155001

Quest Exploration Pty Ltd

EL. 3/67 & 9/65.

67-484

SCOUT DRILLING OF THE EAST COAST AREA OF KING ISLAND

CONTENTS:

P. N. JOHNSTON

1967

See loose plan

ISG REFER REPORT 70-0676

1. INTRODUCTION

This report describes the scout exploration of an area covered under Tasmanian Exploration Licences No. 3/67 held by Quest Exploration Pty. Ltd. Agreement had been reached with Quest for W.T.N.L. to investigate this area.

The area of the exploration leases investigated comprises the coastal strip about 7 miles wide from the Sea Elephant River northwards to the N.E. coast, with a complex area in the southern half excepted (this belonging to Hawkes Alluvial). The approximate area of the leases is 65 square miles. The area can be roughly divided into three N - S strips, -

1) the modern coastal dunes 30 - 80 chains wide, -
2) a long permanent swamp 30 - 50 chains wide and, -
3) a roughly flat area stretching from the swamp to the western boundary of the area. This flat area has a vaguely defined ridge running parallel to the swamp and is broken by isolated sand ridges and hills. The general drainage is from the west into the swamp by numerous small creeks and the only outlet from the swamp is south into the Sea Elephant River. This swamp virtually isolates the coastal dune area, the only access being around the northern end.

Mount Counsel (Sea Elephant Hill) is the only prominent feature and consits of a weathered granite intrusion into highly micaceous schists. The area south of Mount Counsel is inaccessable except in very dry periods and appears to be the alluvial plain of the Sea Elephant River. This is further confirmed by the small alluvial tin workings in this area.

2. SUMMARY

From the results of the limited drilling carried out it does not appear that the area is of significant economic interest. The heavy mineral assemblage is so low in rutile and zircon that the area of deposit required to be of economic significance for a potential mine for these minerals would be very large, and it is unlikely to have been missed even with the scout drilling described. Based on the heavy assemblage, a deposit containing 6-10% heavy mineral is required, whereas the average of the holes drilled is in the region of 0.1%.

3. DRILLING

On instruction from the Western Titanium N.L. consulting geologist, Mr. Forman, investigation was centered on the ridges

running parallel to the swamp with lateral lines running E.W. from this line. No attention was to be payed to the recent dunes.

In June a line was cleared from a point S.S.E. of Penny's Lagoon on a magnetic bearing of 174° to a point due E of Mount Counsel. This line was pegged at 8 chain intervals and the relative heights of the pegs ascertained. A point on an E.W. ridge near the middle of the line was taken as the datum point "OO" and all drilling was done in relation to this point.

In June when the line was finished it was possible to drive down its full length; by the middle of July it was possible to traverse the line even with the Snocat without numerous detours. Unfortunately, an access track cleared from Mount Counsel to Reekara Road proved unusable due to flooding in the paddocks at the end of Reekara Road. The creek at the north end of the line was also impassable so that the only access was through the gate opposite 8ON. The gate was approximately 3½ miles from the nearest point on the line and it frequently took over an hour to get from the gate to the drilling site.

Drilling was started at the north end of the line in the third week in July and continued southward at 8 chain intervals, staying whenever possible, on the line. The ridges proved to be barren at the northern end and to be mostly wind blown sand. Between 8ON and the creek at 40S the underlying weathered mica schist was only 9 ft. down and this undoubtedly caused the heavy ti-tree growth. Some schist in fact outcrops at the creek. The area between 4ON and 8OS was generally barren sands with the appearance of being wind blown and in fact the relatively high E-W ridge at OO proved to have no "rock" core, but to be sand to over 50 feet. From 8OS to 144S the ground to the west of the line was heavily timbered and gave the appearance of having weathered mica schists near the surface. These were in fact found 12 chains west at 128S 1 foot below the surface. This area was too heavily timbered to enter with the Snocat. South of 144 was a swampy area with deep bog to the west and rising gradually from 200S onwards. From 200S to the end of the line weathered rock was found just under the surface.

Having reached the southern end of the line it was decided to put in lateral lines where ever this was possible. The most obvious place to start was in the area around 136S where some enrichment had been found. This was a difficult area with very heavy timber and swamp; some sort of pattern was drilled more or less outlining the enrichment (see separate note for this area).

No further lateral lines were possible until 00 was reached. Here lines were drilled as far east and west as possible. Some slight enrichment was found at 0034W and a small pattern laid out for drilling. The enrichment however, proved very small and to be only at about 17-25 feet. This enrichment is probably associated with the creek running through it. The sand in the ridges in this area all had the appearance of being wind blown. It was now decided that every effort should be made to drill a lateral line as far west as possible and 104N was chosen, as the ground to the west was only timbered in patches. It was hoped that the N-S track could be reached to give access from both ends. Eventually after reaching 112N 128W there was so much standing water that it was impossible to drilland we came out south to the track leading into 80N. We then drilled along this track and up the N.S. track to Scots Road.

a) Drilling Methods

A standard gemco drill was used with 3" x 6' solid auger rods and rock bit. There being surface water over much of the area and a very high water table it was obvious that if any samples were to be taken, drilling had to be done below the water table. Although no gemco technique gives particularly accurate results, the corkscrew method was adopted as the only way to get samples under water. This method was then used for all holes to avoid different types of errors. On the whole, good recoveries were obtained and whenever possible 12' or 18' of rod was pulled at a time to avoid too much distrubance of the saturated sands. In certain places no samples could be collected at depth. This applied particularly on the line running north from 80N 168W where there was clay and dry sand over very wet sands. In general the quality of the sample dropped off with depth except where peaty material was encountered.

In the conditions encountered on King Island it is not considered that the errors inherent in the Gemco augering techniques were serious. It is extremely unlikely that the sample was ever contaminated by as much as 50% and if seriously contaminated, then seldom by more than 25%. No-where does it appear that barren sand occurred under enrichment so that all errors will have tended to lower the apparent grade. Considering then that our error produced an apparent grade 25% below the true grade the effect would be to lower 5% material to 3.8%, and 1% material to 0.8% and 0.5% to 0.4%. This would only be serious in borderline areas. With an average rutile content of 6% in the heavy mineral and a cut off of 0.5% rutile, the economic level might be an apparent grade of 7% instead of 8.3%. In only two holes was the apparent grade anywhere near this level.

b) Sampling & Testing

Samples were collected at 6' intervals but in most cases the top foot of each hole was rejected as the root matter caused blockages in the table feed system. The samples were sorted and when they were too small for tabling bulked proportionally with the next sample from the same hole. Spear samples were then taken for moisture calculation. The sample was then weighed and tabled, the middlings being retabled. The concentrate was then dried and weighed. The dry weight of the sample was calculated from the result of the moisture determination and the weight of the concentrate calculated as a percentage of the dry weight of the sample. A home made oven heated by bottled gas was used for drying and although the running temperature was only about 180°F this was quite adequate for clean sands. Occasional samples with high clay content had to be puddled before tabling.

Checks on the tailings for heavy mineral showed a maximum loss of about 0.04%. The sample as received was weighed to the nearest 10 gms. and the concentrate to ± 2 gms. With a sample weighing 8 kilos and a concentrate weighing 500 gms., this would give a maximum error of about ± 0.03%. The heavy mineral was determined using bromoform and weighed with a maximum error of ± 0.02 gms. This gave, with a head sample of 25 gms. and a heavy mineral of 1.2 gms. (i.e. 5% H.M. in the concentrate), an error of 0.1% i.e. if the concentrate was 10% of the total sample, an error of 0.01%. If the heavy mineral were 50.0% of the concentrate the error was 0.08% or 0.008% of the total sample.

4. DRILLING RESULTS

a) General (See Appendix A "Drilling Plan", and Appendix B "Drilling Results".)

Only one area of enrichment was found during drilling and this was small (see below). Unfortunately the pattern of drilling was very much dictated by the nature of the country and the large areas of standing water. The scant drilling pattern makes it impossible to draw up any detailed geological conclusions; only one obvious shore line was discovered over a small area. However, certain general assumptions can be made.

Two rock areas were found, the obvious outcrop at Mount Counsel, which strectches northwards for at least a mile and another small less obvious area between 40N and 80N. There is also some evidence of rock about 180 chains west of 80N. The only other surface rock in the area is a quartz quarry about 1 mile north of the bridge over the drain on Scots Road. The sand hills

and ridges all have the appearance of being wind blown. Over most of the area a layer of "peat", more correctly fine organic matter and staining, was found near the bottom of the sand. In one or two places fairly angular pubbles were found, suggesting old stream beds. The line of holes drilled northwards at 187W had a layer of hard slity clay about 3 ft. thick near the surface.

The general impression is that most of the area is an old swamp lying on the schists and shales and filled in by wind blown sands and some detrital material. The "bottom" seems to be rising generally westwards and there is some suggestion that the old shore lines may have run more N W from Mount Counsel, but there is very little real evidence to support this.

Although the drilling done has been very limited, it does not appear that the area is of significant economic interest. The mineral assemblages are disappointing (see separate report), and the area of deposit require with these low grade rutile concentrates would be so large that it is unlikely that an area of this size has been missed. The average heavy mineral content for all the holes drilled is in the region of 0.1%. If there were a large deposit of the necessary 6-10% heavy mineral concentration, then the average grade of the sand could be expected to be higher.

a) Area of Enrichment

The only area with any significant enrichment that was found lies between 122S and 152S. This is on the eastern edge of an area of heavy timber. The presence of heavy timber often dignified the presence of weathered shale and schist near the surface. The only place where it was possible to drill west of the line in fact revealed clay one foot below the surface at 11 chains west of 128S.

The weathered shales also approach the surface to the south being only 5 ft. deep at 168S and there is no sand cover from there to Mount Counsel.

Even in this area only one hole showed a H.M. value over 5.0%. The area showing heavy mineral values over 1% is very small and not well defined but at the best might be 8 chains wide by 40 chains long with an average depth of 25 ft. The only holes with heavy mineral content over 1% are listed below together with the percentage of rutile and zircon and the depth in each case.

Location	% H.M.	% Rutile	% Zircon	Depth
112S	1.3	0.08	0.12	23'
120S	1.0	0.06	0.11	23'
128S 4W	2.3	0.25	0.38	8'
128S	3.8	0.16	0.38	29'
136S 2E	11.1	0.46	1.07	25'
144S	5.1	0.32	0.73	11'
144S 4E	1.2	0.08	0.12	19'
168S 3W	1.2	*0.08	*0.12	5'

* No heavy mineral assemblage done. Figures are based on average of other results.

The variation between holes relatively close together makes it impossible to calculate with reasonable accuracy the heavy mineral content of the area. The area of enrichment may be larger than that found by drilling but the mineral assemblage and very difficult terrain made further drilling appear unnecessary.

c) Mineralogy

Fifteen separate samples were made up for analysis of their heavy mineral contents. These fall into three geographical groups; (i) sample S6 from the recent dunes near Boulder Point (ii) composite samples from holes 152N 0-4-6E and 160N 0-2-4-6E and (iii) composits of 12 holes between 112S and 144S.

Approx. Percentage (By Weight)

Location	Zircon	Rutile	Ilmenite	Leucoxene	Garnet	Trash
S6	14	5	14	2	13	52
152N	10	4	35	10	6	35
160N	11	4	36	6	5	38
112S	9	6	13	2	40	30
120S	11	6	12	1	15	55
128S	10	4	8	1	22	55
128S 4W	16	11	12	6	6	49
128S 2E	7	5	8	2	14	64
136S 2E	10	4	6	0	44	36
136S 12E	11	3	7	3	13	63
136S 24E	18	11	22	7	18	24
136S 28E	19	12	36	10	11	12
144S	14	6	14	1	12	53
144S 4E	10	6	8	3	27	46
144S 20E	17	7	28	3	18	27
Average	12	6	17	4	18	43

Very little significant difference can be found between the groups, there being too few samples in groups (i) and (ii). However, group two does seem to have a high ilmenite content.

The trash mineral content (tourmaline, hypersthene) is very high and there is very little intermediate material between ilmenite and leucoxene. These two features possibly indicate that the heavy mineral "concentration" has not been subjected to much weathering or wave action and has perhaps been derived direct from a crystaline source and not by the reworking of a heavy mineral bearing sediment.

The average Rutile and Zircon contents of the heavy mineral assemblage is 6% and 12% respectively. With this low rutile and zircon content the possibility of finding economic deposits is much reduced.

Much of the zircon and rutile was minus 100 mesh B.S.S. in size.

Attention is drawn to the similarity between these assemblages and those found by Billingshurst (1) in his previous work on King Island material.

Ref:

(1) Billingshurst W.M. "Investigation of Beach Sands from East Coast, King Island. 11.4.67."

APPENDIX "A"

DRILLING PLAN

LAKE MARTHA LAVINIA

PENNYS LAGOON

LAVINIA POINT

Drain

Scott Rd

Track

Patches Heavy Scrub
Light scrub
& open swamp

80%
Under Water
8/67

Track

112N
187W

Approx

128W

Open Swamp

Heavy timber patches

Scrub & Swamp

80N
168W

GATE

Track

Track

224N

Drain

200N

SWAMP
Draining South

Swampy scrub

160N

120N

SWAMP

Ridge

80N

Tree Patch

Rock at surface

Coastal Sand Plains

40N

Permanent Swamp
Draining South

Creek

Gum Tree Patch

00

Bearing 246° mag

40S

Creek

Gum Tree Patch

HEAVY TIMBER

80S

Permanent Swamp
Draining South

120S

Clay 1'

HEAVY TIMBER

160S

Swamp

200S

Ridge
Weathered rock close to surface
Ridge

240S

line bears 174-354 mag.

284

Rock 1'

44 40 36 32 28W

04N
00
04S

112S
120S
128S
136S
144S
152S

4 8 12 16 20 24 28 32 36 40E

MT COUNSEL TRIG (Sea Elephant Hill)

king Island

drilling plan

1967

Western Titanium NL

10 chains
20
30
40
50
60
70
80

20 chains to 1. inch

5 cm

N (mag)

To accompany report by P.N. JOHNSTON 1967
as APPENDIX "A"

67-484

155010

013

APPENDIX "B"

DRILLING RESULTS

010

155012

LAB. NO.	LOCATION	DEPTH	% H.M.	COMPOSITE
015	220N	0-15	0.03	
016		15-25	0.04	.2
017	216N	0-10	0.05	
018		10-18	0.09	.2
019	208N	0-10	0.09	
020		10-18	0.24	0.2
021	199N	0- 8	0.17	
022		8-18	0.29	
023		18-23	0.29	0.25
024	192N	0- 6	0.17	
025		8-17	0.17	0.2
026	184N	0- 5	0.08	
027		6-17	0.05	< 0.1
028	176N	0-11	0.02	
029		11-23	0.16	0.1
030	152N 4E	0-16	0.05	
031		16-29	0.12	0.1
032	152N 6E	0-17	0.03	
033		17-26	0.18	0.1
034	160N 6E	0-10	0.04	
035		10-18	0.06	< 0.1
036	160N 4E	0-16	0.04	
037		16-22	0.19	< 0.1
038	160N 2E	0-10	0.07	
039		10-28	0.18	< 0.1
040	160N	0-11	0.22	
041		11-25	0.22	0.2
042	168N	0-10	0.06	
043		10-22	0.15	< 0.1
044	152N	0-17	0.06	
045		17-34	0.15	0.1
046	144N	0-17	0.07	
047		17-29	0.25	0.1
048	144N 4E	0-17	0.05	
049		17-29	0.11	
050		29-41	0.20	0.1
051	144N 8E	1-17	0.22	
052		17-22	0.09	0.2
053	136N 6E	1-17	0.03	
054		17-29	0.12	
055		29-41	0.22	0.1
056	128N 9E	1-17	0.09	
057		17-29	0.1	< 0.1
058	120N 10E	1-17	0.05	
059		17-23	0.07	
060		23-35	0.07	< 0.1
061	112N 8E	1-17	0.03	
062		17-23	0.09	
063		23-35	0.15	< 0.1
064	112N 12E	1-23	0.07	
065		23-35	0.12	< 0.1

.....2

011

155013

LAB. NO.	LOCATION	DEPTH	% H.M.	COMPOSITE
066	104N 4E	1-11	0.04	
067		11-23	0.12	< 0.1
068	96N 6E	1-11	0.04	
069		11-23	0.17	.1
070	88N	1-11	0.13	
071		11-14	0.4	0.19
072	80N	1-11	0.14	0.14
073	72N	1- 9	0.1	0.1
074	64N	1- 9	0.33	0.33
075	56N	1- 9	0.21	0.21
076	46N	1-17	0.21	0.21
077	40N	1-11	0.09	
078		11-17	0.24	0.18
079	32N	1-11	0.03	
080		11-17	0.17	< 0.1
081	24N 8E	1-11	0.04	
082		11-23	0.05	
083	24N 8E	23-35	0.10	< 0.1
084	16N 8E	1-11	0.05	
085		11-23	0.03	
086		23-29	0.04	< 0.1
087		29-41	0.06	
088	08N 8E	1-11	0.03	
089		11-23	0.03	
090		23-35	0.03	< 0.1
091	00N	1-11	0.08	
092		11-23	0.09	
093		23-29	0.05	
094		29-41	0.08	< 0.1
095	8S	1-11	0.02	
096		11-23	0.02	
097		23-35	0.02	< 0.1
098	16S	1-11	0.05	
099		11-17	0.15	
100		17-29	0.09	< 0.1
101	24S	1-11	0.16	
102		11-23	0.10	0.13
103	32S 10E	1-11	0.06	
104		11-23	0.07	< 0.1
105	40S 3E	1-11	0.18	
106		11-17	0.70	0.36
107	48S 2E	1-11	0.12	
108		11-17	0.46	
109		17-23	0.73	0.37
110		23-29	0.36	
111	56S	1- 2	0.16	
112		2-11	0.36	0.23
113	64S 3E	1-11	0.19	
114		11-17	0.12	
115		17-23	0.04	0.13
116	72S 3E	1-11	0.13	
117		11-17	0.38	0.21
118	80S 2E	1-11	0.17	
119		11-17	0.27	
120		17-29	0.49	0.34

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012

155014

LAB. NO.	LOCATION	DEPTH	% H.M.	COMPOSITE
121	88S 2E	1-11	0.39	
122		11-17	0.58	
123		17-23	0.32	0.41
124	96S	1-11	0.43	0.4
125	104S	1-11	0.38	0.4
126	112S	1-11	1.08	
127		11-17	1.82	1.34
128	120S	1-11	1.40	
129		11-17	0.99	
130		17-23	0.45	1.0
131	128S	1-11	2.05	
132		11-17	7.75	
133		17-23	3.94	3.85
134	136S 2E	1-11	15.5	
135		11-17	8.0	
136		12-23	7.6	11.1
137	144S	1- 6	5.5	5.5
138	152S	1- 5	0.1	
139		5-19	0.05	< 0.1
140	160S 2W	1- 5	0.87	
141		5-14	0.81	< 0.1
142	168S 3W	1- 5	1.25	
143	8S	0- 3	0.2	0.2
144	7S	0-10	0.3	0.3
145	6S	0-10	0.7	0.7
146	128S 2E	1-11	0.58	
147		11-17	1.1	
148		17-23	1.3	0.85
149	176S 2W	0- 3	0.14	0.14
150	192S	0- 5	0.21	
151		5-11	0.23	0.2
152	200S	3-10	0.4	0.4
153	216S	1- 3	0.02	< 0.1
154	5S	0-10	0.31	0.3
155	128S 6E	1-17		
156	128S 6E	17-27	0.09	
157	128S 10E	0-17		
158		17-34	0.16	
159	136S 4E	1- 5	0.13	
160		5-11		
161		11-20	0.63	
162	136S 8E	1-17	0.09	
163		17-25	0.08	< 0.1
164	136S 16E	1-17	0.26	
165		17-28	0.59	0.39
166	136S 20E	1-17	0.38	
167		17-28	0.42	0.40
168	136S 24E	1-11	0.67	
169		11-22	0.61	0.64
170	136S 28E	1-11	0.61	
171		11-23	1.16	0.88

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LAB. NO.	LOCATION	DEPTH	% H.M.	COMPOSITE
172	136S 12E	1-11	0.76	
173		11-17	1.74	
174		17-27	1.07	1.10
175	120S 4E	1-11	0.45	
176		11-17	0.08	
177		17-25	0.12	0.25
178	120S 8E	1-11	0.33	
179		17-28	0.21	0.27
180	120S 12E	1-11	0.30	
181		11-17	0.31	0.3
182	120S 16E	1-11	0.40	
183		11-17	0.43	
184	120S 16E	17-24	0.96	0.58
185			0.34	
186	120S 20E	1-11	0.24	
187		11-17	0.16	
188		17-29	0.17	0.19
189	120S 4W	1- 8	2.31	2.31
190	120S 8W	1-12	0.05	0.05
191	120S 24E	1-11	0.26	
192		11-17	0.46	
193		17-29	0.37	
194		29-37	0.26	0.33
195	120S 28E	1-11	0.31	
196		11-17	0.23	
197		17-23	0.19	0.26
198	120S 32E	1-11	0.38	
199		11-17	0.41	
200		17-23	0.42	
201		23-29	0.42	0.40
202	120S 36E	1-11	0.42	
203		11-27	0.72	0.60
204	120S 40E	1-11	0.59	
205		11-17	0.33	
206		17-23	0.27	
207		23-32	0.36	0.41
208	136S	1-11	0.20	
209		11-22	0.89	0.56
210	144S 4E	1-11	0.49	
211		11-19	2.04	1.18
212	144S 8E	1-11	0.10	
213		11-17	0.21	
214		17-26	0.13	0.15
215	144S 12E	1-11	0.16	
216		11-17	0.23	
217		17-30	0.19	0.19
218	144S 16E	1-11	0.46	
219		11-17	0.55	
220		17-23	0.49	0.52
221	144S 20E	1-11	0.47	
222		11-17	0.63	
223		17-28	0.39	0.47
224	80S	1-11	0.53	0.53
225	80S 12E	1- 7	0.13	0.13

LAB. NO.	LOCATION	DEPTH	% H. M.	COMPOSITE
226	80S 8E	1-11	0.20	
227		11-17	0.41	
228		17-25	0.28	0.28
229	80S 4E	1-11	0.24	
230		11-22	0.49	0.37
231	004E/2	0-10	0.25	
232		10-15	0.07	< 0.19
233	004E	1-11	0.13	
234		11-17	0.11	
235		17-23	0.05	
236		23-29	0.04	
237		29-35	0.06	
238		35-41	0.07	< 0.1
239	008E	1-11	0.07	
240		11-17	0.07	
241		17-23	0.05	
242		23-35	0.08	< 0.1
243	0012E	1-11	0.09	
244		11-17	0.02	
245		17-23	0.03	
246		23-29	0.05	< 0.1
247	0016E	1-11	0.10	
248		11-17	0.06	
249		17-23	0.10	< 0.1
250		23-29	0.10	
251		29-41	0.09	0.1
252	00 20E	1-11	0.12	
253		11-23	0.13	
254		23-35	0.1	0.11
255	00 24E	1-11	0.06	
256		11-17	0.05	
257		17-29	0.35	
258		29-35	0.23	
259		35-46	0.24	0.20
260	00 8W	1-11	0.17	
261		11-17	0.20	
262		17-29	0.11	
263		29-35	0.17	0.15
264	00 12W	1-17	0.35	
265		17-29	0.11	
266		29-41	0.22	
267		41-47	0.16	0.23
268	00 16W	1-11	0.13	
269		11-23	0.26	
270		23-35	0.11	
271		35-53	0.21	0.18
272	00 20W	1-11	0.29	
273		11-17	0.20	
274		17-29	0.20	
275		29-41	0.24	
276		41-50	0.28	0.25
277	00 4W	1-11	0.26	0.26
278	00 24W	1-11	0.24	
279		11-17	0.21	
280		17-29	0.29	
281		29-41	0.82	
282		41-54	0.67	0.48

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LAB. NO.	LOCATION	DEPTH	% H.M.	COMPOSITE
283	00 28W	1-11	0.24	
284		11-23	0.28	
285		23-35	0.95	0.51
286	00 32W	1-11	0.29	
287		11-17	0.12	
288		17-25	1.50	0.65
289	00 40W	1-14	0.11	0.11
290	00 44W	1-13	0.52	0.52
291	104N 8W	1-13	0.13	0.13
292	104N 12W	1-11	0.09	
293		11-22	0.11	0.10
294	104N 16W	1-11	0.07	
295		11-24	0.12	0.1
296	104N 20W	1-11	0.05	
297		11-23	0.08	
298		23-34	0.12	0.1
299	104N 24W	1-11	0.05	
300		11-23	0.15	
301		23-35	0.09	0.1
302	104N 28W	1-11	0.12	
303		11-23	0.09	
304		23-27	0.19	0.14
305	104N 32W	1-17	0.13	
306		17-29	0.09	0.11
307	104N 36W	1-11	0.13	
308		11-17	1.05	
309		17-30	0.36	0.41
310	104N 40W	1-11	0.05	
311		11-25	0.06	0.1
312	112N 40W	1-11	0.08	
313		11-21	0.08	0.1
314	112N 44W	1-11	0.07	
315		11-23	0.14	0.11
316	112N 48W	1-17	0.07	
317		17-23	0.11	0.1
318	112N 52W	1-17	0.04	
319		17-30	0.15	0.1
320	112N 56W	1-17	0.04	
321		17-30	0.04	0.1
322	112N 60W	1-11	0.07	
323		11-21	0.22	0.14
324	112N 64W	1-11	0.06	
325		11-20	0.17	0.11
326	112N 68W	1- 7	0.10	0.1
327	80N 4E	1-15	0.08	0.1
328	80N 8E	1-11	0.03	
329		11-22	0.25	0.14
330	80N 12E	1-11	0.04	
331		11-17	0.06	
332		17-21	0.16	0.1
333	04S 28W	1-11	0.05	
334		11-17	0.09	
335		17-23	0.29	
336		23-29	0.13	
337		29-35	0.11	
338		35-40	0.20	0.13

LAB. NO.	LOCATION	DEPTH	% H.M.	COMPOSITE
339	04S 30W	1-11	0.20	
340		11-17	0.17	
341		17-23	0.15	
342		23-30	1.84	0.5
343	04S 32W	1-11	0.50	
344		11-17	0.11	
345		17-25	0.09	
346		23-29	0.79	0.3
347	04S 36W	1-11	0.24	
348		11-17	0.07	
349		17-23	0.11	0.2
350	04N 28W	1-11	0.14	
351		11-17	0.15	
352		17-23	0.29	
353		23-30	0.55	0.3
354	04N 26W	1-11	0.10	
355		11-17	0.09	
356		17-23	0.14	
357		23-26	1.4	0.1
358	04N 30W	1-11	0.14	
359		11-17		
360		17-26		
361		23-34	0.40	0.2
362	04N 32W	0-11	0.24	
363		11-17	0.24	
364		17-26	0.34	0.2
365	04N 36W	1-17	0.10	0.1
366	04N 38W	1-11	0.05	0.1
367	04N 38W	11-18	0.08	
368	04N 40W	1-16	0.07	0.1
369	122N 88W	1-11	0.38	
370		11-17	0.25	
371		17-25	0.20	0.3
372	120N 96W	1-11	0.30	
373		11-22	0.13	0.2
374	120N 104W	1- 5	0.32	
375		5-17	0.25	
376		17-23	0.49	0.3
377	120N 112W	1-11	0.46	
378		11-18	0.36	0.4
379	112N 98W	1-11	0.15	
380		11-15	0.24	0.2
381	112N 104	1-11	0.16	
382		11-17	0.25	
383	112N 112W	0-10	0.53	
384		10-18	0.32	
385	112N 120W	11-19	0.21	0.4
386	80N 128W	1- 8	0.19	0.2
387	80N 136W	1-11	0.11	
388		11-17	0.23	0.2
389	80N 144W	1-11	0.14	
390		11-18	0.23	0.2
391	80N 152W	1-11	0.13	
392		11-17	0.41	
393		17-25	0.23	0.2

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LAB. NO.	LOCATION	DEPTH	% H.M.	COMPOSITE
394	80N 160W	1-11	0.08	
395		11-25	0.08	0.1
396	80N 168W	1-11	0.12	
397		11-23	0.13	0.1
398	88N 173W	1-11	0.15	
399		11-23	0.10	0.1
400	96N 178W	1-11	0.18	
401		11-23	0.10	0.1
402	112N 178W	1-11	0.12	
403		11-23	0.12	0.1
404	120N 178W	1-11	0.12	
405		11-23	0.08	0.1
406	128N 178W	1-11	0.12	
407		11-25	0.31	0.2
408	136N 178W	1-11	0.11	
409		11-17	0.19	0.1
410	144N 178W	1-11	0.12	0.1
411	152N 178W	1-11	0.24	
412		11-17	0.28	0.3
413	160N 178W	1-11	-	
414		11-23	0.27	0.1
415	168N 178W	1-11	-	
416		11-18	0.17	0.1
417	176N 178W	1-10	0.14	0.1
418	184N 178W	1- 9	0.12	0.1
419	192N 178W	1-11	0.67	0.7
420		11-20	0.07	0.1
421	200N 187W	1-11	0.06	
422		11-22	0.09	0.1
423	208N 187W	1-14	0.10	0.1
424	216N 187W	1- 8	-	0.1
425	224N 187W	1-11	0.09	0.1
426	232N 187W	1-15	0.16	0.2
427	240N 187W	1-11	-	0.1
428		11-20	0.10	0.1
429	248N 187W	1-12	-	0.1
430	256N 187W	1- 8	-	0.1