SWY013	140	-60	GDA94_55	270
SWY014	0	-70	GDA94_55	317
SWY014	139	-71.5	GDA94_55	318
SWY014	190	-70	GDA94_55	322
SWY014	191.5	-70	GDA94_55	322

SWY015	0	-85	GDA94_55	359
SWY015	28	-86	GDA94_55	356
SWY015	52	-88	GDA94_55	350
SWY015	79	-86.5	GDA94_55	356
SWY015	105	-86	GDA94_55	359
SWY015	139	-85.5	GDA94_55	359
SWY015	181	-84	GDA94_55	359
SWY016	0	-77	GDA94_55	237
SWY016	39	-77	GDA94_55	237
SWY016	81	-77	GDA94_55	243
SWY016	120	-77.5	GDA94_55	245
SWY016	159	-77	GDA94_55	234
SWY016	201	-77	GDA94_55	239
SWY016	243	-76.5	GDA94_55	242
SWY017	0	-68	GDA94_55	236
SWY017	34	-66.5	GDA94_55	238
SWY017	64	-64.5	GDA94_55	242
SWY017	94	-65	GDA94_55	244
SWY017	124	-64	GDA94_55	242
SWY017	154	-63.5	GDA94_55	244
SWY017	181	-61.5	GDA94_55	247
SWY017	214	-60	GDA94_55	248
SWY017	244	-58	GDA94_55	249
SWY018	0	-50	GDA94_55	357
SWY018	18	-50	GDA94_55	357.5
SWY018	36	-49.5	GDA94_55	358.5
SWY018	77	-48.5	GDA94_55	1
SWY018	107	-46.5	GDA94_55	1
SWY018	135	-44.75	GDA94_55	2.5
SWY018	180	-43	GDA94_55	2
SWY018	210	-40.75	GDA94_55	4
SWY018	234	-39.75	GDA94_55	5

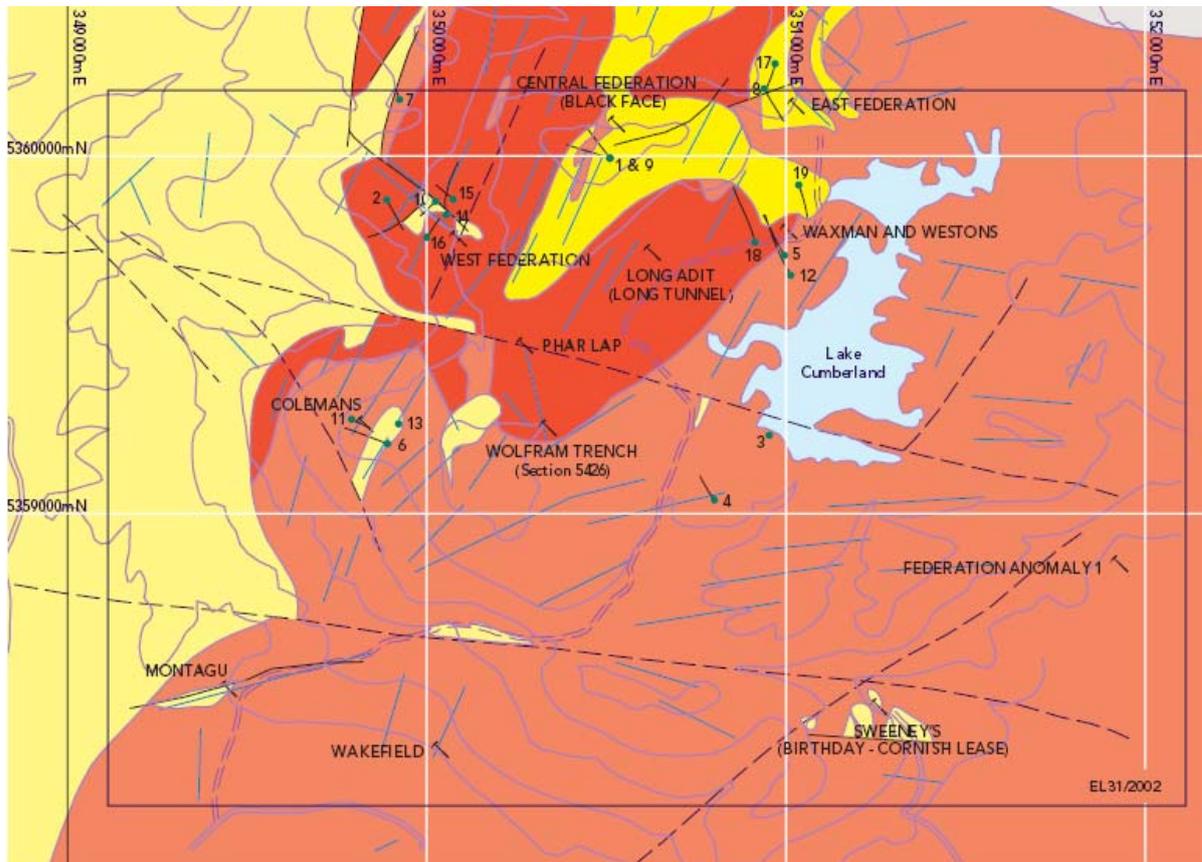
Appendix 3 – Sweeney’s resource report and ASX announcement



STONEHENGE METALS
LIMITED

Zeehan Field Operations

Resource Report – Sweeny's Tin Prospect



April 2008

Compiled T J Hibberd

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Statement of Competency

All information in this report is based on, and accurately reflects, information compiled by Stonehenge Metals Operations staff under the supervision of Todd Hibberd (Managing Director) who is a competent Person as defined in the Australasian Code for Reporting of Identified Mineral Resources and Ore Reserves (the *JORC* Code).

Signature

Name Todd Hibberd
Position Managing Director

Contributing Staff



Signature

Name Todd Hibberd
Position Managing Director
Responsibility Geological review, Data validation and Estimation

1 Executive Summary

The Sweeny's Prospect is located approximately 12km west of the Zeehan near the base of Mt Agnew in North West Tasmania. The prospect is contained within the exploration license EL31/2002 (held 100% by Stonehenge Metals).

Tin-zinc-silver mineralisation is predominantly hosted in altered granite within a broad zone of "greisen" style mineralisation containing quartz tourmaline veining. Mineralisation appears to be closely associated with faulting and cracking of the granite. The mineralization contains abundant black sphalerite with pyrite and small amounts of stibnite and chalcopyrite in a gangue of quartz, siderite, fluorite, and tourmaline. Modeling data indicates that the ore body is lenticular, strike North-South and dips steeply to the West.

The Sweeny's resource is classified as Inferred based on irregular drill hole spacing and contains 562,000 tonnes at 0.5% tin, 1.4% zinc and 657,000 ounces of silver. The resource was calculated using a 0.2% tin cut-off grade.

Tonnes	Sn (%)	Zn (%)	Ag (g/t)	Tin Metal (tonnes)	Zinc Metal (tonnes)	Silver Metal (oz)
562,000	0.5	1.4	36.4	2,869	8,000	657,000

The Sweeny's resource has a number of positive attributes that bode well for its potential commercial development:

- Mineralisation starts at the surface and is open in all directions
- The bulk of the resource is shallow and is potentially amenable to open pit mining
- Potential to expand the resource and add additional resources from the adjacent Anomaly One deposit
- The deposit is located adjacent to a road and is within 12km of milling infrastructure

Metallurgical test work will be required to establish if the tin-silver and zinc can be separated economically.

2 Geology and Resource Generation

2.1 Introduction

EL 31/2002 covers an area of six square kilometres and is located approximately twelve kilometres west of Zeehan on the west coast of Tasmania. The lease was transferred to Stonehenge Metals Limited in 2006 subject to Stonehenge's subsequent listing on the Australian Stock Exchange on 20th December 2006. Stonehenge Metals Limited began active exploration of the tenement in January 2007. Its principal targets of interest are Proterozoic greisen style tin-zinc-silver deposits, and shear hosted tin deposits.

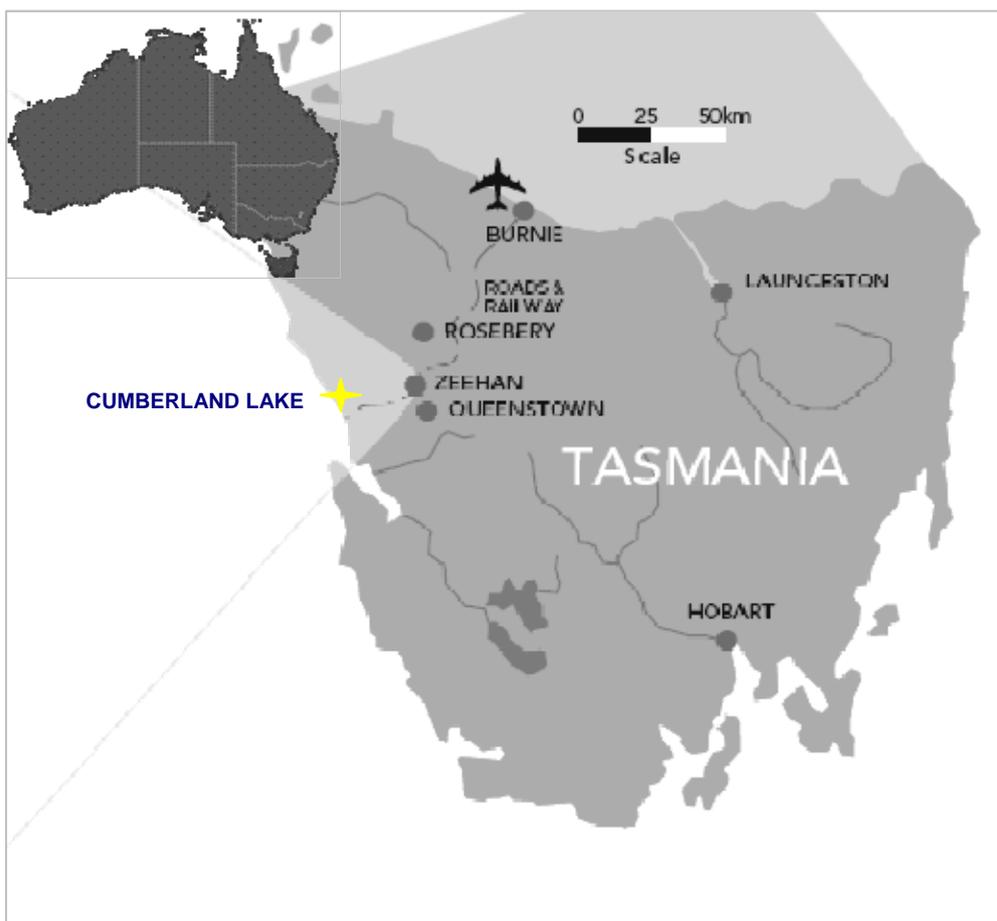


Figure 1 Map showing location of the Cumberland Lake lease.

2.2 Location, Access and Tenure

The tenement lies about 12km west of Zeehan (Tasmania, Australia) and includes Lake Cumberland. All co-ordinates used are referenced to the GDA94 datum. The tenement is located in UTM Zone 55. The tenement is located approximately at Latitude: -41.907° , Longitude: 145.201° . Access to the prospects of interest is from the southeast via the Trail Harbour road. The existing roads are cut into the granite and have a generally well-compacted surface suitable for 4WD during the wet, winter months or two-wheel drive during drier periods.

The topography provides varied foot access, ranging from gently to moderately sloping, fairly open, button grass covered granite to, heavily forested gullies and incised steep hill slopes (inaccessible by foot) with relief of three to five hundred metres. The annual rainfall in the area is usually heavy – up to

two and a half metres, with most falling in the winter months. Outcrop over both open ground and hill slopes is generally good; with road cuttings and existing workings providing excellent rock exposures.

The tenement is held 100% by Stonehenge Metals Limited. In January 2007 EL21/2002 was transferred from McDermott Mining. Prior to this EL 31/2002 was granted to Marshall Resources on December 18th, 2002. Marshall Resources was unable to raise capital for a comprehensive exploration program and invited McDermott Mining to joint venture the licence. A dealing was registered with MRT, giving McDermott Mining 66% of the joint venture, and a program consisting of the following was drawn up for submission to MRT. Marshall Resources subsequently withdrew from further active involvement in 31/2002.

2.3 Regional Geology

The main features of the regional geology are a large granite dome which intruded a sequence of Proterozoic sedimentary rocks (older than 600 My) during Late Devonian times (c.390 My ago). The granite is known as the Mt Heemskirk granite with the mountain of that name being located in the north east of the granite outcrop and rising to 742m. Mt Agnew, another significant topographic feature, is located in the south eastern area of the granite outcrop, rises to 848m, and lies 9km due west of the township of Zeehan.

The broad regional geology is presented in Figure 2 and the tenements that Stonehenge is acquiring are also shown on this map. The tenements are close to the main roads providing good access to the tenements but due to topography and marshy areas access to some areas within the tenements is more difficult.

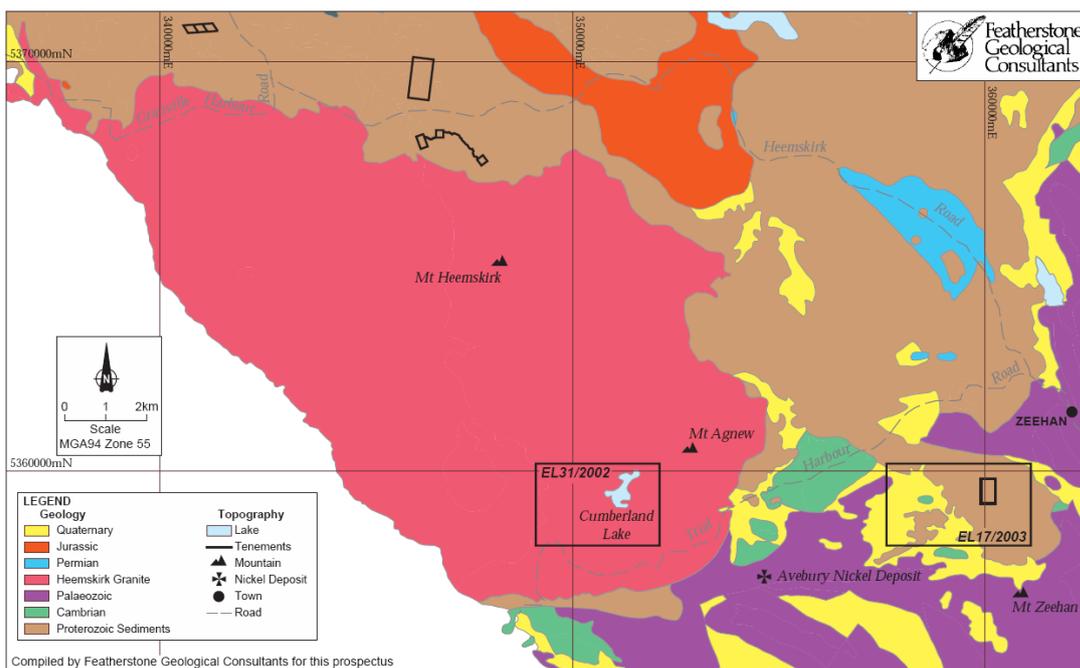


Figure 2. Regional Geology of the Zeehan Area.

The granite is a coarse grained tourmaline rich muscovite granite. Its outcrop is roughly oval in shape, elongated E-W, with the western portions extending to the west under the sea. The outcrop is 10km north to south and the granite is not homogeneous with several different variations able to be mapped. The intrusion shows chilled margins within 2m to 3m of the contact where it is a fine grained, white, aplitic granite. The main body of the intrusion is formed of a red granite but in some areas a white granite is present and tin mineralization may be associated with the white granite.

The Proterozoic rocks are mainly quartzite, micaceous quartzite, and black shale of the Oonah Formation. Carbonate rich beds are also present. These rocks have undergone medium grade regional metamorphism and may also have been subjected to contact metamorphic effects close to

the granite where they were heated by the granite magma. In the south east and the south rocks of Cambrian age are present and these are also intruded by the granite. These are mostly sedimentary but also include some ultramafic bodies which are attracting attention as part of a new geological model for economic nickel deposits such as that being currently developed at Avebury.

The late stages in the crystallization of the granite resulted in the production of hot saline solutions containing various metallic elements. Stresses produced by the intrusion resulted in faults and fractures in the country rocks and also fractures in the granite itself in some places. The solutions carrying the metallic ions were able to enter some of the fissures and as the solutions travelled along them they began to cool and precipitate minerals which crystallised on the walls of the fissure and formed a vein. Such fissures are called lodes and such mineralization is referred to as hydrothermal mineralization. Since different metallic minerals crystallize at different temperatures those that crystallize at higher temperatures are deposited first and the others further along, or up, the lode. This results in a zonation of the mineralization with high temperature minerals near the granite and lower temperature minerals further away.

2.4 Mine Geology

The tenement is entirely within a granite dome known as the Mt Heemskirk granite which has intruded a sequence of Proterozoic sedimentary rocks during the Late Devonian. The Heemskirk granite is a multiphase intrusion with tin mineralization being related to the latest phase. The licence covers a number tin bearing lodes in an area known as the South Heemskirk Tinfield.

A number of tin exploration targets occur within the granite near the southern contact. Historic mines here were mainly based on lode style mineralization, however at Sweeney's the mineralization is greisen tin-zinc style. A defined magnetic anomaly to the west of Sweeney's may be caused by another body of greisen mineralization and is being investigated.

The focus of exploration is the Sweeney's tin-zinc prospect. During the late nineteen seventies a total of eighteen diamond drill holes were drilled into the Sweeney's mine. Although eight of these missed the target mineralisation, information from the remaining ten holes was used to assign a tonnage and grade estimate to the mineralisation of 500,000 tonnes at 0.6% tin. The tin mineralisation was open at depth and along (an interpreted SSE) strike. The most northerly adit contained 47 metres at 0.6% tin, 0.96% zinc and 7 g/t silver.

2.5 Mineralisation and Structure

Tin-zinc-silver mineralisation is predominantly hosted in altered granite within a broad zone of "greisen" style mineralisation containing quartz tourmaline veining. Mineralisation appears to be closely associated with faulting and cracking of the granite. The mineralization contains abundant black sphalerite with pyrite and small amounts of stibnite and chalcopyrite in a gangue of quartz, siderite, fluorite, and tourmaline. Modeling data indicates that the ore body is lenticular, strike North-South and dips steeply to the West. The modeled ore body appears to be cut off by a cross cutting fault to the North.

3 Data Quality and Sampling Procedures

3.1 Data Locations

All data relating to this resource report is located on the Stonehenge Server in the following directory:
S:\Projects\EL31-2002-Federation\04-Mapping\VulcanSweenies

Specific files are detailed in the following table:

File Type	Name	Description
Access drilling database	she.mdb	S:\Projects\Databases\She.mdb
Composited assay data	tasswy.cmp.isis	Vulcan composite assay drill hole data
Ore triangulation/model	swy_ore.00t fed_contours.00t	3D ore volume model Topography surface model
Assay data set for stats	Swy_Sn stats.csv Swy_Zn stats.csv Swy_Ag stats.csv	Assay data within ore triangulation
Recovery data for statistics	NA	Core recovery dataset
Variography file	NA	Supervisor variography file
Block model definition file	tasswy0907.bdf	
Block estimation file	tasswy0907.bef	
Block model file	tassun0907.bmf	
Resource documentation	Resource_swy_0408.doc	

3.2 Drilling Type and Orientation

All drilling carried out at Sweeny's was via diamond core. A total of 18 diamond core holes were drilling. Results of the drilling are summarised below:

Hole ID	Hole Type	Orig Grid	Orig East	Orig North	Orig RL	Dip	Orig Azimuth	Max Depth
SWY001	DD	GDA94_55	351277	5358521	285.55	-43.5	222	149
SWY002	DD	GDA94_55	351112	5358461	353.42	-89.5	12	101.5
SWY003	DD	GDA94_55	351211	5358445	332	-45	352	152.5
SWY004	DD	GDA94_55	351229	5358481	319.52	-45.8	109	101
SWY005	DD	GDA94_55	351228	5358481	319.44	-81	112	80.4
SWY006	DD	GDA94_55	351324	5358494	292.3	-45	246	155.2
SWY007	DD	GDA94_55	351268	5358447	322.58	-70	337	95.5
SWY008	DD	GDA94_55	351269	5358444	322.53	-60	245	137.3
SWY009	DD	GDA94_55	351272	5358444	322.36	-60	102	102.5
SWY010	DD	GDA94_55	351211	5358441	332.11	-60	142	92.4
SWY011	DD	GDA94_55	351273	5358447	322.6	-60	192	134.3
SWY012	DD	GDA94_55	351313	5358370	323.24	-80	265	191.5
SWY013	DD	GDA94_55	351313	5358370	323.24	-63	272	140
SWY014	DD	GDA94_55	351313	5358370	323.1	-70	317	191.5
SWY015	DD	GDA94_55	351313	5358370	323.24	-85	359	254.5
SWY016	DD	GDA94_55	351316	5358434	313.13	-77	237	257.4
SWY017	DD	GDA94_55	351395	5358382	296.17	-68	236	245.2
SWY018	DD	GDA94_55	351269	5358084	270.62	-50	357	249.1

Table 1 Sweenies drill hole data

This drilling attempted to elucidate the shape of the mineralized zone however the topography in the area makes establishing suitable drill sites very difficult. This resulted in the holes being drilled in various directions, being collared at different heights, and is totally irregular. The shape of this body of mineralization is also irregular which resulted in a significant number of the holes (11 out of 17) failing to make satisfactory intersections. The results obtained were modelled to define the shape of this zone of mineralisation. Various geophysical surveys were conducted to see if they could aid in defining the limits of the mineralization but were of only limited value.

During 1978-79 a further DC hole was drilled at Sweeney's, (Swy 18. 249m), which failed to locate any mineralisation.

In addition the following Table summarises the success of the drilling

Hole No.	Intercept (m)	Tin Grade %	Zinc Grade %	Silver g/t	Comment
Swy 1-3	Failed to intersect main greisen zone				
Swy 4	51	0.50	2.7	14	
Swy 5	Drilled in margin of greisen				
Swy 6	Drilled below the greisen				
Swy 7	38	0.75	2.84	31	
Swy 8	32	0.41	1.03	23	
Swy 9	Drilled to the south of the greisen				
Swy 10	Drilled to the south of the greisen (intersected altered granite)				
Swy 11	23	1.17	1.7	121	Stannite & Topaz
Swy 12	In margin of greisen				
Swy 13	In margin of greisen				
Swy 14	23.6	0.27	0.52	42	In top of greisen
Swy 15	31.4	0.62	1.92	31	
Swy 16-17	Failed to intersect main greisen zone				

Table 2 Summary of Sweenies mineralised drill intersections

3.3 Ground Conditions

Based on the diamond core logs from the historical drilling core recovery was greater than 99% for all holes and ground conditions were excellent.

3.4 Surveying

Historical drilling was compiled in local coordinates and converted to GDA 94 using high resolution ortho-linear rectified aerial photography. The conversion was field verified using Magellan GPS units with accuracies of within five metres. Drill hole orientations were field verified using the orientation of the drill hole collars and compiling historical down hole single shot surveys.

3.5 Sampling and Logging Procedures

Sampling and logging procedures have not been specified in the historical reports however, the geological logging, assays and hole details are all recorded in detail. The bulk of the work was carried out by Renison Goldfields.

3.6 Analytical Methods

Analytical methods have not been specified in the historical report however, the bulk of the analysis was carried out by Renison Goldfields at the Renison- Bell laboratory in Zeehan.

3.7 Databases

3.7.1 Assay data and Assay quality control checks

Assay data is validated and compiled from historical hard copy reports. Data is stored in Microsoft Access on the Stonehenge server. Historical assay quality control checks are not specified.

4 Resource Statistics

4.1 Geological Modelling Criteria

Mineralised intersections were wire framed on 25m sections normal to the interpreted strike of mineralisation. Wire frames were constructed using an edge cut off grade of 0.2% Tin and maximum 2m of internal dilution. Intersections below the 0.2% were included in wire frames where lithological or structural information indicated continuity. Wire frame boundaries were extended halfway to the next non-mineralised hole or extended 20m past the last intersection and tapered to restrict tonnage.

4.2 Domains

Geophysical chargeability maps indicate the ore body is lenticular and strikes NNW-SSE. Geological modelling supports this interpretation. Mineralisation wire frames were combined into solid volumes by lode and grouped into a single major structural domain. Sweenies strikes at a bearing of 350 degrees (grid GDA 94z55) and dips steeply to the West.

4.3 Statistical Analysis

Samples were composited on a variable length basis using the straight option in Envisage and flagged if within an ore triangulation. The map file was stripped of assays that fell outside the ore triangulations. Note that the majority of results were sampled in one metre intervals and statistical analysis was carried out on a length weighted basis to eliminate bias in the grade variability

Sample statistics within ore wire frames indicate a near lognormal grade distribution. Note that the sample statistics have not been de-clustered so may have some bias.

Statistics	Sn	Zn	Ag	Assay Percentiles	Sn	Zn	Ag
Samples	184	199	206	10%	0.19	0.2	2.29
Minimum	0.09	0.05	0.89	20%	0.25	0.32	4.16
Maximum	3.94	19.38	227	30%	0.29	0.54	8.85
Mean	0.63642	2.02201	37.23	40%	0.35	0.7	11
Standard deviation	0.5679	2.86981	48.8368	50%	0.44	0.96	13.59
CV	0.892334	1.41928	1.31176	60%	0.61	1.4	21
Variance	0.32251	8.23582	2385.03	70%	0.71	1.97	33
Skewness	2.52834	3.21504	1.83805	80%	0.9	2.94	65
Log samples	184	199	206	90%	1.2	4.93	118
Log mean	-0.752539	-0.01543	2.77453	95%	1.65	8.1	149
Log variance	0.59274	1.53635	1.92139	97.50%	2.31	9.2	182
Geometric mean	0.471169	0.984691	16.0311	99%	2.8	12.53	200
Top Cuts					3.0	10	160

Table 3 Sample Statistic

Based on log histogram plots and log probability plots, top cuts of 3.0% tin, 10% zinc and 160 g/t silver were applied. The top cuts represent 99.5% of the assay percentile. The coefficient of variance (CV) is low for tin but greater than one suggesting some nugget effect for zinc and silver. The sample distribution is moderately skewed for all metals indicating that the majority of metal will be in the estimate will result for a small number of samples. Based on the above statistics it will be difficult to produce a good local estimate however a global estimate is adequate to calculate an inferred resource.

5 Resource Variography

Variography was attempted but useful variograms could not be generated due to the irregular spacing and orientation of drill holes. Geophysical chargeability maps indicate the ore body is lenticular and strikes NNW-SSE. Geological modelling supports this interpretation but these orientations are not discernable in the variograms. A secondary issue is the limited number of samples which also affects the variography.

The search ellipse orientation has been set to the strike and dip of the wire frame (transformed into ZYX axes rotations). The search distance has been set to approximately twice the drill spacing.

6 Resource Modelling

6.1 Estimation Methodology

The resource estimate is based on 18 diamond core drill holes designed to intersect the mineralisation on variable spacing. The deposit was been modelled in three dimensions using cross sectional interpretations of the mineralisation. The deposit boundary was defined by a cut-off grade of 0.2% tin (Sn) which coincides with the geological boundary of the shear zone.

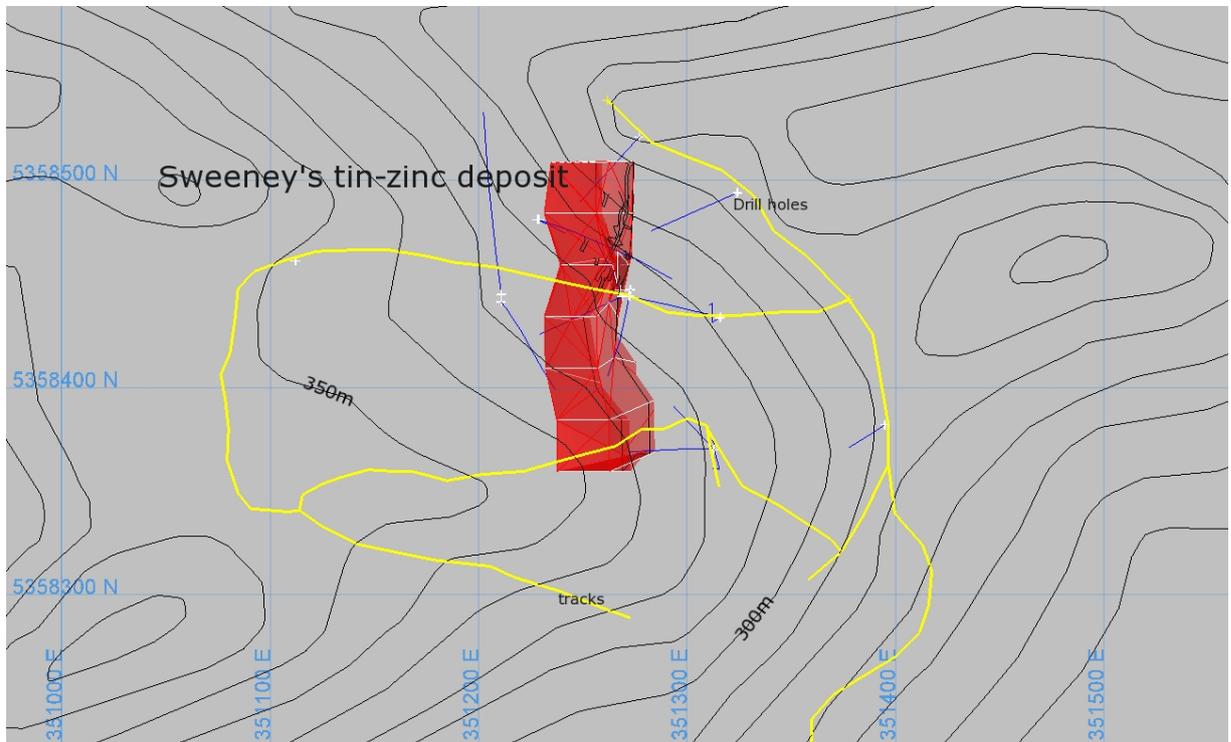


Figure 1 Three dimensional model of the Sweeney's tin-zinc-silver deposit with drill holes traces in blue and elevation contours in black.

Individual blocks were defined around drill hole intersections with block boundaries on and between cross sections were defined by the midpoints between adjacent holes and by geological constraints. Based on statistical analysis, maximum sample assays were reduced to 3.0% tin, 10% zinc and

160gpt silver (top cuts) and all grades were length weighted. Block densities were assigned based on density analysis of samples collected from surface pits and the underground adit. Estimation methodology was restricted to inverse distance squared.

6.2 Bulk Density

Densities for mineralised Sweeny's ore are based on two rock chip samples taken from the surface pits and the underground adit. The surrounding barren material is predominantly sericitized altered granite which has a density of approximately 2.75

Rock Type	Density
Open Pit Ore	2.57
Underground Adit Ore	2.46
Altered Granite	2.75
Average Ore	2.50

6.3 Sample Recovery

Historical logging indicated that core recovery was excellent with most core having 100% recovery

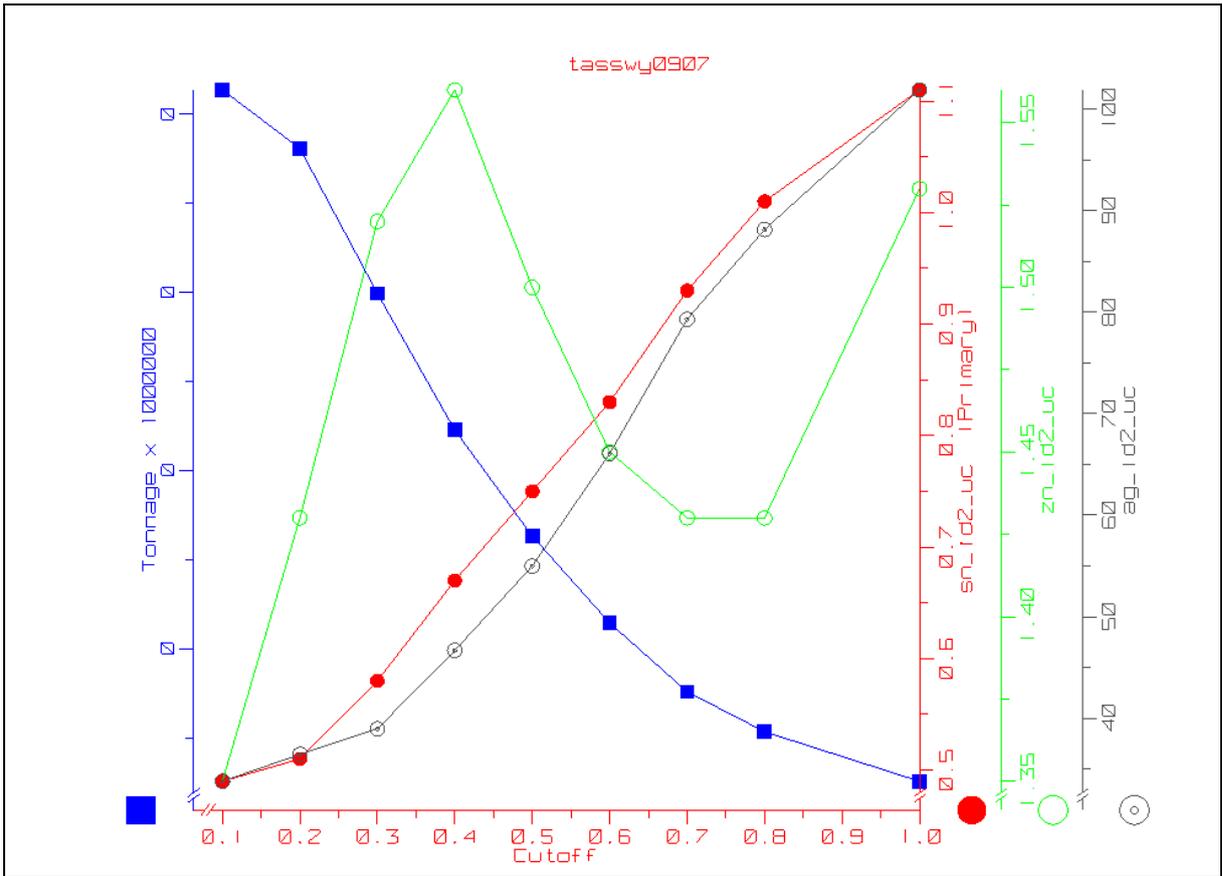
6.4 Resource Estimate

The Sweeny's resource is classified as Inferred due to irregular drill hole spacing and contains 562,000 tonnes at 0.5% tin, 1.4% zinc and 657,000 ounces of silver. The resource was calculated using a 0.2% tin cut-off grade.

Tonnes	Sn (%)	Zn (%)	Ag (g/t)	Tin Metal (tonnes)	Zinc Metal (tonnes)	Silver Metal (oz)
562,000	0.5	1.4	36.4	2,869	8,000	657,000

6.5 Grade Tonnage Curves

The block model contains estimated grades down to zero so that the lower cut can be optimised using specific mining costs relevant to the 12km distance between the Sweeny's resource and the nearest mill. All assays within the ore wire frames were used in the grade estimation.



6.6 Discussion and Recommendations

The resource estimation for the Sweenies deposit can only be considered Inferred due to the limited bulk density samples, irregular spaced drilling and lack of quality control data. From a geological and structural perspective the model appears robust with geophysical chargeability data supporting the modelled orientation.

To improve the standard of the resource estimate it is recommended that further exploration work includes quality control samples (standards and blanks plus sample duplicates), density sampling of at least 10% of core samples and preliminary metallurgical test work.

The Sweeny's resource has a number of positive attributes that bode well for its potential commercial development:

- Mineralisation starts at the surface and is open in all directions
- The bulk of the resource is shallow and is potentially amenable to open pit mining
- Potential to expand the resource and add additional resources from the adjacent Anomaly One deposit
- The deposit is located adjacent to a road and is within 12km of milling infrastructure

7 Appendices

7.1 Sample Statistics

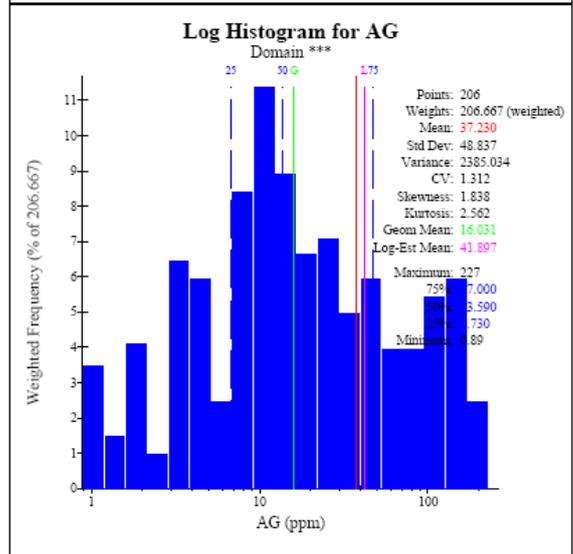
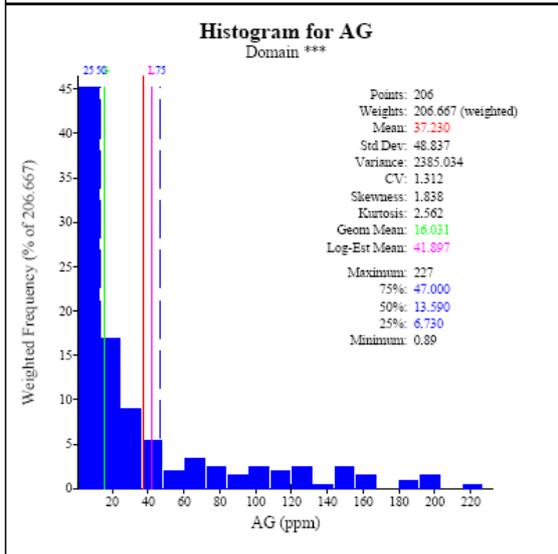
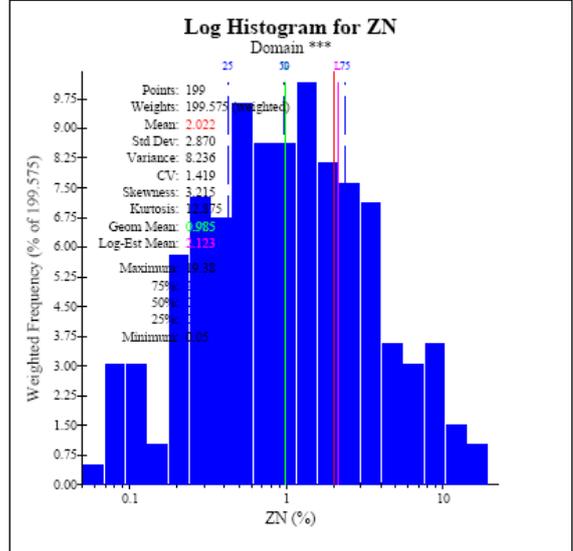
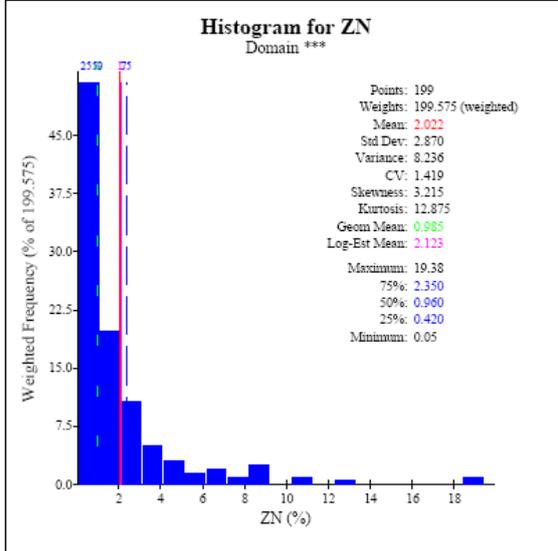
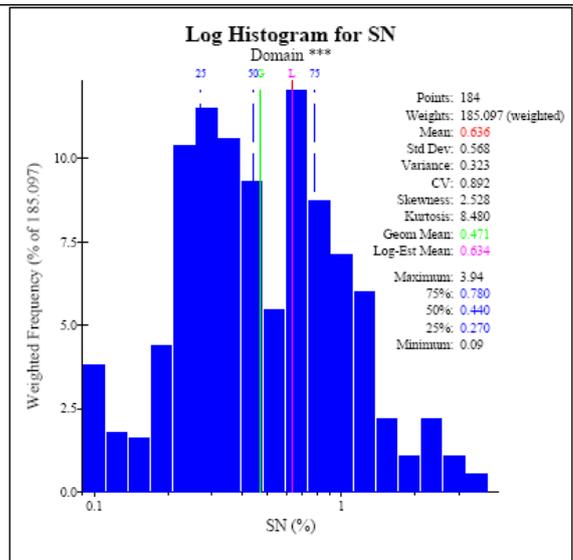
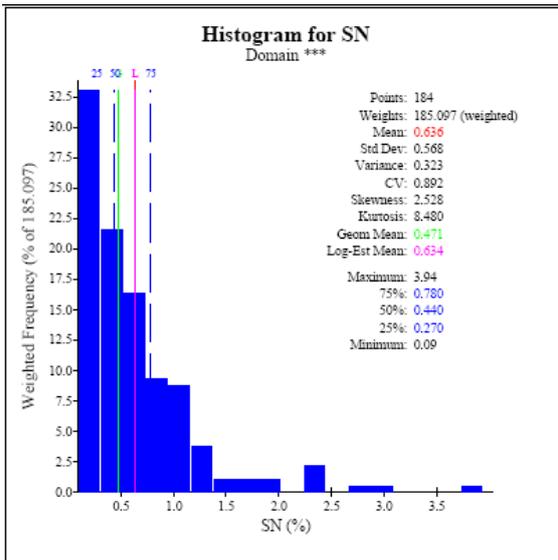
Statistic	Sn	Lode	Comments
Samples	227	184	
Minimum	0.01	0.09	
Maximum	3.94	3.94	
Mean	0.527846	0.63642	
Standard deviation	0.561313	0.5679	
CV	1.0634	0.892334	
Variance	0.315072	0.32251	(population estimate - based on N-1)
Skewness	2.50564	2.52834	(population estimate - based on N-1)
Log samples	227	184	(excludes non-positive sample values)
Log mean	-1.18805	-0.752539	
Log variance	1.3596	0.59274	
Geometric mean	0.304815	0.471169	
	10%	0.05	0.19
	20%	0.09	0.25
	30%	0.22	0.29
	40%	0.28	0.35
	50%	0.34	0.44
	60%	0.44	0.61
	70%	0.64	0.71
	80%	0.8	0.9
	90%	1.13	1.2
	95%	1.5	1.65
	97.50%	2.25	2.31
	99%	2.8	2.8

Statistic	Zn	Lode	Comments
Samples	227	199	
Minimum	0.01	0.05	
Maximum	19.38	19.38	
Mean	1.77982	2.02201	
Standard deviation	2.7686	2.86981	
CV	1.55555	1.41928	
Variance	7.66515	8.23582	(population estimate - based on N-1)
Skewness	3.36128	3.21504	(population estimate - based on N-1)
Log samples	227	199	(excludes non-positive sample values)
Log mean	-0.52354	-0.01543	
Log variance	3.27293	1.53635	
Geometric mean	0.592421	0.984691	
	10%	0.02	0.2
	20%	0.2	0.32
	30%	0.32	0.54
	40%	0.58	0.7
	50%	0.8	0.96

60%	1.12	1.4
70%	1.6	1.97
80%	2.53	2.94
90%	4.34	4.93
95%	7.9	8.1
97.50%	9	9.2
99%	12.53	12.53

Statistic	Ag	Lode	Comments
Samples	227	206	
Minimum	0.001	0.89	
Maximum	227	227	
Mean	33.8953	37.23	
Standard deviation	47.791	48.8368	
CV	1.40996	1.31176	
Variance	2283.98	2385.03	(population estimate - based on N-1)
Skewness	1.95198	1.83805	(population estimate - based on N-1)
Log samples	227	206	(excludes non-positive sample values)
Log mean	1.90725	2.77453	
Log variance	9.42745	1.92139	
Geometric mean	6.73454	16.0311	
10%	1	2.29	
20%	3	4.16	
30%	5.3	8.85	
40%	9.27	11	
50%	12.44	13.59	
60%	18	21	
70%	29	33	
80%	50	65	
90%	110	118	
95%	146	149	
97.50%	160	182	
99%	200	200	

7.2 Sample histograms and log probability plots



21 April 2008

ASX Code: SHE

Maiden Resource Estimate and Investor Update

Highlights

- **Initial Inferred Resource of 562,000t at 0.5% tin, 1.4% zinc and 36 g/t silver containing 2,869 tonne of tin, 8,000 tonnes of zinc and 657,000 ounces of silver.**
- **Mill Refurbishment and tin exploration progress**

Stonehenge Metals Limited is pleased to announce a maiden Inferred Resource estimate for the Sweeny's tin-zinc-silver deposit (Figure 1) in Tasmania based on compiled historical diamond drilling results. The Inferred Resources, using a 0.2% tin cut-off grade is summarised below:

Tonnes	Sn (%)	Zn (%)	Ag (g/t)	Tin Metal (tonnes)	Zinc Metal (tonnes)	Silver Metal (oz)
562,000	0.5	1.4	36.4	2,860	8,000	657,000

Note: The resource estimate was completed by Stonehenge Metals Limited in accordance with the 2004 Guidelines of the Australasian Joint Ore Reserves Committee (JORC) Code for reporting Mineral Resources and Ore Reserves (JORC, 2004)

The delineation of the Sweeny's resource is a significant accomplishment by Stonehenge as it moves toward tin production. The Sweeny's resource has a number of positive attributes that bode well for its potential commercial development:

- Mineralisation starts at the surface and is open in all directions
- The bulk of the resource is shallow and is potentially amenable to open pit mining
- Potential to expand the resource and add additional resources from the adjacent Anomaly One deposit
- The deposit is located adjacent to a road and is within 10km of milling infrastructure

The company has initiated a preliminary scoping study to assess the potential commercial development of the project. Further work will focus on bulk sampling to test the metallurgical characteristics of the mineralisation and exploration modelling to determine trenching and drilling locations. Exploration will also commence on Anomaly One with the objective of identifying additional resources to complement the Sweeny's resource.

Resource Estimation Methodology:

The resource estimate is based on 17 diamond drill holes designed to intersect the mineralisation on a nominal 50m by 50m spacing. The deposit was been modelled in three dimensions using cross sectional interpretations of the geology and mineralisation. The deposit boundary was defined by a 0.2% Tin (Sn) cut-off grade which coincides with the geological boundary of the shear zone. Individual blocks were defined around drill hole intersections with block boundaries on and between cross sections were defined by the midpoints between adjacent holes and by geological constraints. Estimation methodologies included inverse distance squared and ordinary kriging. Based on statistical analysis, maximum sample assays were reduced to 3% Tin, 10% zinc and 160gpt silver (top cuts) and all grades were length weighted. Block densities were assigned based on sampling from Sweeny's underground adit and surface pits.

Mill Refurbishment and tin exploration progress

Mill refurbishment is nearing completion with all major components now in position. The magnetic separator and rolls crusher have been refurbished and new ore feed hoppers have been completed. Remaining work includes installation of the electrical system to power the plant and finalisation on tailings and water supply piping.

Commissioning and tin production has been scheduled to commence in mid to late May and there is sufficient stockpiled ore to continue ore production for three months. The stockpiles consist of 6000-7000 tonnes of soft free milling oxide ore at a grade of around 1% tin. Production costs are estimated at \$43 per ore tonne

Negotiations with tin smelters to process the tin concentrate are continuing and will be announced in due course.

Tin exploration is currently focussing on Central Big H adjacent to the Mill where a series of trenches have been planned with follow up drilling where required. The deposit has a similar magnetic signature to the Granville East deposit and has previously been mined for alluvial tin. A drill hole on the Northern boundary of the lease intersected 1.25 metres of tin grading 0.45%.

Exploration at Granville East has been hampered by heavy water inflows into the pit limiting work to chip sampling. Bulk sampling and drilling have been rescheduled for later this year once the mill is operational.

Additional exploration is planned for the 50 hectare Heemskirk alluvial lease located one kilometre north of the Heemskirk mill. Previous sampling has identified up to 0.9kg of tin per cubic metre of alluvial gravel. The gravel wash is up to 20 metres deep and covers the majority of the lease. The company will carry out costeaning and sampling of the gravels during April and May to identify any contained alluvial tin mineralisation.

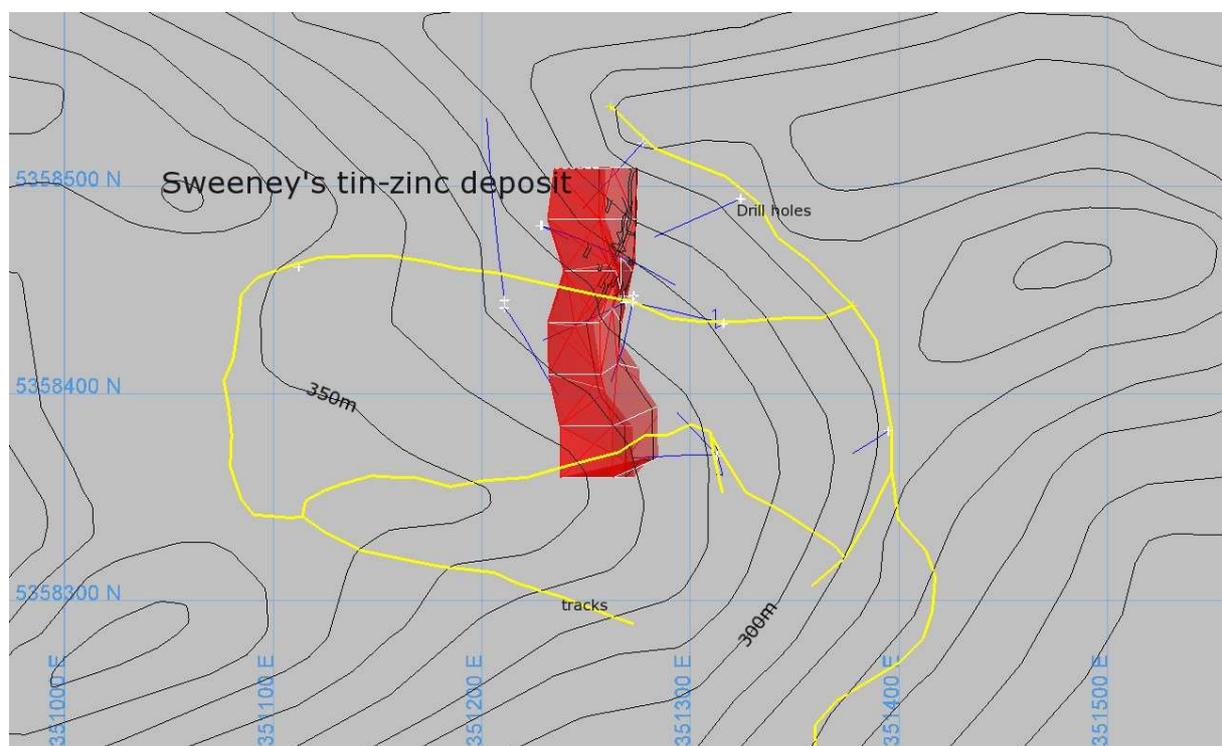


Figure 1. Three dimensional model of the Sweeney's tin-zinc-silver deposit with drill holes traces in blue and elevation contours in black.

About Stonehenge Metals Limited

Stonehenge Metals Limited is an exploration company formed in 2006 to explore a portfolio of highly prospective tin, nickel and zinc exploration projects in North West Tasmania. In late 2007 the company acquired the right to explore the Mandiodo nickel laterite deposit on the island of Sulawesi in Indonesia.

Mandiodo Nickel Project: Mandiodo is located in Southeast Sulawesi, Indonesia and consists of two permits totaling 31 square kilometres. Extensive historical drilling has identified a nickel laterite blanket covering an area of 4.2 km long by 1.0 km wide and up to 20 metres deep with significant potential for expansion. The average grade of the historical drilling is 1.3% nickel. Existing metallurgical work indicates that a proportion of the deposit is amenable to direct smelting hence the deposit may be exploited by simple mining and shipping. Stonehenge is currently finalising acquisition of the project.

Stonehenge Nickel Project: The Stonehenge exploration lease has the potential to host significant nickel deposits. The lease contains the same rock units and aeromagnetic anomalies that have produced Allegiance Mining NL's Avebury nickel mine on adjacent ground. The anomalies have not been tested by drilling and could be related to significant nickel mineralisation. The drilling of this magnetic anomaly will be a priority and the magnetic data covering this tenement will be reviewed to identify all magnetic targets.

Stonehenge Base Metals Project: In addition to nickel, the Stonehenge exploration lease has the potential to host significant lead-zinc-silver deposits. The lease contains the same rock units and structural corridors that have produced Zeehan Zinc's Comstock mine on adjacent ground. There are approximately 7km of strike length to explore on three trends each of which contain several historical mines. Preliminary channel sampling at Sunshine has identified 10m @ 22% zinc. The drilling of the Sunshine and Swansea deposits will be a priority and the historical data covering this tenement will be reviewed to identify all base metal targets.

Granville Tin Project: The Granville East tin deposit appears to be a strata-bound, carbonate replacement deposit (skarn). Sampling has established the presence of some very high grade zones of ore and recent mining has confirmed the open pit to be a potential source of ore of good grade and character. Early tin production from stockpiles, waste dumps, some pit ore and reprocessing of tailings is planned to proceed, in tandem, with the current resource drilling.

The Central Big 'H' tin prospect appears to be similar to Granville East's. Its magnetic anomaly size and strength (200nT) indicates that it may be a smaller, lower-grade (+1%) analogue of the Granville East tin skarn. Stonehenge Metals will conduct an initial, two to four hole, reconnaissance drilling program over the prospect to test this possibility.

Federation Tin Project: The Federation lease covers a number of tin bearing lodes in an area known as the South Heemskirk Tin field the country rock underlying this tenement is a part of the Heemskirk granite which is a multiphase intrusion with the tin mineralization being related to the latest phase. The major Tin prospects are Sweeny's, Federation and an untested magnetic anomaly West of Sweeny's.

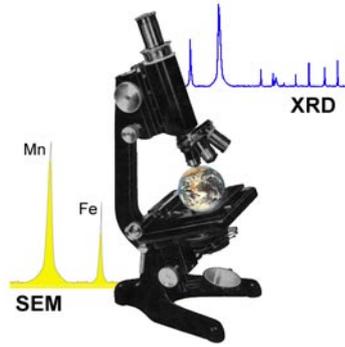
Interview River Tungsten Project: The Interview River Licence covers a number of tungsten bearing lodes in an area known as Interview River. The country rock underlying this tenement is a part of the Interview granite which is a multiphase intrusion with the tungsten and tin mineralization being related to the latest phase. Further east the tenement covers folded and faulted sediments with elevated copper results.

The Information in this report that relates to exploration results, mineral resources or ore reserves is based on information compiled by Mr Todd Hibberd, who is a member of the Australian Institute of Mining and Metallurgy. Mr Hibberd is a full time employee of the company. Mr Hibberd has sufficient experience which is relevant to the style of mineralisation and type of deposits under consideration and to the activity that he is undertaking to qualify as a Competent Person as defined in the 2004 edition of the 'Australian Code for Reporting Exploration Results, Mineral Resources and Ore Reserves (the JORC Code)'. Mr Hibberd consents to the inclusion of this information in the form and context in which it appears in this report.

For further information please contact:

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Managing Director
Stonehenge Metals Limited
Tel: +618 94812277 Fax: +618 94812355
Website: www.stonehengemetals.com.au

Appendix 4 – Petrology Report, sample from Sweeney's adit



Roger Townend and Associates Consulting Mineralogists

Unit 4, 40 Irvine drive, Malaga Western Australia 6062

Phone: (08) 9248 1674

email: rogertownend@westnet.com.au

Fax: (08) 9248 1502

MIKE COWIN

9-7-2008

STONEHENGE METALS LTD,

LEVEL 3

1292 HAY STREET,

WEST PERTH

WESTERN AUSTRALIA 6005

Our reference 22300

Preparation of one polished thin section of one rock and petrographic/mineragraphic description.

Roger Townend

Correspondence to Box 3129, Malaga D.C. WA 6945

ACN 069 920 476 ABN 92 076 109 663

SAMPLE 318555

ROCK SPECIMEN

POLISHED THIN SECTION

QUARTZ	MAJOR
SERICITE	MAJOR
MUSCOVITE	ACCESSORY
CHLORITE	ACCESSORY
CASSITERITE	TRACE
PYRITE	MAJOR
SPHALERITE	ACCESSORY
CHALCOPYRITE	ACCESSORY
GALENA	TRACE

CLASSIFIED AS A CASSITERITE SPHALERITE BEARING PYRITE SERICITE QUARTZ ROCK.

The rock is dominantly composed of quartz and secondary sericite plus pyrite. The major sericite often appears as 2 millimetre plus masses suggesting replacement of coarse feldspar, although none was preserved. There may be some yellow brown chlorite present within it. The associated quartz is variable in fabric with a distinct association with the coarse pyrite. Muscovite sensu stricto occurs as occasional rather ragged flakes mostly on the margins or intergrown with the pyrite.

The primary rock may therefore have been dominantly feldspar, such as plagioclase i.e. of dioritic nature.

The quartz flanking the coarse pyrite is similarly coarse and sometimes undulose suggestive of a vein nature.

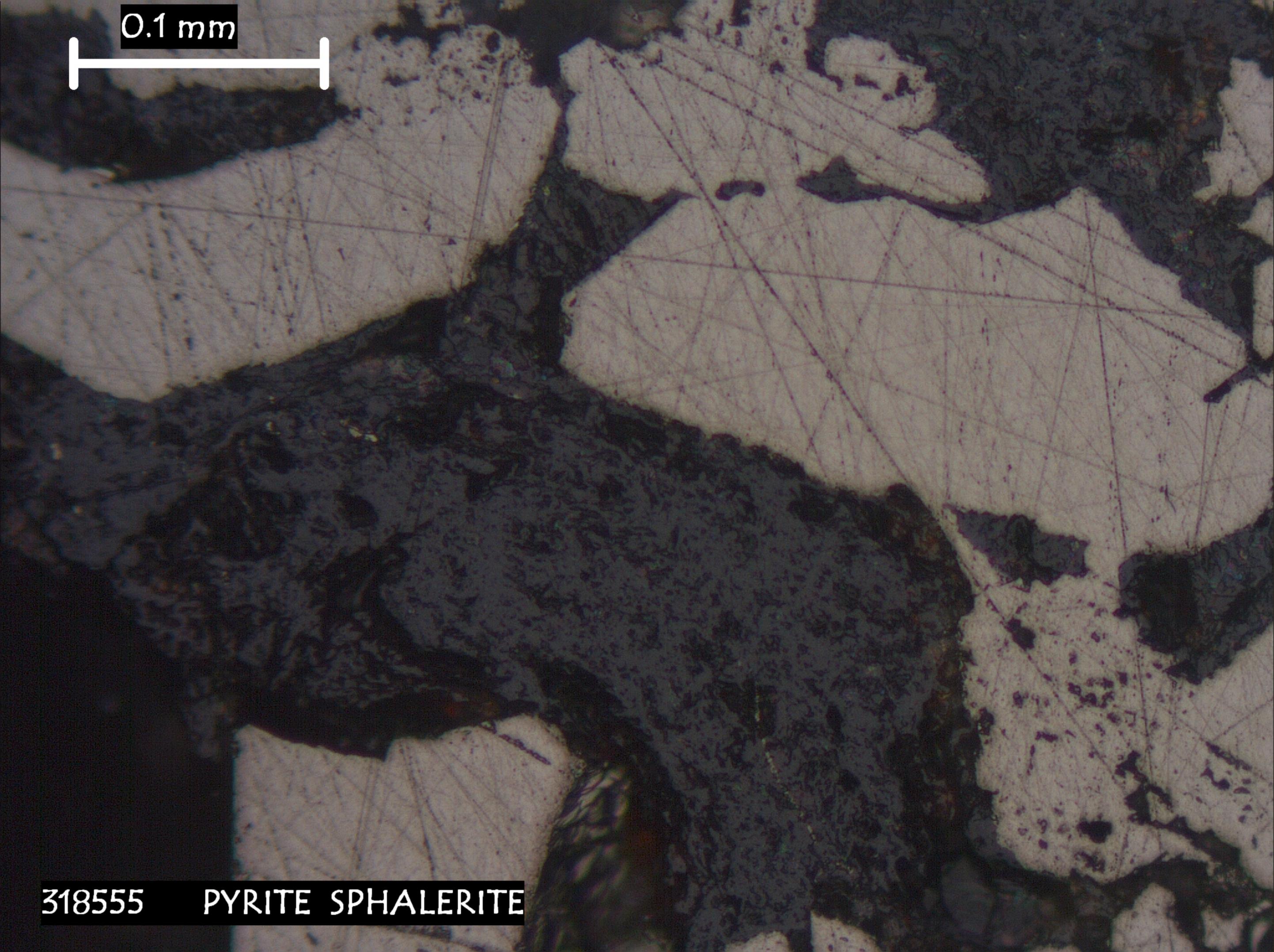
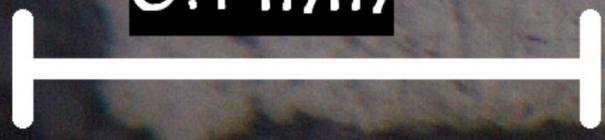
The rock contains a major content of pyrite. The pyrite occurs in several habits/generations. These are dominantly aggregates of euhedral crystals and later irregular often vein like pyrite, around the former and as veins in muscovite. This euhedral pyrite appears to be of later formation, associated with quartz and coarse muscovite.

Sphalerite always containing fine chalcopyrite and with a significant iron content, is usually associated with the pyrite as anhedral margins and also penetrating possibly replacing the pyrite.

Traces of galena were present as fine inclusions both in sphalerite and as short veins in pyrite.

Cassiterite was detected in several clusters, associated with or included in pyrite and rutile. The grainsize range was from less than 5 to 25 microns. See SEM images (cassiterite grey white, pyrite grey, silicates dark grey)

0.1 mm



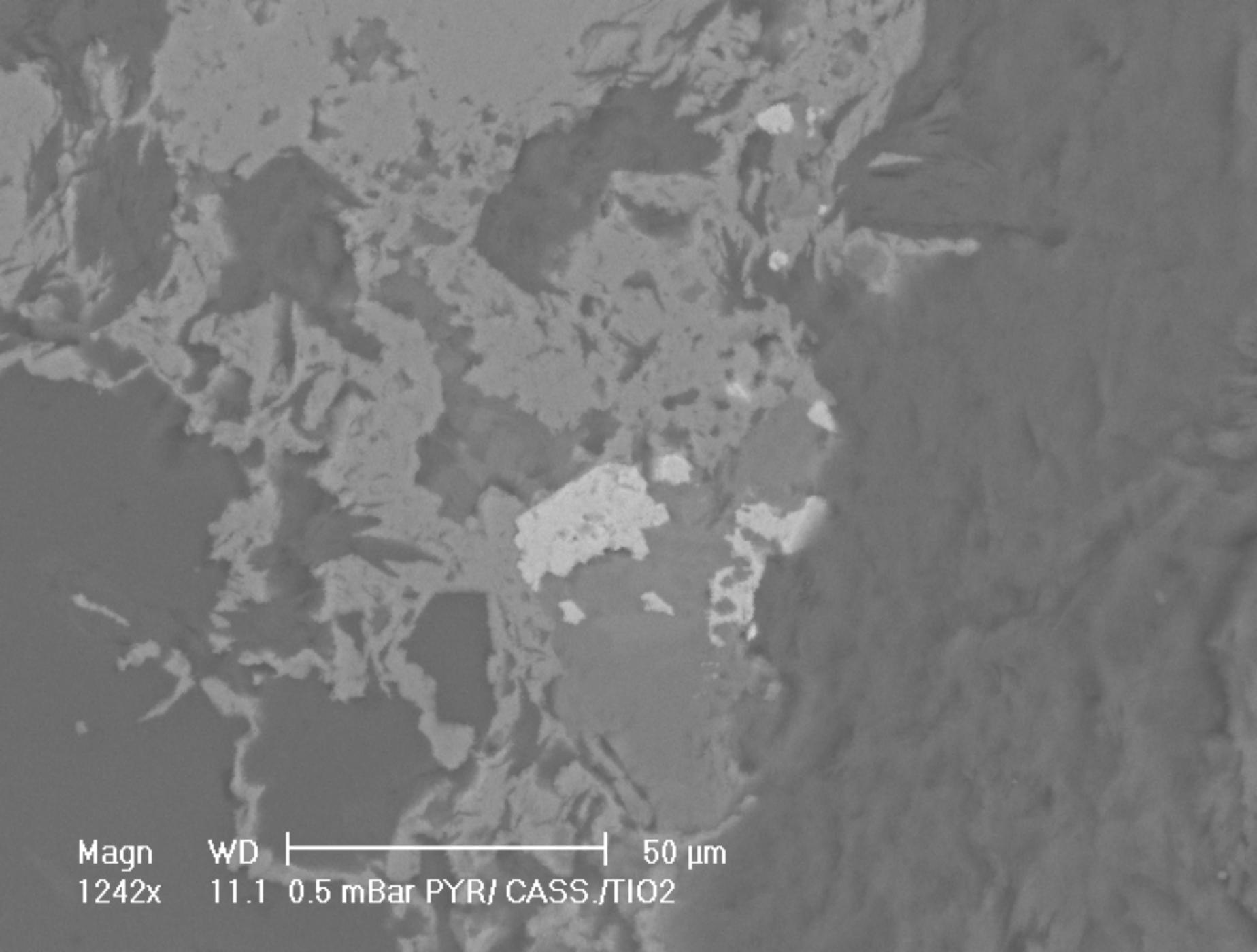
318555 PYRITE SPHALERITE

0.5 mm

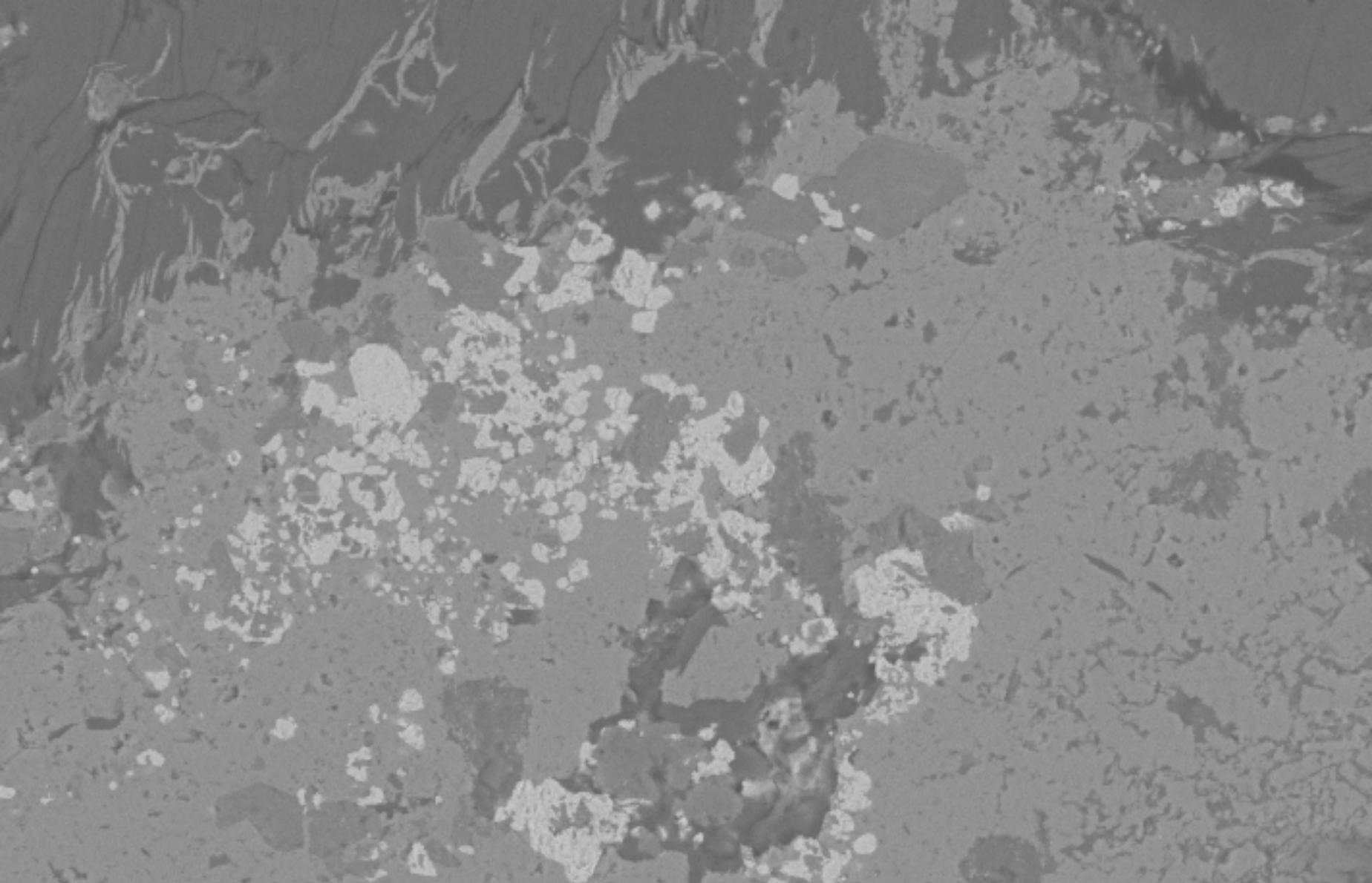
PYRITE IN QUARTZ

318555 SERICITE EX.? FELDSPAR,





Magn 1242x WD 11.1 0.5 mBar PYR/ CASS./TiO2 50 μm



Magn
621x

WD
11.1



100 μm

0.5 mBar PYR/ CASS./TiO₂/2