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GEOPEKO LIMITED

KING ISLAND GROUP

REPORT ON ORE RESOURCE OF THE No. 1 OREBODY - KING ISLAND

AUGUST, 1969

By

P. Le Messurier and N. Kinnane

KING ISLAND

SEPTEMBER, 1969.

001

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1. SUMMARY

The ore resource of the No. 1 Orebody, King Island, has been re-calculated as at 26th August, 1969. This calculation has been of an area bounded by the No. 10 Fault on Line 15 + 80 in the West and the No. 3 Fault on Line 00 in the East and extending to a depth of 230 feet below sea level.

The calculation is based on a minimum mining cut off of 0.25% WO_3.

The results of this calculation are summarised below.

	TONNAGE	MEAN GRADE % WO_3	LOWER 90% CONFIDENCE GRADE % WO_3
B LENS	256,200	0.593	0.522
C LENS (Wedge Block)	785,500	0.550	0.528
C LENS (Main Open Cut)	2,913,100	0.622	0.609
TOTAL	3,954,800	0.606	

N. Kinnane,
GEOLOGIST.

P. Le Messurier,
SUPERVISING GEOLOGIST.

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2. INTRODUCTION

The ore resource of the No. 1 Orebody has been completely re-calculated for this report. New cross sections and floor plans have been prepared from basic drilling data.

The floor plans prepared have been for absolute levels as stated and not for the corresponding mining level which are in fact at varying elevations.

Calculations have been made from the cross sections with some checking from the plans.

Reserves are presented separately for B Lens, C Lens in the main body of the Open Cut and C Lens in a faulted area high on the footwall known as the "Wedge Block".

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3. METHOD OF CALCULATION

Grade Calculation

The following methods were used in the calculation of the grade:-

1. The minimum grade cut off applied was 0.25% WO_3. All sections of assay less than 0.25% WO_3 were excluded from the calculation except where lower grade portions formed part of the normal population within areas of above cut off grade.

2. All data was treated on an assay foot basis.

3. Grades were calculated on a section by section basis, with grades for each Lens or distinct portion of the orebody being calculated separately.

4. An area of influence was determined at half the distance between adjacent sections, and at 50 feet in the vertical plane above and below the limits of the calculation.

5. The upper limit for calculation was present pit or ground surface, the lower limit was a level of 230 feet below sea level.

6. Data was initially grouped in natural arithmetic increments of 0.05% WO_3. Histograms were drawn of this grouped data, section by section and for the total orebody in each Lens. These histograms indicate that the distribution closely approximates to the log normal type.

7. The data was regrouped on a lognormal basis and the grades calculated in accordance with the methods of Sichel. A mean grade was calculated and the lower 90% confidence limit determined.

Tonnage Calculation

1. Tonnages were calculated on a section by section basis.

2. The area of influence for each section was taken as half the distance between adjacent section. On the Western and Eastern extremities of the area the terminating fault was used to delineate the area of influence.

3. A check calculation was made from the floor plans.

4. The areas of ore on each section were measured with a planimeter, with repeated measurements being made and averaged to reduce error.

5. The tonnage was calculated on the basis of -

$$\frac{(a + 6b + c) \times f \times i}{8p}$$

006

3. Method of Calculation (Contd.)

where
- a Planimeter reading Western Section
- b Planimeter reading Prime Section
- c Planimeter reading Eastern Section
- f Planimeters factor
- i Area of Influence Prime Section
- p Density factor ($ft.^3$ per ton)

6. The density factor used was 11.5 cubic feet per ton. This figure was supplied by the Mining Section of King Island Scheelite (1947) Limited as the figure that has been traditionally used. Although no recent investigations have been made to test the validity of this figure, experience has shown it to be generally applicable in determining ore mined in comparison with mill throughput, area excavated etc.

4. DISCUSSION

1. Possible Sources of Errors

a. Inaccuracy in data location. Only a small percentage of the drill holes in the orebody have been surveyed. Although on surveyed holes the deflections are not excessive, sufficient deviation to displace ore boundaries has probably occurred in some places.

This type of error can be reduced by co-ordinating up to date bench mapping with the drill data. This will be done as soon as staff are available to carry out open cut mapping.

b. Doubt as to early assays. Much of the data used in the calculation is derived from drilling carried out some 20 years ago. Some doubt has been expressed as to the accuracy of the assay results on some of these early holes. No real evidence for or against this view is available.

c. Variance from perfect distribution. Although tests have shown the distribution of grade values to most closely approximate to a log normal distribution rather than any other, the distributions on some sections show quite important variations from a perfect lognormal curve. Such variations will lead to small errors in the determined grade due to the unbalanced weighting of values in the calculation based on a more perfect curve.

d. Non-linear changes between sections. To obtain a workable formulae which does not involve complicated and lengthy calculations, it is necessary to assume straight line changes in the ore outline from section to section. This is obviously not so and minor discrepancies will occur because of this. It is considered however, that many of these variations will be self compensating and the final result a fair estimate. This type of error will be mainly present where cross faulting occurs.

e. Variable weighting of adjacent sections. Again to obtain workable mathematics the weighting of adjacent sections in the tonnage formulae is based on sections being equally spaced. This is not so in the No. 1 Orebody where the interval between sections varies from 85 to 140 feet. Where the interval between the prime section and each of the adjacent sections is greatly different, an error will occur since the weighting of the closer adjacent section should be more than that of the farther.

4. Discussion (Contd.)

1. Possible Sources of Errors (Contd.)

f. Oblique Terminations. The terminations of the orebody by faults oblique to the section means an average area of influence parallel to the section has to be applied and minor tonnage errors will occur on the two end sections.

g. Tonnage factor. This factor is unverified and some very preliminary tests as to the specific gravity of some ore samples suggests that the factor may be lower than the 11.5 used. Any lowering of the tonnage factor will lead to an overall increase in tonnage.

2. General

a. This resource calculation was terminated at the level of 230 feet below sea level. There is additional ore below this level particularly in the eastern end of the pit, however, the down dip continuation of the orebody is insufficiently defined to be included in the resource calculation. Drilling is currently in progress to further define this extension of the orebody. In 1967 and 1968 a tonnage of ore between the minus 230 level and the minus 300 level was included in the reserve estimate; this has been omitted in this report.

b. Also in 1967 and 1968 a mining cut off grade of 0.5% WO_3 was applied, as stated previously, a cut off grade of 0.25% WO_3 has been used in this report. This cut off has however been rigidly applied to measured assays prior to grouping into ore sections. Many areas of lower grade between ore zones have been omitted from the calculation.

c. This resource figure is a geological estimate of the ore in situ and no allowance has been made in respect to the 'mineability' of some small ore lenses or areas of waste within the orebody. It is considered beyond the scope of this report to anticipate the probable mining programme and determine a grade of ore as mined.

d. The Western end of the No. 1 Orebody from Line 16 to Line 22 has been covered in the re-evaluation of ore inter-sections. Plans and sections covering this area are included in this report, however, due to a lack of information ore in this area has not been included in the resource total. This area requires additional study and drilling as a good potential for ore exists.

4. Discussion (Contd.)

2. General

e. The B Lens orebody has been included in the resource total where it is adequately defined. This Lens is most likely more continuous than is indicated, however, information is very limited on some sections and it is not possible to define B Lens completely.

f. The total grades for each Lens unit have been calculated by two methods. Firstly the unit has been treated as a whole and a statistical count carried out and a Sichel average obtained and secondly a total grade has been derived as a weighted arithmetic average of the individual sections in each unit. These two values vary by up to 0.05% WO_3. This variance is readily explained by statistical theory and because it is based on larger sample of data the Sichel average is considered the more accurate and is therefore quoted.

g. The calculation of this ore resource has been made unnecessarily complicated by the fact that there is a change in the direction of the drilling cross sections in the No. 1 Orebody. These sections cross each other obliquely in the eastern end of the Open Cut. With drill coverage suddenly switching from Line 5 to Line 3S. This has required a careful distribution of area of influence and a cross transfer to obtain a complete coverage of the area where the sections cross.

5. REFERENCES

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TABLE I

No. 1 OREBODY

ORE RESERVES SUMMARY

	TONNAGE	MEAN GRADE % WO_3	LOWER 90% CONFIDENCE GRADE % WO_3
B LENS	256,200	0.593	0.522
C LENS (Wedge Block)	785,500	0.550	0.528
C LENS (Main Open Cut)	2,913,100	0.622	0.609
TOTAL	3,954,800	0.606	

TABLE II

No. 1 OREBODY

C LENS - MAIN OPEN CUT

Section	Tonnage	Mean Grade % WO_3	Lower 90% Confidence Grade % WO_3
00	76,500	0.620	0.571
1S	207,600	0.667	0.607
2S	206,000	0.764	0.711
3S	193,300	0.549	0.498
5	18,400	0.555	0.498
6	112,900	0.621	0.551
7	234,900	0.511	0.475
8	245,300	0.476	0.427
9	220,300	0.639	0.574
10	364,700	0.553	0.516
11	174,000	0.696	0.640
12	264,300	0.520	0.475
13	245,300	0.577	0.528
14	150,800	0.430	0.397
15	128,900	0.572	0.528
15 + 80	69,900	0.664	0.627
All Sections	2,913,100	0.622	0.609

TABLE III

No. 1 OREBODY

C LENS - WEDGE BLOCK

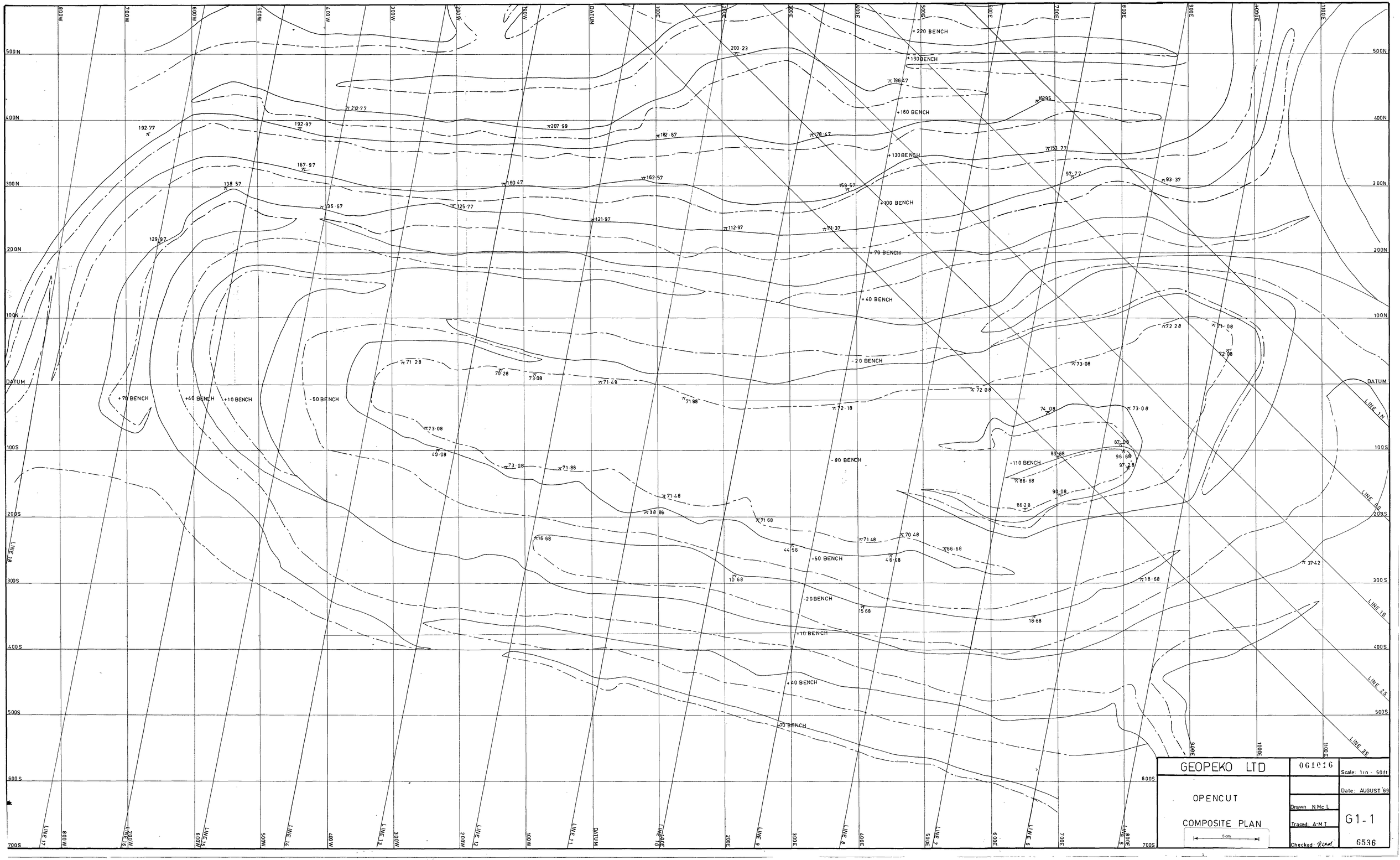
Section	Tonnage	Mean Grade % WO_3	Lower 90% Confidence Grade % WO_3
8	17,500	0.765	0.735
9	70,800	0.545	0.498
10	71,900	0.647	0.603
11	142,300	0.493	0.456
12	201,300	0.457	0.428
13	109,700	0.437	0.423
14	73,700	0.574	0.557
15	87,400	0.464	0.415
15 + 80	10,900	0.464	0.415
All Sections	785,500	0.550	0.528

TABLE IV

No. 1 OREBODY

B LENS

Section	Tonnage	Mean Grade % WO_3	Lower 90% Confidence Grade % WO_3
00	50,100	0.449	0.363
1S	30,400	0.720	0.565
7	53,300	0.416	0.363
8	35,800	0.486	0.432
9	36,100	1.394	1.239
10	50,500	0.579	0.470
All Sections	256,200	0.593	0.522



GEOPEKO LTD

061016

OPENCUT

COMPOSITE PLAN

5 cm

Scale: 1in - 50ft

Date: AUGUST '69

Drawn N.Mc.L.

Traced: A.M.T.

Checked:

G1-1

6536

2

00

300

200

100

00

-100

-200

-300

-400

-500

-600

DDH 182

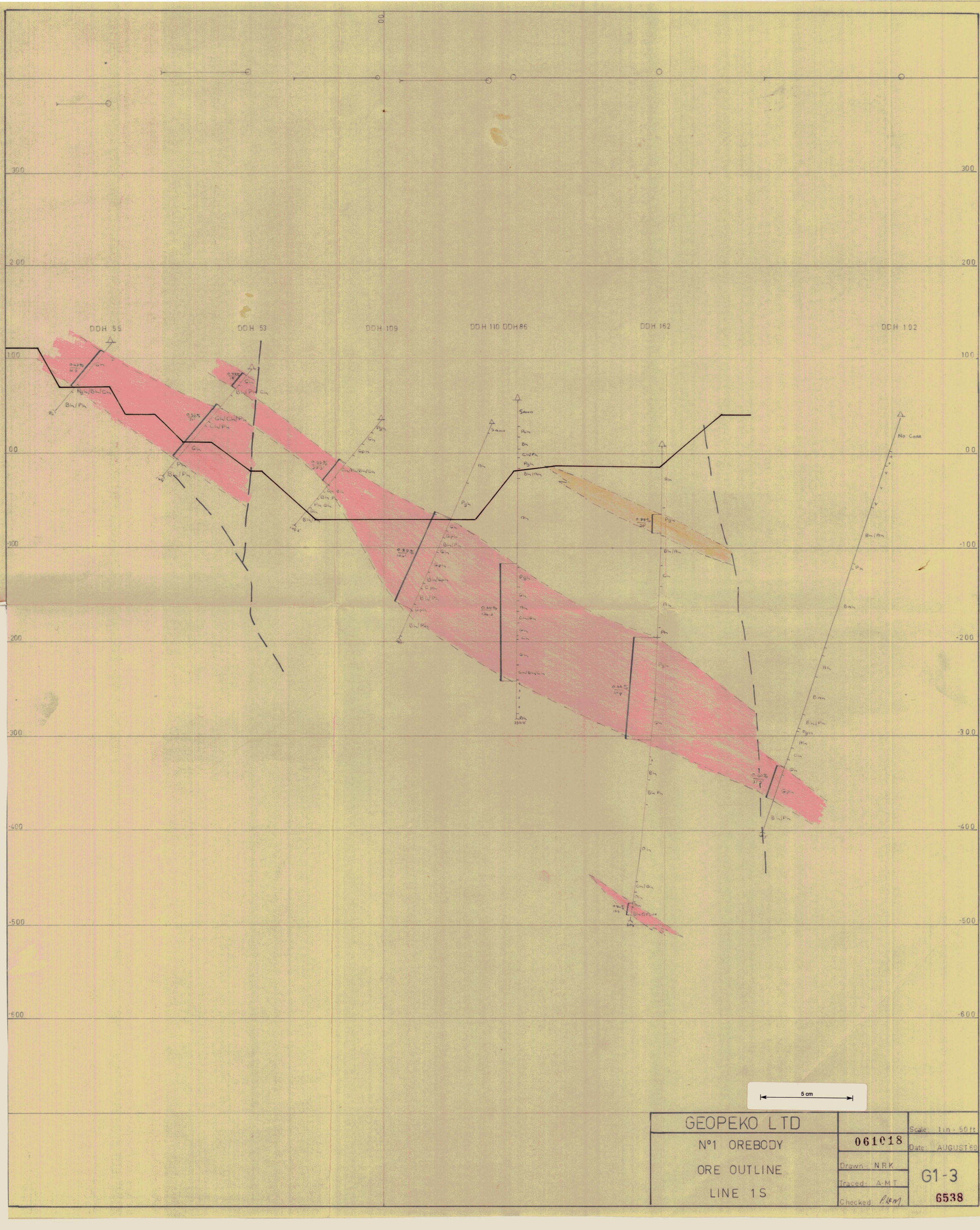
DDH 193, 195

No core

5 cm

GEOPEKO LTD.		SCALE: 1in 50 ft
Nº1 OREBODY ORE OUTLINE LINE 00	061017	DATE: AUGUST '69
	DRAWN: N R K TRACED: D MW CHECKED: P.Lem.	G1 - 2 6537

3



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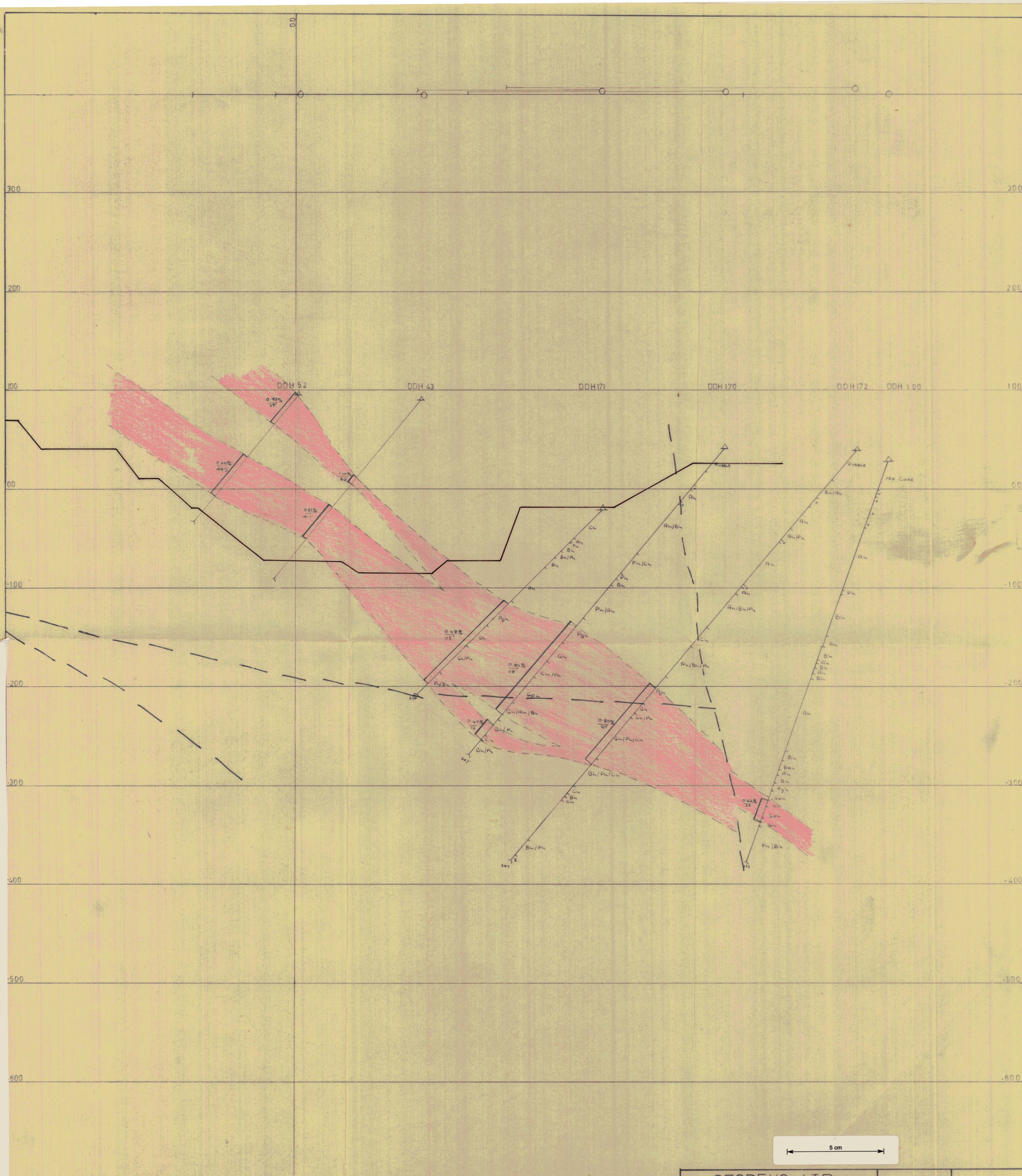
N°1 OREBODY	061018	Date: AUGUST'69
ORE OUTLINE	Drawn: N.R.K	G1-3
LINE 1S	Traced: A.M.T	
	Checked: R.Kem.	6538



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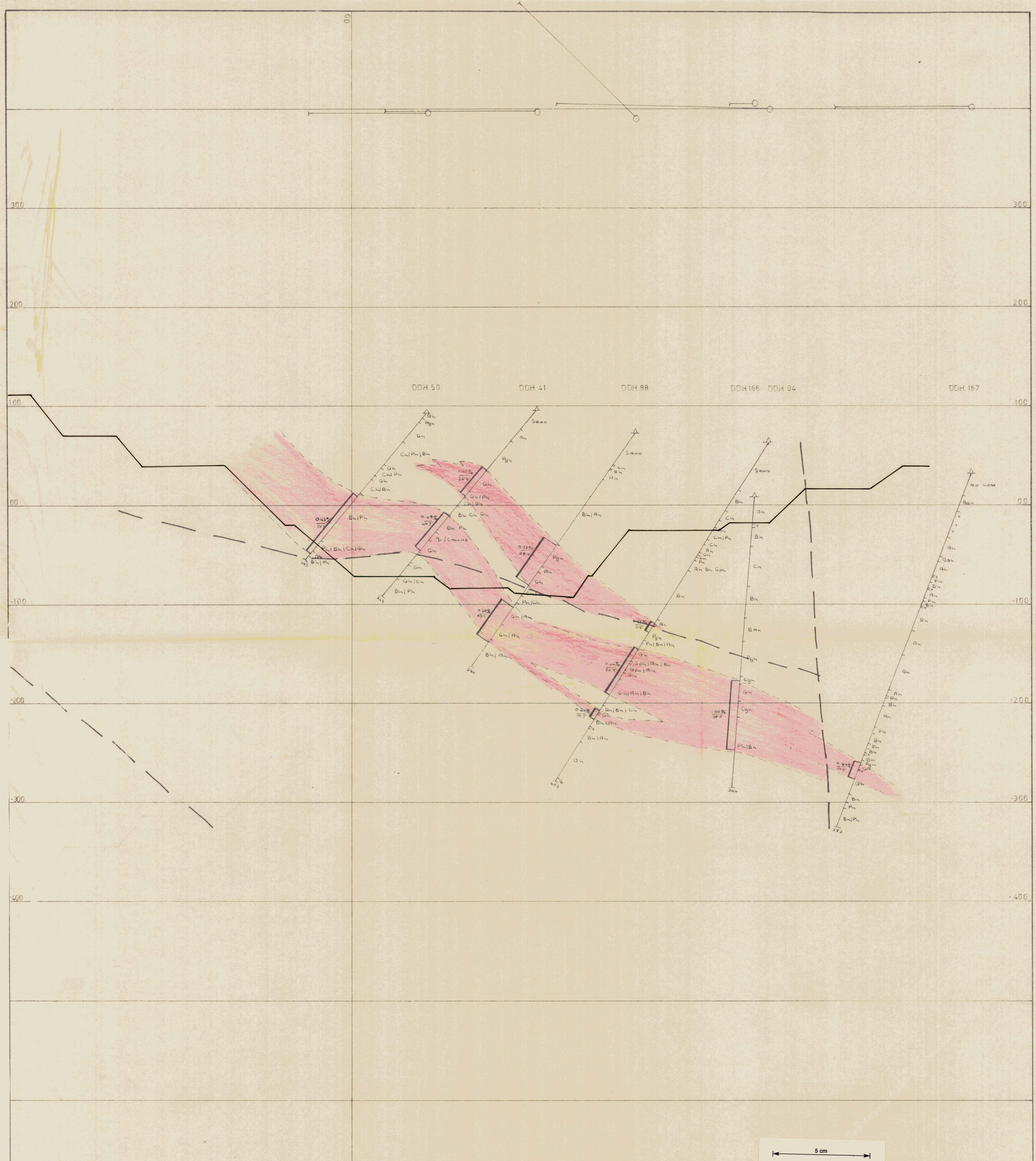
Nº1 OREBODY	061019	Date: AUG '69
ORE OUTLINE	Drawn: NRK	G1 - 4
LINE 2S	Traced: AMT	6539
	Checked: P.Lem	



GEOPEKO LTD		Scale: 1in - 50ft
N°1 OREBODY	061C20	Date: AUGUST 69
ORE OUTLINE	Drawn: NRK	G1-5
LINE 3S	Traced: AMT	
	Checked: P.L.M	6540


6
00
300
200
100
00
-100
-200
-300
-400
-500
-600
DDH 272 DDH 219
DDH 126
Sand
Bh
Bgn
Brecciated / Bh
Pgh
Gph
Aplite
Gh
0.07%
43-75'
Bh/Ph
Gph/Gh
Gh/Gph/Ph
Gh/Ph/Gh
Ch
374
Oh
0.32%
Ph/Bh
Ph/Gh
Ph/Bh/Gh
735
5 cm
GEOPEKO LTD
N°1 OREBODY
ORE OUTLINE
LINE 5
061021
Scale: 1in. 50ft
Date: AUGUST '69
Drawn: NRK
Traced: A.M.T
Checked: P. Lem.
G1-6
6541

7

00

300

200

100

00

-100

-200

-300

-400

-500

DDH 274

DDH 213

DDH 164

Sand

Oh

Ah

Ah/Bh/Ph

Bah

Pgh

Barren

Gph to Gh

Gh/Gph

Gh

Bh/Ph/Ch

Bh/Ph

Older

Ch

Ph

Gph

Ch/Bh/Ph

Bh/Ch/Gh

0.44% 6'

0.55% 42'

0.33% 20'

0.58% 6'

1.29% 25.5'

0.40% 38.5'

0.32% 5'

1.30% 7.2'

0.29% 5'

272

350

5 cm

GEOPEKO LTD		Scale: 1in. 50ft
N°1 OREBODY ORE OUTLINE LINE 6	061022 Drawn: NRK Traced: AMT Checked: P.Kem.	Date: AUGUST '69 G1-7 6542

8

00

300

200

DDH 56 ?

DDH 104 DDH 106 DDH 207 DDH 125

DDH 174

DDH 112

100

00

-100

-200

-300

-400

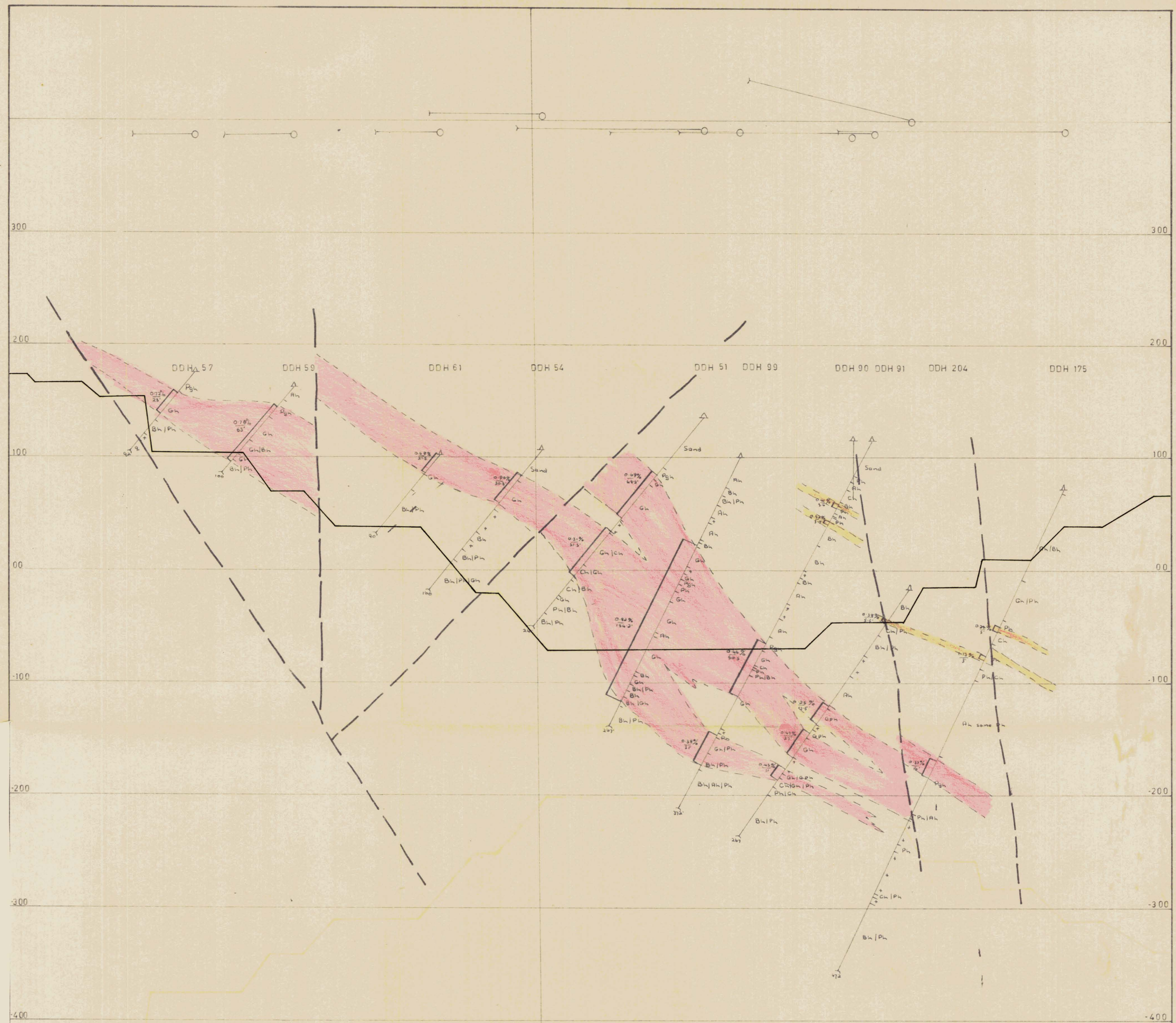
-500

-600

-700

5 cm

GEOPEKO LTD		Scale: 1in.- 50ft
N°1 OREBODY ORE OUTLINE LINE 7	061023	Date: AUGUST '69
	Drawn: N.R.K.	G1-8
	Traced: A.M.T.	6543
	Checked: P.K.M.	



GEOPEKO LTD

N°1 OREBODY

ORE OUTLINE

LINE 8

061024

Drawn: N.R.K

Traced: A.M.T

Checked: P.L.M

Scale: 1in 50ft

Date: AUGUST'69

G1 - 9

6544

DDH 60 DDH 58 DDH 27 DDH 40 DDH 30 DDH 28 DDH 98 DDH 36 DDH 205 DDH 101 DDH 271 DDH 147 DDH 130

300 200 100 00 -100 -200 -300 -400 -500 -600

Sand

5 cm

GEOPEKO LTD		Scale: 1in. 50ft
N°1 OREBODY	061025	Date: AUGUST 69
ORE OUTLINE	Drawn: NRK	G1-10
LINE 9	Traced: A.MT	6545
	Checked: P.Lem	

11

DDH 72 DDH 62 DDH 26 DDH 25 DDH 23 DDH 38 DDH 95 DDH 31 DDH 201 DDH 148 DDH 128

300 200 100 00 -100 -200 -300 -400 -500

GEOPEKO LTD

N°1 OREBODY

ORE OUTLINE

LINE 10

061026

Drawn: N.R.K.

Traced: A.M.T.

Checked: P.Kent.

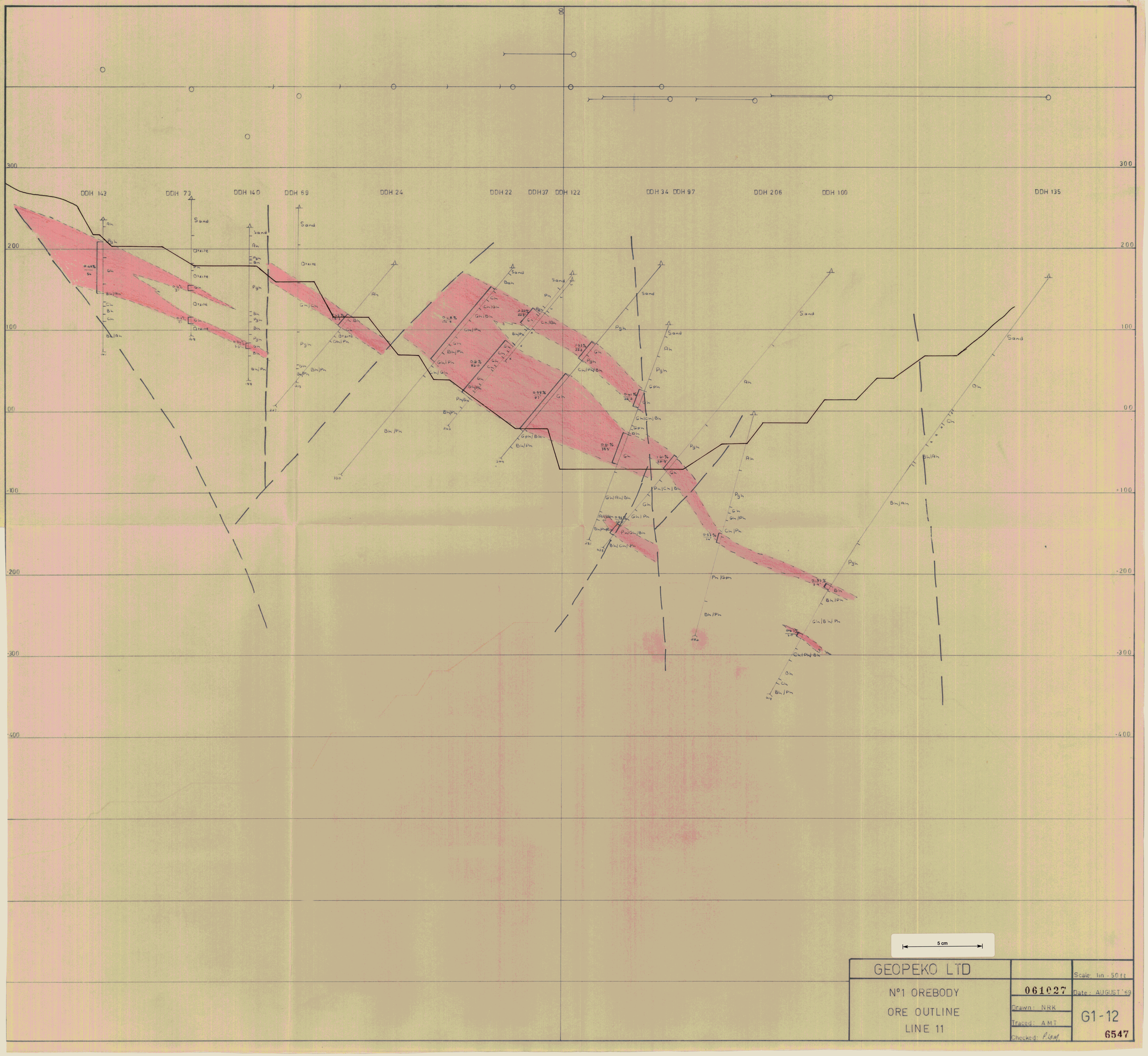
Scale: 1in - 50ft

Date: AUGUST'69

G1-11

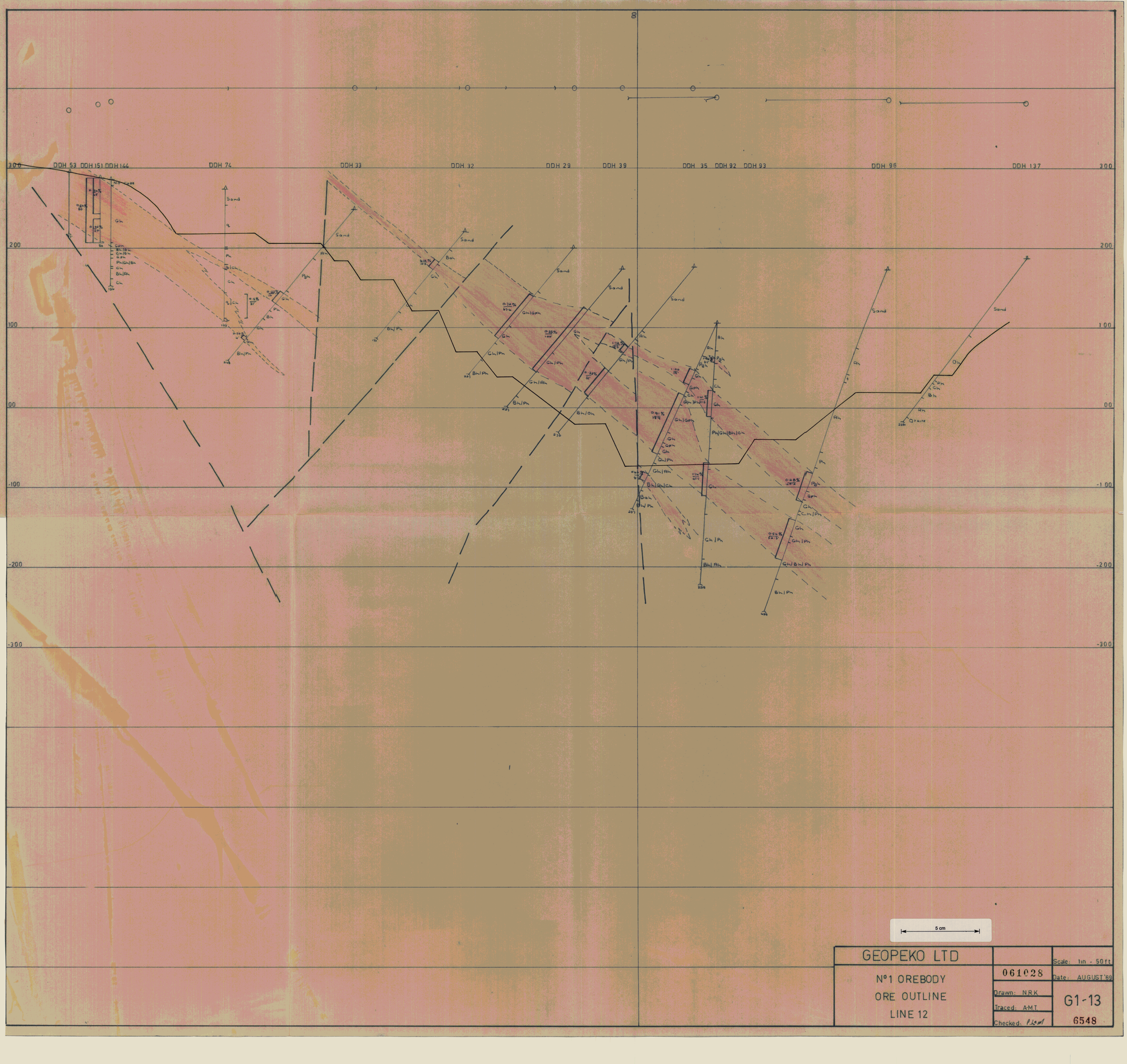
6546

12



5 cm

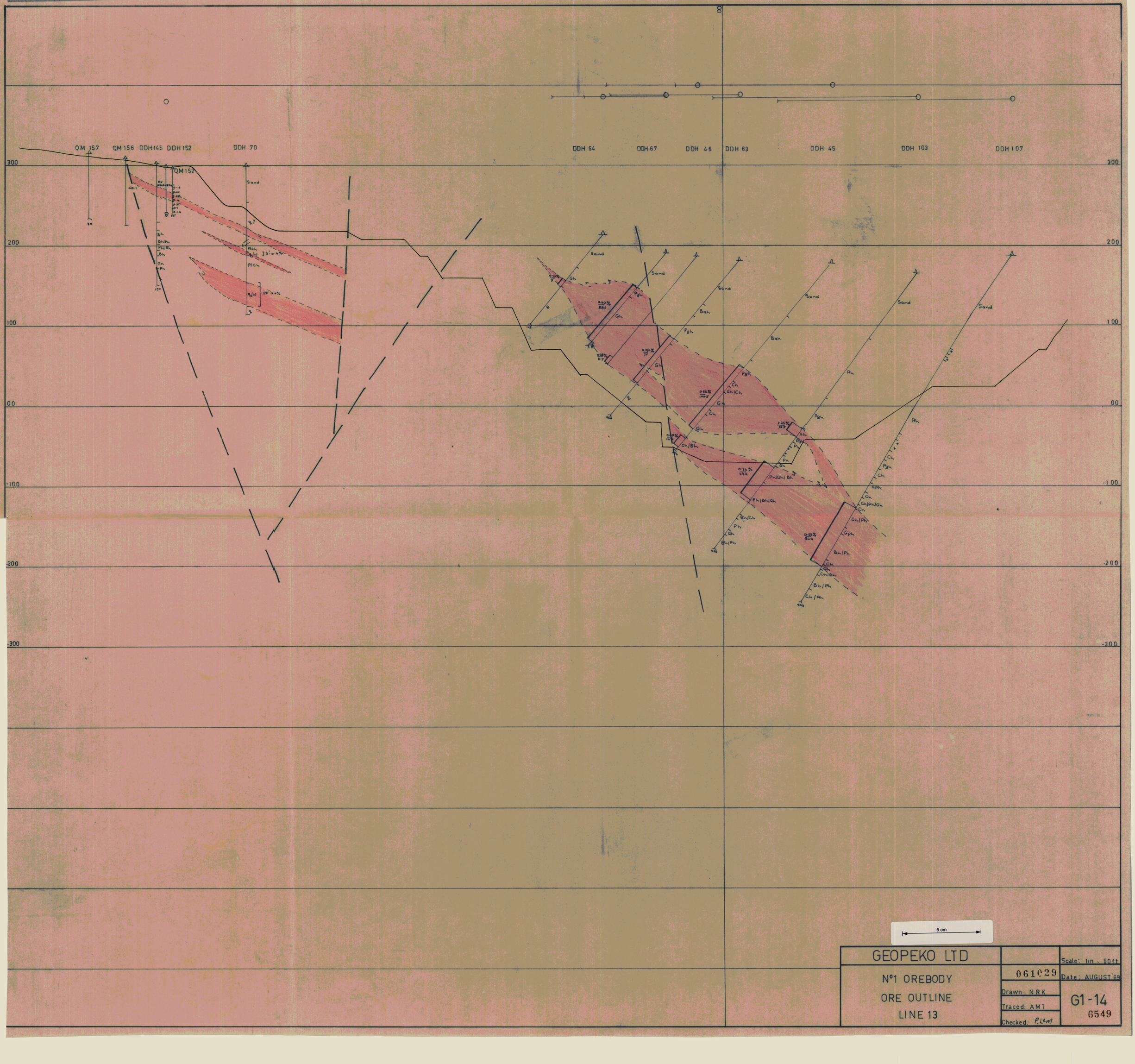
GEOPEKO LTD		Scale: 1in. - 50 ft
N°1 OREBODY ORE OUTLINE LINE 11	061027 Drawn: NRK Traced: AMT Checked: R.Lem.	Date: AUGUST '69 G1-12 6547



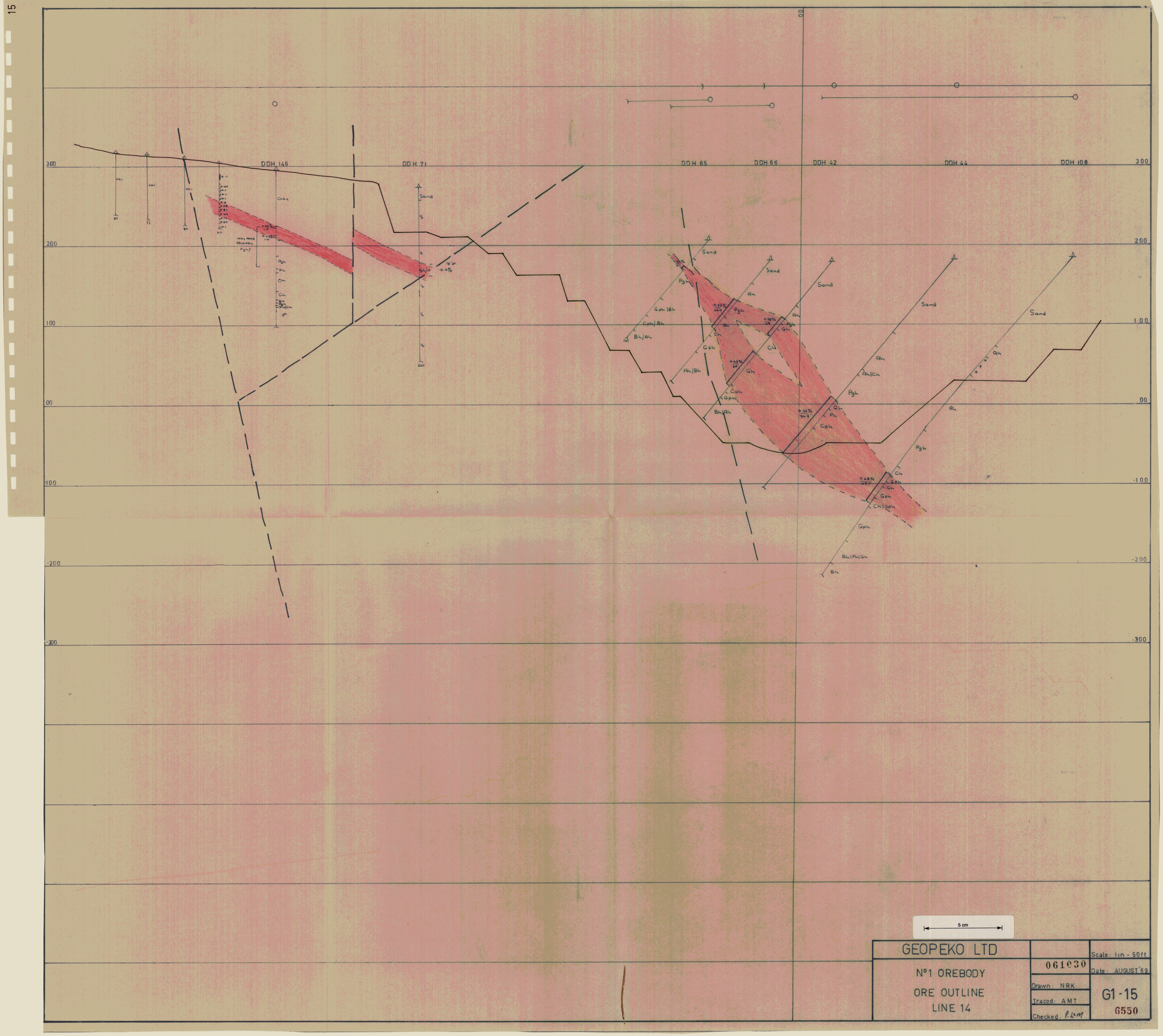
5 cm

GEOPEKO LTD		Scale: 1in - 50ft
N°1 OREBODY ORE OUTLINE LINE 12	061028 Drawn: N.R.K. Traced: A.M.T. Checked: P.Lam	Date: AUGUST'69 G1-13 6548

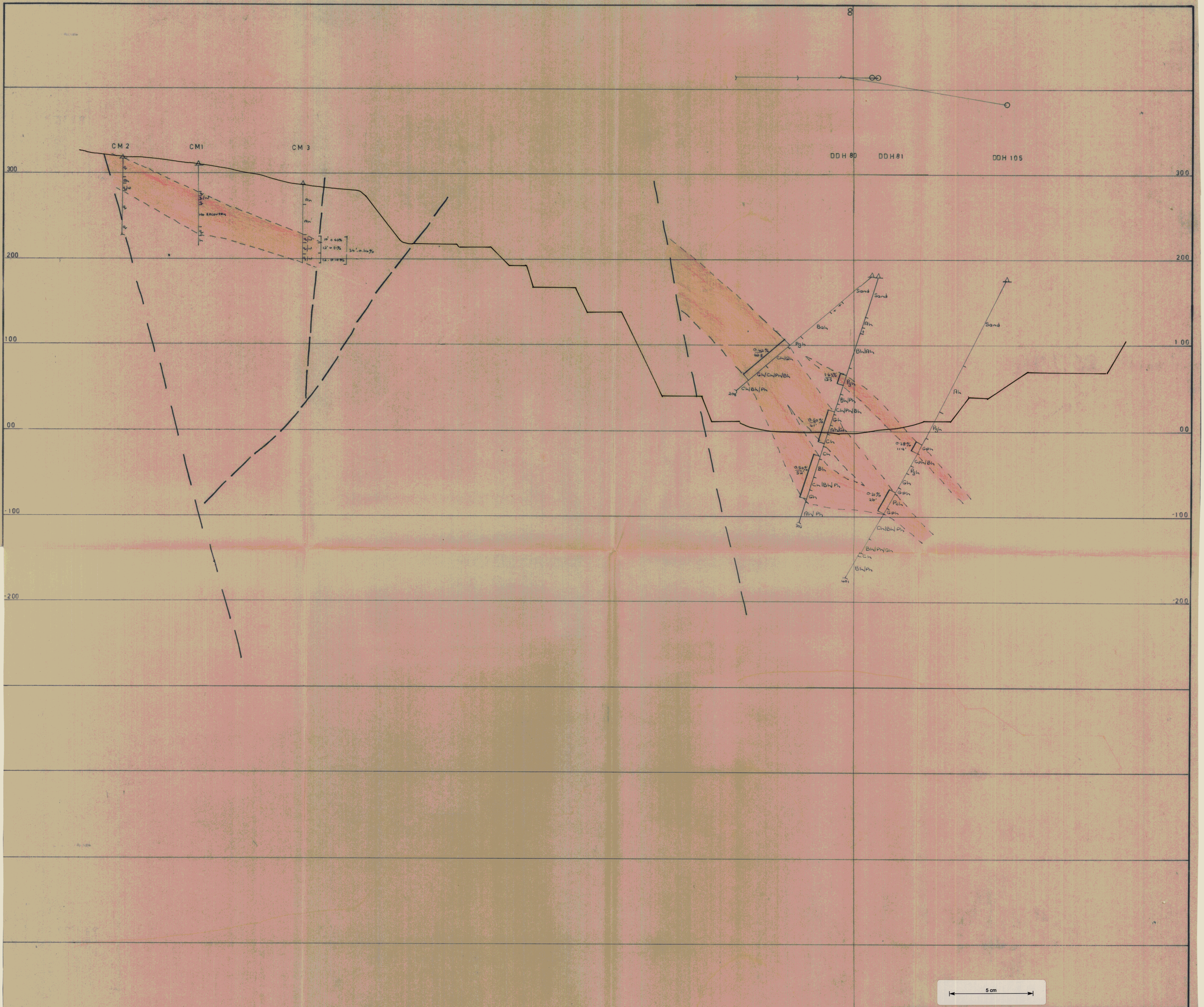
14



GEOPEKO LTD		Scale: 1in. : 50ft
N°1 OREBODY ORE OUTLINE LINE 13	061029 Drawn: N.R.K. Traced: A.M.T. Checked: P.L.M.	Date: AUGUST '69 G1-14 6549



15
DDH 146
DDH 71
DDH 65
DDH 66
DDH 42
DDH 44
DDH 108
300
200
100
00
-100
-200
-300
Sand
Ah
Ah/Ch
Pgh
Gph
Ch
Bh/Ah
Gph/Bh
Ah/Bh
Ch/Gph
Bh/Ph/Gh
Bh
5 cm
GEOPEKO LTD
Nº1 OREBODY
ORE OUTLINE
LINE 14
061030
Scale: 1in - 50ft
Date: AUGUST '69
Drawn: NRK
Traced: AMT
Checked:
G1-15
6550



5 cm

GEOPEKO LTD		Scale: 1in - 50ft
Nº1 OREBODY ORE OUTLINE LINE 15	061031	Date: AUGUST '69
	Drawn: N.R.K Traced: A.M.T. Checked: P.LeM	G1-16 6551

17

00

200

100

00

-100

-200

-300

00

DDH 115 (42°)

DDH 116 (50°)

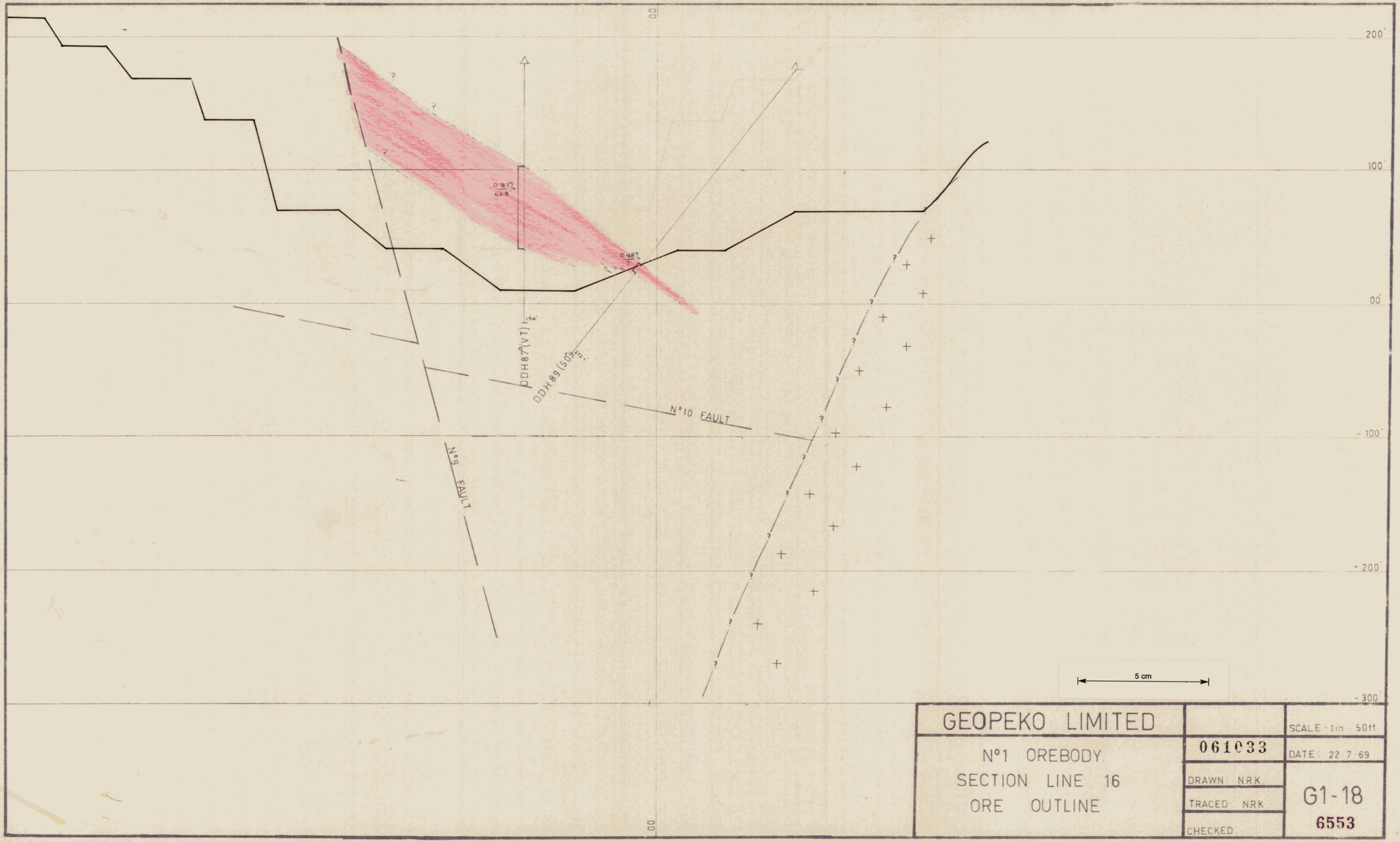
N°9 FAULT

N°10 FAULT

5 cm

GEOPEKO LIMITED		SCALE: 1in : 50ft
N°1 OREBODY. SECTION- LINE. 15+80'- ORE OUTLINE	061032	DATE: 23 7 69
	DRAWN: NRK	G1-17
	TRACED: NRK	
	CHECKED:	6552

18



GEOPEKO LIMITED		SCALE - 1in : 50ft
N°1 OREBODY. SECTION LINE 16 ORE OUTLINE	061033	DATE: 22 7 69
	DRAWN: NRK TRACED: NRK CHECKED:	G1-18 6553

19

GEOPEKO LIMITED		SCALE - 1in : 50ft
N°1 OREBODY. SECTION LINE 17 ORE OUTLINE	061064	DATE - 23-7-69
	DRAWN - N.R.K.	G1-19
	TRACED - N.R.K.	
	CHECKED -	6554

20

00

200

100

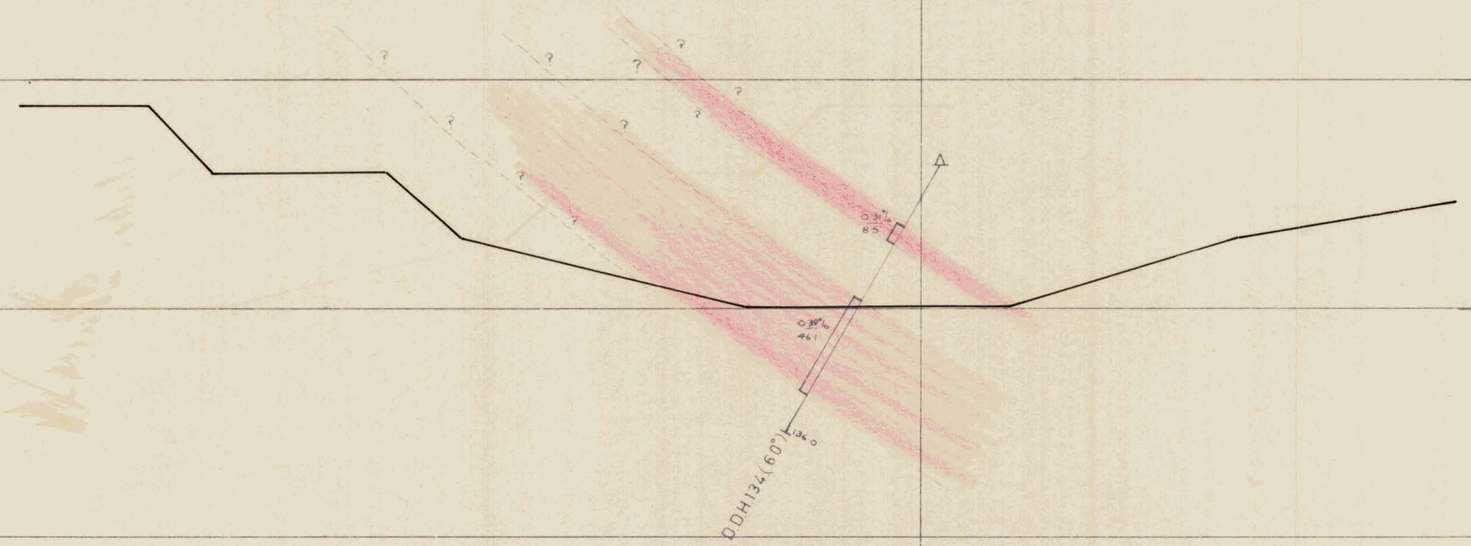
00

-100

-200

-300

00

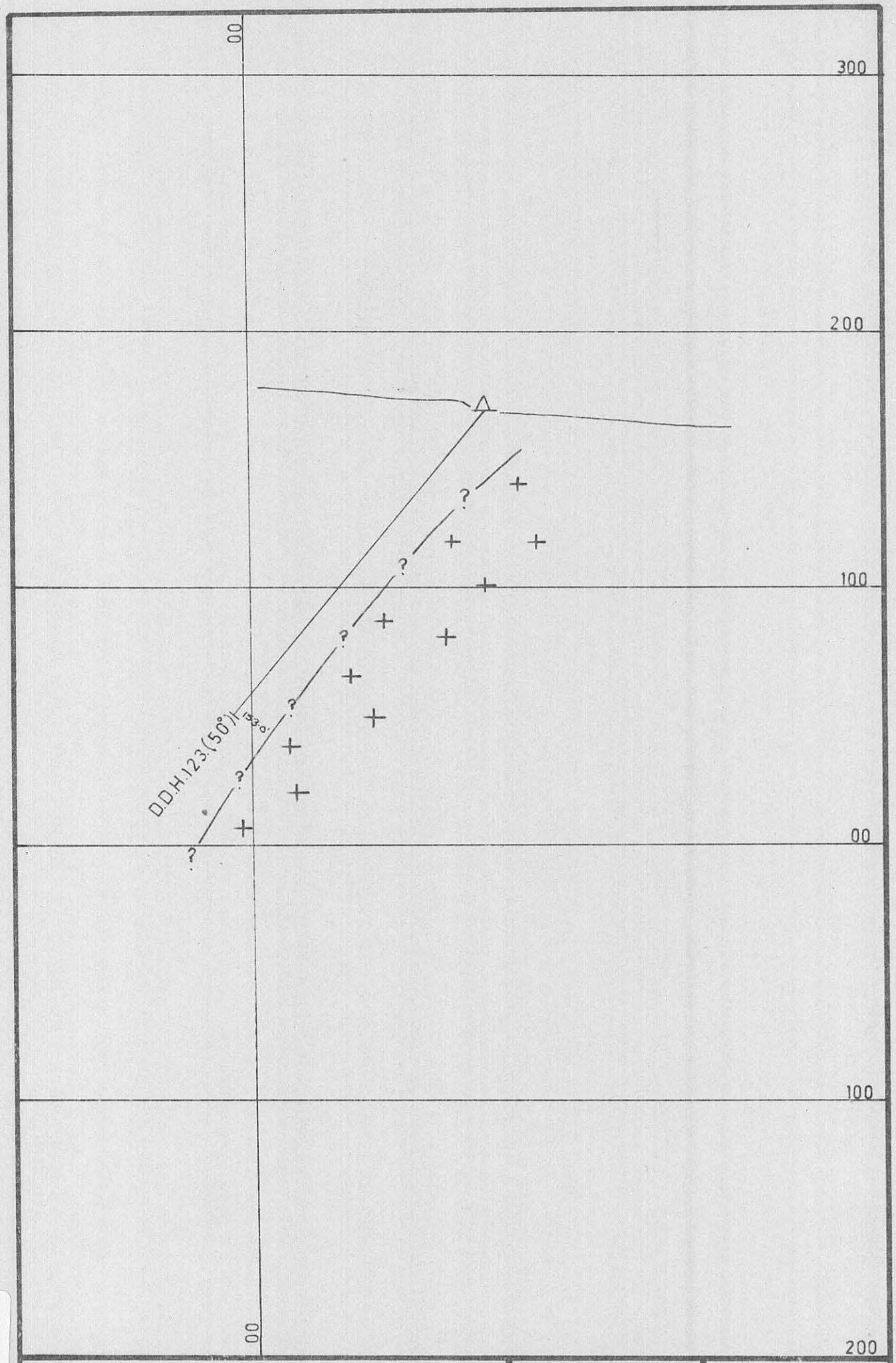


5 cm

GEOPEKO LIMITED		SCALE - 1in: 50ft
N°1 OREBODY. SECTION LINE 17+80 ORE OUTLINE	061035	DATE - 24 7 69
	DRAWN: N.R.K TRACED: N.R.K CHECKED:	G1-20 6555

GEOPEKO LIMITED		SCALE 1 in 50 ft
N°1 OREBODY	061036	DATE 24 7 69
SECTION LINE 18	DRAWN NRK	G1-21
ORE OUTLINE	TRACED N.R.K.	6556
	CHECKED	

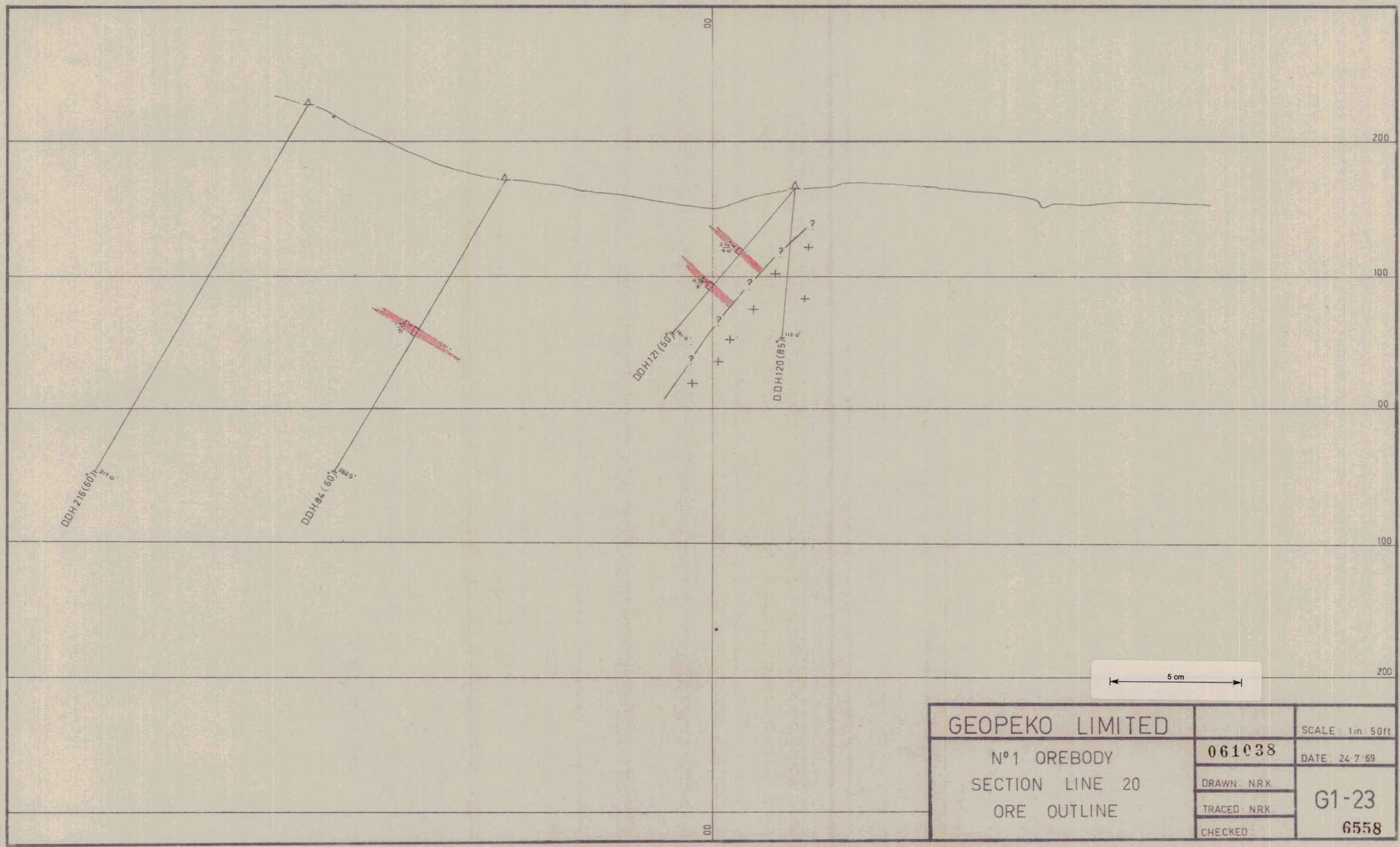
22



5 cm

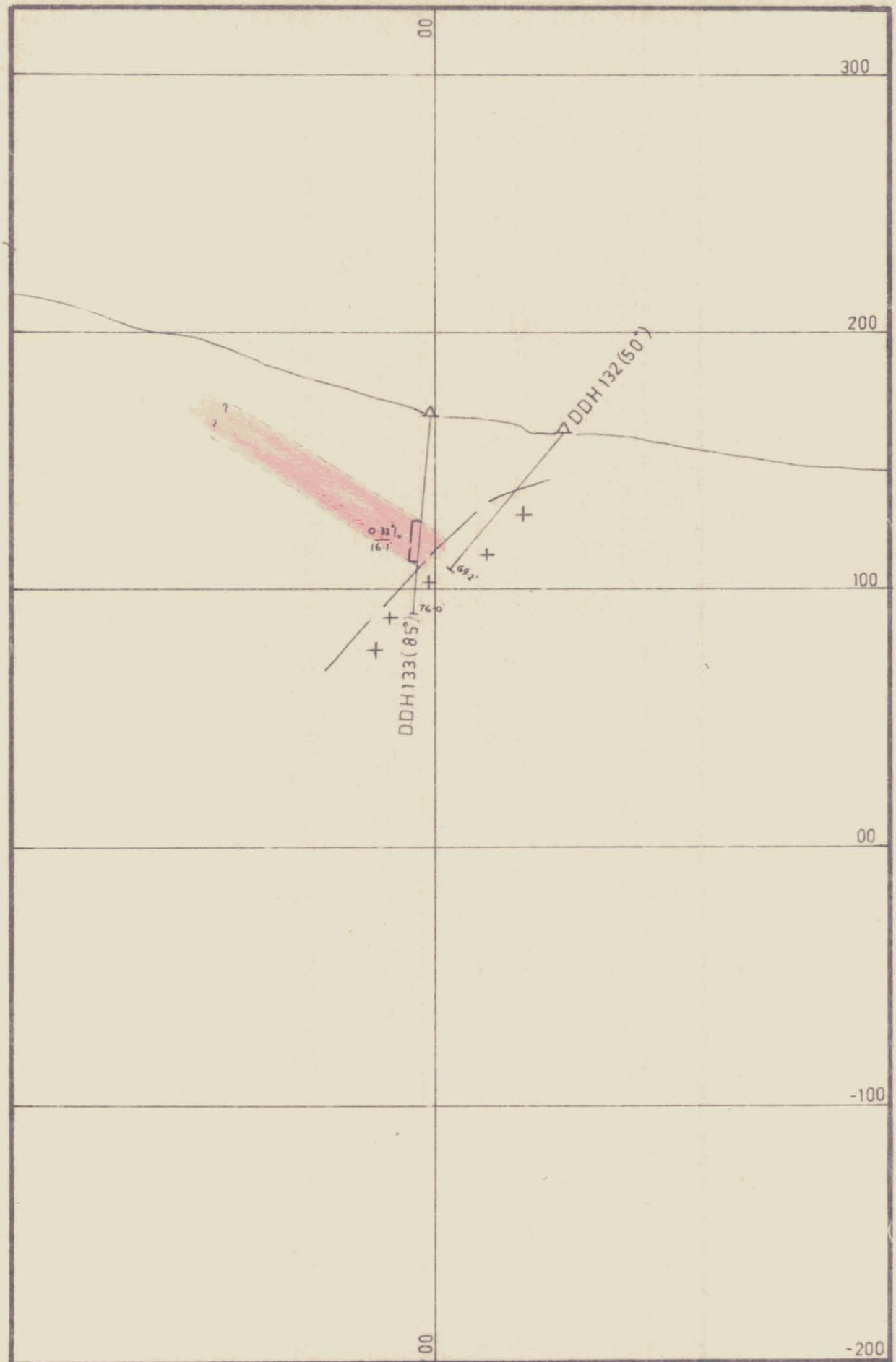
GEOPEKO LIMITED		SCALE: 1in : 50ft
N°1 OREBODY SECTION LINE 19 ORE OUTLINE	061037	DATE: 24·7·69
	DRAWN: N.R.K.	G1-22
	TRACED N.R.K.	
	CHECKED P.Lem	6557

23



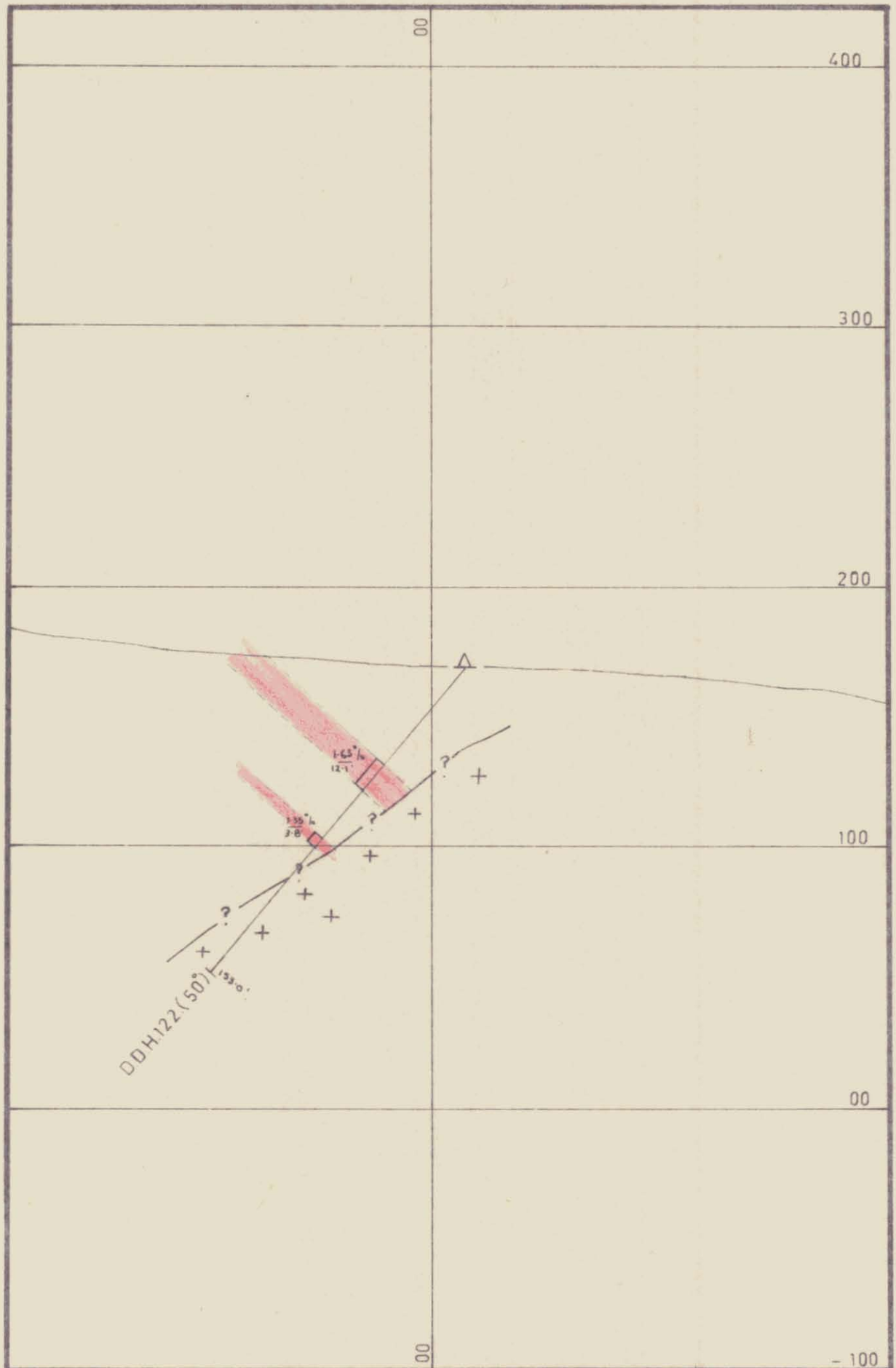
GEOPEKO LIMITED		SCALE : 1in : 50ft
N°1 OREBODY SECTION LINE 20 ORE OUTLINE	061038	DATE : 24·7·69
	DRAWN : N.R.K.	G1-23
	TRACED : N.R.K.	
	CHECKED :	6558

24



GEOPEKO LIMITED		SCALE :- 1in : 50ft
N°1 OREBODY SECTION LINE 21 ORE OUTLINE	061039	DATE :- 25·7·69
	DRAWN :- N.R.K.	G1-24
	TRACED :- N.R.K.	
	CHECKED :- P.Lem.	6559

5 cm



GEOPEKO LIMITED

N° 1 OREBODY.
SECTION LINE 22
ORE OUTLINE

5 cm

061040

SCALE :- 1in : 50ft

DATE - 25 7 69

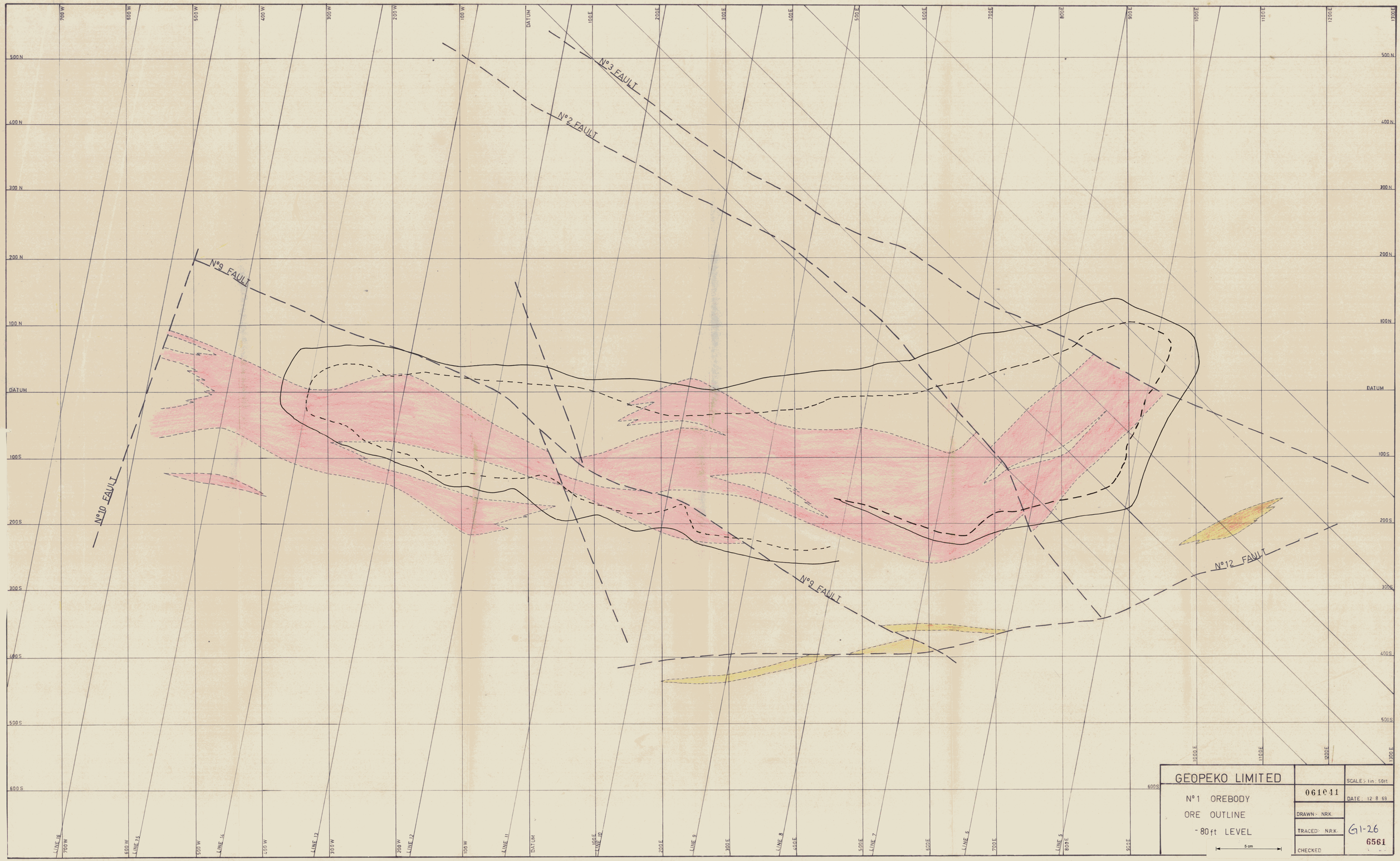
DRAWN :- N.R.K.

TRACED :- N.R.K.

CHECKED :- P.Lem

G1-25

6560



GEOPEKO LIMITED

N°1 OREBODY

ORE OUTLINE

-80ft LEVEL

061041

DRAWN: NRK.

TRACED: NRK.

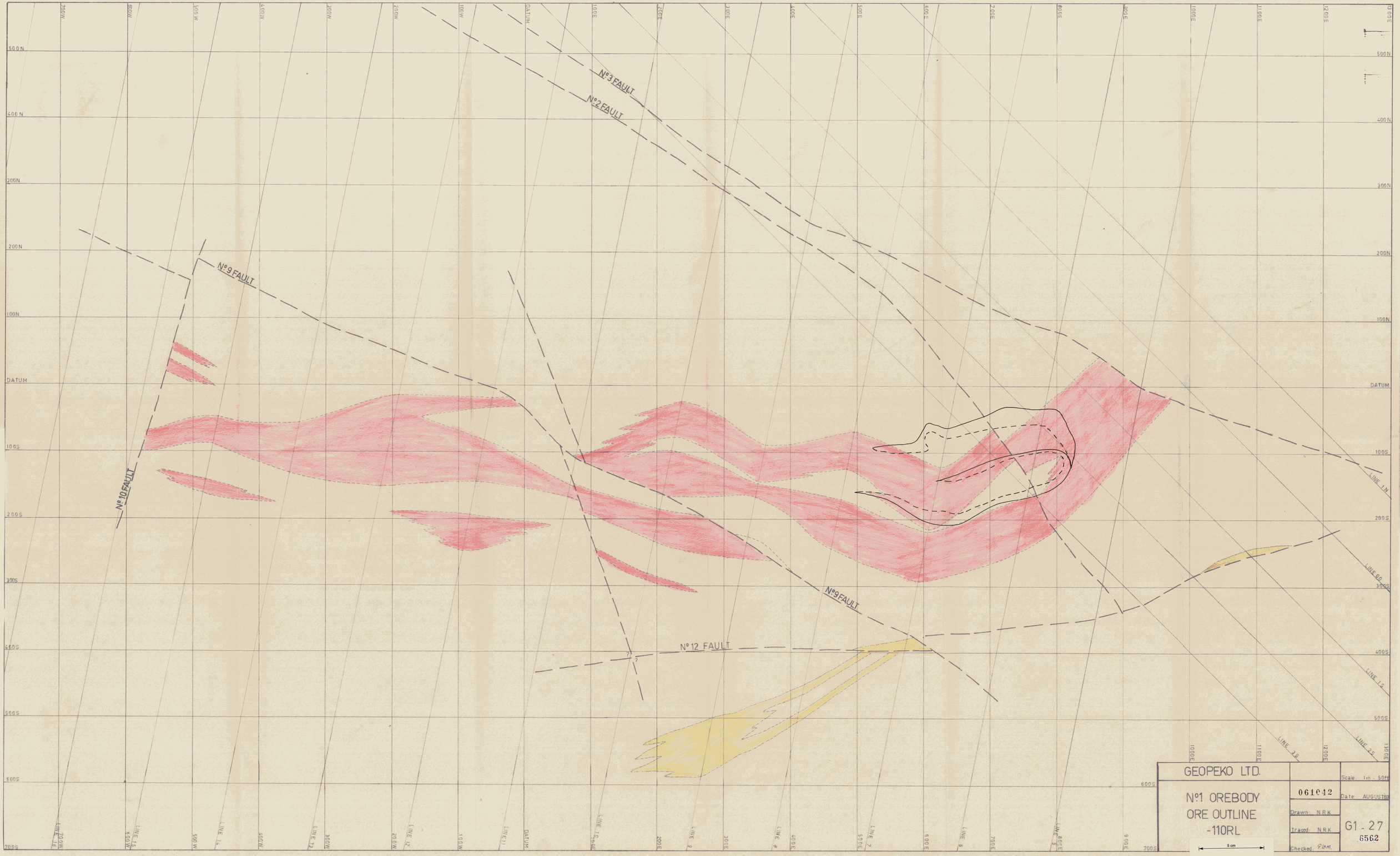
CHECKED

SCALE: 1in: 50ft

DATE: 12 8 69

G1-26

6561



GEOPEKO LTD.

No1 OREBODY
ORE OUTLINE
-110RL

061042

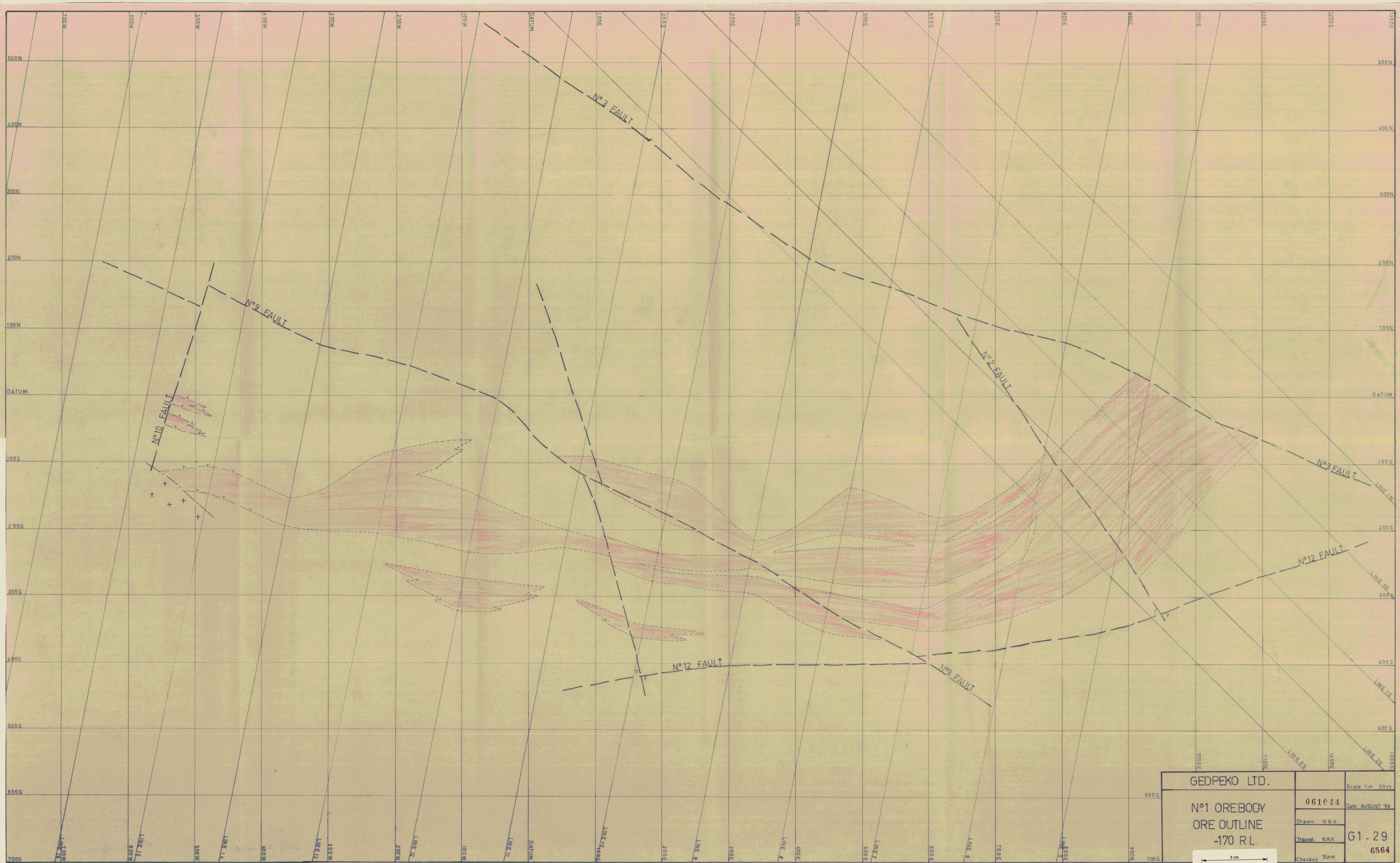
Drawn: N.R.K.
Traced: N.R.K.
Checked: P.C.M.

Scale: 1in. = 50ft
Date: AUGUST 69

G1 - 27
6562

5 cm


Nº3 FAULT
Nº2 FAULT
Nº9 FAULT
Nº10 FAULT
Nº12 FAULT
500N
400N
300N
200N
100N
DATUM
100S
200S
300S
400S
500S
600S
700S
700W
600W
500W
400W
300W
200W
100W
100E
200E
300E
400E
500E
600E
700E
800E
900E
1000E
1100E
1200E
1300E
LINE 3S
LINE 2S
GEOPEKO LTD.
Nº1 OREBODY
ORE OUTLINE
-140RL
5 cm
061043
Drawn: NRK
Traced: NRK
Checked:
Scale: 1in - 50ft
Date: AUGUST'69
G1-28
6563



GEOPEKO LTD.

N°1 OREBODY
ORE OUTLINE
-170 R.L.

Scale 1in 50ft

061044

Date: AUGUST '69

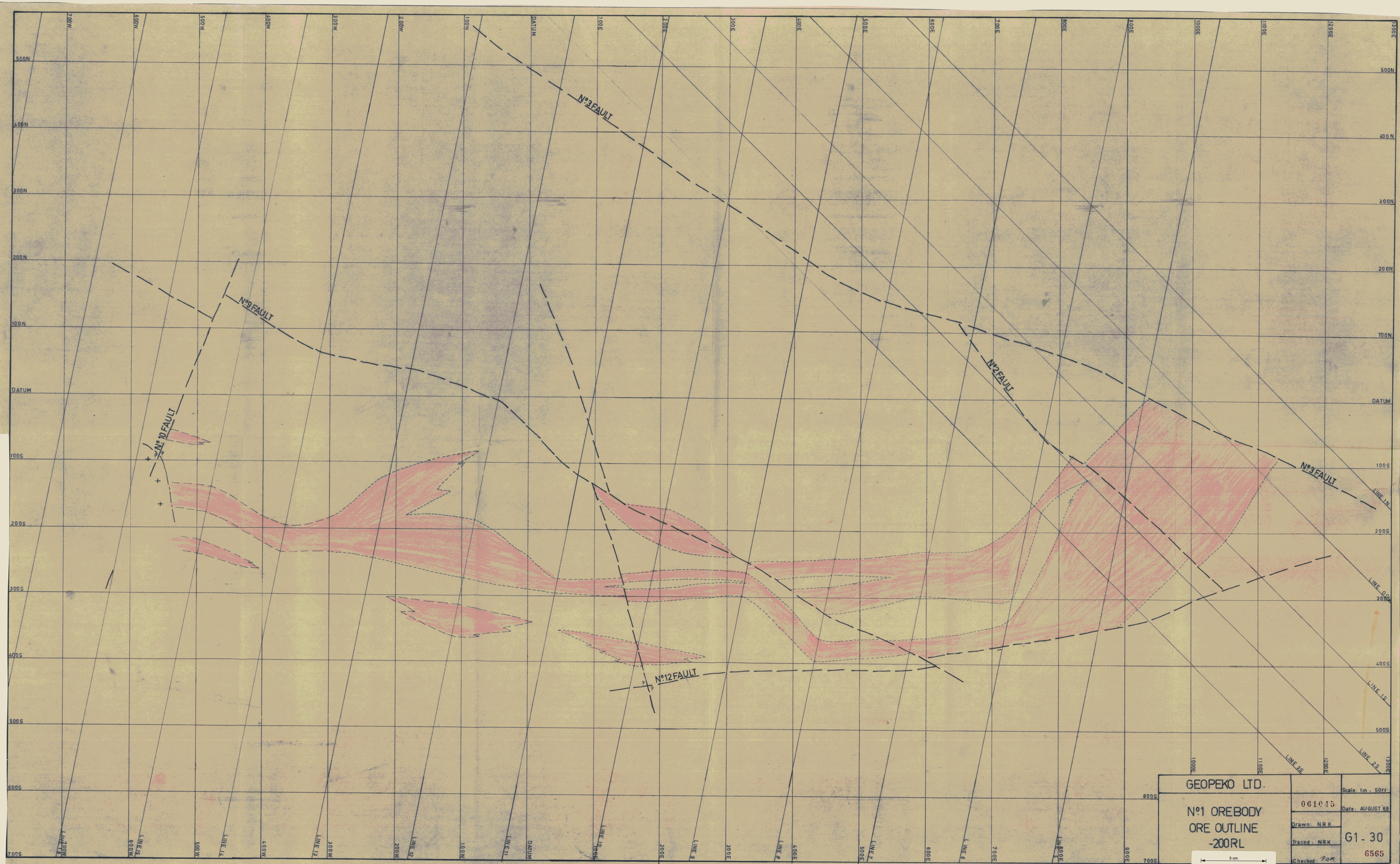
Drawn N.R.K.

Traced N.R.K.

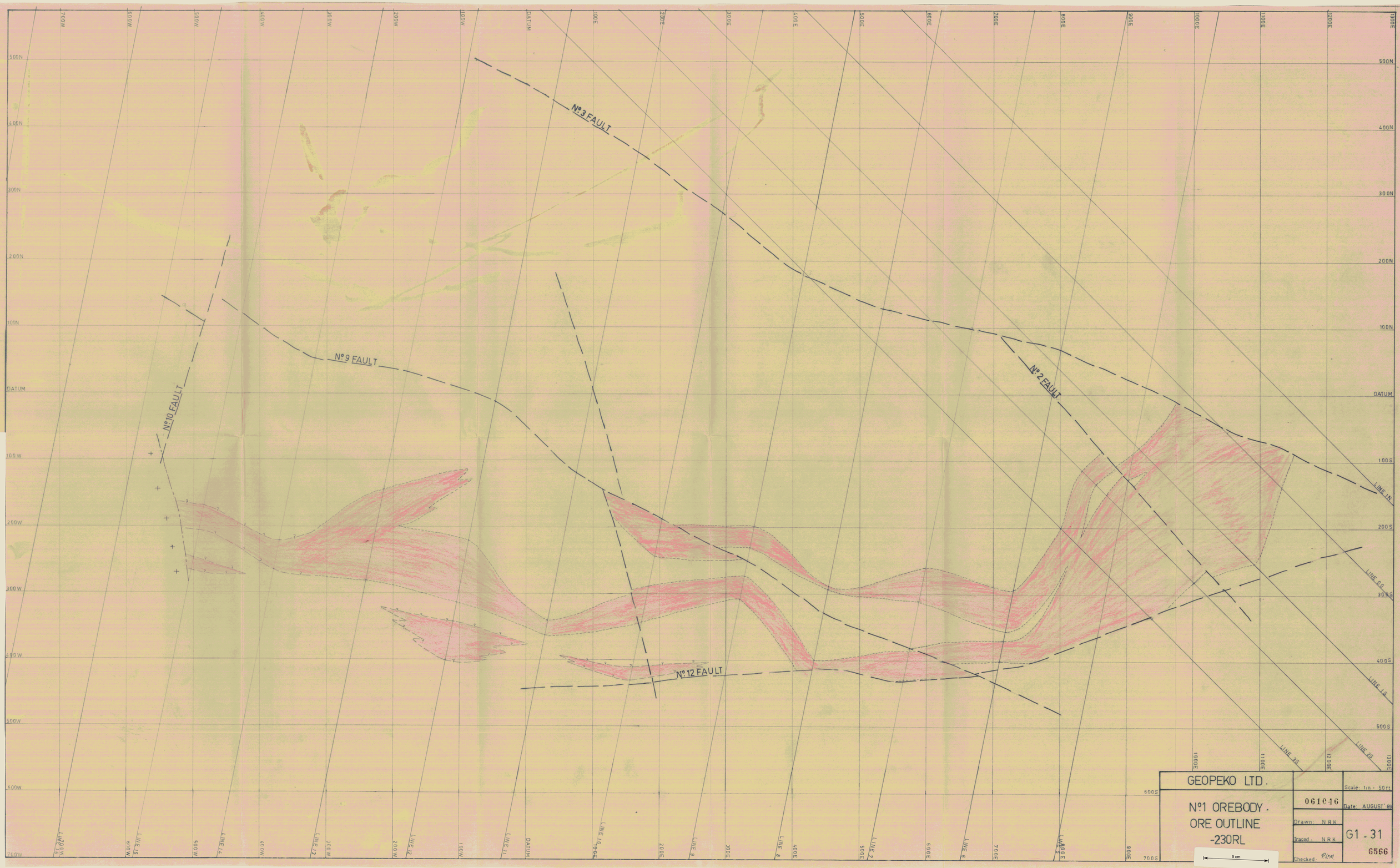
Checked

G1 - 29

6564


700W
600W
500W
400W
300W
200W
100W
DATUM
100E
200E
300E
400E
500E
600E
700E
800E
900E
1000E
1100E
1200E
1300E
500N
400N
300N
200N
100N
DATUM
100S
200S
300S
400S
500S
600S
700S
No 3 FAULT
No 9 FAULT
No 10 FAULT
No 2 FAULT
No 12 FAULT
LINE 14
LINE 15
LINE 16
LINE 13
LINE 12
LINE 11
LINE 10
LINE 9
LINE 8
LINE 7
LINE 6
LINE 5
LINE 4
LINE 3
LINE 2
LINE 1N
LINE 1S
LINE 2S
GEOPEKO LTD.
No 1 OREBODY
ORE OUTLINE
-200 RL
061045
Drawn: N.R.K
Traced: N.R.K
Checked: P.G.M
Scale: 1in - 50ft
Date: AUGUST '69
G1 - 30
6565
5 cm

31



GEOPEKO LTD.

Nº1 OREBODY.
ORE OUTLINE
-230RL

Scale: 1in - 50ft

061046

Date AUGUST '69

Drawn: N.R.K.

Traced: N.R.K.

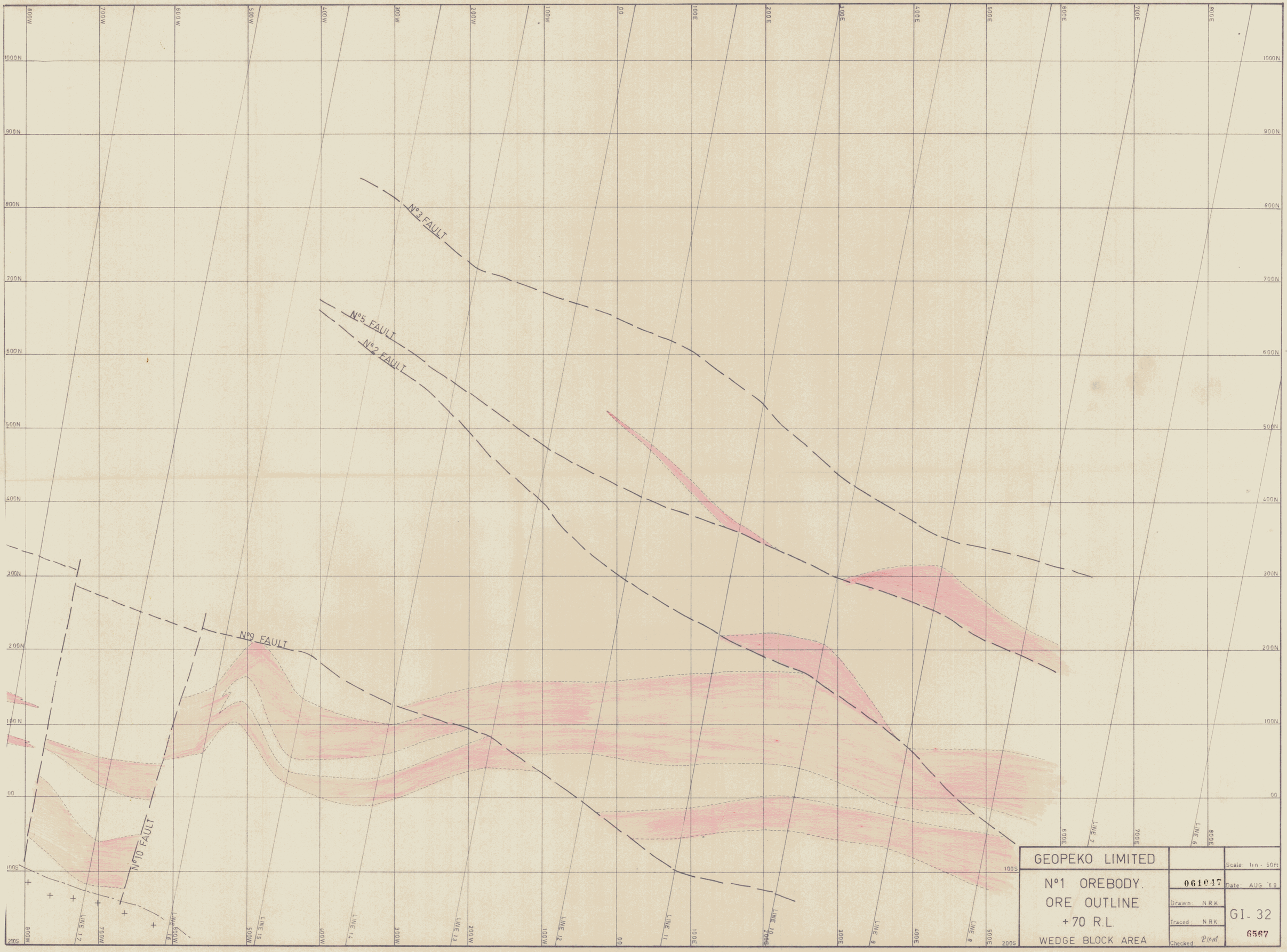
Checked: R.C.M.

G1 - 31

6566

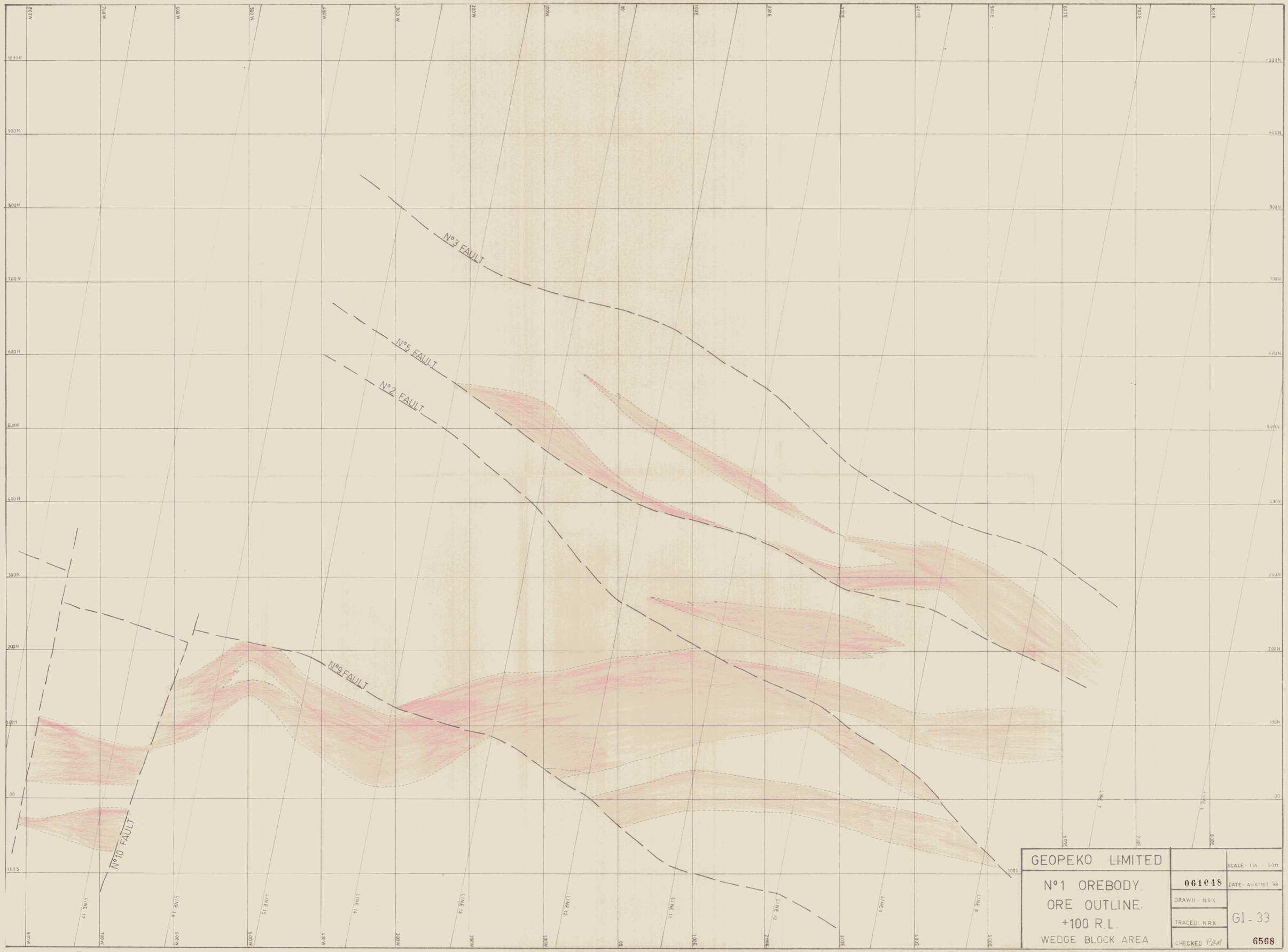
5 cm

32

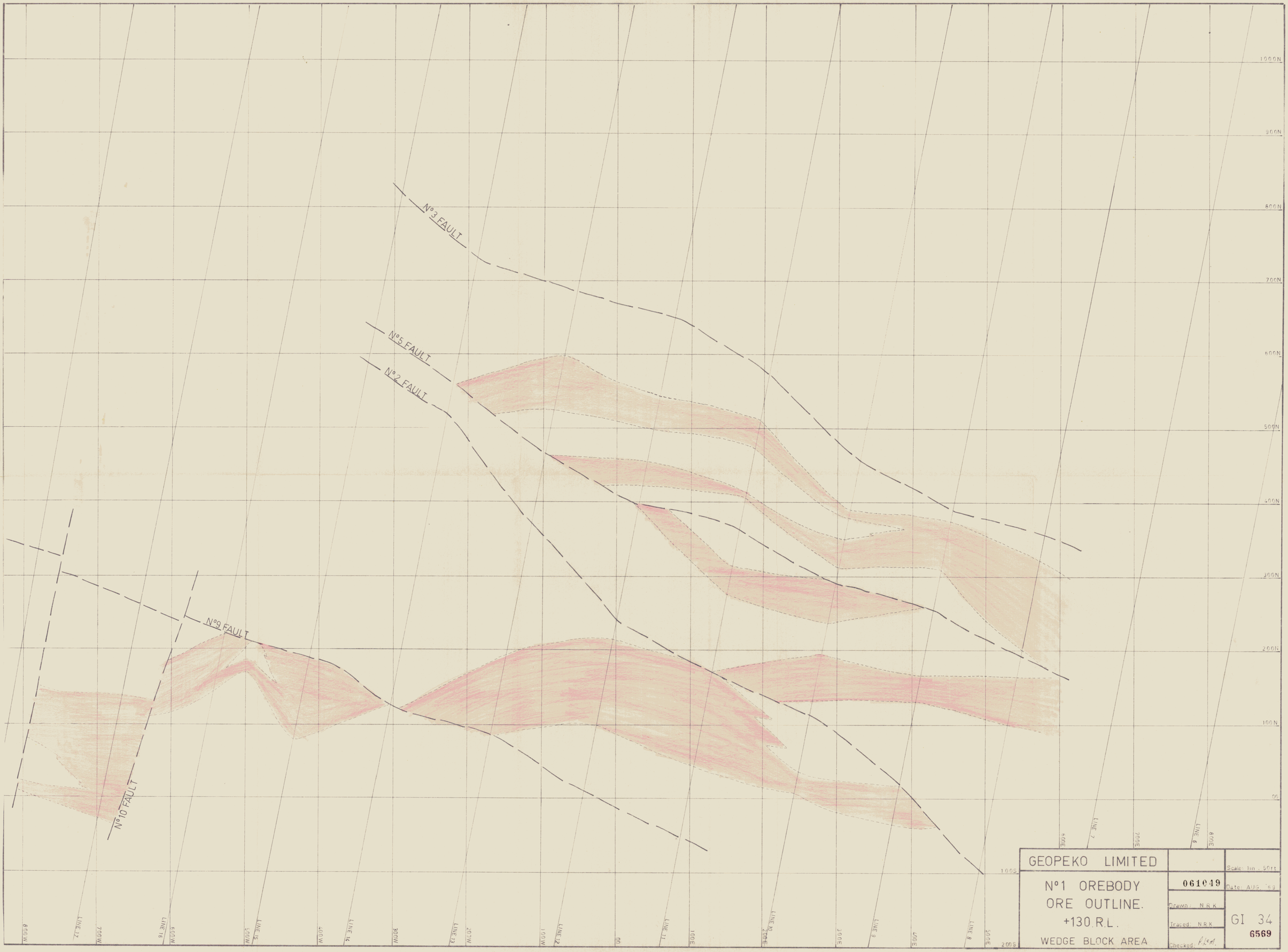


GEOPEKO LIMITED		Scale: 1in - 50ft
N°1 OREBODY. ORE OUTLINE +70 R.L. WEDGE BLOCK AREA	061047	Date: AUG '69
	Drawn: N.R.K.	GI-32
	Traced: N.R.K.	
	Checked: Rlem.	6587

33

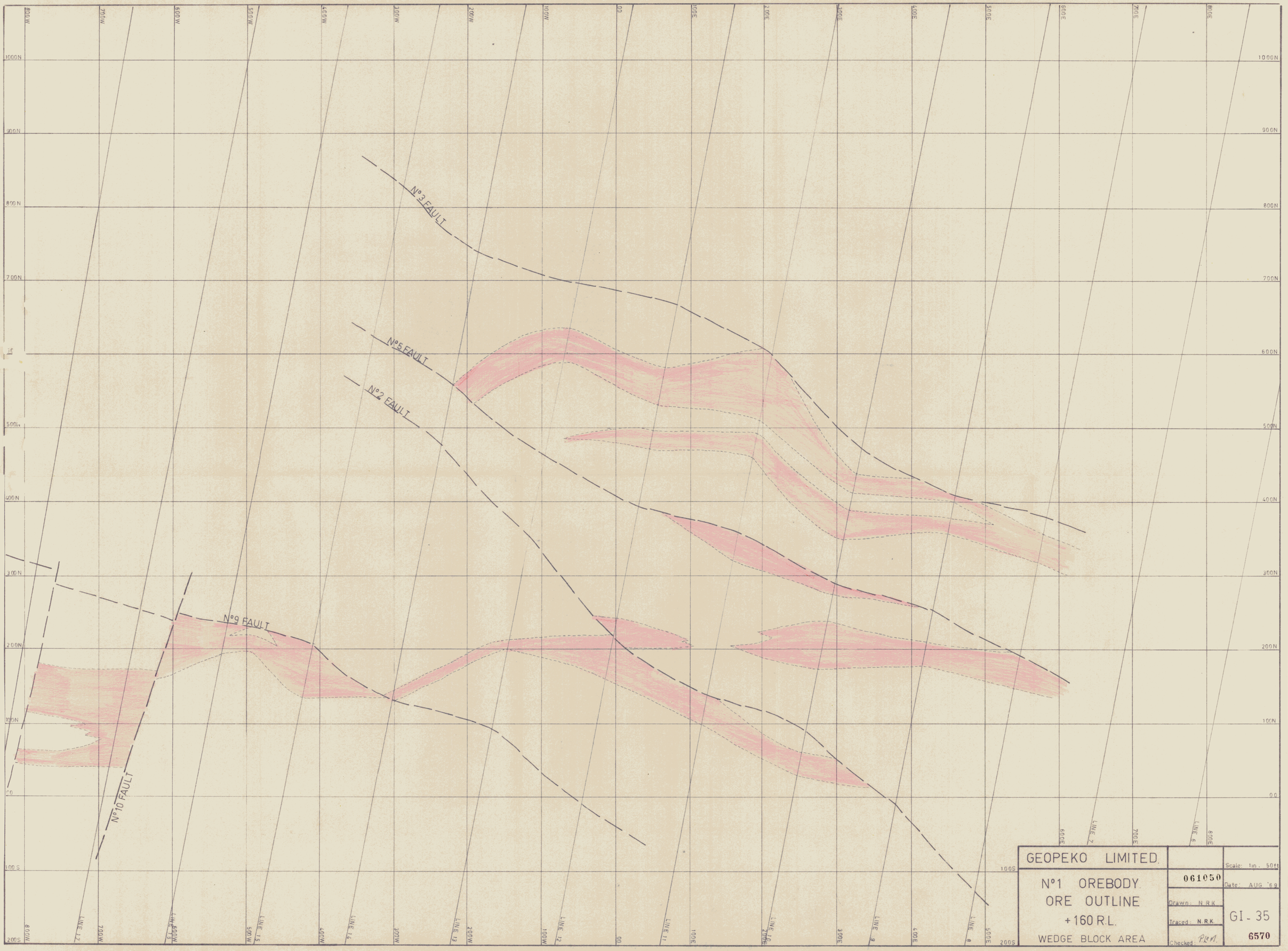

N°3 FAULT
N°5 FAULT
N°2 FAULT
N°9 FAULT
N°10 FAULT
5 cm
GEOPEKO LIMITED
N°1 OREBODY.
ORE OUTLINE.
+100 R.L.
WEDGE BLOCK AREA
061048
DRAWN: N.R.K.
TRACED: N.R.K.
CHECKED
SCALE: 1in = 50ft
DATE: AUGUST '69
GI-33
6568

34

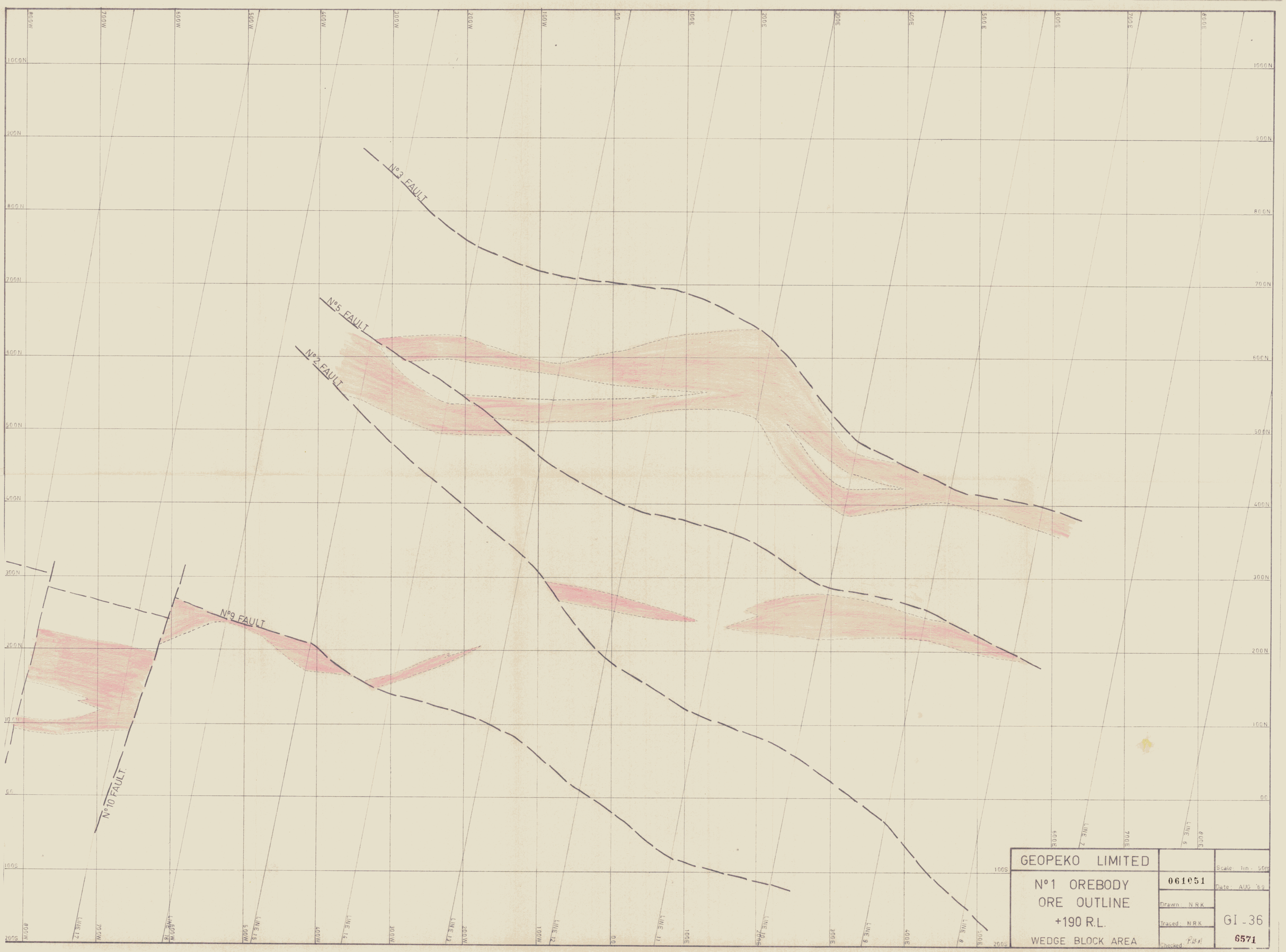


GEOPEKO LIMITED		Scale: 1in. : 50ft.
No 1 OREBODY ORE OUTLINE. +130 R.L. WEDGE BLOCK AREA	061049	Date: AUG. '69
	Drawn: N.R.K.	GI 34 6569
	Traced: N.R.K.	
	Checked: A.G.M.	

35

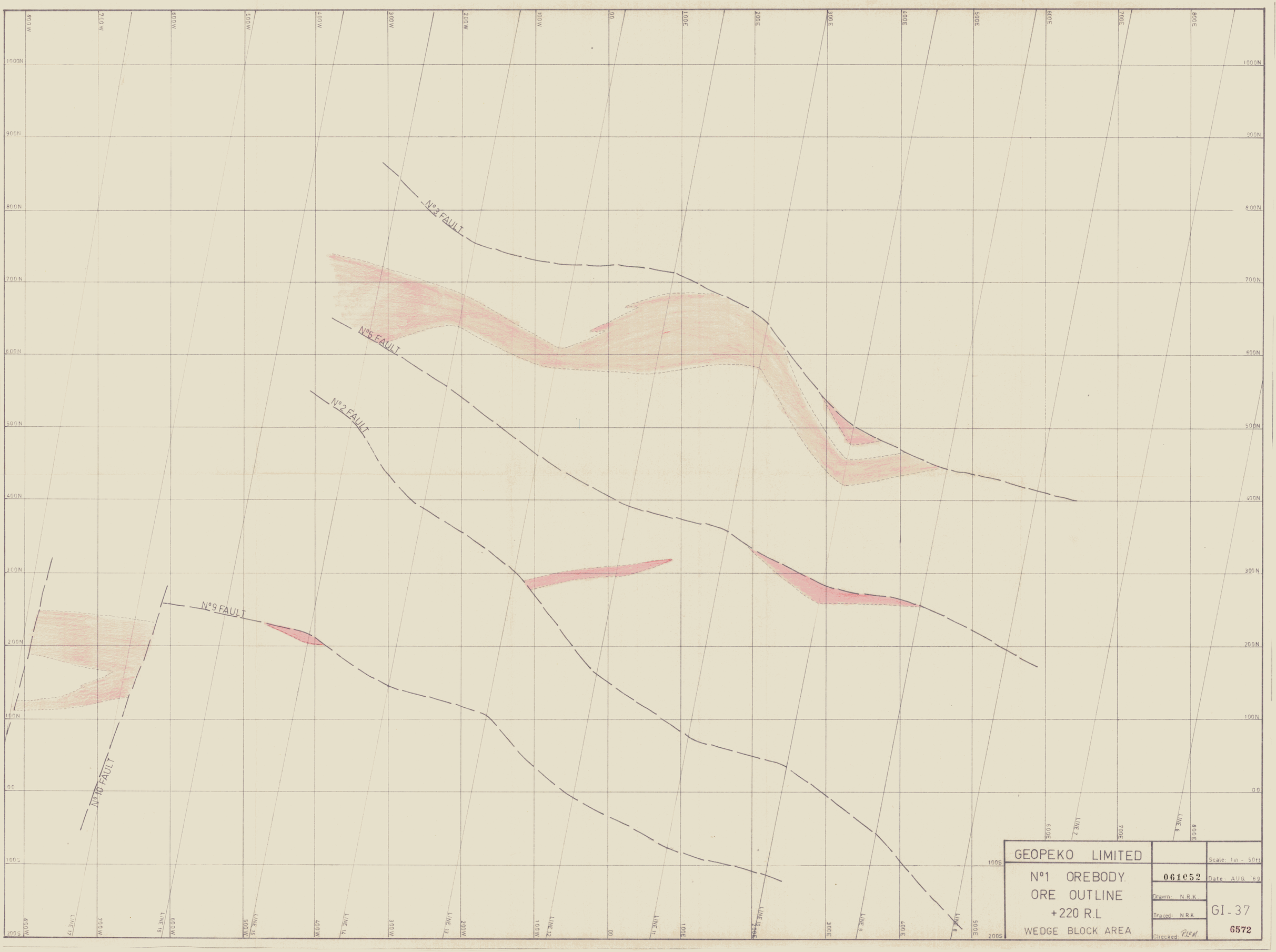

N°3 FAULT
N°5 FAULT
N°2 FAULT
N°9 FAULT
N°10 FAULT
1000N
900N
800N
700N
600N
500N
400N
300N
200N
100N
0.0
100S
200S
1000N
900N
800N
700N
600N
500N
400N
300N
200N
100N
0.0
100S
200S
5cm
GEOPEKO LIMITED
N°1 OREBODY
ORE OUTLINE
+160 R.L.
WEDGE BLOCK AREA
061050
Drawn: N.R.K.
Traced: N.R.K.
Checked: P.L.M.
Scale: 1in. 50ft
Date: AUG '69
GI-35
6570

36



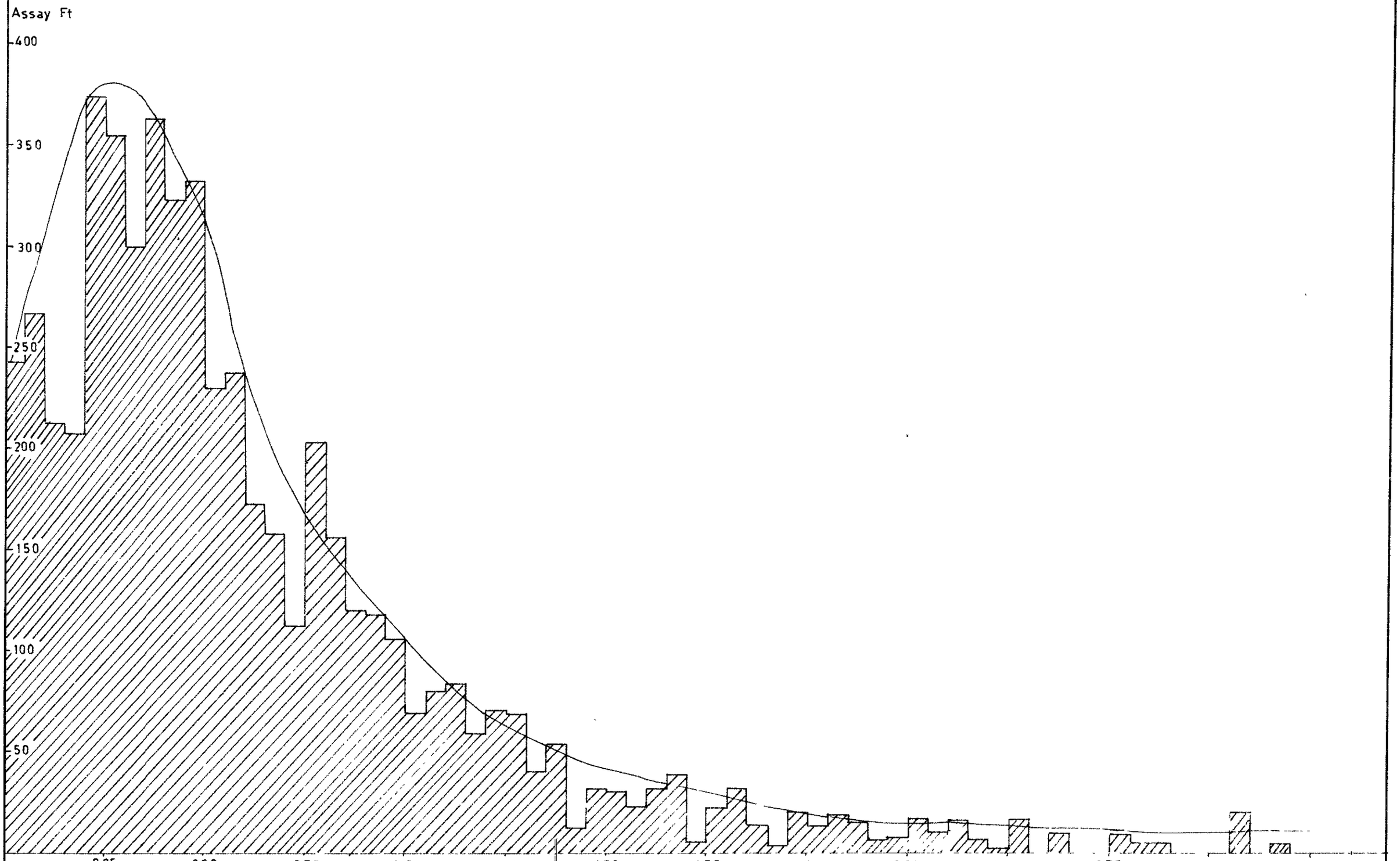
GEOPEKO LIMITED		Scale: 1in. = 50ft
No1 OREBODY ORE OUTLINE +190 R.L. WEDGE BLOCK AREA	061051	Date: AUG '69
	Drawn: N.R.K.	GI-36
	Traced: N.R.K.	
	Checked:	6571

37



GEOPEKO LIMITED		Scale: 1in - 50ft
N°1 OREBODY ORE OUTLINE +220 R.L WEDGE BLOCK AREA	061052	Date: AUG. '69
	Drawn: N.R.K.	GI-37
	Traced: N.R.K.	
	Checked: P.L.M.	6572

38



061053

5 cm

GEOPEKO LTD

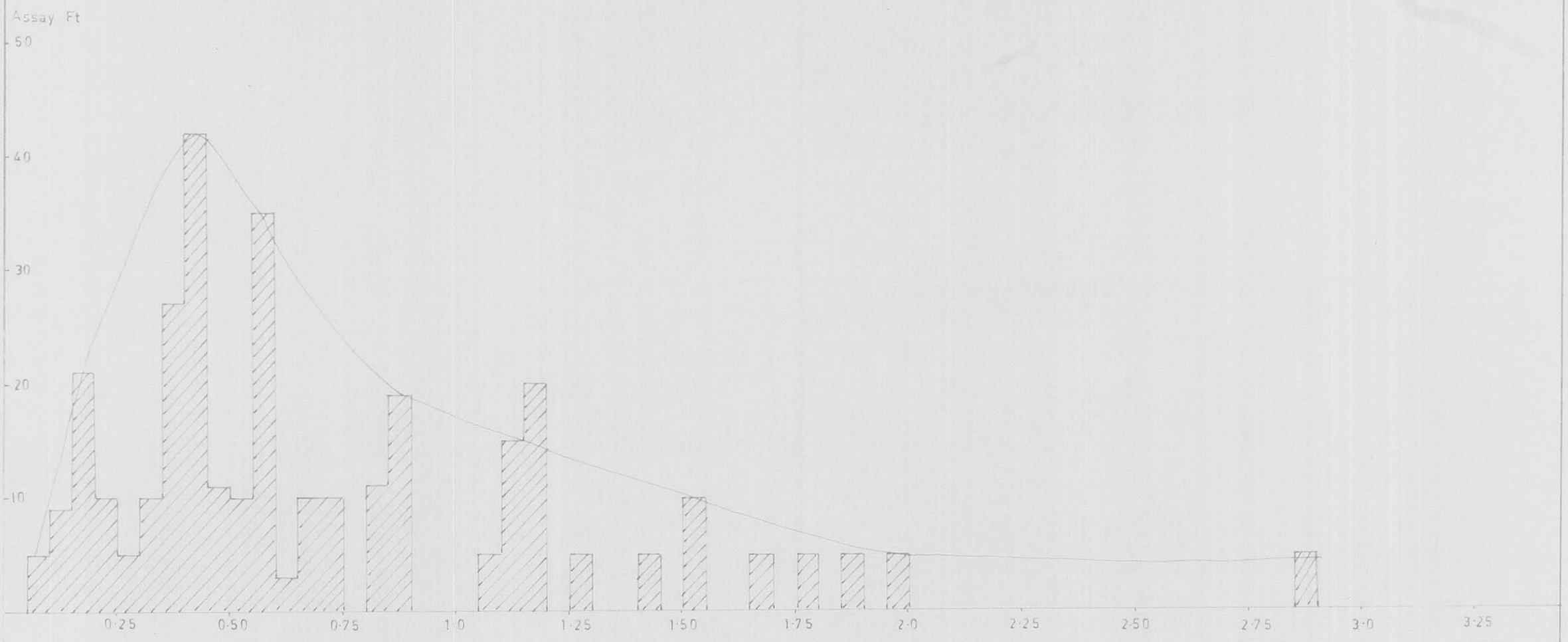
ASSAY HISTOGRAM
C LENS
N° 1 OREBODY

Drawn A.MT.
Traced A.MT
Checked P. Lem

Scale
Date AUG 69

GI-38
6573

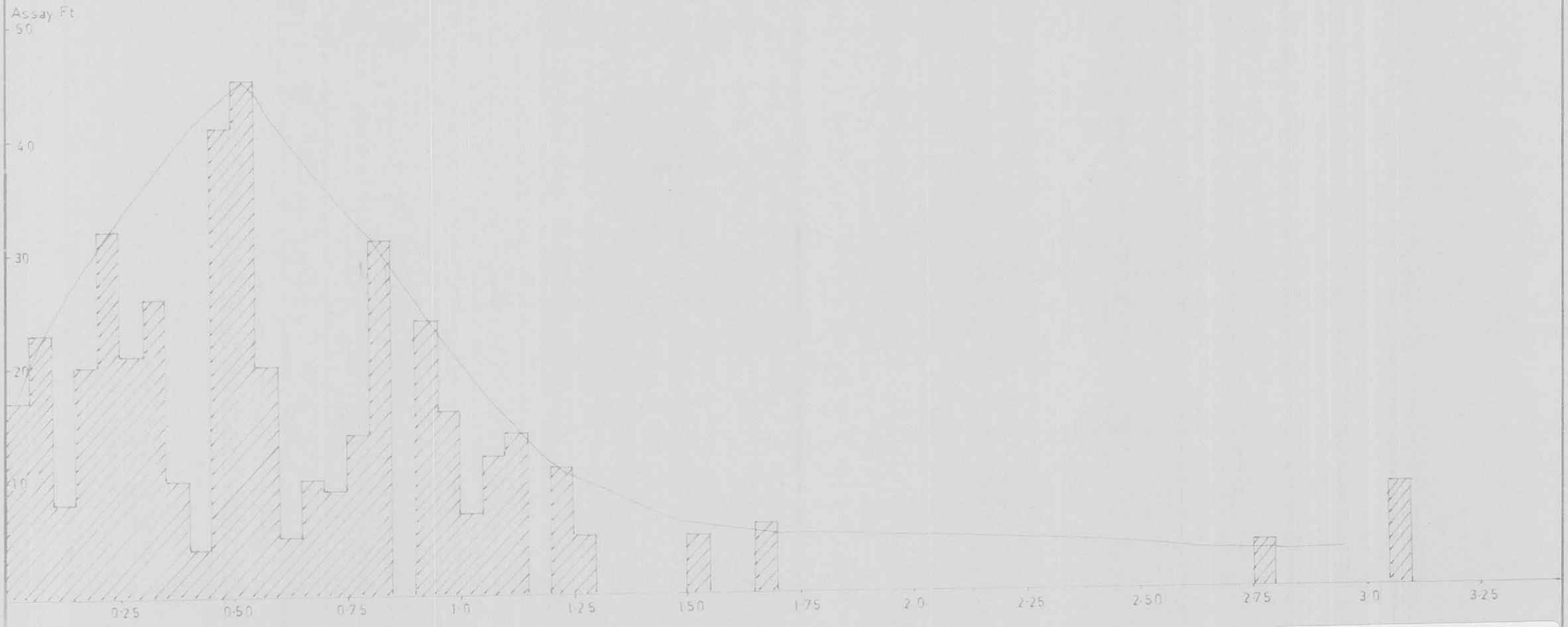
39



5 cm

061054

GEOPEKO LTD		Scale :
ASSAY HISTOGRAM C LENS LINE 2S Nº1 OREBODY	Drawn : AMT Traced : AMT Checked: PLeM	Date : AUG 69 GI-39 6574



5 cm

061055

GEOPEKO LTD		Scale :
ASSAY HISTOGRAM C LENS LINE 13 N° 1 OREBODY		Date : AUG 69
	Drawn : AMT Traced : AMT Checked : P Lem	GI-40 6575