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PENNZOIL OF AUSTRALIA LIMITED

FINAL REPORT ON EXPLORATION

LOONGANA

E.L. 2/76

TASMANIA

J. Chapman
Advanced Geologist

May, 1979

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Transparencies in Veltiplan

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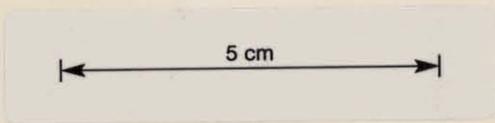
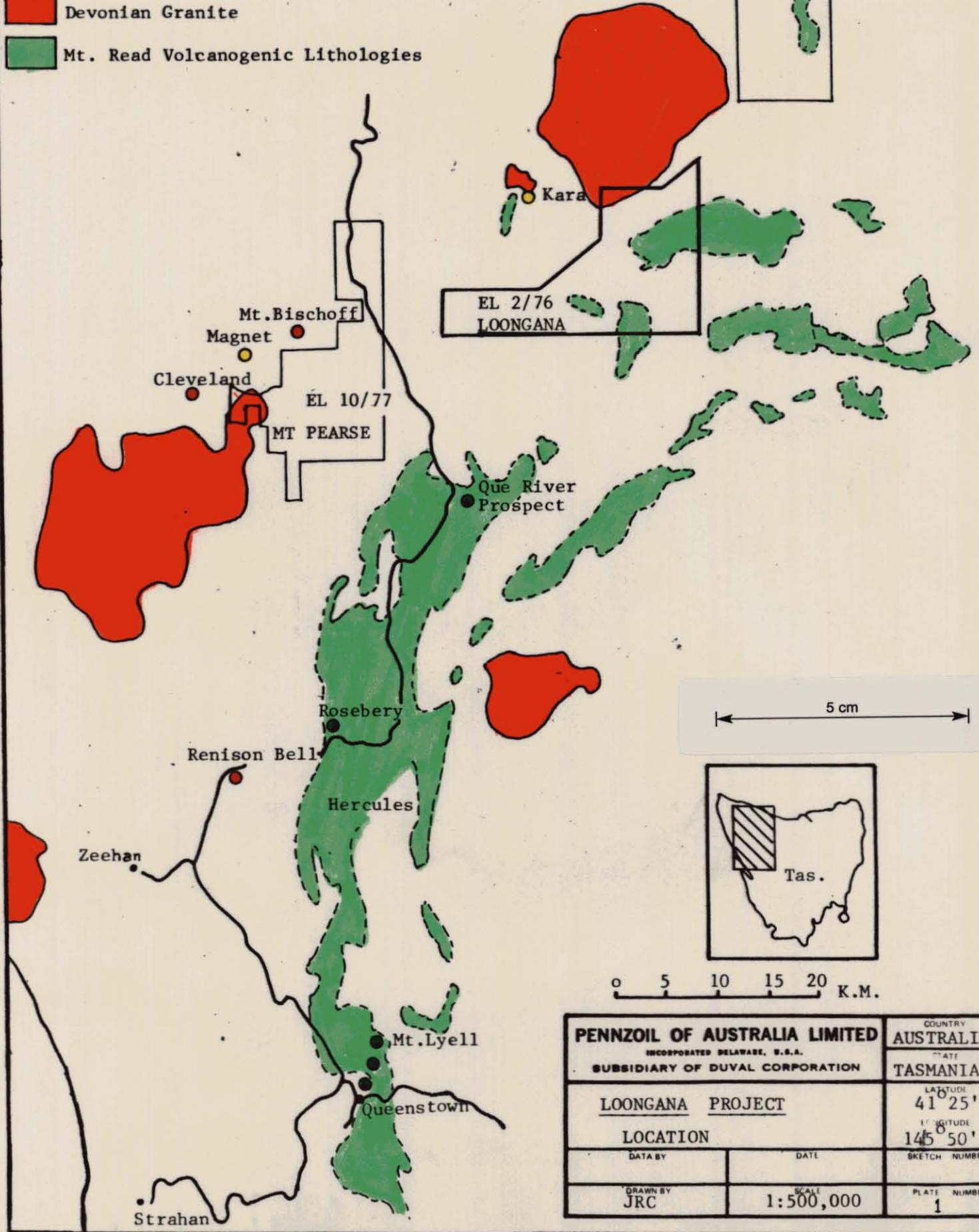
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- Volcanogenic Deposit
- Major Tin Deposit
- Hydrothermal/Metasomatic Mineralisation

- Devonian Granite
- Mt. Read Volcanogenic Lithologies

DIAL RANGE

Ulverstone



0 5 10 15 20 K.M.

PENNZOIL OF AUSTRALIA LIMITED <small>INCORPORATED DELAWARE, U.S.A.</small>		COUNTRY AUSTRALIA
SUBSIDIARY OF DUVAL CORPORATION		STATE TASMANIA
LOONGANA PROJECT		LATITUDE 41° 25'
LOCATION		LONGITUDE 145° 50'
DATA BY	DATE	SKETCH NUMBER
DRAWN BY JRC	SCALE 1:500,000	PLATE NUMBER 1

003

INTRODUCTION

Exploration Licence 2/76 (the Loongana Project) covering 195 square km in North West Tasmania is jointly held by Peko-Wallsend Operations Limited, Geopeko Division (Geopeko), and Electrolytic Zinc Company of Australasia Limited (E.Z.). In March 1978 Pennzoil was offered joint venture participation in the project. After a review of the exploration data and a field inspection, Pennzoil entered the Joint Venture by way of a letter of intent on 27th July 1978.

The main criteria for participation was the untested volcanogenic base metal potential of the Challenger III environment. Pennzoil adequately tested this environment without success. The remaining potential of this and other targets within E.L. 2/76 was not considered good enough to warrant continued participation, and Pennzoil withdrew from the Joint Venture on 11th April 1979.

GEOLOGICAL SETTING

The project area is situated within the West Tasmanian section of the highly productive Palaeozoic Tasman Orogenic Zone. This tectonic setting is host to the major tin deposits of Renison Bell and Cleveland and the volcanogenic base metal deposits of Mt. Lyell, Rosebery and Que River (Plate 1).

Briefly the local geology consists of inliers of the Cambrian Mt. Read volcanics and related sedimentary rocks surrounded by predominantly Cambro-Ordovician sedimentary sequences and flat lying basalt of Tertiary age. The Devonian Mt. Husetop granite intrudes the pre-Devonian rocks in the northern portion of the E.L. (Plate 2).

A comprehensive description of the geology is contained in Geopeko's annual progress reports on E.L. 2/76 by M. Rogers (1976) and G. Buckland (1977).

PREVIOUS WORK

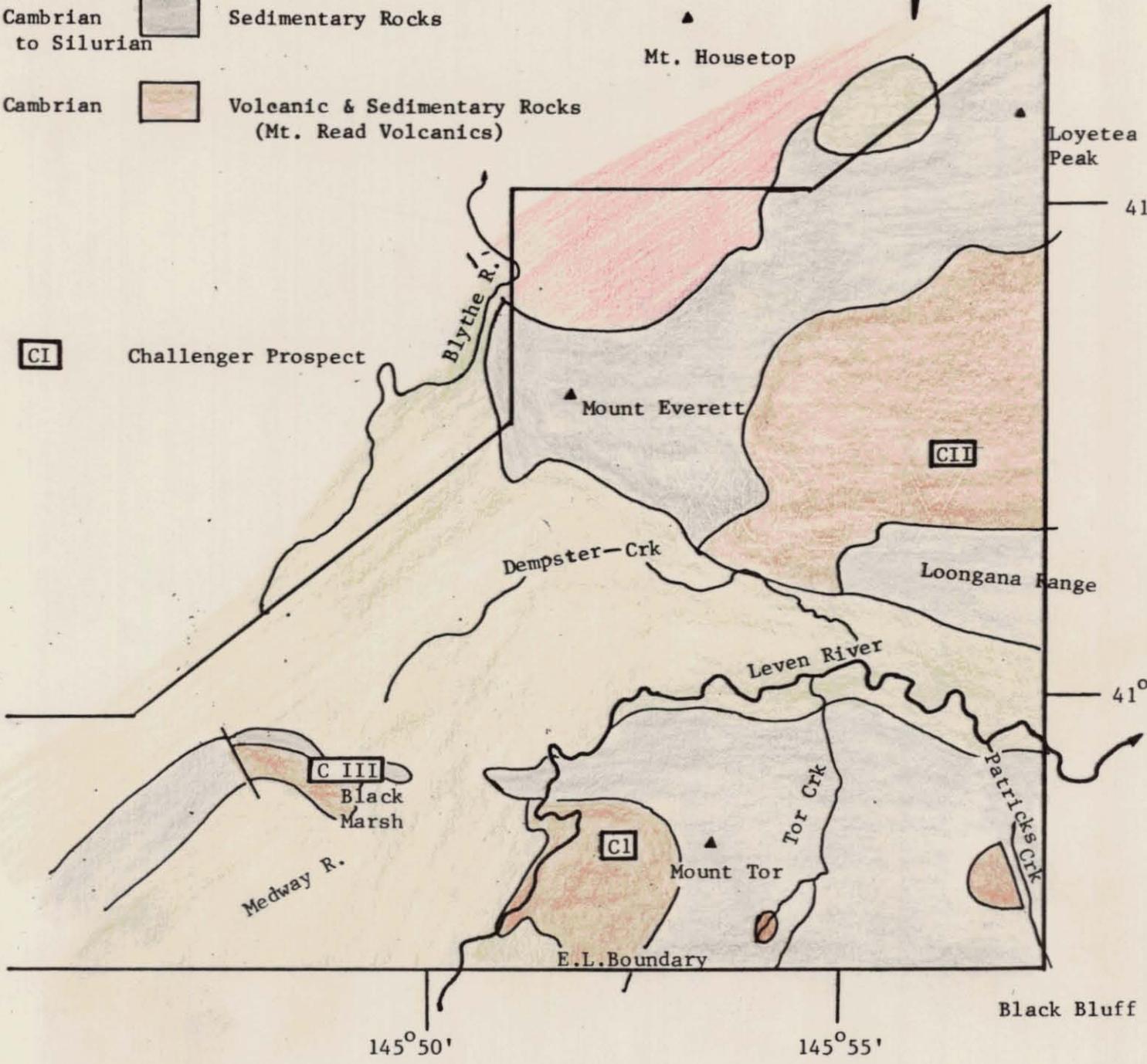
Prior to the granting of E.L. 2/76 no systematic base metal exploration had been carried out in the area. Australia and New Zealand Exploration Company (ANZECO), in a Joint Venture with Tasminex, had executed a skarn exploration program with little success.

From 1976 to 1978 Geopeko, the managers of the Geopeko - E.Z. Joint Venture, undertook a comprehensive program of mapping and stream sediment sampling of the Cambrian inliers. This phase outlined three main prospective areas designated Challenger I, II and III that were further evaluated by gridding, soil and rock geochemistry and detailed geological mapping. No drill targets emerged from this follow-up work. At this stage Geopeko and E.Z. decided to invite participation by a third party in the Joint Venture. The results of Geopeko's exploration program are fully documented in the annual progress reports by M. Rogers (1976) and G. Buckland (1977).

LEGEND

- Tertiary Basalt
- Devonian Granite (Mt. Housetop Gt.)
- Cambrian to Silurian Sedimentary Rocks
- Cambrian Volcanic & Sedimentary Rocks (Mt. Read Volcanics)

G.N.
T.N. M.N.



5 cm

PENNZOIL OF AUSTRALIA LIMITED		COUNTRY
INCORPORATED DELAWARE, U.S.A.		Australia
SUBSIDIARY OF DUVAL CORPORATION		STATE
		Tasmania
LOONGANA E.L. 2/76		LATITUDE
PROSPECT LOCATION		41° 20'
		LONGITUDE
		145° 50'
DATA BY	DATE	SKETCH NUMBER
	MAY 1979	
DRAWN BY	SCALE	PLATE NUMBER
JRC	1:100,000	2

CRITERIA FOR PENNZOIL PARTICIPATION

Pennzoil's decision to participate in the project was based primarily on the untested potential of the Challenger III prospect. Here a black shale horizon, anomalous in lead (maximum 1400 ppm) and zinc (maximum 1760 ppm), occurs in a volcanic sequence of amygdaloidal rhyolite, ash flow lithic crystal tuffs, vitric tuffs/lavas and some tuffaceous sediments. Good lead soil geochemical anomalies are associated with the shale and other lithologies and barite mineralisation occurs in fissures in the volcanics. The importance of geochemically anomalous black shales as ore horizon lateral facies variants in volcanogenic environments was considered pertinent to this locality, occurring only 20 km along strike from the Que River base metal deposit.

With the exception of a magnetometer survey no geophysics had been employed by Geopeko. The Rapid Reconnaissance Induced Polarization (RRMIP) system was considered ideal for the evaluation of this prospect, much of which is concealed by superficial buttongrass swamp. Specifically we hoped to be able to geophysically trace and test the black shale horizon beneath surrounding Tertiary basalt cover.

Familiarization of the area would enable Pennzoil to evaluate the feasibility of pursuing other potential targets.

These included:-

1. Geophysical evaluation of the Challenger II prospect.
2. Skarn exploration along the Mt. Husetop Granite contact.
3. Evaluation of untested stream sediment geochemical anomalies generated by Geopeko's reconnaissance program.
4. Exploration for undiscovered acid volcanic inliers occurring south of the Leven River.

SUMMARY OF WORK PROGRAMChallenger III

- a) Fill in auger soil sampling (68 samples) was used to better delineate the anomalies generated by Geopeko.
- b) A reorientated grid (14 line km) was cut, pegged and surveyed with the RRMIP system.

Reconnaissance

- a) Geological reconnaissance and stream sediment sampling was carried out in the headwaters of Patricks and Tor Creeks.
- b) Geological reconnaissance and selected stream sediment sampling was carried out along the Mt. Husetop Granite contact.

BASE METAL RECONNAISSANCE (Refer Map No. 48322)

Expectations of the presence of undiscovered Cambrian acid volcanic inliers occurring to the south of the Leven River led to limited reconnaissance of this area.

Patricks Creek Area

The cropping out of a varied sequence of predominantly acid tuffs was confirmed

to the south and west of the headwaters of Patricks Creek. The creek itself forms a fault boundary to the inlier and the volcanic and associated sedimentary lithologies of the inlier are variably (intensely in part) foliated due to north west oriented shearing. Steep terrain and thick vegetation prevented detailed mapping of the area.

Stream sediment samples were collected from Patricks Creek and north flowing tributaries. No anomalous results were generated. (Maximum values - 10 ppm Cu, 60 ppm Pb, 130 ppm Zn.)

Tor Creek Area

Tor Creek and its tributaries were sampled from approximately 5km upstream, northwards to its confluence with the Leven River. No geochemical anomalies were encountered (Maximum values - 10 ppm Cu, 10 ppm Pb, 25 ppm Zn) At the southernmost sample locality float of andesitic tuffs indicate that Cambrian volcanics crop out further upstream. The inaccessability of this area and the limited quantity of volcanic float however, deterred further reconnaissance.

From the results of the Patricks Creek and Tor Creek reconnaissance Pennzoil does not consider further work is justified in these areas.

SKARN RECONNAISSANCE (Refer Map No. 48321)

Geopeko's work along the Mt. Housetop granite contact consisted of reconnaissance geology and limited stream sediment sampling. The sampling was conducted in the vicinity of a tungsten anomaly previously generated by ANZECCO. The anomaly was not repeated.

Pennzoil's approach was to evaluate the potential of carbonate rocks (or their metamorphosed equivalent), which could act as a host to skarn mineralisation, occurring in proximity to the granite.

Reconnaissance geology failed to locate any evidence for outcropping carbonates except for sporadic minor calc-silicate banding in the hornfelsed Ordovician clastic sequences. Regional structural interpretation however, does indicate the possibility of Gordon Limestone occurring within the contact aureole just outside E.L. 2/76 in the Loyetee area and the Blythe River/Mt. Everett area.

Selected stream sediment geochemistry carried out in conjunction with the geological reconnaissance did not produce any significant results.

The importance of this contact zone is emphasised by the occurrence of skarn mineralisation currently being prospected by Commonwealth Aluminium Corporation (Comalco) outside the northern boundry of E.L. 2/76 at Loyetee. The best method of further exploration in this zone would be by means of an airborne magnetic survey. However the potential is not considered sufficient to justify the substantial cost of such a survey.

CHALLENGER III

Previous Work

Geopeko's exploration of the Challenger III prospect involved detailed geological mapping (Refer Map No. 48323) and deep auger soil sampling on a 50 metre by 200 metre grid spacing. In addition a magnetic survey was used to outline the edge

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of the basalt and detailed auger sampling was carried out over the prominent black shale horizon.

Geochemistry (Refer Map Nos 48324 to 48326)

Fill in deep auger soil sampling was used by Pennzoil to better define the lead anomalies produced by Geopeko. This sampling confirmed the patterns previously evident, i.e. low order anomalies (200ppm to 400ppm) following lithological strike, particularly the black shale horizon and a crystal tuff. These anomalies contain spot highs of up to 880ppm Pb. It appears that spot lead highs of this order are common within certain environments in the Cambrian volcanics and do not necessarily indicate substantial mineralisation. It is unknown whether the lead occurs disseminated through the host rock or in small sulphide veins. The persistent association of lead anomalies with shale horizons within the volcanics suggest that some of the anomalies over tuffs at Challenger III may be derived from undetected minor shale intercalations.

Zinc results are generally low except for a spot high of 820ppm and those results that are weakly anomalous correlate only approximately with the lead anomalies. No significant copper results were obtained.

It is concluded that the anomalies generated at Challenger III do not represent significant mineralisation but do indicate a prospective environment for base metal accumulations.

Geophysics (Refer Map No. 48327)

a) Introduction

The RRMIP system was used to test the subsurface environment of the Cambrian inlier and to follow this environment, specifically the black shale horizon, along strike beneath the basalt.

A reoriented grid to conform with local strike was installed with 200 metre spacing between lines. Readings were taken at 25 metre intervals along lines of 1km length. Electrode spacing was 1.8km and 3 arrays were required to survey the grid. Electrode location and other information is incorporated with the computer plotted profiles in Appendix A.

Some background information on the RRMIP system is incorporated in Appendix B.

b) General Comment on Results

This survey gave us an excellent opportunity to study the effect that overlying basalt has on bedrock responses. All three arrays had one electrode in basalt and the other in bedrock and all three had varying thickness and amount of basalt cover. The interpretation of the RRMIP results is based on the geology as mapped by Geopeko with minor additions by Pennzoil.

First some general observations that appear applicable here as on other projects.

The reliability of the Relative Phase Shift (R.P.S. - represents chargeability) results appear to be dependant on the intensity of current flow within the circuit. With approximately 2km electrode spacing, a

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low current e.g. 3 amps tend to give high but variable R.P.S. readings. In this situation it is suspected that "noise" is substantially affecting the readings inevitably giving rise to false or pseudo anomalies. With a higher current flow e.g. 4 amps the R.P.S. values are lower but profiles are smoother reflecting less "noise" contamination. This phenomenon gives rise to two distinctive features.

1. With a low current circuit the low current densities occurring at the end of lines, mainly the lines closest to the electrodes, results in an increase in the R.P.S. levels giving "valley" shaped profiles.
2. With a low current, cultural features and specifically the magnetic field generated by the circuit loops ("wire effect") can contaminate to the extent of obscuring meaningful results in portions of the array.

c) Results

The more prominent results of the survey are:

1. A line of moderate Magnetometric Resistivity (M.M.R. - represents conductivity) anomalies (maximum 17%) occur immediately east of the base line from 1800S 1025E to 2600S 1075E. There is no R.P.S. contrast over these anomalies indicating a lack of substantial sulphides within the trend.

These anomalies coincide with the black shale horizon. To the north of 2600N this unit is cut off by an unconformity while to the south the anomalous response of the shale is masked by the conductive basalt. Significantly the anomaly is evident on line 2600S where, because of its outcrop configuration with respect to the electrodes, the covering basalt has not masked the response from the shale.

2. A line of similar, although of lesser magnitude, M.M.R. anomalies occurs from 2200S 1250E to 2600S 1350E. This trend occurs over a crystal lithic tuff unit with possible shale intercalations that is anomalous in lead. Again the lack of associated anomalous R.P.S. results implies a lack of substantial sulphides.
3. Strong M.M.R. levels occur over basalt where good current pathways between the electrodes exist, e.g. on lines 1200S to 2000S where the basalt contact is approximately aligned with the current flow. Where the basalt is impersistent and thin e.g. around 1800S 1200E there appears to be little effect on the M.M.R.

These high M.M.R. levels have the effect of masking the bedrock M.M.R. responses and is the cause of the attenuation of the anomalies described in (1) & (2) above.

Sounding of the basalt elsewhere in Tasmania indicate a resistivity of about 80 ohm metres. Thus a sulphide body would necessarily be substantially more conductive than this if its response is to be seen through a thick cover of basalt.

4. Significantly the survey has shown no contrast in chargeability (R.P.S.) between the Cambrian rocks and the basalt. This suggests that no masking will take place if a chargeable source lies beneath the basalt. Two weak R.P.S. anomalies at 2400S, 625E and 2600S 1400E are not considered significant.

5. A distinctive broad, strong M.M.R. anomaly is centred on 300S 1150E with a similar anomaly but of lesser magnitude situated on the adjacent line (3200S 1125E). This is interpreted as being due to either thicker basalt, filling a pre-existing depression e.g. a creek, or a sub-basaltic aqueous saturated unit such as a deep lead or swamp derived clays.

CONCLUSIONS

Pennzoil's participation in the Loongana Joint Venture was based primarily on the potential of the Challenger III prospect.

The soil geochemical and RRMIP surveys have adequately tested this locality and results indicate additional work is not warranted. The main findings from the RRMIP survey are:-

1. Moderate conductive but nonchargeable ("E type") anomalies are caused by the black shale. Response from the shale is masked where covered by basalt preventing the tracing of this unit any practicable distance beneath the basalt.
2. No significant chargeable anomalies were encountered indicating no strong concentration of sulphides.

Two new inliers of acid volcanics were identified south of the Leven River but these are of limited extent and do not warrant extensive exploration.

The Mt. Housetop granite contact zone remains prospective for skarn mineralisation but the potential is not sufficient to justify any substantial exploration effort.

Pennzoil does not consider the potential of the above targets, and others generated by Geopeko, sufficient to warrant continued joint venture participation.

LIST OF INCLUSIONS

Appendix A	Computer plotted RRMIP profiles.
Appendix B	RRMIP Information
Appendix C	Expenditure on E.L. 2/76
Map No. 48321	Skarn Recon: Geology/Geochem.
48322	Camb. Recon: Geology/Geochem.
48323	Challenger III Geology
48324	Challenger III Geochem Cu.
48325	Challenger III Geochem Pb.
48326	Challenger III Geochem Zn.
48327	Challenger III Geophysics RRMIP.

APPENDIX A

The R.R.M.I.P. survey at Loongana was carried out by Scintrex Pty. Limited on the Loongana Area between 26th January and 3rd February 1979. The results of the survey are presented in the form of computer plotted line printographs included in this report.

APPENDIX B

Enclosed is some Scintrex derived information on the R.R.M.I.P. system, the parameters used and some typical anomaly forms.

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**Frequency Domain
IP Measurements using
Harmonically Related Components**
Application Brief 76-1

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FREQUENCY DOMAIN IP MEASUREMENTS USING HARMONICALLY RELATED COMPONENTS

INTRODUCTION

The earliest and still most prevalent method of IP measurement in the frequency domain entails the comparison of earth resistivities at two widely spaced frequencies, often a decade apart. Such comparisons require, in fact, four measurements, two of current and two of voltage, using sequential transmission of current at the two frequencies. Usually a constant current source is employed which, within certain limits of load variation, keeps the ground current constant.

In any event, the traditional frequency domain method, producing the so-called PFE or Percent Frequency Effect, requires at least two measurements of voltage, a constant current source and, for greater accuracy, a measurement of the deviation of the primary current between the two measurements. The errors entailed in these measurements are additive, of course.

More recently, a second method of IP measurement in the frequency domain has come into use, in the form of the phase angle between measured voltages in the ground and the primary current. Publications by Katsube and Collett (1973), Zonge (1975) and Wynn (1975), Hall of (1974), Van Voorhis (1973), Hohmann (1975) and Seigel (1974) show the general equivalence of the measurement of the phase angle θ , at a specific frequency in the IP range, with the P.F.E. over two frequencies spanning this range.

One of the obvious advantages of phase angle measurement is that only a single frequency need be transmitted, not two frequencies sequentially, as in the older PFE measurement. Also the necessity of rigid current stabilization is eliminated. Less obvious are its disadvantages. Firstly there is the necessity of providing a phase, or time reference. This has usually been accomplished by one of two schemes, firstly radio transmission of a reference phase and, more popularly, through the use of two matched and synchronized crystal clocks. The first suffers from the usual problems of radio links, viz. blind spots and licensing problems. The latter is more successful, although requiring additional instrumentation and periodic synchronization from time to time for high accuracy.

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The second problem with phase angle measurements is that they are rather more susceptible to E.M. induction effects than are the equivalent PFE measurements, because they are quadrature measurements and PFE's are amplitude (mainly in-phase) measurements. Most IP workers who have the common misfortune to work in geologic environments which include moderate-to-highly conducting near-surface formations, have found that electromagnetic induction effects are particularly troublesome. In order to attempt the removal of these E.M. effects from the observed phase angles and thereby reveal the true IP contribution, various workers have proposed the measurement of phase angles at two or more frequencies; (eg. Hall of (1974) and Wynn and Zonge (1975)). In general, it is clear, that it would be foolhardy to measure phase angles at only one frequency in such an environment. To yield interpretable phase angle results, one must, therefore transmit currents with at least two widely spaced frequencies, bringing us back to the old PFE requirement.

Once one returns to a multi-frequency approach one might as well measure complex resistivities at each frequency. The totality of this information may be employed in an attempt to strip the EM coupling effects (eg. Hall of (1974) and Wynn and Zonge (1975) and to differentiate between IP sources of differing natures (eg. Zonge (1975)).

THE IPRF-2 APPROACH

The current wave form commonly employed in frequency domain IP is a square wave, simply because it is easy to create by solid state switching. It is well known that a square wave contains the fundamental and its odd harmonics, each harmonic having an amplitude inversely proportional to its order. It has always been theoretically possible to use any of these various frequency components, transmitted simultaneously, in order to obtain the desired IP information. In practice this has been rather difficult to achieve instrumentally until the advent of active filters and phase locking.

The subject of this paper is a frequency domain IP receiver, the IPRF-2, which works on the principle of the simultaneous comparison of amplitude and phase of two or more harmonically related components transmitted simultaneously in a single square wave.

Figure 1 shows, in block diagram form, the basic operation of this receiver. The input is coupled to the preamplifier by a band pass filter which eliminates any D.C. component and attenuates harmonics of order higher than three, as well as higher frequency interferences such as power lines etc.

Two additional band pass filters separate the fundamental and the third harmonic components and feed them into separate phase lock loop circuits.

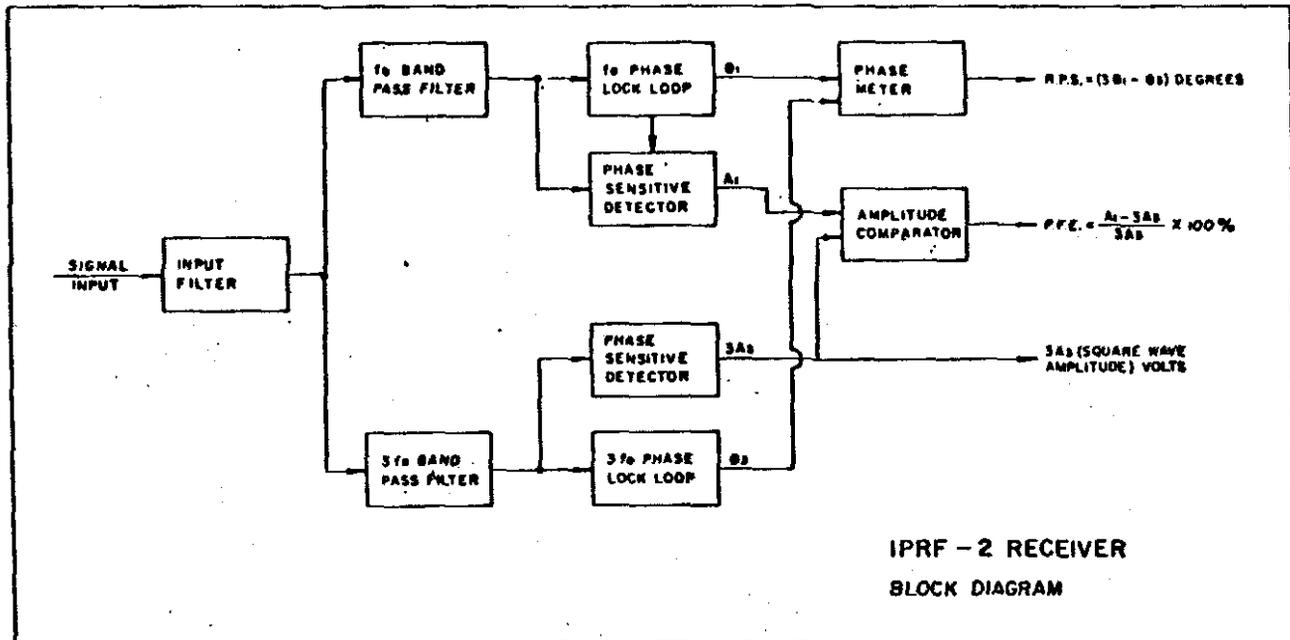


Figure 1

Phase sensitive detectors produce D.C. output voltages which are proportional to the amplitude A_1 of the fundamental and A_3 of the third harmonic of the input waveform. These two quantities are fed into an amplitude comparator, to produce the PFE (see below). The quantity A_3 is taken out separately, to be used as a measure of the square wave amplitude.

The relative phase (time shift) between the fundamental and third harmonic signals is compared on a phase meter which produces the RPS quantity (see also below).

QUANTITIES MEASURED

The quantities actually measured by the IPRF-2 are

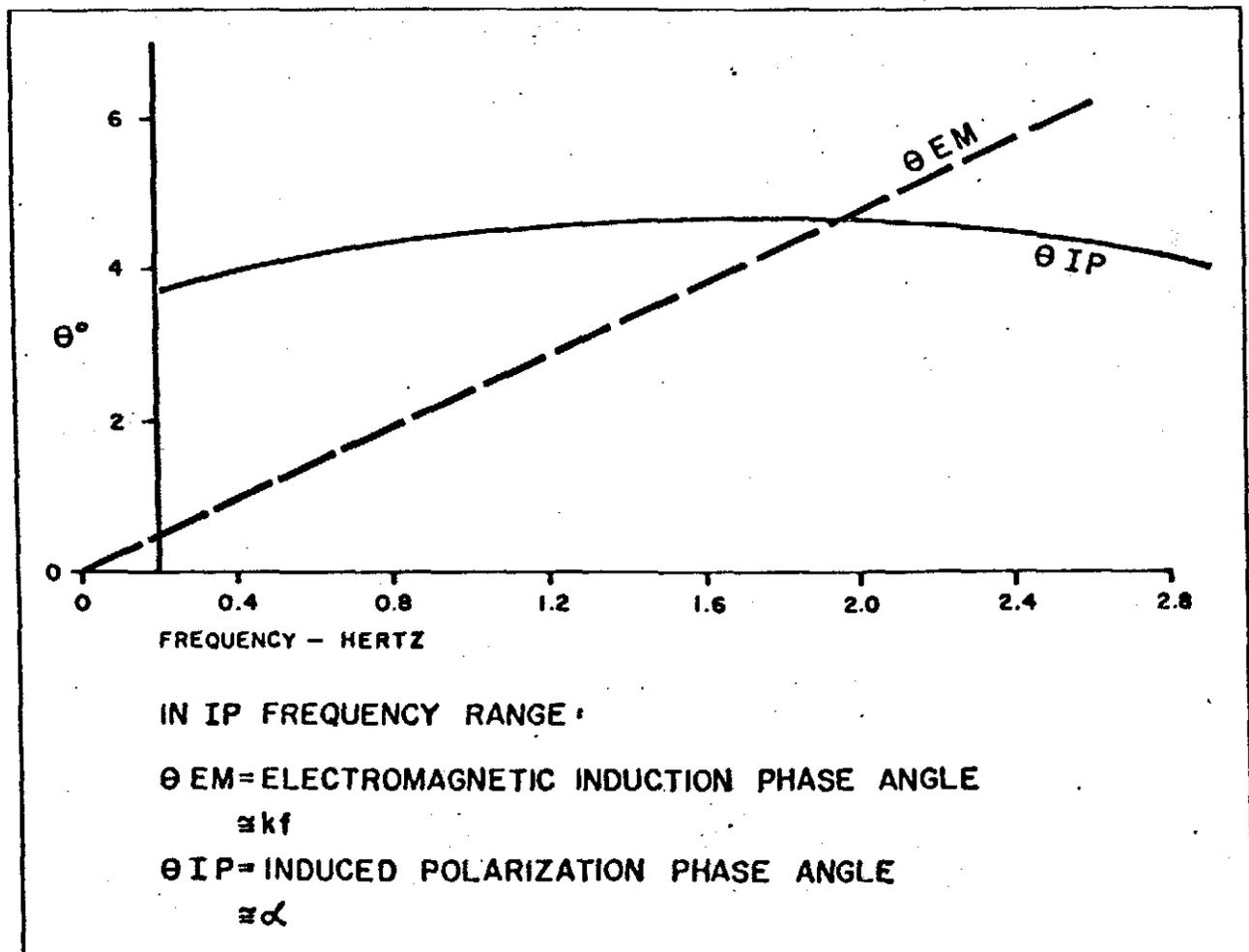
- a) The amplitude (A_3) of the square wave signal
- b) The PFE defined as $\frac{A_1 - 3A_3}{3A_3} \times 100\%$ where A_1 and A_3 are the amplitudes of the fundamental and third harmonic ground signal respectively, and
- c) The Relative Phase Shift or RPS, defined as $3\theta_1 - \theta_3$ where θ_1 is the phase lag of the measured voltage of the fundamental and θ_3 is the phase lag of the measured voltage of the third harmonic relative to the transmitted components of the current.

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The significance of the PFE measurement needs no comment. It is the classical frequency domain IP measurement, albeit only over a frequency difference of a factor of three rather than the more typical factor of 10. The resultant PFE's are therefore about one half of those observed over a decade change in frequency. This decrease in amplitude is more than compensated by the facts that a) the basic instrumental noise levels are less than 0.05% PFE and 0.05° RPS and b) the measurements are made simultaneously on the components of one square wave. These components will largely increase or decrease in the same proportion when the ground load changes (resistively). Measurements of PFE are thus largely unaffected by moderate ground load changes and, in fact, accuracies of 0.1% PFE are attainable with transmitters that are not current stabilized.

The significance of the RPS measurement is illustrated by Figure 2. All the field experimental evidence to date suggests that the IP phase lag θ is a slowly varying function of frequency and is, in effect, relatively constant over a factor of (say) three in frequency. Thus the RPS, as expressed by the IPRF-2, is very nearly $2\theta_1$. On the other hand, the phase shift due to

Figure 2



EM Induction in the earth is almost proportional to the frequency employed, at least at very low frequencies. This fact has been remarked upon by other workers in this field, such as Hall of (1974). - For phase angles of EM origin, within the limits of the validity of the proportionality of these angles with frequency, the RPS will therefore vanish, since $\theta_3 = 3\theta_1$.

We thus come to the interesting conclusion that the IPRF-2 automatically eliminates EM coupling effects, at least at a first approximation. Field results shown by Hall of (1974) and Wynn and Zonge (1975) from actual field cases in the western U.S.A. demonstrate that EM coupling is effectively removed by this means.

EM coupling is still present in the PFE measurement and divergence between the PFE and RPS values could reflect the influence of EM effects and indicate its presence.

So far, we have mentioned only the operation of the IPRF-2 on the fundamental and third harmonic, and the information that can thereby be determined. Since the primary current wave form has many more harmonics than these, other measurements are possible, providing that the signal strength is adequate. For example, the third harmonic may be used as a false fundamental, in which case the ninth harmonic becomes the false third.

If PFE and RPS measurements are also made using the third and ninth harmonic, then additional information becomes available for use in EM coupling elimination and in discrimination between different sources of IP response.

For example it can be shown that the quadratic frequency terms in the EM coupling in the PFE and RPS may be removed, using their values obtained by employing the original fundamental and then the third harmonic as a second fundamental. To be specific, if $(PFE)_1$ and $(PFE)_3$ and $(RPS)_1$ and $(RPS)_3$ are the respective values, then the EM quadratic-stripped values become

$$PFE = (9(PFE)_1 - (PFE)_3)/8$$

$$RPS = (9(RPS)_1 - (RPS)_3)/8$$

When measurements are made using more than one fundamental frequency, then one can use the results thereof to obtain a better approximation to actual phase angles θ rather than the RPS. For example, if f and $3f$ are used sequentially as fundamental frequencies, then

$$(RPS)_1 = 3\theta_1 - \theta_3 \text{ and } (RPS)_2 = 3\theta_3 - \theta_9$$

$$\text{Thus } (RPS)_1 + \frac{1}{3}(RPS)_2 = 3\theta_1 - \frac{\theta_9}{3} \approx \frac{8\theta_1}{3} \text{ (stripped of Induction effects)}$$

Based upon a large number of field experimental results, (eg. Scott, 1971) the normal equivalence between the two quantities measured by the IPRF-2 should be approximately given by

$$\text{RPS (degrees)} = 1.6 \text{ PFE (percent)} (\pm 10\%)$$

Any major departure from this equivalence would signify an anomalous ground response, EM coupling, measuring error, etc.

FIELD RESULTS

Figure 3 shows the IPRF-2 at work in the field.

Figure 4 shows a typical 2.5 kw transmitter being used in the field in conjunction with it.

Figure 5 shows PFE and RPS profiles over a small lead-zinc body in carbonate rocks, in the Pine Point area, Northwest Territories, Canada, together with the corresponding time domain chargeability and resistivity profiles. The similarity of all IP profiles may be noted. No attempt has been made to make the scales comparable on the various IP profiles. It can be deduced, from the regularity of the IPRF-2 field profiles that the noise level from all sources is less than 0.1% PFE and 0.1° RPS.

Figure 6 shows a 200' dipole-dipole profile over a standard test line in the Cavendish test range, Ontario. Two sulphide zones are known on this line, of which the one near 15W is more massive than the one near 9W. An operating frequency of 0.3 Hz was employed.

It is interesting to note that the westerly conductor is not as clearly indicated on the PFE values as on the RPS values. This may reflect the fact that EM induction effects are present.

SUMMARY

In summary, the IPRF-2 frequency domain IP receiver has the following novel features.

1. It operates on a single square wave, thus potentially speeding up the field procedure.
2. It is insensitive to slow changes in ground voltages, thus reducing the dependence on the primary current stabilization.



Figure 3

Figure 4

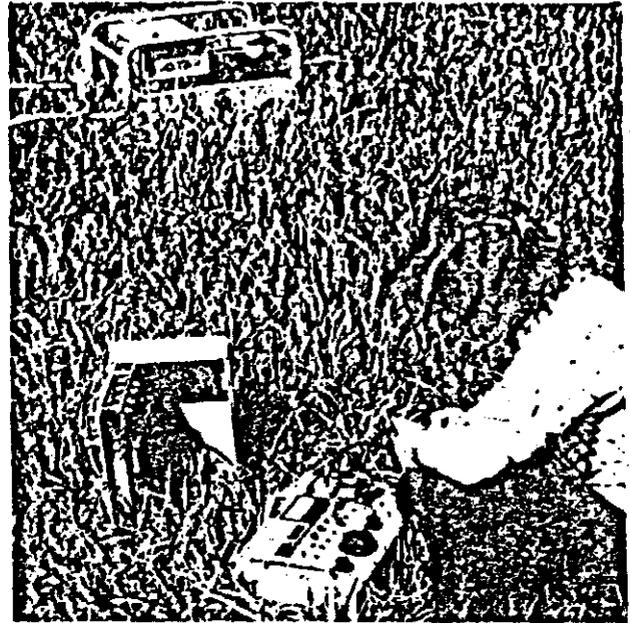
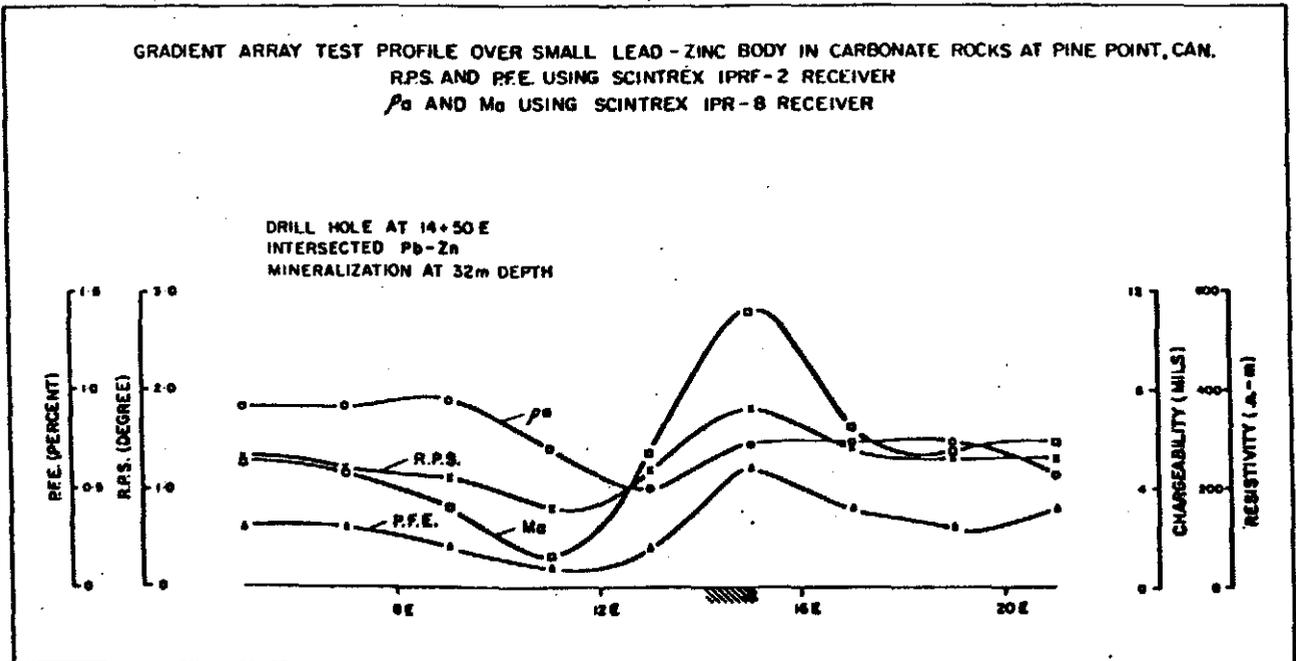


Figure 5



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- Zonge, K.L. and Wynn, J.C. 1975. Recent Advances and Applications in Complex Resistivity Measurements: Geophysics v.40, p.851-864

023

201024

19 AUG 1977

SCINTREX LIMITED

August 4, 1977

Dr. Graham Linford
 Scintrex Pty. Limited
 1031 Wellington Street
 West Perth, W. Australia 6005

Dear Graham:

In reply to your telex of August 1, 1977, I would like to summarize the various frequency domain MIP parameters which are presented.

The quantities measured by the IPRF-2 are H_p , RPS and PFE. From these parameters, other fields may be calculated to emphasize anomalous zones of high conductivity or high chargeability.

The first quantity, H_p is generated by the primary current flow in the ground. Since the distribution of the primary current flow is very much dependent on electrode location, it is useful to calculate H_N , as follows:

$$H_N = \frac{H_p}{H_{pNormal}} \times 100\% \quad \text{---- (1)}$$

The normalized magnetic field, H_N is calculated from the primary field, H_p by dividing it by the magnetic field that would be observed for the current distribution in a horizontally stratified earth, that is, if the earth were made up of a number of horizontal layers of the same or varying conductivities. It should be noted that the primary magnetic field is independent of the horizontal layering. Hence, H_N is a good indicator of zones of lateral inhomogeneities and detects anomalous conductors in the ground.

A different parameter is presented in the magnetometric resistivity (MMR) method and is termed MMR anomaly.

$$\text{MMR anomaly} = \frac{(H_p - H_{pNormal}) \times 100\%}{\left(\frac{200 I}{l} \right)} \quad \text{---- (2)}$$

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Dr. Linford

August 4, 1977

Page Two.

Hence, the normal primary field is subtracted from the observed primary field which is then normalized by the normal field midway between the current electrodes, $200 I$. This parameter is really a normalized secondary field component associated with anomalous current flow in the ground. Nigel Edwards claims that it is a more useful parameter than H_N to interpret by comparing it with theoretical curves. One problem, however, with this presentation is that conductors in regions of high current density are emphasized.

The next parameter is associated with the polarization characteristics of the ground and is termed relative phase shift, RPS. It is defined by

$$RPS = 3 \theta_1 - \theta_3 \quad \text{-----(3)}$$

where θ_1 = Phase shift of first harmonic relative to the transmitted waveform

θ_3 = Phase shift of third harmonic relative to the transmitted waveform

For a pure square wave, $3 \theta_1 = \theta_3$ and $RPS = 0$. It, of course, provides a first order correction for electromagnetic induction effects. Also, since there is little change in phase shift due to polarizability with change in frequency, the RPS is given approximately by 2θ , twice the IP phase shift.

The sign convention for the IPRF-2 is to represent the phase shift between the primary current, I_p and the secondary current, I_s within a polarizable body as positive so that directly over such a body where the interior current dominates, a positive RPS is observed and off to the sides of the body where the exterior current dominates a negative RPS is observed.

An alternate presentation to the RPS is the quadrature magnetic field H_{SQ} divided by the primary current level I defined by

$$\frac{H_{SQ}}{I} \approx \frac{H_p}{I} \sin \phi/2 \text{ where } \phi = RPS \approx 2 \theta$$

$\frac{H_{SQ}}{I}$ is usually expressed in milligammas per amp.

$$i.e. \frac{H_{SQ}}{I} = \frac{H_p}{I} \times 1000 \sin \left(\frac{RPS}{2} \right) \quad \text{----4.} \quad [m\gamma/r]$$

Dr. Linford

August 4, 1977

Page Three.

H_{SQ} is analogous to the MMR anomaly parameter defined by equation (2). It is the secondary field produced by quadrature current flow in the ground due to induced polarization. The H_{SQ} field emphasizes chargeable media in the central region where the current density is higher. The RPS, however, tends to enhance anomalies on the flanks. Clearly, there is an equivalence between H_{SQ} or RPS with H_S or M in the time domain.

The percent frequency effect, PFE is defined by

$$PFE = \frac{A_1 - 3 A_3}{3 A_3} \times 100\% \quad \text{----(5)}$$

where A_1 = Amplitude of first harmonic

A_3 = Amplitude of third harmonic

For a pure square wave, $3A_3 = A_1$ and $PFE = 0$. The sign convention is chosen so that a negative PFE is observed directly over a polarizable body and positive off to the sides.

There is also an alternate presentation to the PFE which is termed the in phase change H_{sp} , defined by

$$\frac{H_{sp}}{I} \approx \frac{H_p \times PFE \times 1000}{100 I} \quad [m\gamma/I] \quad \text{----(6)}$$

Again, H_{sp} is a secondary field associated with polarization characteristics and emphasizes anomalies in higher current density regions.

We present H_N together with the RPS and PFE or $\frac{H_{SQ}}{I}$ and $\frac{H_{sp}}{I}$.

201027

Page 111

026

Dr. Linford

August 4, 1977

Page Four.

I hope this summary will help you decide which presentation is most satisfactory for your surveys in the future.

Please let us know if you have any further questions about MIP presentation.

Best regards,

SCINTREX LIMITED

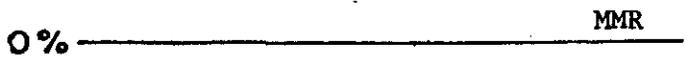
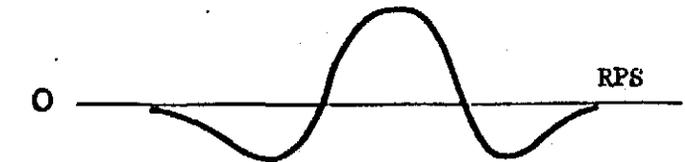
Doug
Douglas H. Pitcher, M.Sc.,
Research & Development

DHP:mk

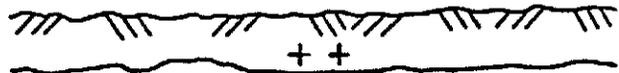
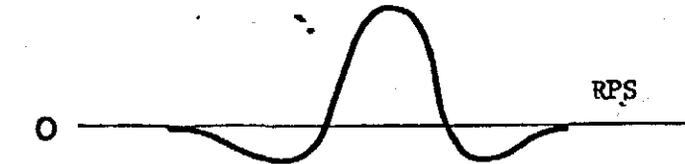
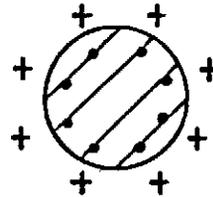
TYPICAL M.I.P. ANOMALY FORMS

THEORETICAL MODEL

CHARGEABLE SOURCE
NO RESISTIVITY
CONTRAST

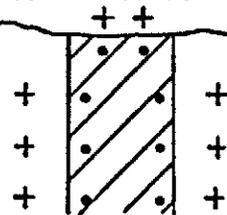


- + External current flow into plane of paper
- Internal current flow out of plane of paper



TYPE A

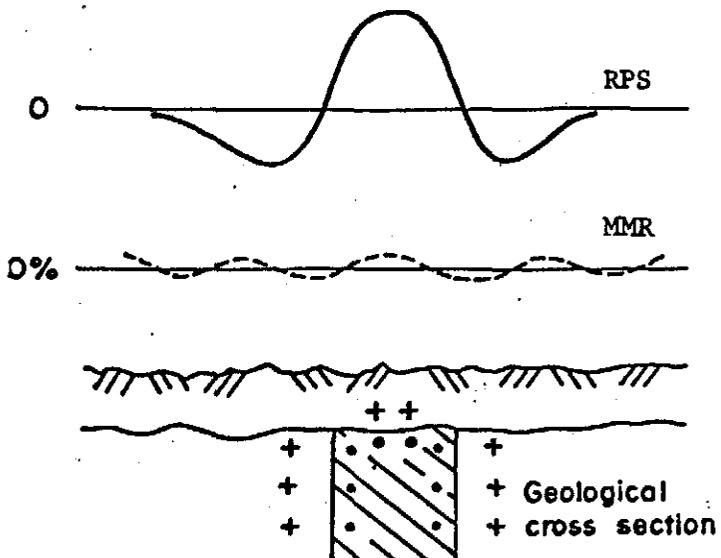
CHARGEABLE SOURCE
RESISTIVE SOURCE



TYPICAL M.I.P. ANOMALY FORMS

TYPE B

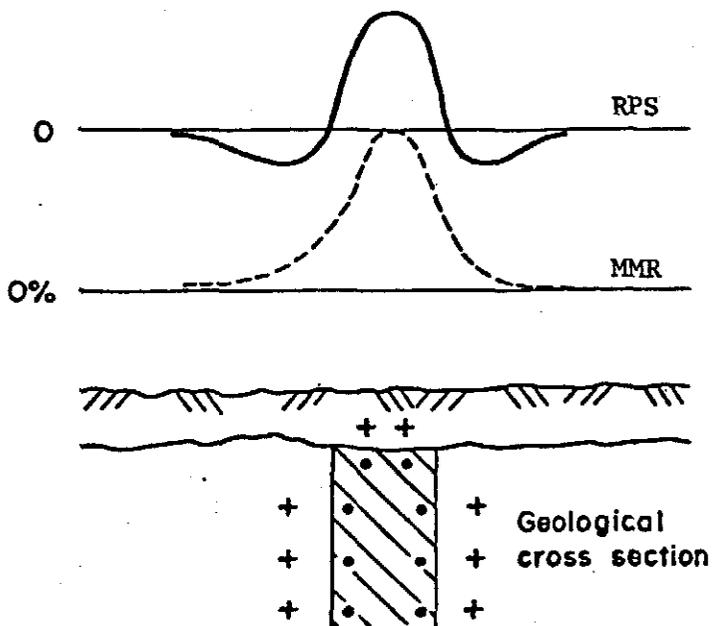
CHARGEABLE SOURCE
HOMOGENEOUS



- + External current flow into plane of paper.
- Internal current flow out of plane of paper.

TYPE C

CHARGEABLE SOURCE
CONDUCTIVE



+ Geological cross section

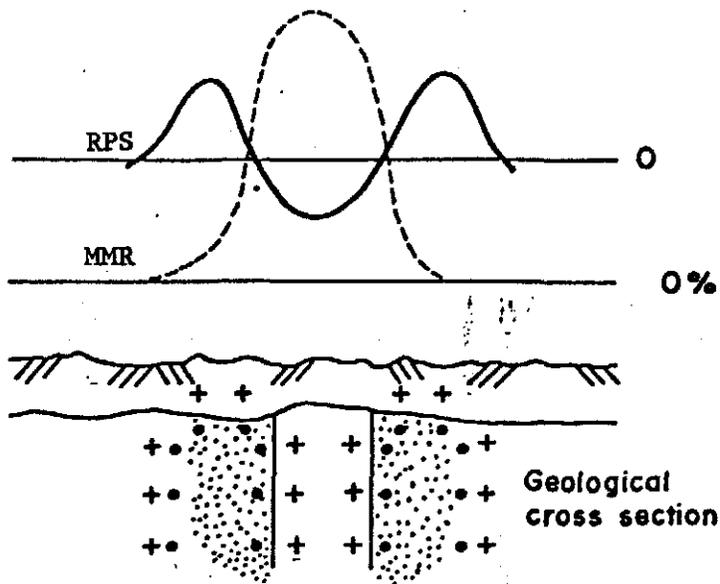
029

TYPICAL M.I.P. ANOMALY FORMS

TYPE D

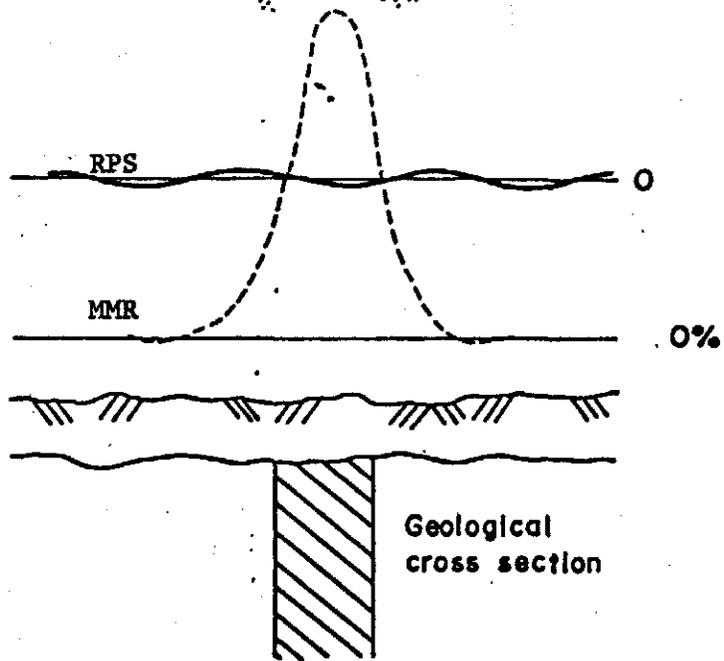
CHARGEABLE SOURCE VERY CONDUCTIVE WITH DISSEMINATED HALO

- + External current flow into plane of paper.
- Internal current flow out of plane of paper.



TYPE E

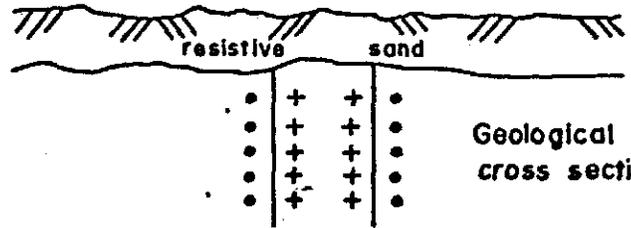
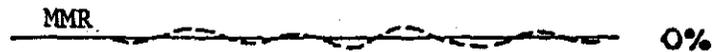
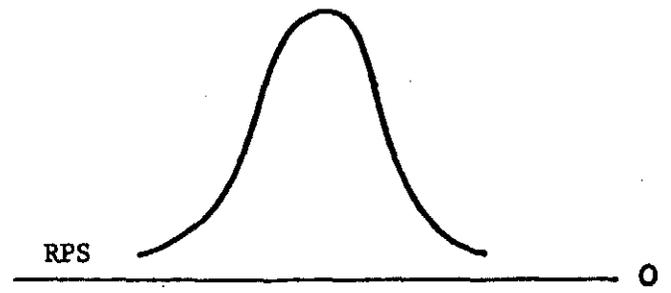
SOURCE VERY CONDUCTIVE BUT WITH LITTLE OR NO APPRECIABLE DISSEMINATED HALO



TYPICAL M.I.P. ANOMALY FORMS

TYPE F

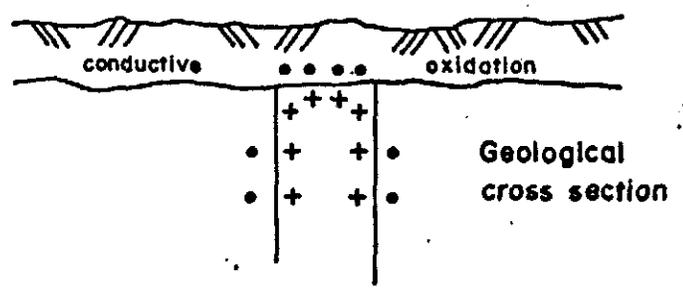
CHARGEABLE SOURCE HOMOGENEOUS
(AS B) UNDER DESSICATED
RESISTIVE SAND COVER



- + External current flow into plane of paper.
- Internal current flow out of plane of paper.

TYPE G

CHARGEABLE SOURCE HOMOGENEOUS
(AS C) UNDER HIGHLY
CONDUCTIVE COVER



031

APPENDIX C

Enclosed is the total amount and breakdown of all expenses incurred by Pennzoil in relation to E.L. 2/76.

032

Period TOTAL EXPENDITURE

The following are transcribed from the Pennzoil of Australia Limited expenditure records.

Project..... LOONGANA

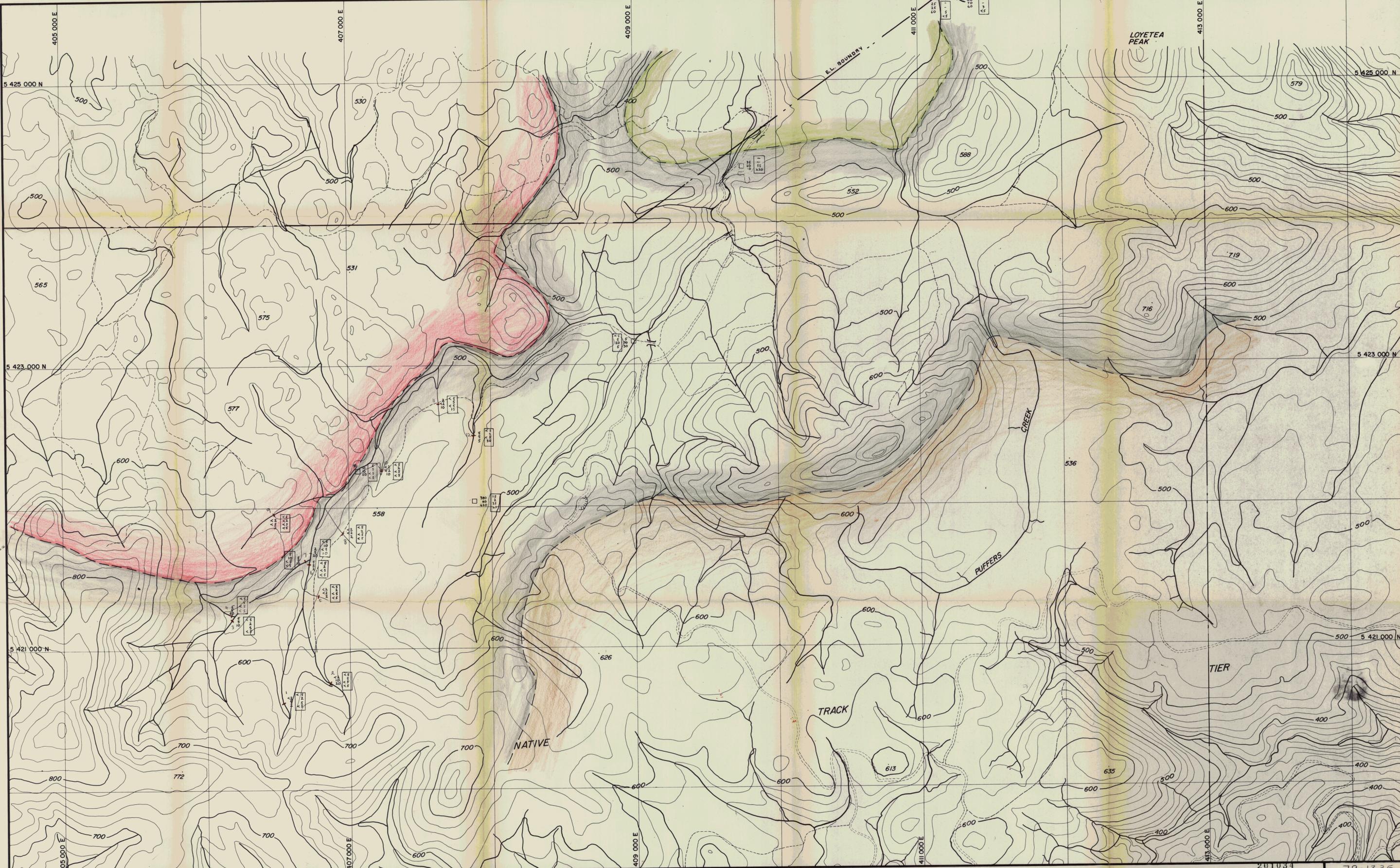
Expenses

001	Surface Rights
		1506.60
002	Mineral Rights
		5820.25
101	Geological Surveys
		13042.98
102	Geophysical/Geochemical
103	Site Prep. for Drilling
104	Diamond Drilling
105	Assays, Augering166.85.....
		942.95
106	Travel, General
		2226.91
107	Administration Expense
		789.50
108	Vehicle & Equipment
		<u>24496.04</u>

TOTAL EXPENDITURE THIS PERIOD

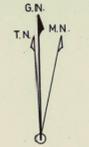
TOTAL PREVIOUSLY REPORTED

\$24,496.04



* - Stream sediment sample
 □ - Rock chip sample
 10 ppm Cu
 20 ppm Pb
 10 ppm Zn
 10 ppm B
 10 ppm Mn
 10 ppm Fe
 10 ppm S

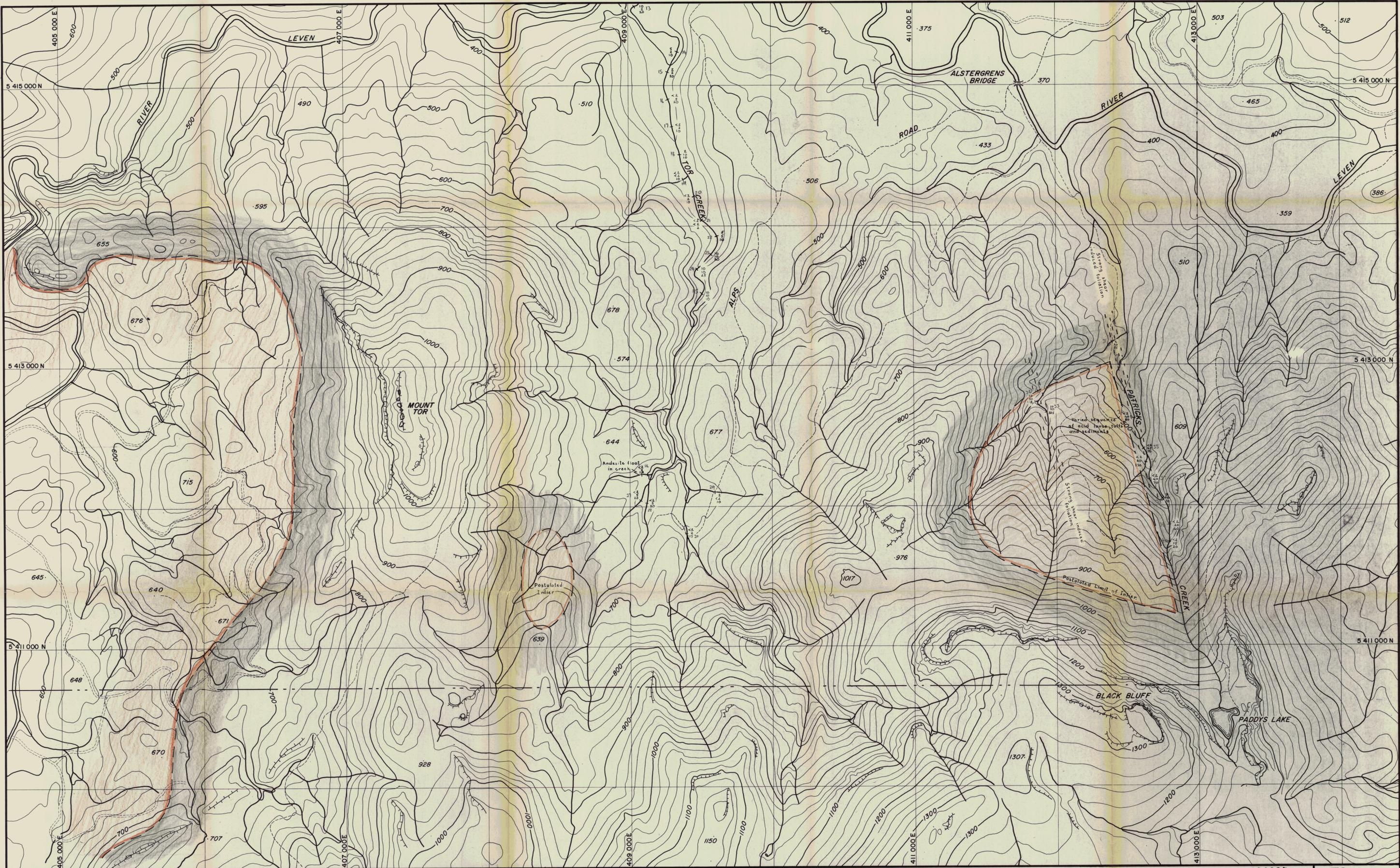
Tertiary Basalt
 Devonian Granite
 Cambro(?) Ordovician clastic sediments
 Cambrian volcanics and related sediments



NOTE: This map has been compiled from blow-ups of the Tasmanian Lands Department's aerial photo overlays.

Scale 1:10,000

PENNZOIL OF AUSTRALIA LIMITED SUBSIDIARY OF DUVAL CORPORATION LOONGANA E.L. 2176 Skarn recon. - Geology / Geochem.		201034 79-1325 GEOPEK'S PLAN LOCATION
COUNTRY: Australia STATE: Tasmania LATITUDE: L + 20 LONGITUDE: L + 55	DRAWN BY: Geochem. J.R.C. DATE: May 1979 MAP No: 48.321 PLATE No:	KT2/76-5 KT2/76-2 KT2/76-4 KT2/76-3



Stream sediment sample.



Cambrian-Ordovician sediments

Cambrian volcanics and related sediments.



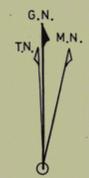
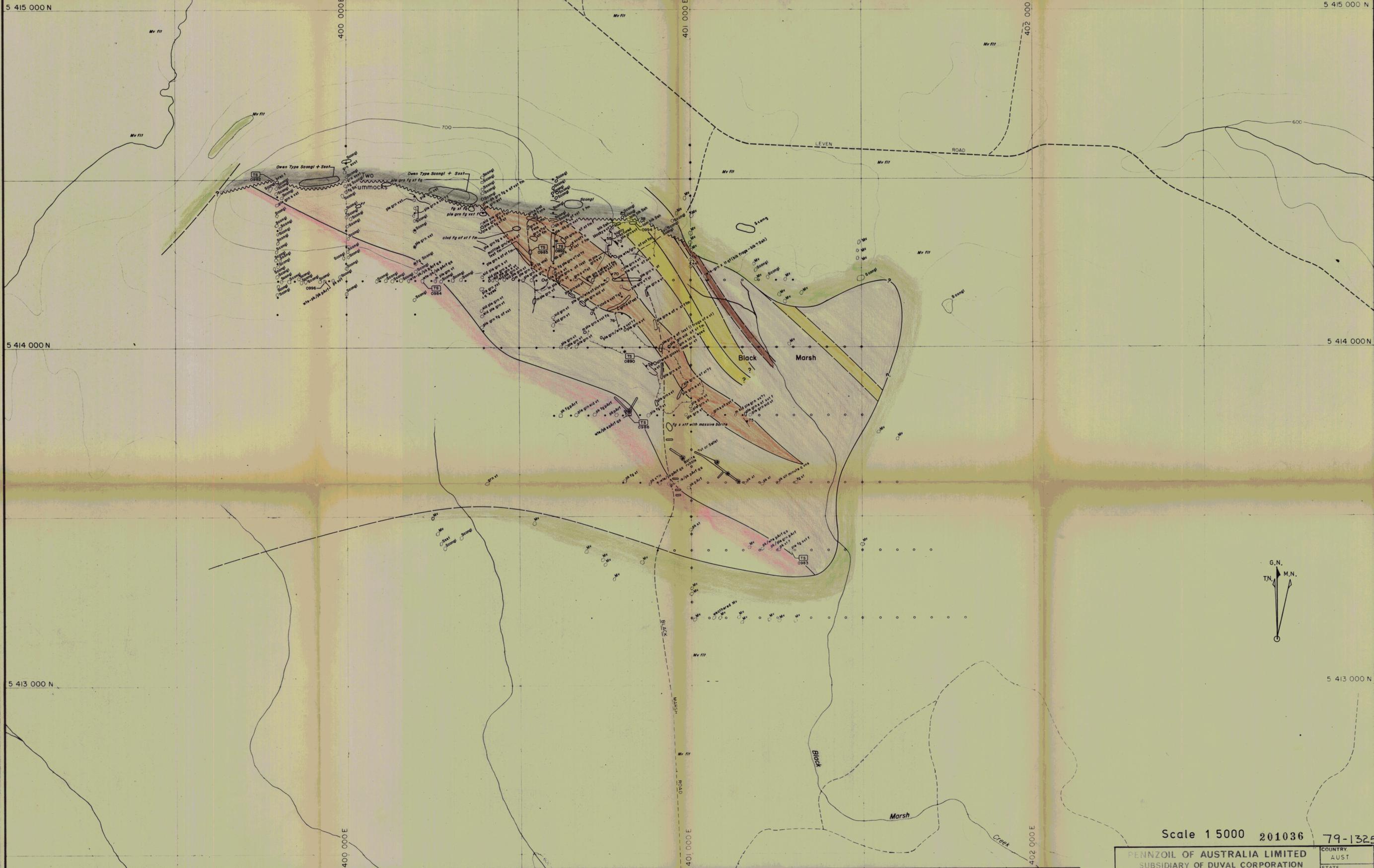
NOTE:
This map has been compiled from blow-ups
of the Tasmanian Lands Department's
aerial photo overlays.

Scale 1:10,000

201035		COUNTRY	Australia
PENNZOIL OF AUSTRALIA LIMITED		STATE	Tasmania
SUBSIDIARY OF DUVAL CORPORATION		LATITUDE: 41° 20'	
LOONGANA E.L. 2/76		LONGITUDE: 145° 50'	
Camb. recon. - Geology / Geochem		MAP No.	48.322
DATE: 1976	DRAWN BY: G. J. R.	DATE: May 1976	PLATE No.

79-1325
GEOPEKS PLAN
LOCATION
KT2/76-1
KT2/76-5
KT2/76-2
KT2/76-4
KT2/76-3





Scale 1 5000 201036 79-1325

PENNZOIL OF AUSTRALIA LIMITED
 SUBSIDIARY OF DUVAL CORPORATION

LOONGANA - E.L. 2/76

Challenger III - Geology

Geopko, P.I.	DRAWN BY Geopko J.R.C.	DATE May 1974	COUNTRY AUSTRALIA
			STATE TASMANIA
			LATITUDE 41° 20'
			LONGITUDE 145° 50'
			MAP No. 48,323
			PLATE No.

TOPOGRAPHICAL SYMBOLS:		SEDIMENTARY:		STRUCTURAL SYMBOLS:		COLOURS:		SILICATE MINERALOGY:		GEOLOGICAL INTERPRETATION:		ROCK GEOCHEMISTRY: (ppm)	
Bulldozed track	Bulldozed trench	Saltat	Sandstone	Outcrop limit	Rubble boundary	pk	pink	q	quartz	19-47	TERT	Basalt (flows) (Mv)	Si
Rubble heap	Quarry	Sast	Sandstone	Approximate contact	Interpreted contact	grn	green	f	feldspar	19-70	UE?	Conglomerate (S congl) Sandstone (Sast)	Ca
		Sq	quartzite	bedding	primary foliation	bls	black	c	chlorite	19-56	E	Fine grained ? tuffaceous sediment (fg?)	Fe
		Scngl	conglomerate	jointing	fault	pu	purple		sericite	19-08	E	Crystal lithic tuff (xt)	Al
				unconformity	minor fault	wh	white			19-01	E	Laminated shale (lsm sh)	Mg
						pie	pink			19-01	E	Ashflow tuffs (at lsm fm., of lsm fm)	Zn
						dk	dark			19-21	E	Glassy fine grained lava (vst f)	Ag
						fg	fine grained (clim)			19-15	E	Porphyritic amygdaloidal rhyolite (prt qa)	Mn
													As
													Co
													Ni
													Pb
													Cu
													Mo
													U
													Th
													K
													Na
													Cl
													S
													P
													O
													H
													C
													N
													Ar
													Kr
													Xe
													Rn

5 415 000 N

5 415 000 N

400 000 E

401 000 E

402 000 E

5 414 000 N

5 414 000 N

5 413 000 N

5 413 000 N

400 000 E

401 000 E

402 000 E

LEGEND:

SYMBOLS:

- Geological contact, approximate
- Hand cupped sample
- Power auger sample
- Sample not received by A.C.S.L. for assay

ANALYTICAL NOTES:

Analytical Method: Cu by AAS following hot conc. HCl leach and HCl/HNO₃ leach in latter stages for 1 hr. of 0.25g sample.

Size fraction analysed: -80 mesh.

Analytical results in ppm:

50 Original sample assay (50ppm)	45 Duplicate sample assay (45ppm)	(30) Reaugered sample assay (30ppm)	(25) Reaugered duplicate sample assay (25ppm)	20 Original sample assay (20ppm)	10 Sample taken at 1.0m	5 Sample taken at 1.5m (E.O.H.)	40 Denotes A.C.S.L. repeat and check assay (40ppm)	30 Denotes A.C.S.L. repeat and check assay on reaugered sample (30ppm)	60 Sample taken at 2.0m	50 Sample taken at 2.5m (E.O.H.)	10 Sample taken at 4.0m	15 " " " " 5.0m	20 " " " " 6.0m
(10) Reaugered sample assay (10ppm)	5 Original sample assay (5ppm)	30 Reaugered sample assay (30ppm)	20 Original sample assay (20ppm)	30 Duplicate sample assay (30ppm)									

201037
Scale 1: 5000



FENNZOIL OF AUSTRALIA LIMITED
SUBSIDIARY OF DUVAL CORPORATION

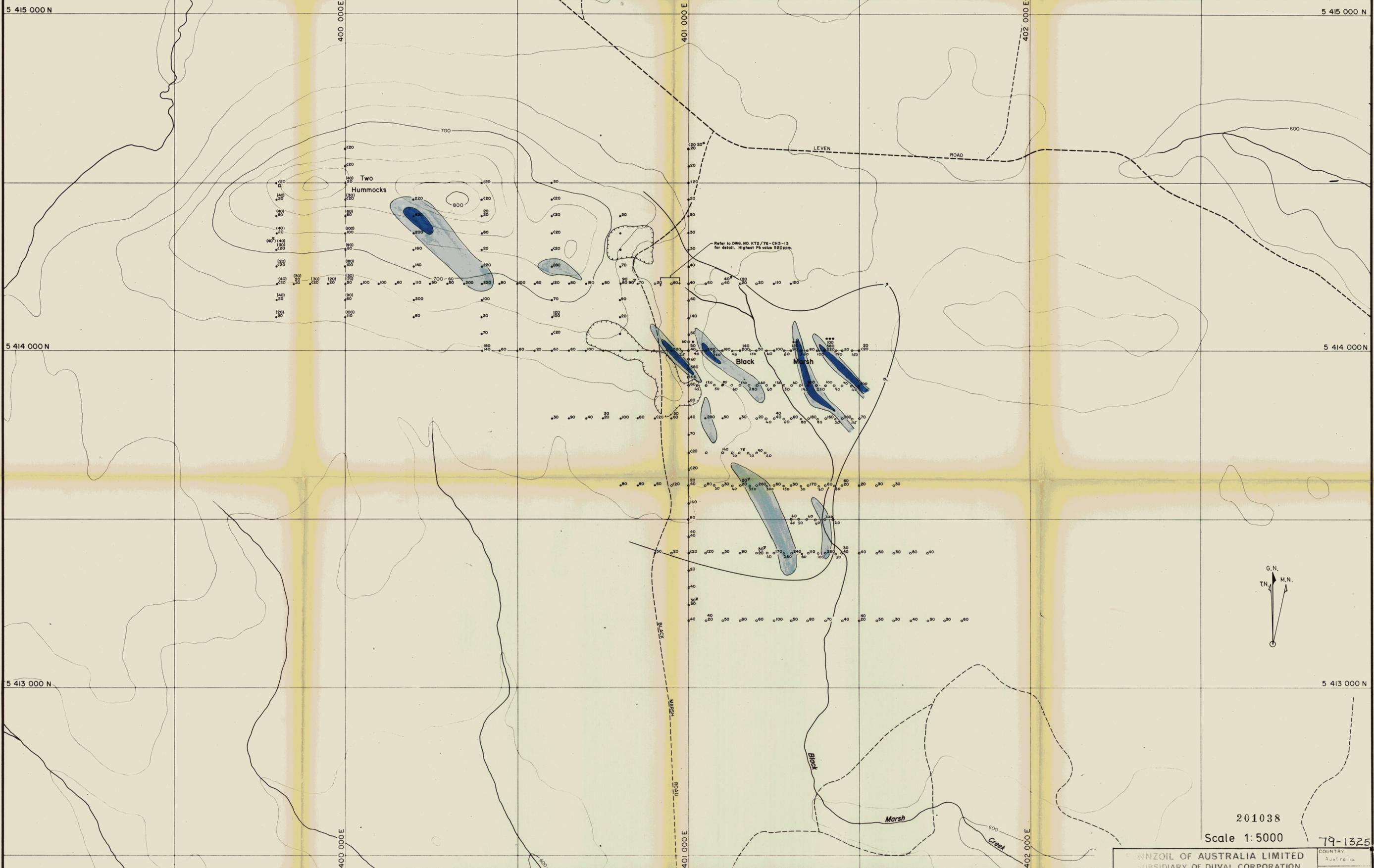
LOONGANA EL 2/76

Challenger III - Geochem. Cu.

COUNTRY: AUSTRALIA
STATE: TASMANIA
LATITUDE: 42° 42'
LONGITUDE: 145° 50'

MAP No. 48324
DATE: May 1974
DRAWN BY: URSALIA J.R.
PLATE No.

5 cm
4062 79-1325 Q36/29



LEGEND:

SYMBOLS:

- Geological contact, approximate
- Hand dugger sample
- Power auger sample
- Sample not received by A.C.S.L. for assay

ANALYTICAL NOTES:

Analytical Method: Pb by AAS following hot conc. HCl leach and HCl/HNO₃ leach in latter stages for 1hr. of 0.25g sample.

Size fraction analysed: -80 mesh

Analytical results in ppm.

180.....Original sample assay (180ppm)
 *140.....Duplicate sample assay (140ppm)

(40).....Reaugered sample assay (40ppm)
 (30).....Reaugered duplicate sample assay (30ppm)
 *20.....Original sample assay (20ppm)

30^v.....Denotes A.C.S.L. repeat and check assay (30ppm)
 *40^v.....Denotes A.C.S.L. repeat and check assay on reaugered sample (40ppm)

80.....Sample taken at 1.0m
 *90....." " " 1.5m (E.O.H.)

**.....Sample taken at 2.0m
 *90....." " " 3.6m (E.O.H.)

100.....Sample taken at 4.0m
 280....." " " 5.0m
 *220....." " " 6.5m (E.O.H.)

CONTOURS

- 200 ppm
- 400 ppm



201038
 Scale 1:5000

COUNTRY	Australia
STATE	Tasmania
LATITUDE	41° 20'
LONGITUDE	145° 50'
MAP No.	48325
PLATE No.	

MINZSOIL OF AUSTRALIA LIMITED
 SUBSIDIARY OF DUVAL CORPORATION

LOONGANA E.L. 2/76

Challenger III - Geochem Pb

DRAWN BY: J. COOK
 DATE: May 1976

5 415 000 N

5 415 000 N

400 000 E

401 000 E

402 000 E

5 414 000 N

5 414 000 N

5 413 000 N

5 413 000 N

400 000 E

401 000 E

402 000 E

Two Hummocks

Black Marsh

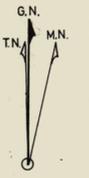
Marsh

Creek

LEVEN ROAD

BLACK MARSH ROAD

Refer to DWG. No. KT2/76-CH3-13 for detail. Highest Zn value 1760ppm



201039 Scale 1:5000

79-1325

LEGEND:

SYMBOLS:
Geological contact, approximate
Hand dugger sample
Power auger sample
Sample not received by A.C.S.L. for assay.

ANALYTICAL NOTES:
Analytical Method: Zn by AAS following hot conc. HCl leach and FeO/PbO₂ wash in latter stages for 1 hr. of 0-25g sample.
Size fraction analysed: -80 mesh
Analytical results in ppm.

20 Original sample assay (20ppm)
22 Duplicate sample assay (20ppm)

30 Reaugured sample assay (30ppm)
10 Original sample assay (10ppm)

30 Reaugured sample assay (30ppm)
40 Reaugured duplicate sample assay (40ppm)
10 Original sample assay (10ppm)

100 Denotes A.C.S.L. repeat and check assay (100ppm)
100 Denotes A.C.S.L. repeat and check assay on reaugured sample (100ppm)

15 Sample taken at 1.0m
15 Sample taken at 1.5m (E.O.H.)

30 Sample taken at 2.0m
110 Sample taken at 3.5m (E.O.H.)

30 Sample taken at 4.0m
220 Sample taken at 5.0m
310 Sample taken at 6.5m (E.O.H.)

CONTOURS

200 ppm
400 ppm

PENNZOIL OF AUSTRALIA LIMITED
SUBSIDIARY OF DUVAL CORPORATION

LOONGANA EL 2/76

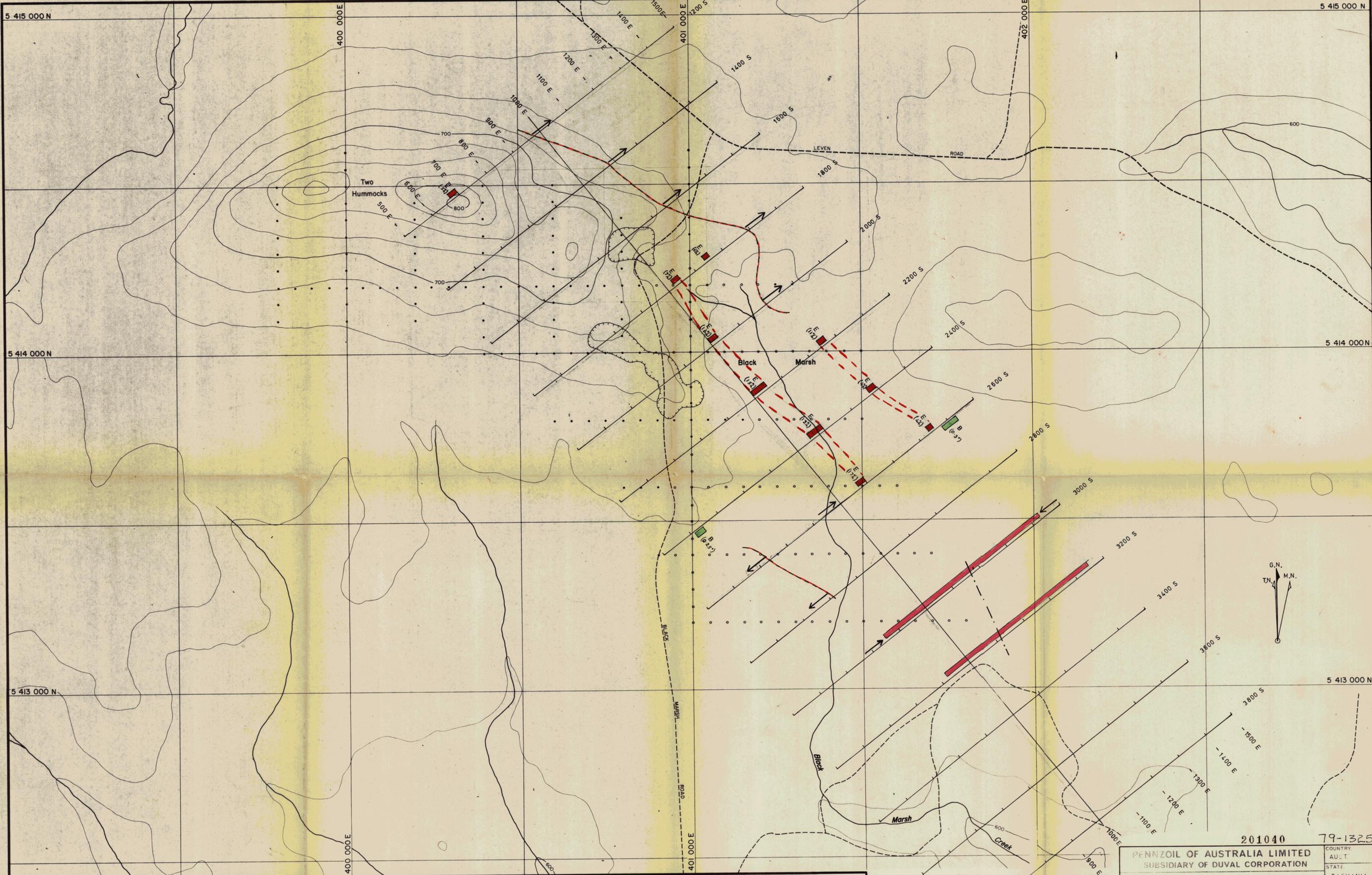
Challenger III - Geochem. Zn

DATA BY: Gcopeko, P.J. DRAWN BY: Gcopeko, J.R.C. DATE: May 1974

COUNTRY: Australia
STATE: Tasmania
LATITUDE: 41° 20'
LONGITUDE: 145° 50'
MAP No: 48,326
PLATE No:



4064 Q36/29



RRMIP Legend

↑ - Substantial increase in MMR (conductivity) values.
 — Broad MMR anomaly with centre line.

E (15%) — "E Type" anomaly (conductive - no chargeable contrast)
 MMR anomaly intensity above background given.
B (0.3%) — "B Type" anomaly (chargeable - no conductive contrast)
 RPS anomaly intensity above background given.

201040 79-1325

PENNZOIL OF AUSTRALIA LIMITED
 SUBSIDIARY OF DUVAL CORPORATION

LOONGANA EL 2176

Challenger III - Geophysics-RRMIP

DATE BY GEOPEKO-PZL	DRAWN BY J.R.C.	DATE MAY 1979	MAP No. 48.327
Scale 1:5,000			PLATE No.

5 cm

033

XTOP= 500.

XINC= 25.00

201041

500.	I *	0.37
525.	I *	0.56
550.	I *	0.57
575.	I*	0.29
600.	I *	0.50
625.	I *	0.31
650.	I *	0.52
675.	I *	0.54
700.	I *	0.55
725.	I*	0.23
750.	I*	0.24
775.	I*	0.25
800.	I*	0.26
825.	I *	0.76
850.	I *	0.78
875.	I *	0.40
900.	I *	0.40
925.	I *	0.40
950.	I *	0.67
975.	I *	0.40
1000.	I *	0.40
1025.	I *	0.40
1050.	I*	0.26
1075.	I*	0.26
1100.	I *	0.53
1125.	I*	0.25
1150.	I*	0.25
1175.	I *	0.49
1200.	I *	0.35
1225.	I *	0.33
1250.	I *	0.34
1275.	I *	0.34
1300.	I*	0.11
1325.	I*	0.10
1350.	*	0.00
1375.	*	0.00
1400.	I*	0.18
1425.	I*	0.16
1450.	I*	0.17
1475.	I *	0.37
1500.	I *	0.34

XBOT= 1500.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3800. S SECONDARY FIELD QUADRATURE H30/I

79-1325

035

XTOP= 500.

XINC= 25.00

201048

500.	I				20.71
525.	I			*	18.03
550.	I			*	18.17
575.	I			*	17.24
600.	I			*	16.22
625.	I			*	17.07
650.	I			*	14.93
675.	I			*	15.67
700.	I			*	14.44
725.	I			*	18.10
750.	I			*	17.88
775.	I			*	21.66
800.	I			*	22.62
825.	I			*	16.91
850.	I			*	17.29
875.	I			*	17.95
900.	I			*	17.96
925.	I			*	15.41
950.	I			*	15.24
975.	I			*	13.56
1000.	I			*	13.32
1025.	I			*	12.58
1050.	I		*		9.37
1075.	I		*		10.52
1100.	I		*		15.03
1125.	I		*		10.13
1150.	I		*		10.44
1175.	I		*		12.02
1200.	I		*		8.92
1225.	I	*			6.00
1250.	I		*		12.01
1275.	I		*		14.18
1300.	I		*		11.50
1325.	I		*		8.83
1350.	I		*		9.06
1375.	I	*			3.38
1400.	I	*			5.46
1425.	*I				-1.35
1450.	I		*		9.36
1475.	I		*		17.05
1500.	I		*		11.91

XBOT= -1500.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 3800. S MAGNETOMETRIC RESESTIVITY MMR

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STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500. E	4.60	0.98	0.00	-0.70	0.10	-0.90	0.17	127.56	20.71	-0.10	0.20	0.37	-0.21	500. E
525. E	4.60	0.98	-0.10	-0.60	0.10	-0.90	0.17	123.16	18.03	-0.20	0.30	0.56	-0.43	525. E
550. E	4.60	1.01	0.00	-0.60	0.10	-0.90	0.18	122.53	18.17	-0.10	0.30	0.57	-0.22	550. E
575. E	4.60	1.03	0.00	-0.70	0.10	-0.85	0.19	120.64	17.24	-0.10	0.15	0.29	-0.22	575. E
600. E	4.60	1.05	0.00	-0.60	0.10	-0.85	0.19	118.75	16.22	-0.10	0.25	0.50	-0.23	600. E
625. E	4.60	1.09	0.00	-0.70	0.10	-0.85	0.20	119.07	17.07	-0.10	0.15	0.31	-0.24	625. E
650. E	4.60	1.10	0.00	-0.60	0.10	-0.85	0.21	116.11	14.93	-0.10	0.25	0.52	-0.24	650. E
675. E	4.60	1.14	0.00	-0.60	0.10	-0.85	0.21	116.35	15.67	-0.10	0.25	0.54	-0.25	675. E
700. E	4.60	1.16	0.10	-0.60	0.10	-0.85	0.22	114.58	14.44	0.00	0.25	0.55	0.00	700. E
725. E	4.60	1.23	0.10	-0.70	0.15	-0.80	0.23	117.70	18.10	-0.05	0.10	0.23	-0.13	725. E
750. E	4.60	1.26	0.00	-0.70	0.15	-0.80	0.23	116.97	17.88	-0.15	0.10	0.24	-0.41	750. E
775. E	4.60	1.33	0.10	-0.70	0.15	-0.80	0.24	119.97	21.66	-0.05	0.10	0.25	-0.14	775. E
800. E	4.60	1.37	0.00	-0.70	0.15	-0.80	0.25	120.31	22.62	-0.15	0.10	0.26	-0.45	800. E
825. E	4.60	1.34	-0.20	-0.50	0.15	-0.80	0.25	114.81	16.91	-0.35	0.30	0.76	-1.02	825. E
850. E	4.60	1.37	-0.10	-0.50	0.15	-0.80	0.26	114.81	17.29	-0.25	0.30	0.78	-0.74	850. E
875. E	4.60	1.40	-0.10	-0.60	0.15	-0.75	0.26	115.09	17.95	-0.25	0.15	0.40	-0.76	875. E
900. E	4.60	1.42	-0.10	-0.60	0.15	-0.75	0.27	114.85	17.96	-0.25	0.15	0.40	-0.77	900. E
925. E	4.60	1.41	0.00	-0.60	0.15	-0.75	0.27	112.58	15.41	-0.15	0.15	0.40	-0.46	925. E
950. E	4.60	1.42	-0.10	-0.50	0.15	-0.75	0.27	112.32	15.24	-0.25	0.25	0.67	-0.77	950. E
975. E	4.60	1.41	0.00	-0.60	0.15	-0.75	0.28	110.90	13.56	-0.15	0.15	0.40	-0.46	975. E
1000. E	4.60	1.41	-0.10	-0.60	0.15	-0.75	0.28	110.69	13.32	-0.25	0.15	0.40	-0.77	1000. E
1025. E	4.60	1.40	-0.10	-0.60	0.15	-0.75	0.28	110.11	12.58	-0.25	0.15	0.40	-0.76	1025. E
1050. E	4.60	1.36	0.00	-0.60	0.15	-0.70	0.27	107.58	9.37	-0.15	0.10	0.26	-0.44	1050. E
1075. E	4.60	1.36	0.00	-0.60	0.15	-0.70	0.27	108.59	10.52	-0.15	0.10	0.26	-0.44	1075. E
1100. E	4.60	1.39	-0.10	-0.50	0.15	-0.70	0.27	112.42	15.03	-0.25	0.20	0.53	-0.76	1100. E
1125. E	4.60	1.32	-0.10	-0.60	0.20	-0.70	0.26	108.51	10.13	-0.30	0.10	0.25	-0.86	1125. E
1150. E	4.60	1.30	-0.20	-0.60	0.20	-0.70	0.26	108.95	10.44	-0.40	0.10	0.25	-1.13	1150. E
1175. E	4.60	1.29	-0.10	-0.50	0.20	-0.70	0.25	110.53	12.02	-0.30	0.20	0.49	-0.84	1175. E
1200. E	4.60	1.23	-0.10	-0.50	0.20	-0.65	0.25	108.01	8.92	-0.30	0.15	0.35	-0.80	1200. E
1225. E	4.60	1.17	-0.10	-0.50	0.20	-0.65	0.24	105.54	6.00	-0.30	0.15	0.33	-0.76	1225. E
1250. E	4.60	1.20	-0.20	-0.50	0.20	-0.65	0.23	111.40	12.01	-0.40	0.15	0.34	-1.04	1250. E
1275. E	4.60	1.19	-0.10	-0.50	0.20	-0.65	0.23	113.87	14.18	-0.30	0.15	0.34	-0.78	1275. E
1300. E	4.60	1.13	-0.10	-0.60	0.20	-0.65	0.22	111.61	11.50	-0.30	0.05	0.11	-0.74	1300. E
1325. E	4.60	1.07	-0.10	-0.60	0.20	-0.65	0.21	109.21	8.83	-0.30	0.05	0.10	-0.70	1325. E
1350. E	4.60	1.04	0.00	-0.60	0.20	-0.60	0.21	109.78	9.06	-0.20	0.00	0.00	-0.45	1350. E
1375. E	4.60	0.95	0.00	-0.60	0.20	-0.60	0.20	103.77	3.38	-0.20	0.00	0.00	-0.41	1375. E
1400. E	4.60	0.94	-0.20	-0.50	0.20	-0.60	0.19	106.31	5.46	-0.40	0.10	0.18	-0.82	1400. E
1425. E	4.60	0.84	-0.10	-0.50	0.20	-0.60	0.19	98.39	-1.35	-0.30	0.10	0.16	-0.55	1425. E
1450. E	4.60	0.92	-0.30	-0.50	0.20	-0.60	0.18	111.61	9.36	-0.50	0.10	0.17	-1.00	1450. E
1475. E	4.60	0.97	-0.30	-0.40	0.20	-0.60	0.17	121.90	17.05	-0.50	0.20	0.37	-1.05	1475. E
1500. E	4.60	0.89	-0.30	-0.40	0.20	-0.60	0.17	115.85	11.91	-0.50	0.20	0.34	-0.97	1500. E

037

XTOP= 500.

XINC= 25.00

201045

500.	I *	0.35
525.	I *	0.36
550.	I*	0.28
575.	I*	0.28
600.	I*	0.29
625.	*	0.10
650.	I*	0.30
675.	I *	0.31
700.	I*	0.10
725.	I *	0.32
750.	I *	0.32
775.	I *	0.44
800.	I *	0.44
825.	I *	0.46
850.	I *	0.46
875.	I *	0.47
900.	I *	0.46
925.	I *	0.58
950.	I *	0.58
975.	I *	0.59
1000.	I *	0.59
1025.	I *	0.57
1050.	I *	0.34
1075.	I *	0.57
1100.	I *	0.68
1125.	I *	0.45
1150.	I *	0.44
1175.	I *	0.44
1200.	I *	0.44
1225.	I *	0.44
1250.	I *	0.55
1275.	I *	0.32
1300.	I *	0.30
1325.	I *	0.51
1350.	I *	0.49
1375.	I *	0.39
1400.	I *	0.55
1425.	I *	0.55
1450.	I *	0.36
1475.	I *	0.36
1500.	I *	0.53

XBOT= 1500.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3600. S SECONDARY FIELD QUADRATURE HSQ/I

039

XTOP= 500.

XINC= 25.00

201047

500.	I	*	13.53
525.	I	*	13.46
550.	I	*	15.34
575.	I	*	15.26
600.	I	*	15.19
625.	I	*	14.16
650.	I	*	14.14
675.	I	*	15.14
700.	I	*	14.24
725.	I	*	15.37
750.	I	*	14.63
775.	I	*	16.92
800.	I	*	15.42
825.	I	*	16.99
850.	I	*	17.72
875.	I	*	17.64
900.	I	*	15.77
925.	I	*	15.07
950.	I	*	14.56
975.	I	*	16.21
1000.	I	*	16.11
1025.	I	*	12.30
1050.	I	*	11.63
1075.	I	*	13.12
1100.	I	*	12.84
1125.	I	*	12.75
1150.	I	*	12.83
1175.	I	*	14.05
1200.	I	*	15.42
1225.	I	*	14.97
1250.	I	*	16.59
1275.	I	*	17.33
1300.	I	*	12.29
1325.	I	*	15.14
1350.	I	*	12.18
1375.	I	*	13.18
1400.	I	*	10.30
1425.	I	*	11.35
1450.	I	*	11.42
1475.	I	*	15.42
1500.	I	*	14.51

XBOT= 1500.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 3600. S MAGNETOMETRIC RESESTIVITY MMR

LINE=

040

3600. S

FREQUENCY=3HZ N003

201048

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500. E	4.60	0.92	0.10	-0.70	0.10	-0.90	0.17	117.69	13.53	0.00	0.20	0.35	0.00	500. E
525. E	4.60	0.94	-0.10	-0.70	0.10	-0.90	0.17	117.15	13.46	-0.20	0.20	0.36	-0.41	525. E
550. E	4.60	0.98	0.00	-0.80	0.10	-0.95	0.18	119.05	15.34	-0.10	0.15	0.28	-0.21	550. E
575. E	4.60	1.00	-0.10	-0.80	0.10	-0.95	0.18	118.48	15.26	-0.20	0.15	0.28	-0.43	575. E
600. E	4.60	1.02	0.00	-0.80	0.10	-0.95	0.19	117.96	15.19	-0.10	0.15	0.29	-0.22	600. E
625. E	4.60	1.03	0.00	-0.90	0.10	-0.95	0.19	116.35	14.16	-0.10	0.05	0.10	-0.22	625. E
650. E	4.60	1.05	0.00	-0.80	0.10	-0.95	0.20	115.96	14.14	-0.10	0.15	0.30	-0.23	650. E
675. E	4.60	1.08	0.00	-0.80	0.10	-0.95	0.20	116.73	15.14	-0.10	0.15	0.31	-0.23	675. E
700. E	4.60	1.09	-0.10	-0.90	0.10	-0.95	0.21	115.42	14.24	-0.20	0.05	0.10	-0.47	700. E
725. E	4.60	1.12	-0.10	-0.80	0.05	-0.95	0.21	116.32	15.37	-0.15	0.15	0.32	-0.37	725. E
750. E	4.60	1.13	0.00	-0.80	0.05	-0.95	0.21	115.25	14.63	-0.05	0.15	0.32	-0.12	750. E
775. E	4.60	1.17	0.00	-0.80	0.05	-1.00	0.22	117.35	16.92	-0.05	0.20	0.44	-0.13	775. E
800. E	4.60	1.17	-0.10	-0.80	0.05	-1.00	0.22	115.57	15.42	-0.15	0.20	0.44	-0.38	800. E
825. E	4.60	1.20	0.00	-0.80	0.05	-1.00	0.22	116.92	16.99	-0.05	0.20	0.46	-0.13	825. E
850. E	4.60	1.22	0.00	-0.80	0.05	-1.00	0.23	117.44	17.72	-0.05	0.20	0.46	-0.13	850. E
875. E	4.60	1.23	-0.10	-0.80	0.05	-1.00	0.23	117.18	17.64	-0.15	0.20	0.47	-0.40	875. E
900. E	4.60	1.22	0.00	-0.80	0.05	-1.00	0.23	115.23	15.77	-0.05	0.20	0.46	-0.13	900. E
925. E	4.60	1.22	0.00	-0.80	0.05	-1.05	0.23	114.45	15.07	-0.05	0.25	0.58	-0.13	925. E
950. E	4.60	1.22	0.00	-0.80	0.05	-1.05	0.23	113.90	14.56	-0.05	0.25	0.58	-0.13	950. E
975. E	4.60	1.24	-0.10	-0.80	0.05	-1.05	0.23	115.43	16.21	-0.15	0.25	0.59	-0.40	975. E
1000. E	4.60	1.24	-0.10	-0.80	0.05	-1.05	0.23	115.31	16.11	-0.15	0.25	0.59	-0.40	1000. E
1025. E	4.60	1.20	-0.10	-0.80	0.05	-1.05	0.23	111.70	12.30	-0.15	0.25	0.57	-0.39	1025. E
1050. E	4.60	1.19	0.00	-0.90	0.05	-1.05	0.23	111.10	11.63	-0.05	0.15	0.34	-0.13	1050. E
1075. E	4.60	1.20	-0.10	-0.80	0.05	-1.05	0.23	112.58	13.12	-0.15	0.25	0.57	-0.39	1075. E
1100. E	4.60	1.19	-0.10	-0.80	0.05	-1.10	0.23	112.40	12.84	-0.15	0.30	0.68	-0.39	1100. E
1125. E	4.60	1.18	-0.10	-0.90	0.00	-1.10	0.23	112.41	12.75	-0.10	0.20	0.45	-0.26	1125. E
1150. E	4.60	1.17	-0.20	-0.90	0.00	-1.10	0.23	112.63	12.83	-0.20	0.20	0.44	-0.51	1150. E
1175. E	4.60	1.17	-0.10	-0.90	0.00	-1.10	0.22	114.00	14.05	-0.10	0.20	0.44	-0.26	1175. E
1200. E	4.60	1.17	-0.10	-0.90	0.00	-1.10	0.22	115.57	15.42	-0.10	0.20	0.44	-0.26	1200. E
1225. E	4.60	1.15	-0.10	-0.90	0.00	-1.10	0.22	115.35	14.97	-0.10	0.20	0.44	-0.25	1225. E
1250. E	4.60	1.15	-0.10	-0.90	0.00	-1.15	0.21	117.29	16.59	-0.10	0.25	0.55	-0.25	1250. E
1275. E	4.60	1.14	-0.20	-1.00	0.00	-1.15	0.21	118.40	17.33	-0.20	0.15	0.32	-0.50	1275. E
1300. E	4.60	1.07	0.00	-1.00	0.00	-1.15	0.21	113.30	12.29	-0.00	0.15	0.30	-0.00	1300. E
1325. E	4.60	1.08	-0.20	-0.90	0.00	-1.15	0.20	116.73	15.14	-0.20	0.25	0.51	-0.47	1325. E
1350. E	4.60	1.03	-0.20	-0.90	0.00	-1.15	0.20	113.76	12.18	-0.20	0.25	0.49	-0.45	1350. E
1375. E	4.60	1.02	-0.20	-1.00	0.00	-1.20	0.19	115.22	13.18	-0.20	0.20	0.39	-0.45	1375. E
1400. E	4.60	0.97	-0.20	-0.90	0.00	-1.20	0.19	112.17	10.30	-0.20	0.30	0.55	-0.42	1400. E
1425. E	4.60	0.96	-0.30	-0.90	0.00	-1.20	0.18	113.74	11.35	-0.30	0.30	0.55	-0.63	1425. E
1450. E	4.60	0.94	-0.30	-1.00	0.00	-1.20	0.18	114.19	11.42	-0.30	0.20	0.36	-0.62	1450. E
1475. E	4.60	0.96	-0.40	-1.00	0.00	-1.20	0.17	119.64	15.42	-0.40	0.20	0.36	-0.84	1475. E
1500. E	4.60	0.93	-0.40	-0.90	0.00	-1.20	0.17	118.97	14.51	-0.40	0.30	0.53	-0.81	1500. E

041

201049

XTOP= 500.

XINC= 25.00

500.	*	0.08
525.	*	0.08
550.	*	-0.09
575.	*	0.09
600.	*	-0.09
625.	*	-0.09
650.	*	0.09
675.	*	-0.09
700.	*	0.09
725.	*	-0.09
750.	*I	-0.29
775.	*I	-0.30
800.	*I	-0.30
825.	*I	-0.30
850.	*I	-0.31
875.	*I	-0.32
900.	*I	-0.11
925.	*I	-0.34
950.	*I	-0.12
975.	*I	-0.34
1000.	*I	-0.33
1025.	*I	-0.11
1050.	*I	-0.34
1075.	*I	-0.12
1100.	*I	-0.11
1125.	*I	-0.34
1150.	*I	-0.34
1175.	*I	-0.11
1200.	*I	-0.11
1225.	*I	-0.11
1250.	*I	-0.11
1275.	*I	-0.11
1300.	*I	-0.10
1325.	*I	-0.10
1350.	*	-0.10
1375.	*	-0.10
1400.	*	-0.09
1425.	*	-0.09
1450.	*I	-0.28
1475.	*I	-0.26
1500.	*	-0.09

XBOT= 1500.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3400. S SECONDARY FIELD QUADRATURE HSQ/I

042

XTOP= 500.

XINC= 25.00

500.	I*	0.05
525.	I*	0.05
550.	*I	-0.05
575.	I*	0.05
600.	*I	-0.05
625.	*I	-0.05
650.	I*	0.05
675.	*I	-0.05
700.	I*	0.05
725.	*I	-0.05
750.	* I	-0.15
775.	* I	-0.15
800.	* I	-0.15
825.	* I	-0.15
850.	* I	-0.15
875.	* I	-0.15
900.	*I	-0.05
925.	* I	-0.15
950.	*I	-0.05
975.	* I	-0.15
1000.	* I	-0.15
1025.	*I	-0.05
1050.	* I	-0.15
1075.	*I	-0.05
1100.	*I	-0.05
1125.	* I	-0.15
1150.	* I	-0.15
1175.	*I	-0.05
1200.	*I	-0.05
1225.	*I	-0.05
1250.	*I	-0.05
1275.	*I	-0.05
1300.	*I	-0.05
1325.	*I	-0.05
1350.	*I	-0.05
1375.	*I	-0.05
1400.	*I	-0.05
1425.	*I	-0.05
1450.	* I	-0.15
1475.	* I	-0.15
1500.	*I	-0.05

XBOT= 1500.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 3400. S RELATIVE PHASE SHIFT RPS

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LINE# 044 3400. S FREQUENCY=3HZ N003

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFF	RPS	FFE	RPS								
500. E	4.60	0.85	-0.80	1.30	-0.60	1.25	0.17	108.82	6.74	-0.20	0.05	0.08	-0.37	500. E
525. E	4.60	0.86	-0.80	1.30	-0.60	1.25	0.17	107.56	5.92	-0.20	0.05	0.08	-0.37	525. E
550. E	4.60	0.99	-0.80	1.20	-0.60	1.25	0.18	121.06	16.85	-0.20	-0.05	-0.09	-0.43	550. E
575. E	4.60	0.90	-0.70	1.30	-0.60	1.25	0.18	107.68	6.28	-0.10	0.05	0.09	-0.20	575. E
600. E	4.60	0.92	-0.60	1.20	-0.60	1.25	0.19	107.78	6.49	0.00	-0.05	-0.09	0.00	600. E
625. E	4.60	0.94	-0.70	1.20	-0.60	1.25	0.19	107.92	6.75	-0.10	-0.05	-0.09	-0.20	625. E
650. E	4.60	0.95	-0.60	1.30	-0.60	1.25	0.19	106.99	6.07	0.00	0.05	0.09	0.00	650. E
675. E	4.60	0.97	-0.60	1.20	-0.60	1.25	0.20	107.27	6.43	0.00	-0.05	-0.09	0.00	675. E
700. E	4.60	1.00	-0.70	1.30	-0.60	1.25	0.20	108.70	7.83	-0.10	0.05	0.09	-0.22	700. E
725. E	4.60	1.00	-0.80	1.20	-0.60	1.25	0.20	106.96	6.37	-0.20	-0.05	-0.09	-0.43	725. E
750. E	4.60	1.03	-0.80	1.10	-0.60	1.25	0.21	108.54	7.92	-0.20	-0.15	-0.29	-0.45	750. E
775. E	4.60	1.04	-0.70	1.10	-0.60	1.25	0.21	108.10	7.62	-0.10	-0.15	-0.30	-0.23	775. E
800. E	4.60	1.05	-0.70	1.10	-0.60	1.25	0.21	107.79	7.42	-0.10	-0.15	-0.30	-0.23	800. E
825. E	4.60	1.07	-0.70	1.10	-0.60	1.25	0.21	108.63	8.32	-0.10	-0.15	-0.30	-0.23	825. E
850. E	4.60	1.10	-0.70	1.10	-0.60	1.25	0.22	110.60	10.31	-0.10	-0.15	-0.31	-0.24	850. E
875. E	4.60	1.13	-0.80	1.10	-0.60	1.25	0.22	112.68	12.44	-0.20	-0.15	-0.32	-0.49	875. E
900. E	4.60	1.15	-0.80	1.20	-0.60	1.25	0.22	113.89	13.72	-0.20	-0.05	-0.11	-0.50	900. E
925. E	4.60	1.21	-0.80	1.10	-0.60	1.25	0.22	119.19	19.06	-0.20	-0.15	-0.34	-0.53	925. E
950. E	4.60	1.22	-0.80	1.20	-0.60	1.25	0.22	119.72	19.66	-0.20	-0.05	-0.12	-0.53	950. E
975. E	4.60	1.20	-0.80	1.10	-0.60	1.25	0.22	117.48	17.47	-0.20	-0.15	-0.34	-0.52	975. E
1000. E	4.60	1.17	-0.90	1.10	-0.60	1.25	0.22	114.46	14.46	-0.30	-0.15	-0.33	-0.76	1000. E
1025. E	4.60	1.21	-0.80	1.20	-0.60	1.25	0.22	118.46	18.45	-0.20	-0.05	-0.11	-0.53	1025. E
1050. E	4.60	1.20	-0.80	1.10	-0.60	1.25	0.22	117.75	17.70	-0.20	-0.15	-0.34	-0.52	1050. E
1075. E	4.60	1.25	-0.70	1.20	-0.60	1.25	0.22	123.13	22.97	-0.10	-0.05	-0.12	-0.27	1075. E
1100. E	4.60	1.21	-0.80	1.20	-0.60	1.25	0.22	119.83	19.59	-0.20	-0.05	-0.11	-0.53	1100. E
1125. E	4.60	1.18	-0.80	1.10	-0.60	1.25	0.22	117.66	17.33	-0.20	-0.15	-0.34	-0.51	1125. E
1150. E	4.60	1.20	-0.80	1.10	-0.60	1.25	0.22	120.65	20.09	-0.20	-0.15	-0.34	-0.52	1150. E
1175. E	4.60	1.19	-0.90	1.20	-0.60	1.25	0.21	120.81	20.06	-0.30	-0.05	-0.11	-0.78	1175. E
1200. E	4.60	1.18	-0.90	1.20	-0.60	1.25	0.21	121.14	20.14	-0.30	-0.05	-0.11	-0.77	1200. E
1225. E	4.60	1.15	-1.00	1.20	-0.60	1.25	0.21	119.53	18.38	-0.40	-0.05	-0.11	-1.00	1225. E
1250. E	4.60	1.15	-0.90	1.20	-0.60	1.25	0.21	121.18	19.66	-0.30	-0.05	-0.11	-0.75	1250. E
1275. E	4.60	1.11	-1.00	1.20	-0.60	1.25	0.20	118.73	17.13	-0.40	-0.05	-0.11	-0.97	1275. E
1300. E	4.60	1.09	-0.90	1.20	-0.60	1.25	0.20	118.48	16.63	-0.30	-0.05	-0.10	-0.71	1300. E
1325. E	4.60	1.08	-1.10	1.20	-0.60	1.25	0.20	119.43	17.19	-0.50	-0.05	-0.10	-1.17	1325. E
1350. E	4.60	1.04	-1.10	1.20	-0.60	1.25	0.19	117.13	14.88	-0.50	-0.05	-0.10	-1.13	1350. E
1375. E	4.60	1.02	-1.00	1.20	-0.60	1.25	0.19	117.11	14.58	-0.40	-0.05	-0.10	-0.89	1375. E
1400. E	4.60	0.98	-1.10	1.20	-0.60	1.25	0.19	114.81	12.36	-0.50	-0.05	-0.09	-1.07	1400. E
1425. E	4.60	0.96	-1.10	1.20	-0.60	1.25	0.18	114.86	12.15	-0.50	-0.05	-0.09	-1.04	1425. E
1450. E	4.60	0.97	-1.10	1.10	-0.60	1.25	0.18	118.61	14.89	-0.50	-0.15	-0.28	-1.05	1450. E
1475. E	4.60	0.93	-1.00	1.10	-0.60	1.25	0.17	116.32	12.76	-0.40	-0.15	-0.26	-0.81	1475. E
1500. E	4.60	0.94	-0.90	1.20	-0.60	1.25	0.17	120.34	15.54	-0.30	-0.05	-0.09	-0.61	1500. E

045

XTOP= 500.

XINC= 25.00

201053

500.	*	-0.07
525.	*	0.08
550.	*	-0.08
575.	*	0.09
600.	*	0.09
625.	*	0.09
650.	*	-0.09
675.	*	0.09
700.	I*	0.29
725.	I*	0.30
750.	I*	0.10
775.	I*	0.10
800.	I*	0.11
825.	I*	0.11
850.	*I	-0.11
875.	I*	0.12
900.	I*	0.12
925.	I*	0.12
950.	I*	0.12
975.	*	0.00
1000.	I*	0.25
1025.	I*	0.26
1050.	*	0.00
1075.	I*	0.25
1100.	I*	0.27
1125.	*	0.00
1150.	*	0.00
1175.	I*	0.26
1200.	*	0.00
1225.	*	0.00
1250.	*	0.00
1275.	*	0.00
1300.	I*	0.23
1325.	I*	0.23
1350.	I*	0.22
1375.	I*	0.42
1400.	I*	0.21
1425.	I*	0.20
1450.	I*	0.19
1475.	I*	0.18
1500.	*	0.10

XBOT= 1500.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3200. S SECONDARY FIELD QUADRATURE HSQ/I

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201054

XTOP= 500.

XINC= 25.00

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XBOT= 1500.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 3200.9 RELATIVE PHASE SHIFT RPS

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LINE# 048 3200. S FREQUENCY=3HZ N003

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500. E	4.62	0.78	-0.50	1.20	-0.55	1.25	0.17	99.35	-0.50	0.05	-0.05	-0.07	0.08	500. E
525. E	4.62	0.84	-0.60	1.30	-0.55	1.25	0.17	104.23	3.32	-0.05	0.05	0.08	-0.09	525. E
550. E	4.62	0.85	-0.70	1.20	-0.55	1.25	0.18	102.81	2.26	-0.15	-0.05	-0.08	-0.28	550. E
575. E	4.62	0.91	-0.70	1.30	-0.55	1.25	0.18	107.35	6.07	-0.15	0.05	0.09	-0.30	575. E
600. E	4.62	0.94	-0.70	1.30	-0.55	1.25	0.19	108.23	6.97	-0.15	0.05	0.09	-0.31	600. E
625. E	4.62	0.93	-0.60	1.30	-0.55	1.25	0.19	104.60	3.98	-0.05	0.05	0.09	-0.10	625. E
650. E	4.62	0.96	-0.60	1.20	-0.55	1.25	0.20	105.57	4.93	-0.05	-0.05	-0.09	-0.10	650. E
675. E	4.62	0.99	-0.60	1.30	-0.55	1.25	0.20	106.54	5.92	-0.05	0.05	0.09	-0.11	675. E
700. E	4.62	1.03	-0.60	1.40	-0.55	1.25	0.21	108.59	7.94	-0.05	0.15	0.29	-0.11	700. E
725. E	4.62	1.05	-0.70	1.40	-0.55	1.25	0.21	108.58	8.08	-0.15	0.15	0.30	-0.34	725. E
750. E	4.62	1.08	-0.60	1.30	-0.55	1.25	0.21	109.68	9.28	-0.05	0.05	0.10	-0.12	750. E
775. E	4.62	1.11	-0.60	1.30	-0.55	1.25	0.22	110.85	10.58	-0.05	0.05	0.10	-0.12	775. E
800. E	4.62	1.16	-0.60	1.30	-0.55	1.25	0.22	114.09	13.95	-0.05	0.05	0.11	-0.13	800. E
825. E	4.62	1.16	-0.60	1.30	-0.55	1.25	0.22	112.53	12.58	-0.05	0.05	0.11	-0.13	825. E
850. E	4.62	1.18	-0.60	1.20	-0.55	1.25	0.23	113.10	13.31	-0.05	-0.05	-0.11	-0.13	850. E
875. E	4.62	1.22	-0.60	1.30	-0.55	1.25	0.23	115.72	16.14	-0.05	0.05	0.12	-0.13	875. E
900. E	4.62	1.22	-0.60	1.30	-0.55	1.25	0.23	114.73	15.26	-0.05	0.05	0.12	-0.13	900. E
925. E	4.62	1.27	-0.60	1.30	-0.55	1.25	0.23	118.63	19.43	-0.05	0.05	0.12	-0.14	925. E
950. E	4.62	1.29	-0.60	1.30	-0.55	1.25	0.23	119.91	20.87	-0.05	0.05	0.12	-0.14	950. E
975. E	4.62	1.31	-0.60	1.30	-0.55	1.30	0.23	121.42	22.51	-0.05	0.00	0.00	-0.14	975. E
1000. E	4.62	1.35	-0.60	1.40	-0.55	1.30	0.23	125.00	26.30	-0.05	0.10	0.25	-0.15	1000. E
1025. E	4.62	1.40	-0.60	1.40	-0.55	1.30	0.23	129.76	31.27	-0.05	0.10	0.26	-0.15	1025. E
1050. E	4.62	1.36	-0.60	1.30	-0.55	1.30	0.23	126.42	27.68	-0.05	0.00	0.00	-0.15	1050. E
1075. E	4.62	1.30	-0.60	1.40	-0.55	1.30	0.23	121.43	22.35	-0.05	0.10	0.25	-0.14	1075. E
1100. E	4.62	1.45	-0.60	1.40	-0.55	1.30	0.23	136.36	37.66	-0.05	0.10	0.27	-0.16	1100. E
1125. E	4.62	1.41	-0.60	1.30	-0.55	1.30	0.23	133.74	34.65	-0.05	0.00	0.00	-0.15	1125. E
1150. E	4.62	1.40	-0.60	1.30	-0.55	1.30	0.23	134.18	34.74	-0.05	0.00	0.00	-0.15	1150. E
1175. E	4.62	1.38	-0.60	1.40	-0.55	1.30	0.22	133.88	34.01	-0.05	0.10	0.26	-0.15	1175. E
1200. E	4.62	1.38	-0.70	1.30	-0.55	1.30	0.22	135.73	35.38	-0.15	0.00	0.00	-0.45	1200. E
1225. E	4.62	1.31	-0.70	1.30	-0.55	1.30	0.22	130.83	30.07	-0.15	0.00	0.00	-0.43	1225. E
1250. E	4.62	1.30	-0.70	1.30	-0.55	1.30	0.21	132.02	30.71	-0.15	0.00	0.00	-0.42	1250. E
1275. E	4.62	1.24	-0.70	1.30	-0.55	1.30	0.21	128.22	26.59	-0.15	0.00	0.00	-0.40	1275. E
1300. E	4.62	1.22	-0.70	1.40	-0.55	1.30	0.21	128.62	26.44	-0.15	0.10	0.23	-0.40	1300. E
1325. E	4.62	1.20	-0.80	1.40	-0.55	1.30	0.20	129.14	26.37	-0.25	0.10	0.23	-0.65	1325. E
1350. E	4.62	1.15	-0.80	1.40	-0.55	1.30	0.20	126.46	23.44	-0.25	0.10	0.22	-0.62	1350. E
1375. E	4.62	1.11	-0.80	1.50	-0.55	1.30	0.19	124.85	21.52	-0.25	0.20	0.42	-0.60	1375. E
1400. E	4.62	1.12	-0.80	1.40	-0.55	1.30	0.19	128.96	24.50	-0.25	0.10	0.21	-0.61	1400. E
1425. E	4.62	1.07	-0.90	1.40	-0.55	1.30	0.18	126.23	21.65	-0.35	0.10	0.20	-0.81	1425. E
1450. E	4.62	1.00	-0.80	1.40	-0.55	1.30	0.18	120.95	16.87	-0.25	0.10	0.19	-0.54	1450. E
1475. E	4.62	0.95	-0.90	1.40	-0.55	1.30	0.17	117.88	14.04	-0.35	0.10	0.18	-0.72	1475. E
1500. E	4.62	1.05	-0.90	1.40	-0.55	1.35	0.17	133.74	25.80	-0.35	0.05	0.10	-0.80	1500. E

049

201057

XTOP= 500.

XINC= 25.00

500.	*	-0.07
525.	I*	0.13
550.	I*	0.14
575.	*	0.00
600.	I*	0.15
625.	I*	0.17
650.	*	0.00
675.	*	0.00
700.	*	0.00
725.	*	0.00
750.	*	0.00
775.	*	0.00
800.	*	0.00
825.	*	0.00
850.	*	0.00
875.	*	0.00
900.	*	0.00
925.	*	0.00
950.	*	0.00
975.	*	0.00
1000.	*	0.00
1025.	I *	0.33
1050.	I*	0.17
1075.	I*	0.17
1100.	I*	0.17
1125.	I*	0.17
1150.	I*	0.17
1175.	I*	0.17
1200.	I*	0.16
1225.	I*	0.16
1250.	I *	0.47
1275.	I *	0.44
1300.	I *	0.41
1325.	I*	0.13
1350.	I*	0.13
1375.	I*	0.12
1400.	I*	0.11
1425.	I*	0.11
1450.	I*	0.10
1475.	I*	0.10
1500.	*	0.09

XBOT= 1500.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3000. S SECONDARY FIELD QUADRATURE HSQ/I

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500. E	4. 60	0. 70	-0. 60	1. 20	-0. 60	1. 25	0. 17	91. 12	-6. 68	0. 00	-0. 05	-0. 07	0. 00	500. E
525. E	4. 60	0. 71	-0. 70	1. 30	-0. 60	1. 20	0. 17	89. 22	-8. 39	-0. 10	0. 10	0. 13	-0. 15	525. E
550. E	4. 60	0. 76	-0. 70	1. 30	-0. 60	1. 20	0. 18	92. 20	-6. 29	-0. 10	0. 10	0. 14	-0. 17	550. E
575. E	4. 60	0. 78	-0. 60	1. 20	-0. 60	1. 20	0. 19	91. 36	-7. 22	0. 00	0. 00	0. 00	0. 00	575. E
600. E	4. 60	0. 80	-0. 60	1. 30	-0. 60	1. 20	0. 19	90. 48	-8. 24	0. 00	0. 10	0. 15	0. 00	600. E
625. E	4. 60	0. 90	-0. 60	1. 30	-0. 60	1. 20	0. 20	98. 31	-1. 51	0. 00	0. 10	0. 17	0. 00	625. E
650. E	4. 60	0. 77	-0. 60	1. 20	-0. 60	1. 20	0. 21	81. 28	-17. 35	0. 00	0. 00	0. 00	0. 00	650. E
675. E	4. 60	0. 99	-0. 70	1. 20	-0. 60	1. 20	0. 21	101. 04	1. 00	-0. 10	0. 00	0. 00	-0. 22	675. E
700. E	4. 60	0. 98	-0. 60	1. 20	-0. 60	1. 20	0. 22	96. 80	-3. 17	0. 00	0. 00	0. 00	0. 00	700. E
725. E	4. 60	1. 04	-0. 60	1. 20	-0. 60	1. 20	0. 23	99. 52	-0. 49	0. 00	0. 00	0. 00	0. 00	725. E
750. E	4. 60	1. 05	-0. 60	1. 20	-0. 60	1. 20	0. 23	97. 47	-2. 66	0. 00	0. 00	0. 00	0. 00	750. E
775. E	4. 60	1. 17	-0. 60	1. 20	-0. 60	1. 20	0. 24	105. 54	6. 00	0. 00	0. 00	0. 00	0. 00	775. E
800. E	4. 60	1. 29	-0. 70	1. 20	-0. 60	1. 20	0. 25	113. 28	14. 79	-0. 10	0. 00	0. 00	-0. 28	800. E
825. E	4. 60	1. 23	-0. 60	1. 20	-0. 60	1. 20	0. 25	105. 39	6. 15	0. 00	0. 00	0. 00	0. 00	825. E
850. E	4. 60	1. 28	-0. 60	1. 20	-0. 60	1. 20	0. 26	107. 27	8. 49	0. 00	0. 00	0. 00	0. 00	850. E
875. E	4. 60	1. 40	-0. 60	1. 20	-0. 60	1. 20	0. 26	115. 09	17. 95	0. 00	0. 00	0. 00	0. 00	875. E
900. E	4. 60	1. 46	-0. 70	1. 20	-0. 60	1. 20	0. 27	118. 09	21. 88	-0. 10	0. 00	0. 00	-0. 32	900. E
925. E	4. 60	1. 55	-0. 60	1. 20	-0. 60	1. 20	0. 27	123. 76	29. 11	0. 00	0. 00	0. 00	0. 00	925. E
950. E	4. 60	1. 58	-0. 70	1. 20	-0. 60	1. 20	0. 27	124. 98	30. 89	-0. 10	0. 00	0. 00	-0. 34	950. E
975. E	4. 60	1. 68	-0. 70	1. 20	-0. 60	1. 20	0. 28	132. 14	39. 97	-0. 10	0. 00	0. 00	-0. 37	975. E
1000. E	4. 60	1. 70	-0. 70	1. 20	-0. 60	1. 20	0. 28	133. 45	41. 69	-0. 10	0. 00	0. 00	-0. 37	1000. E
1025. E	4. 60	1. 74	-0. 70	1. 30	-0. 60	1. 20	0. 28	136. 85	45. 84	-0. 10	0. 10	0. 33	-0. 38	1025. E
1050. E	4. 60	1. 77	-0. 70	1. 20	-0. 60	1. 15	0. 27	140. 01	49. 48	-0. 10	0. 05	0. 17	-0. 38	1050. E
1075. E	4. 60	1. 80	-0. 70	1. 20	-0. 60	1. 15	0. 27	143. 72	53. 57	-0. 10	0. 05	0. 17	-0. 39	1075. E
1100. E	4. 60	1. 81	-0. 60	1. 20	-0. 60	1. 15	0. 27	146. 40	56. 11	0. 00	0. 05	0. 17	0. 00	1100. E
1125. E	4. 60	1. 80	-0. 70	1. 20	-0. 60	1. 15	0. 26	147. 97	57. 08	-0. 10	0. 05	0. 17	-0. 39	1125. E
1150. E	4. 60	1. 78	-0. 70	1. 20	-0. 60	1. 15	0. 26	149. 17	57. 40	-0. 10	0. 05	0. 17	-0. 39	1150. E
1175. E	4. 60	1. 75	-0. 70	1. 20	-0. 60	1. 15	0. 25	149. 94	57. 02	-0. 10	0. 05	0. 17	-0. 38	1175. E
1200. E	4. 60	1. 72	-0. 80	1. 20	-0. 60	1. 15	0. 25	151. 04	56. 86	-0. 20	0. 05	0. 16	-0. 75	1200. E
1225. E	4. 60	1. 70	-0. 80	1. 20	-0. 60	1. 15	0. 24	153. 34	57. 85	-0. 20	0. 05	0. 16	-0. 74	1225. E
1250. E	4. 60	1. 64	-0. 80	1. 30	-0. 60	1. 15	0. 23	152. 24	55. 05	-0. 20	0. 15	0. 47	-0. 71	1250. E
1275. E	4. 60	1. 56	-0. 80	1. 30	-0. 60	1. 15	0. 23	149. 28	50. 38	-0. 20	0. 15	0. 44	-0. 68	1275. E
1300. E	4. 60	1. 45	-0. 80	1. 30	-0. 60	1. 15	0. 22	143. 22	42. 81	-0. 20	0. 15	0. 41	-0. 63	1300. E
1325. E	4. 60	1. 42	-0. 80	1. 20	-0. 60	1. 15	0. 21	144. 93	43. 06	-0. 20	0. 05	0. 13	-0. 62	1325. E
1350. E	4. 60	1. 37	-0. 80	1. 20	-0. 60	1. 15	0. 21	144. 61	41. 34	-0. 20	0. 05	0. 13	-0. 60	1350. E
1375. E	4. 60	1. 28	-0. 80	1. 20	-0. 60	1. 15	0. 20	139. 82	35. 66	-0. 20	0. 05	0. 12	-0. 56	1375. E
1400. E	4. 60	1. 19	-0. 80	1. 20	-0. 60	1. 15	0. 19	134. 58	29. 91	-0. 20	0. 05	0. 11	-0. 52	1400. E
1425. E	4. 60	1. 16	-0. 90	1. 20	-0. 60	1. 15	0. 19	135. 87	29. 96	-0. 30	0. 05	0. 11	-0. 76	1425. E
1450. E	4. 60	1. 10	-1. 00	1. 20	-0. 60	1. 15	0. 18	133. 45	26. 97	-0. 40	0. 05	0. 10	-0. 96	1450. E
1475. E	4. 60	1. 06	-1. 00	1. 20	-0. 60	1. 15	0. 17	133. 21	25. 85	-0. 40	0. 05	0. 10	-0. 92	1475. E
1500. E	4. 60	1. 00	-1. 00	1. 20	-0. 60	1. 15	0. 17	130. 17	22. 67	-0. 40	0. 05	0. 09	-0. 87	1500. E

053

053

201061

UNITS FLAG= 0 CURRENT ELECTRODE CO-ORDS= 1000. E 2500. S 1000. 4300. S

PLOT SCALE= 2500. HN SCALE 10. PFE & RPS SCALE= 1. HSQ & HSP SCALE= 1.

ORIGIN CO-ORDS= 500. E 3800. S ARRAY IDENTIFIER= LN03 ANNOTATION SUPPRESSION FLAG= 0

SPLINE INTERVAL= 0.

PLOT BASE LEVELS FOR PFE, RPS, HSQ, HSP ARE 0.00 0.00 0.00 0.00

PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

HN	=	0
MMR	=	1
PFE	=	0
RPS	=	1
HSQ	=	1
HSP	=	0

FOR HN , MMR 100.00 0.00

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05A LINE FLAG= 0 GRIDDATA TAPE FLAG= 0

201062

LINE POSITIONING MULTIPLYING FACTOR= 1.0

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201063

PROGRAM MIP2 . CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

3HZ RRMIP SURVEY LOONGANA AREA TAS 068R ARRAY N003

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057

XTOP= 500.

XINC= 25.00

201065

500.	I	*	0.40
525.	I	*	0.40
550.	I	*	0.30
575.	I	*	0.20
600.	I	*	0.20
625.	I	*	0.10
650.	I	*	0.10
675.	*		0.00
700.	I	*	0.10
725.	I	*	0.20
750.	I	*	0.30
775.	I	*	0.20
800.	I	*	0.30
825.	I	*	0.40
850.	I	*	0.40
875.	I	*	0.30
900.	I	*	0.40
925.	I	*	0.30
950.	I	*	0.30
975.	I	*	0.40
1000.	I	*	0.30
1025.	I	*	0.15
1050.	I	*	0.25
1075.	I	*	0.25
1100.	I	*	0.15
1125.	I	*	0.15
1150.	I	*	0.25
1175.	I	*	0.35
1200.	I	*	0.35
1225.	I	*	0.45
1250.	I	*	0.45
1275.	I	*	0.45
1300.	I	*	0.55
1325.	I	*	0.55
1350.	I	*	0.55
1375.	I	*	0.45
1400.	I	*	0.55
1425.	I	*	0.55
1450.	I	*	0.65
1475.	I	*	0.65
1500.	I	*	0.55

XBOT= 1500.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 2800. S RELATIVE PHASE SHIFT RPS

400

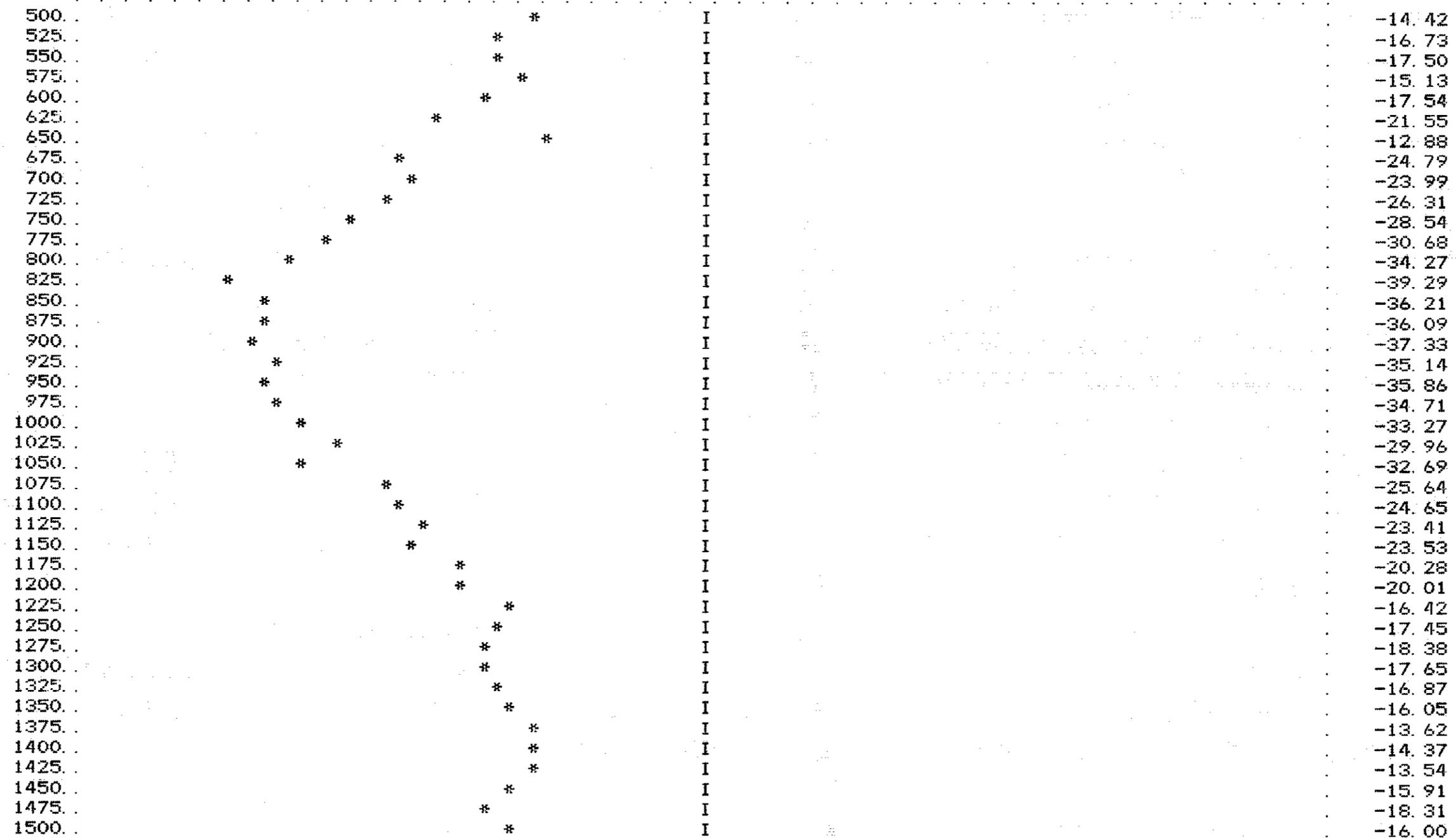
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058

XTOP= 500.

XINC= 25.00

201066



XBOT= 1500.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2800. S MAGNETOMETRIC RESESTIVITY MMR

066

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500. E	2.84	0.39	-1.10	-0.60	-0.40	-1.00	0.17	81.08	-14.42	-0.70	0.40	0.48	-0.96	500. E
525. E	2.84	0.39	-1.00	-0.60	-0.40	-1.00	0.17	78.70	-16.73	-0.60	0.40	0.48	-0.82	525. E
550. E	2.84	0.40	-0.60	-0.70	-0.40	-1.00	0.18	78.37	-17.50	-0.20	0.30	0.37	-0.28	550. E
575. E	2.84	0.43	-0.40	-0.80	-0.40	-1.00	0.19	81.83	-15.13	0.00	0.20	0.26	0.00	575. F
600. E	2.84	0.43	-0.40	-0.80	-0.40	-1.00	0.19	79.53	-17.54	0.00	0.20	0.26	0.00	600. E
625. E	2.84	0.42	-0.50	-0.90	-0.40	-1.00	0.20	75.54	-21.55	-0.10	0.10	0.13	-0.15	625. E
650. E	2.84	0.49	-0.50	-0.90	-0.40	-1.00	0.20	85.77	-12.88	-0.10	0.10	0.15	-0.17	650. E
675. E	2.84	0.43	-0.50	-1.00	-0.40	-1.00	0.21	73.32	-24.79	-0.10	0.00	0.00	-0.15	675. E
700. E	2.84	0.45	-0.60	-0.90	-0.40	-1.00	0.21	74.82	-23.99	-0.20	0.10	0.14	-0.32	700. E
725. E	2.84	0.45	-0.50	-0.80	-0.40	-1.00	0.22	73.05	-26.31	-0.10	0.20	0.28	-0.16	725. E
750. E	2.84	0.45	-0.40	-0.70	-0.40	-1.00	0.22	71.41	-28.54	0.00	0.30	0.41	0.00	750. E
775. E	2.84	0.45	-0.50	-0.80	-0.40	-1.00	0.23	69.92	-30.68	-0.10	0.20	0.28	-0.16	775. E
800. E	2.84	0.44	-0.60	-0.70	-0.40	-1.00	0.23	67.05	-34.27	-0.20	0.30	0.41	-0.31	800. E
825. E	2.84	0.42	-0.80	-0.60	-0.40	-1.00	0.24	62.88	-39.29	-0.40	0.40	0.52	-0.59	825. E
850. E	2.84	0.45	-0.90	-0.60	-0.35	-1.00	0.24	66.32	-36.21	-0.55	0.40	0.55	-0.87	850. E
875. E	2.84	0.46	-0.90	-0.70	-0.35	-1.00	0.24	66.88	-36.09	-0.55	0.30	0.42	-0.89	875. E
900. E	2.84	0.46	-1.00	-0.60	-0.35	-1.00	0.24	66.13	-37.33	-0.65	0.40	0.57	-1.05	900. E
925. E	2.84	0.48	-0.90	-0.70	-0.35	-1.00	0.25	68.40	-35.14	-0.55	0.30	0.44	-0.93	925. E
950. E	2.84	0.48	-1.00	-0.70	-0.35	-1.00	0.25	67.96	-35.86	-0.65	0.30	0.44	-1.10	950. E
975. E	2.84	0.49	-0.90	-0.60	-0.35	-1.00	0.5	69.10	-34.71	-0.55	0.40	0.60	-0.95	975. E
1000. E	2.84	0.50	-1.00	-0.70	-0.35	-1.00	0.25	70.42	-33.27	-0.65	0.30	0.46	-1.14	1000. F
1025. E	2.84	0.52	-0.90	-0.80	-0.35	-0.95	0.25	73.33	-29.96	-0.55	0.15	0.24	-1.01	1025. E
1050. E	2.84	0.50	-0.90	-0.70	-0.35	-0.95	0.25	70.79	-32.69	-0.55	0.25	0.38	-0.97	1050. E
1075. E	2.84	0.54	-1.00	-0.70	-0.35	-0.95	0.25	76.95	-25.64	-0.65	0.25	0.41	-1.24	1075. E
1100. E	2.84	0.54	-1.00	-0.80	-0.35	-0.95	0.24	77.63	-24.65	-0.65	0.15	0.25	-1.24	1100. E
1125. E	2.84	0.54	-0.90	-0.80	-0.35	-0.95	0.24	78.51	-23.41	-0.55	0.15	0.25	-1.05	1125. E
1150. E	2.84	0.53	-1.00	-0.70	-0.35	-0.95	0.24	78.11	-23.53	-0.65	0.25	0.41	-1.21	

LINE= 059 2800. S FREQUENCY=3HZ ND02

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500. E	2.84	0.39	-1.10	-0.60	-0.40	-1.00	0.17	81.08	-14.42	-0.70	0.40	0.48	-0.96	500. E
525. E	2.84	0.39	-1.00	-0.60	-0.40	-1.00	0.17	78.70	-16.73	-0.60	0.40	0.48	-0.82	525. E
550. E	2.84	0.40	-0.60	-0.70	-0.40	-1.00	0.18	78.37	-17.50	-0.20	0.30	0.37	-0.28	550. E
575. E	2.84	0.43	-0.40	-0.80	-0.40	-1.00	0.19	81.83	-15.13	0.00	0.20	0.26	0.00	575. E
600. E	2.84	0.43	-0.40	-0.80	-0.40	-1.00	0.19	79.53	-17.54	0.00	0.20	0.26	0.00	600. E
625. E	2.84	0.42	-0.50	-0.90	-0.40	-1.00	0.20	75.54	-21.55	-0.10	0.10	0.13	-0.15	625. E
650. E	2.84	0.49	-0.50	-0.90	-0.40	-1.00	0.20	85.77	-12.88	-0.10	0.10	0.15	-0.17	650. E
675. E	2.84	0.43	-0.50	-1.00	-0.40	-1.00	0.21	73.32	-24.79	-0.10	0.00	0.00	-0.15	675. E
700. E	2.84	0.45	-0.60	-0.90	-0.40	-1.00	0.21	74.82	-23.99	-0.20	0.10	0.14	-0.32	700. E
725. E	2.84	0.45	-0.50	-0.80	-0.40	-1.00	0.22	73.05	-26.31	-0.10	0.20	0.28	-0.16	725. E
750. E	2.84	0.45	-0.40	-0.70	-0.40	-1.00	0.22	71.41	-28.54	0.00	0.30	0.41	0.00	750. E
775. E	2.84	0.45	-0.50	-0.80	-0.40	-1.00	0.23	69.92	-30.68	-0.10	0.20	0.28	-0.16	775. E
800. E	2.84	0.44	-0.60	-0.70	-0.40	-1.00	0.23	67.05	-34.27	-0.20	0.30	0.41	-0.31	800. E
825. E	2.84	0.42	-0.80	-0.60	-0.40	-1.00	0.24	62.88	-39.29	-0.40	0.40	0.52	-0.59	825. E
850. E	2.84	0.45	-0.90	-0.60	-0.35	-1.00	0.24	66.32	-36.21	-0.55	0.40	0.55	-0.87	850. E
875. E	2.84	0.46	-0.90	-0.70	-0.35	-1.00	0.24	66.88	-36.09	-0.55	0.30	0.42	-0.89	875. E
900. E	2.84	0.46	-1.00	-0.60	-0.35	-1.00	0.24	66.13	-37.33	-0.65	0.40	0.57	-1.05	900. E
925. E	2.84	0.48	-0.90	-0.70	-0.35	-1.00	0.25	68.40	-35.14	-0.55	0.30	0.44	-0.93	925. E
950. E	2.84	0.48	-1.00	-0.70	-0.35	-1.00	0.25	67.96	-35.86	-0.65	0.30	0.44	-1.10	950. E
975. E	2.84	0.49	-0.90	-0.60	-0.35	-1.00	0.5	69.10	-34.71	-0.55	0.40	0.60	-0.95	975. E
1000. E	2.84	0.50	-1.00	-0.70	-0.35	-1.00	0.25	70.42	-33.27	-0.65	0.30	0.46	-1.14	1000. E
1025. E	2.84	0.52	-0.90	-0.80	-0.35	-0.95	0.25	73.33	-29.96	-0.55	0.15	0.24	-1.01	1025. E
1050. E	2.84	0.50	-0.90	-0.70	-0.35	-0.95	0.25	70.79	-32.69	-0.55	0.25	0.38	-0.97	1050. E
1075. E	2.84	0.54	-1.00	-0.70	-0.35	-0.95	0.25	76.95	-25.64	-0.65	0.25	0.41	-1.24	1075. E
1100. E	2.84	0.54	-1.00	-0.80	-0.35	-0.95	0.24	77.63	-24.65	-0.65	0.15	0.25	-1.24	1100. E
1125. E	2.84	0.54	-0.90	-0.80	-0.35	-0.95	0.24	78.51	-23.41	-0.55	0.15	0.25	-1.05	1125. E
1150. E	2.84	0.53	-1.00	-0.70	-0.35	-0.95	0.24	78.11	-23.53	-0.65	0.25	0.41	-1.21	1150. E
1175. E	2.84	0.54	-1.10	-0.60	-0.35	-0.95	0.24	80.84	-20.28	-0.75	0.35	0.58	-1.43	1175. E
1200. E	2.84	0.53	-1.10	-0.60	-0.30	-0.95	0.23	80.76	-20.01	-0.80	0.35	0.57	-1.49	1200. E
1225. E	2.84	0.54	-1.20	-0.50	-0.30	-0.95	0.23	83.90	-16.42	-0.90	0.45	0.75	-1.71	1225. E
1250. E	2.84	0.52	-1.20	-0.50	-0.30	-0.95	0.22	82.52	-17.45	-0.90	0.45	0.72	-1.65	1250. E
1275. E	2.84	0.50	-1.20	-0.50	-0.30	-0.95	0.22	81.17	-18.38	-0.90	0.45	0.69	-1.58	1275. E
1300. E	2.84	0.49	-1.30	-0.40	-0.30	-0.95	0.21	81.47	-17.65	-1.00	0.55	0.83	-1.73	1300. E
1325. E	2.84	0.48	-1.30	-0.40	-0.30	-0.95	0.21	81.85	-16.87	-1.00	0.55	0.81	-1.69	1325. E
1350. E	2.84	0.47	-1.30	-0.40	-0.30	-0.95	0.20	82.27	-16.05	-1.00	0.55	0.79	-1.65	1350. E
1375. E	2.84	0.47	-1.30	-0.50	-0.30	-0.95	0.20	84.53	-13.62	-1.00	0.45	0.65	-1.65	1375. E
1400. E	2.84	0.45	-1.30	-0.40	-0.30	-0.95	0.19	83.23	-14.37	-1.00	0.55	0.76	-1.58	1400. E
1425. E	2.84	0.44	-1.30	-0.40	-0.30	-0.95	0.19	83.73	-13.54	-1.00	0.55	0.74	-1.55	1425. E
1450. E	2.84	0.41	-1.20	-0.30	-0.30	-0.95	0.18	80.33	-15.91	-0.90	0.65	0.82	-1.30	1450. E
1475. E	2.84	0.38	-1.30	-0.30	-0.30	-0.95	0.17	76.68	-18.31	-1.00	0.65	0.76	-1.34	1475. E
1500. E	2.84	0.38	-1.30	-0.40	-0.30	-0.95	0.17	79.00	-16.00	-1.00	0.55	0.64	-1.34	1500. E

061

XTOP= 500.

XINC= 25.00

201070

500.	I	*	0.40
525.	I	*	0.50
550.	I	*	0.50
575.	I	*	0.40
600.	I	*	0.35
625.	I	*	0.25
650.	I	*	0.25
675.	I	*	0.25
700.	I	*	0.25
725.	I	*	0.30
750.	I	*	0.30
775.	I	*	0.30
800.	I	*	0.20
825.	I	*	0.30
850.	I	*	0.35
875.	I	*	0.35
900.	I	*	0.35
925.	I	*	0.25
950.	I	*	0.35
975.	I	*	0.35
1000.	I	*	0.30
1025.	I	*	0.40
1050.	I	*	0.40
1075.	I	*	0.50
1100.	I	*	0.50
1125.	I	*	0.45
1150.	I	*	0.45
1175.	I	*	0.35
1200.	I	*	0.35
1225.	I	*	0.45
1250.	I	*	0.25
1275.	I	*	0.40
1300.	I	*	0.50
1325.	I	*	0.50
1350.	I	*	0.60
1375.	I	*	0.80
1400.	I	*	0.65
1425.	I	*	0.65
1450.	I	*	0.55
1475.	I	*	0.45
1500.	I	*	0.35

XBOT= 1500.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

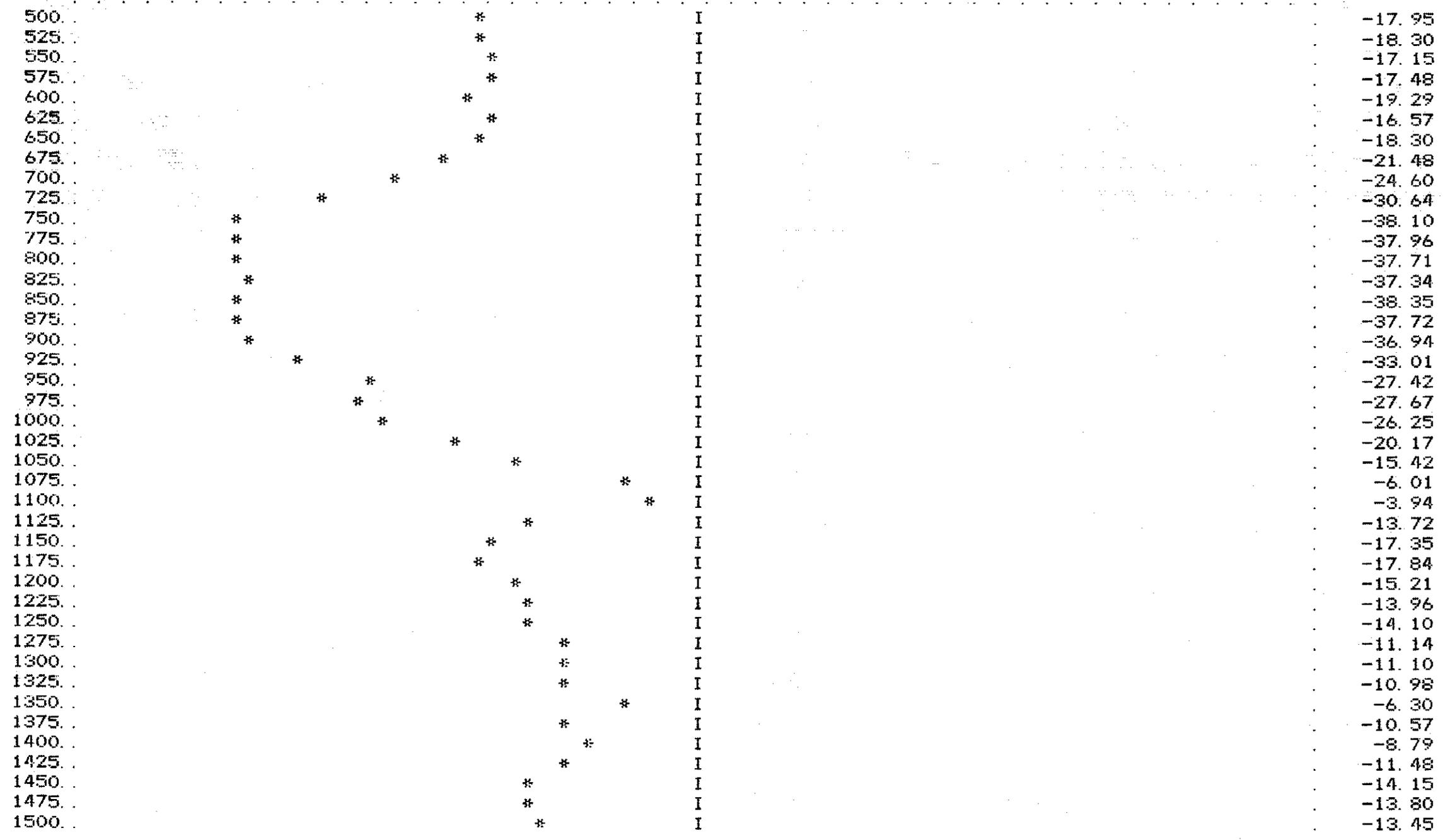
LINE 2600. S RELATIVE PHASE SHIFT RPS

069

201071

XTOP= 500.

XINC= 25.00



XBOT= 1500.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2600. S MAGNETOMETRIC RESESTIVITY MMR

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STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500. E	3.00	0.39	-0.90	-0.10	-0.45	-0.50	0.17	76.52	-17.95	-0.45	0.40	0.45	-0.59	500. E
525. E	3.00	0.40	-1.00	0.00	-0.45	-0.50	0.17	76.62	-18.30	-0.55	0.50	0.58	-0.73	525. E
550. E	3.00	0.42	-0.90	0.00	-0.45	-0.50	0.18	78.60	-17.15	-0.45	0.50	0.61	-0.63	550. E
575. E	3.00	0.43	-0.90	-0.10	-0.45	-0.50	0.18	78.67	-17.48	-0.45	0.40	0.50	-0.65	575. E
600. E	3.00	0.43	-0.90	-0.10	-0.45	-0.45	0.19	76.98	-19.29	-0.45	0.35	0.44	-0.65	600. E
625. E	3.00	0.46	-0.80	-0.20	-0.40	-0.45	0.19	80.64	-16.57	-0.40	0.25	0.33	-0.61	625. E
650. E	3.00	0.46	-0.80	-0.20	-0.40	-0.45	0.19	79.04	-18.30	-0.40	0.25	0.33	-0.61	650. E
675. E	3.00	0.45	-0.70	-0.20	-0.40	-0.45	0.20	75.86	-21.48	-0.30	0.25	0.33	-0.45	675. E
700. E	3.00	0.44	-0.70	-0.20	-0.40	-0.45	0.20	72.85	-24.60	-0.30	0.25	0.32	-0.44	700. E
725. E	3.00	0.41	-0.70	-0.10	-0.40	-0.40	0.20	66.74	-30.64	-0.30	0.30	0.36	-0.41	725. E
750. E	3.00	0.37	-0.80	-0.10	-0.40	-0.40	0.21	59.30	-38.10	-0.40	0.30	0.32	-0.49	750. E
775. E	3.00	0.38	-0.80	-0.10	-0.35	-0.40	0.21	60.03	-37.96	-0.45	0.30	0.33	-0.57	775. E
800. E	3.00	0.39	-0.80	-0.20	-0.35	-0.40	0.21	60.80	-37.71	-0.45	0.20	0.23	-0.59	800. E
825. E	3.00	0.40	-0.90	-0.10	-0.35	-0.40	0.22	61.64	-37.34	-0.55	0.30	0.35	-0.73	825. E
850. E	3.00	0.40	-0.80	0.00	-0.35	-0.35	0.22	61.01	-38.35	-0.45	0.35	0.41	-0.60	850. E
875. E	3.00	0.41	-0.90	0.00	-0.35	-0.35	0.22	61.99	-37.72	-0.55	0.35	0.42	-0.75	875. E
900. E	3.00	0.42	-1.00	0.00	-0.35	-0.35	0.22	63.04	-36.94	-0.65	0.35	0.43	-0.91	900. E
925. E	3.00	0.45	-1.00	-0.10	-0.30	-0.35	0.22	67.16	-33.01	-0.70	0.25	0.33	-1.05	925. E
950. E	3.00	0.49	-1.00	0.00	-0.30	-0.35	0.22	72.83	-27.42	-0.70	0.35	0.50	-1.14	950. E
975. E	3.00	0.49	-1.00	0.00	-0.30	-0.35	0.22	72.65	-27.67	-0.70	0.35	0.50	-1.14	975. E
1000. E	3.00	0.50	-1.00	0.00	-0.30	-0.30	0.23	74.07	-26.25	-0.70	0.30	0.44	-1.17	1000. E
1025. E	3.00	0.54	-1.00	0.10	-0.30	-0.30	0.22	80.07	-20.17	-0.70	0.40	0.63	-1.26	1025. E
1050. E	3.00	0.57	-0.90	0.10	-0.30	-0.30	0.22	84.72	-15.42	-0.60	0.40	0.66	-1.14	1050. E
1075. E	3.00	0.63	-1.00	0.20	-0.25	-0.30	0.22	94.02	-6.01	-0.75	0.50	0.92	-1.57	1075. E
1100. E	3.00	0.64	-1.00	0.20	-0.25	-0.30	0.22	96.06	-3.94	-0.75	0.50	0.93	-1.60	1100. E
1125. E	3.00	0.57	-0.90	0.20	-0.25	-0.25	0.22	86.17	-13.72	-0.65	0.45	0.75	-1.24	1125. E
1150. E	3.00	0.54	-0.90	0.20	-0.25	-0.25	0.22	82.36	-17.35	-0.65	0.45	0.71	-1.17	1150. E
1175. E	3.00	0.53	-0.90	0.10	-0.25	-0.25	0.22	81.67	-17.84	-0.65	0.35	0.54	-1.15	1175. E
1200. E	3.00	0.54	-1.00	0.10	-0.25	-0.25	0.21	84.19	-15.21	-0.75	0.35	0.55	-1.35	1200. E
1225. E	3.00	0.54	-1.10	0.20	-0.20	-0.25	0.21	85.30	-13.96	-0.90	0.45	0.71	-1.62	1225. E
1250. E	3.00	0.53	-1.10	0.00	-0.20	-0.25	0.21	84.94	-14.10	-0.90	0.25	0.39	-1.59	1250. E
1275. E	3.00	0.54	-1.10	0.20	-0.20	-0.20	0.20	87.91	-11.14	-0.90	0.40	0.63	-1.62	1275. E
1300. E	3.00	0.53	-1.20	0.30	-0.20	-0.20	0.20	87.75	-11.10	-1.00	0.50	0.77	-1.77	1300. E
1325. E	3.00	0.52	-1.20	0.30	-0.20	-0.20	0.20	87.66	-10.98	-1.00	0.50	0.76	-1.73	1325. E
1350. E	3.00	0.54	-1.40	0.40	-0.20	-0.20	0.19	92.78	-6.30	-1.20	0.60	0.94	-2.16	1350. E
1375. E	3.00	0.50	-1.60	0.60	-0.20	-0.20	0.19	87.65	-10.57	-1.40	0.80	1.16	-2.33	1375. E
1400. E	3.00	0.50	-1.50	0.50	-0.15	-0.15	0.19	89.51	-8.79	-1.35	0.65	0.95	-2.25	1400. E
1425. E	3.00	0.47	-1.40	0.50	-0.15	-0.15	0.18	85.99	-11.48	-1.25	0.65	0.89	-1.96	1425. E
1450. E	3.00	0.44	-1.30	0.40	-0.15	-0.15	0.18	82.34	-14.15	-1.15	0.55	0.70	-1.69	1450. E
1475. E	3.00	0.43	-1.40	0.30	-0.15	-0.15	0.17	82.37	-13.80	-1.25	0.45	0.56	-1.79	1475. E
1500. E	3.00	0.42	-1.40	0.20	-0.15	-0.15	0.17	82.41	-13.45	-1.25	0.35	0.43	-1.75	1500. E

XTOP= 500.

XINC= 25.00

071

500.	I*	0.28
525.	I*	0.29
550.	I*	0.29
575.	I *	0.42
600.	I *	0.54
625.	I *	0.52
650.	I *	0.44
675.	I *	0.35
700.	I *	0.37
725.	I *	0.36
750.	I *	0.48
775.	I *	0.37
800.	I *	0.37
825.	I *	0.52
850.	I *	0.37
875.	I *	0.53
900.	I *	0.41
925.	I *	0.41
950.	I*	0.28
975.	I*	0.15
1000.	I *	0.31
1025.	*	0.08
1050.	I*	0.26
1075.	I *	0.42
1100.	I *	0.59
1125.	I *	0.55
1150.	I *	0.52
1175.	I *	0.66
1200.	I *	0.65
1225.	I *	0.51
1250.	I *	0.68
1275.	I *	0.66
1300.	I *	0.64
1325.	I *	0.62
1350.	I *	0.59
1375.	I *	0.58
1400.	I *	0.55
1425.	I *	0.53
1450.	I *	0.70
1475.	I *	0.70
1500.	I *	0.62

XBOT= 1500.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 2400. S SECONDARY FIELD QUADRATURE HSQ/I

XTOP# 500.

XINC= 25.00

201074

072

500.	I	*	0.30
525.	I	*	0.30
550.	I	*	0.30
575.	I	*	0.40
600.	I	*	0.50
625.	I	*	0.50
650.	I	*	0.40
675.	I	*	0.30
700.	I	*	0.30
725.	I	*	0.30
750.	I	*	0.40
775.	I	*	0.30
800.	I	*	0.30
825.	I	*	0.40
850.	I	*	0.30
875.	I	*	0.40
900.	I	*	0.30
925.	I	*	0.30
950.	I	*	0.20
975.	I	*	0.10
1000.	I	*	0.20
1025.	I*	*	0.05
1050.	I	*	0.15
1075.	I	*	0.25
1100.	I	*	0.35
1125.	I	*	0.35
1150.	I	*	0.35
1175.	I	*	0.45
1200.	I	*	0.45
1225.	I	*	0.35
1250.	I	*	0.45
1275.	I	*	0.45
1300.	I	*	0.45
1325.	I	*	0.45
1350.	I	*	0.45
1375.	I	*	0.45
1400.	I	*	0.45
1425.	I	*	0.45
1450.	I	*	0.65
1475.	I	*	0.65
1500.	I	*	0.65

XBOT= 1500.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

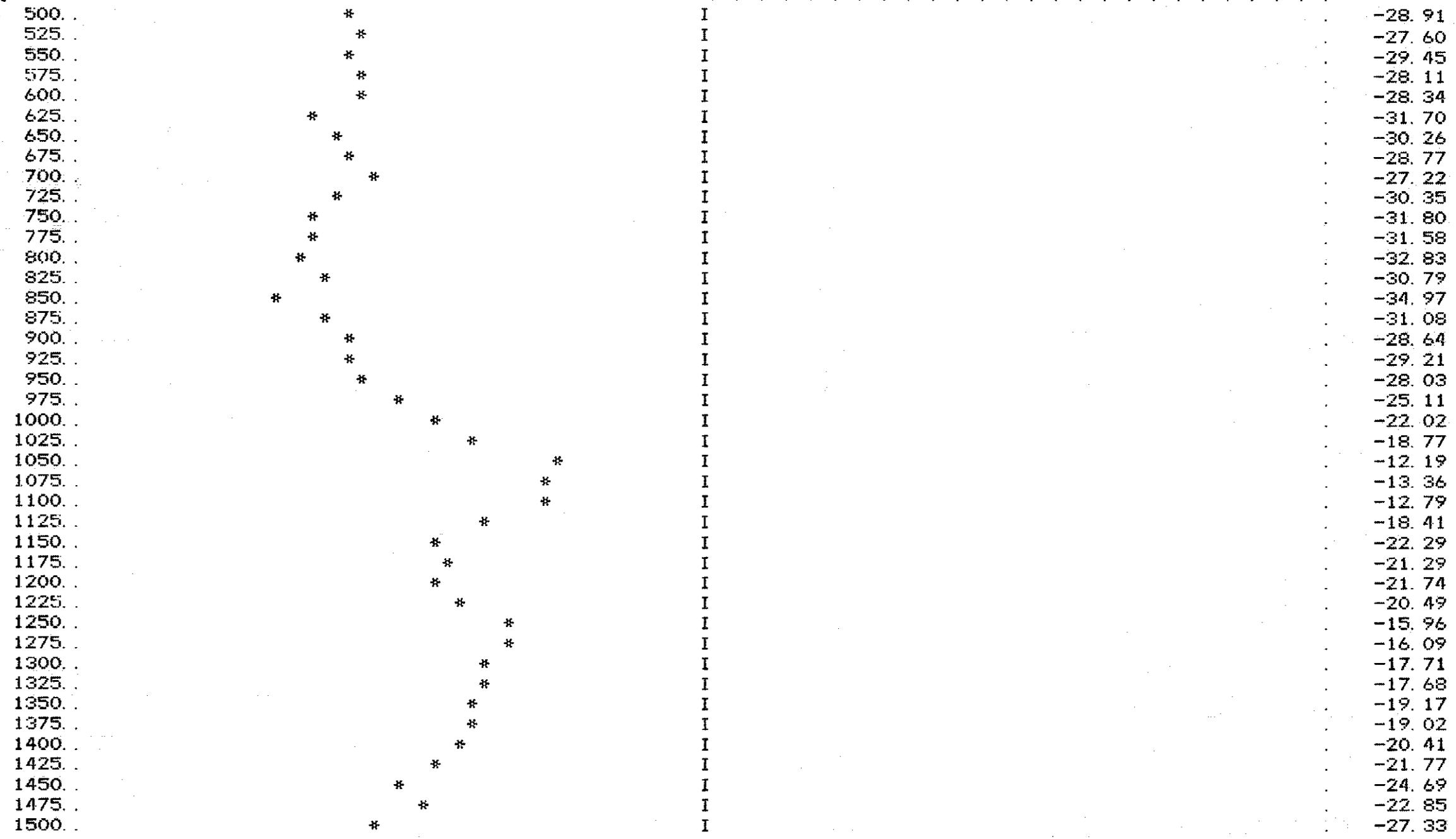
LINE 2400. S RELATIVE PHASE SHIFT RPS

073

XTOP= 500.

XINC= 25.00

201075



XBOT= 1500.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2400. S MAGNETOMETRIC RESESTIVITY MMR

LINE= 2400. S FREQUENCY=3HZ N002

074

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500. E	2.84	0.30	-1.30	1.80	-1.00	1.50	0.17	62.18	-28.91	-0.30	0.30	0.28	-0.32	500. E
525. E	2.84	0.32	-1.50	1.80	-1.00	1.50	0.17	64.75	-27.60	-0.50	0.30	0.29	-0.56	525. E
550. E	2.84	0.32	-1.60	1.80	-1.00	1.50	0.18	63.26	-29.45	-0.60	0.30	0.29	-0.68	550. E
575. E	2.84	0.34	-1.50	1.90	-1.00	1.50	0.18	65.71	-28.11	-0.50	0.40	0.42	-0.60	575. E
600. E	2.84	0.35	-1.60	2.00	-1.00	1.50	0.19	66.18	-28.34	-0.60	0.50	0.54	-0.74	600. E
625. E	2.84	0.34	-1.60	2.00	-1.00	1.50	0.19	62.96	-31.70	-0.60	0.50	0.52	-0.72	625. E
650. E	2.84	0.36	-1.70	1.90	-1.00	1.50	0.19	65.34	-30.26	-0.70	0.40	0.44	-0.89	650. E
675. E	2.84	0.38	-1.80	1.80	-1.00	1.50	0.20	67.67	-28.77	-0.80	0.30	0.35	-1.07	675. E
700. E	2.84	0.40	-1.80	1.80	-1.00	1.50	0.20	69.96	-27.22	-0.80	0.30	0.37	-1.13	700. E
725. E	2.84	0.39	-1.80	1.80	-1.00	1.50	0.20	67.07	-30.35	-0.80	0.30	0.36	-1.10	725. E
750. E	2.84	0.39	-1.80	1.90	-1.00	1.50	0.21	66.02	-31.80	-0.80	0.40	0.48	-1.10	750. E
775. E	2.84	0.40	-1.60	1.80	-1.00	1.50	0.21	66.75	-31.58	-0.60	0.30	0.37	-0.85	775. E
800. E	2.84	0.40	-1.40	1.80	-1.00	1.50	0.21	65.88	-32.83	-0.40	0.30	0.37	-0.56	800. E
825. E	2.84	0.42	-1.40	1.90	-1.00	1.50	0.22	68.37	-30.79	-0.40	0.40	0.52	-0.59	825. E
850. E	2.84	0.40	-1.40	1.80	-1.00	1.50	0.22	64.44	-34.97	-0.40	0.30	0.37	-0.56	850. E
875. E	2.84	0.43	-1.50	1.90	-1.00	1.50	0.22	68.67	-31.08	-0.50	0.40	0.53	-0.76	875. E
900. E	2.84	0.45	-1.50	1.80	-1.00	1.50	0.22	71.35	-28.64	-0.50	0.30	0.41	-0.79	900. E
925. E	2.84	0.45	-1.60	1.80	-1.00	1.50	0.22	70.94	-29.21	-0.60	0.30	0.41	-0.95	925. E
950. E	2.84	0.46	-1.70	1.70	-1.00	1.50	0.22	72.22	-28.03	-0.70	0.20	0.28	-1.13	950. E
975. E	2.84	0.48	-1.60	1.60	-1.00	1.50	0.22	75.18	-25.11	-0.60	0.10	0.15	-1.01	975. E
1000. E	2.84	0.50	-1.60	1.70	-1.00	1.50	0.23	78.25	-22.02	-0.60	0.20	0.31	-1.06	1000. E
1025. E	2.84	0.52	-1.50	1.60	-1.00	1.55	0.22	81.44	-18.77	-0.50	0.05	0.08	-0.92	1025. E
1050. E	2.84	0.56	-1.40	1.70	-1.00	1.55	0.22	87.92	-12.19	-0.40	0.15	0.26	-0.79	1050. E
1075. E	2.84	0.55	-1.60	1.80	-1.00	1.55	0.22	86.71	-13.36	-0.60	0.25	0.42	-1.16	1075. E
1100. E	2.84	0.55	-1.80	1.90	-1.00	1.55	0.22	87.20	-12.79	-0.80	0.35	0.59	-1.55	1100. E
1125. E	2.84	0.51	-1.70	1.90	-1.00	1.55	0.22	81.45	-18.41	-0.70	0.35	0.55	-1.26	1125. E
1150. E	2.84	0.48	-1.80	1.90	-1.00	1.55	0.22	77.33	-22.29	-0.80	0.35	0.52	-1.35	1150. E
1175. E	2.84	0.48	-1.80	2.00	-1.00	1.55	0.22	78.13	-21.29	-0.80	0.45	0.66	-1.35	1175. E
1200. E	2.84	0.47	-1.90	2.00	-1.00	1.55	0.21	77.41	-21.74	-0.90	0.45	0.65	-1.49	1200. E
1225. E	2.84	0.47	-1.80	1.90	-1.00	1.55	0.21	78.43	-20.49	-0.80	0.35	0.51	-1.32	1225. E
1250. E	2.84	0.49	-1.90	2.00	-1.00	1.55	0.21	82.95	-15.96	-0.90	0.45	0.68	-1.55	1250. E
1275. E	2.84	0.48	-2.00	2.00	-1.00	1.55	0.20	82.54	-16.09	-1.00	0.45	0.66	-1.69	1275. E
1300. E	2.84	0.46	-2.00	2.00	-1.00	1.55	0.20	80.45	-17.71	-1.00	0.45	0.64	-1.62	1300. E
1325. E	2.84	0.45	-2.10	2.00	-1.00	1.55	0.20	80.13	-17.68	-1.10	0.45	0.62	-1.74	1325. E
1350. E	2.84	0.43	-2.20	2.00	-1.00	1.55	0.19	78.04	-19.17	-1.20	0.45	0.59	-1.82	1350. E
1375. E	2.84	0.42	-2.20	2.00	-1.00	1.55	0.19	77.77	-19.02	-1.20	0.45	0.58	-1.77	1375. E
1400. E	2.84	0.40	-2.20	2.00	-1.00	1.55	0.19	75.64	-20.41	-1.20	0.45	0.55	-1.69	1400. E
1425. E	2.84	0.38	-2.20	2.00	-1.00	1.55	0.18	73.44	-21.77	-1.20	0.45	0.53	-1.61	1425. E
1450. E	2.84	0.35	-2.40	2.20	-1.00	1.55	0.18	69.19	-24.69	-1.40	0.65	0.70	-1.73	1450. E
1475. E	2.84	0.35	-2.40	2.20	-1.00	1.55	0.17	70.82	-22.85	-1.40	0.65	0.70	-1.73	1475. E
1500. E	2.84	0.31	-2.30	2.20	-1.00	1.55	0.17	64.25	-27.33	-1.30	0.65	0.62	-1.42	1500. E

XTOP= 500.

XINC= 25.00

201077

075

500.	I *	0.35
525.	I *	0.48
550.	I *	0.47
575.	I *	0.48
600.	I *	0.48
625.	I *	0.44
650.	I *	0.34
675.	I *	0.48
700.	I *	0.52
725.	I *	0.46
750.	I *	0.48
775.	I *	0.49
800.	I *	0.51
825.	I *	0.38
850.	I *	0.39
875.	I *	0.24
900.	I *	0.26
925.	*	0.09
950.	I *	0.27
975.	I *	0.38
1000.	I *	0.59
1025.	I *	0.38
1050.	I *	0.39
1075.	I *	0.53
1100.	I *	0.50
1125.	I *	0.48
1150.	I *	0.48
1175.	I *	0.63
1200.	I *	0.61
1225.	I *	0.68
1250.	I *	0.59
1275.	I *	0.55
1300.	I *	0.49
1325.	I *	0.62
1350.	I *	0.75
1375.	I *	0.72
1400.	I *	0.78
1425.	I *	0.79
1450.	I *	0.72
1475.	I *	0.78
1500.	I *	1.04

XBOT= 1500.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 2200. S SECONDARY FIELD QUADRATURE HSQ/I

076

XTOP= 500.

XINC= 25.00

201078

500.	I	*	0.40
525.	I	**	0.50
550.	I	**	0.50
575.	I	**	0.50
600.	I	**	0.50
625.	I	*	0.40
650.	I	*	0.30
675.	I	**	0.40
700.	I	**	0.40
725.	I	*	0.35
750.	I	**	0.35
775.	I	**	0.35
800.	I	*	0.35
825.	I	*	0.25
850.	I	*	0.25
875.	I	*	0.15
900.	I	*	0.15
925.	I*		0.05
950.	I	*	0.15
975.	I	*	0.20
1000.	I	*	0.30
1025.	I	*	0.20
1050.	I	*	0.20
1075.	I	*	0.30
1100.	I	**	0.30
1125.	I	**	0.30
1150.	I	*	0.30
1175.	I	*	0.40
1200.	I	**	0.40
1225.	I	*	0.45
1250.	I	*	0.35
1275.	I	**	0.35
1300.	I	*	0.35
1325.	I	*	0.45
1350.	I	*	0.55
1375.	I	*	0.55
1400.	I	**	0.65
1425.	I	**	0.65
1450.	I	**	0.65
1475.	I	*	0.65
1500.	I	*	0.85

XBOT= 1500.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 2200. S RELATIVE PHASE SHIFT RPS

078

201080

STATION LINE#	CURRENT 2200.8	HP FREQUENCY	---FIELD--- PFE 3HZ NOOZ	---OFFSET--- RFS	HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION		
500. E	3.00	0.30	-1.80	1.80	-1.10	1.40	0.17	59.04	-31.21	-0.70	0.40	0.35	-0.70	500. E
525. E	3.00	0.33	-1.80	1.90	-1.10	1.40	0.17	63.04	-29.02	-0.70	0.50	0.48	-0.77	525. E
550. E	3.00	0.32	-1.80	1.90	-1.10	1.40	0.18	59.35	-32.88	-0.70	0.50	0.47	-0.75	550. E
575. E	3.00	0.33	-1.70	1.90	-1.10	1.40	0.19	59.45	-33.76	-0.60	0.50	0.48	-0.66	575. E
600. E	3.00	0.33	-1.80	1.90	-1.10	1.40	0.19	57.78	-36.17	-0.70	0.50	0.48	-0.77	600. E
625. E	3.00	0.38	-1.70	1.80	-1.10	1.40	0.20	64.70	-31.10	-0.60	0.40	0.44	-0.76	625. E
650. E	3.00	0.39	-1.70	1.70	-1.10	1.40	0.20	64.63	-32.02	-0.60	0.30	0.34	-0.78	650. E
675. E	3.00	0.41	-1.60	1.80	-1.10	1.40	0.21	66.18	-31.42	-0.50	0.40	0.48	-0.68	675. E
700. E	3.00	0.45	-1.50	1.80	-1.10	1.40	0.21	70.83	-27.79	-0.40	0.40	0.52	-0.60	700. E
725. E	3.00	0.45	-1.60	1.80	-1.10	1.45	0.22	69.15	-30.11	-0.50	0.35	0.46	-0.75	725. E
750. E	3.00	0.47	-1.60	1.80	-1.10	1.45	0.22	70.61	-29.35	-0.50	0.35	0.48	-0.78	750. E
775. E	3.00	0.48	-1.50	1.80	-1.10	1.45	0.23	70.60	-29.98	-0.40	0.35	0.49	-0.64	775. E
800. E	3.00	0.50	-1.50	1.80	-1.10	1.45	0.23	72.12	-28.99	-0.40	0.35	0.51	-0.67	800. E
825. E	3.00	0.52	-1.40	1.70	-1.10	1.45	0.24	73.70	-27.84	-0.30	0.25	0.38	-0.52	825. E
850. E	3.00	0.54	-1.40	1.70	-1.05	1.45	0.24	75.34	-26.51	-0.35	0.25	0.39	-0.63	850. E
875. E	3.00	0.56	-1.40	1.60	-1.05	1.45	0.24	77.08	-24.98	-0.35	0.15	0.24	-0.65	875. E
900. E	3.00	0.59	-1.40	1.60	-1.05	1.45	0.24	80.30	-21.71	-0.35	0.15	0.26	-0.69	900. E
925. E	3.00	0.61	-1.40	1.50	-1.05	1.45	0.25	82.28	-19.70	-0.35	0.05	0.09	-0.71	925. E
950. E	3.00	0.62	-1.40	1.60	-1.05	1.45	0.25	83.10	-18.92	-0.35	0.15	0.27	-0.72	950. E
975. E	3.00	0.65	-1.40	1.70	-1.05	1.50	0.25	86.78	-14.85	-0.35	0.20	0.38	-0.76	975. E
1000. E	3.00	0.68	-1.40	1.80	-1.05	1.50	0.25	90.67	-10.50	-0.35	0.30	0.59	-0.79	1000. E
1025. E	3.00	0.66	-1.50	1.70	-1.05	1.50	0.25	88.11	-13.35	-0.45	0.20	0.38	-0.99	1025. E
1050. E	3.00	0.67	-1.60	1.70	-1.05	1.50	0.25	89.80	-11.42	-0.55	0.20	0.39	-1.23	1050. E
1075. E	3.00	0.61	-1.50	1.80	-1.05	1.50	0.25	82.28	-19.70	-0.45	0.30	0.53	-0.91	1075. E
1100. E	3.00	0.57	-1.60	1.80	-1.05	1.50	0.24	77.58	-24.71	-0.55	0.30	0.50	-1.04	1100. E
1125. E	3.00	0.55	-1.70	1.80	-1.05	1.50	0.24	75.70	-26.48	-0.65	0.30	0.48	-1.19	1125. E
1150. E	3.00	0.55	-1.80	1.80	-1.05	1.50	0.24	76.74	-25.01	-0.75	0.30	0.48	-1.38	1150. E
1175. E	3.00	0.54	-1.80	1.90	-1.00	1.50	0.24	76.53	-24.84	-0.80	0.40	0.63	-1.44	1175. E
1200. E	3.00	0.52	-1.80	1.90	-1.00	1.50	0.23	75.01	-25.99	-0.80	0.40	0.61	-1.39	1200. E
1225. E	3.00	0.52	-1.80	2.00	-1.00	1.55	0.23	76.49	-23.98	-0.80	0.45	0.68	-1.39	1225. E
1250. E	3.00	0.58	-1.90	1.90	-1.00	1.55	0.22	87.13	-12.85	-0.90	0.35	0.59	-1.74	1250. E
1275. E	3.00	0.54	-1.80	1.90	-1.00	1.55	0.22	82.98	-16.61	-0.80	0.35	0.55	-1.44	1275. E
1300. E	3.00	0.48	-1.70	1.90	-1.00	1.55	0.21	75.56	-23.29	-0.70	0.35	0.49	-1.12	1300. E
1325. E	3.00	0.47	-1.80	2.00	-1.00	1.55	0.21	75.87	-22.42	-0.80	0.45	0.62	-1.25	1325. E
1350. E	3.00	0.47	-1.90	2.10	-1.00	1.55	0.20	77.88	-20.02	-0.90	0.55	0.75	-1.41	1350. E
1375. E	3.00	0.45	-1.90	2.10	-1.00	1.55	0.20	76.62	-20.60	-0.90	0.55	0.72	-1.35	1375. E
1400. E	3.00	0.41	-2.00	2.20	-1.00	1.55	0.19	71.78	-24.17	-1.00	0.65	0.78	-1.37	1400. E
1425. E	3.00	0.42	-2.00	2.20	-1.00	1.55	0.19	75.66	-20.26	-1.00	0.65	0.79	-1.40	1425. E
1450. E	3.00	0.38	-2.00	2.20	-1.00	1.55	0.18	70.48	-23.88	-1.00	0.65	0.72	-1.27	1450. E
1475. E	3.00	0.41	-2.10	2.20	-1.00	1.55	0.17	78.32	-17.02	-1.10	0.65	0.78	-1.50	1475. E
1500. E	3.00	0.42	-2.20	2.40	-1.00	1.55	0.17	82.66	-13.21	-1.20	0.85	1.04	-1.68	1500. E

079

201081

UNITS FLAG= 0 CURRENT ELECTRODE CO-ORDS= 1000. E 1600. S 1000. E 3400. S
 PLOT SCALE= 2500. HN SCALE 10. PFE & RPS SCALE= 1. HSQ & HSP SCALE= 1.
 ORIGIN CO-ORDS= 500. E 2800. S ARRAY IDENTIFIER= LN02 ANNOTATION SUPPRESSION FLAG= 0
 SPLINE INTERVAL= 0.
 PLOT BASE LEVELS FOR PFE, RPS, HSQ, HSP ARE 0.00 0.00 0.00 0.00

PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

HN = 0
 MMR = 1
 PFE = 0
 RPS = 1
 HSQ = 1
 HSP = 0

FOR HN , MMR 100.00 0.00

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201082

INTERP TAPE FLAG= 0 GRIDDATA TAPE FLAG= 0

LINE POSITIONING MULTIPLYING FACTOR= 1.0

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PROGRAM MIP2 . CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS
 3HZ RRMIP SURVEY LOONGANA AREA TAS 068R ARRAYND02

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082

201084

XTOP# 500.

XINC# 25.00

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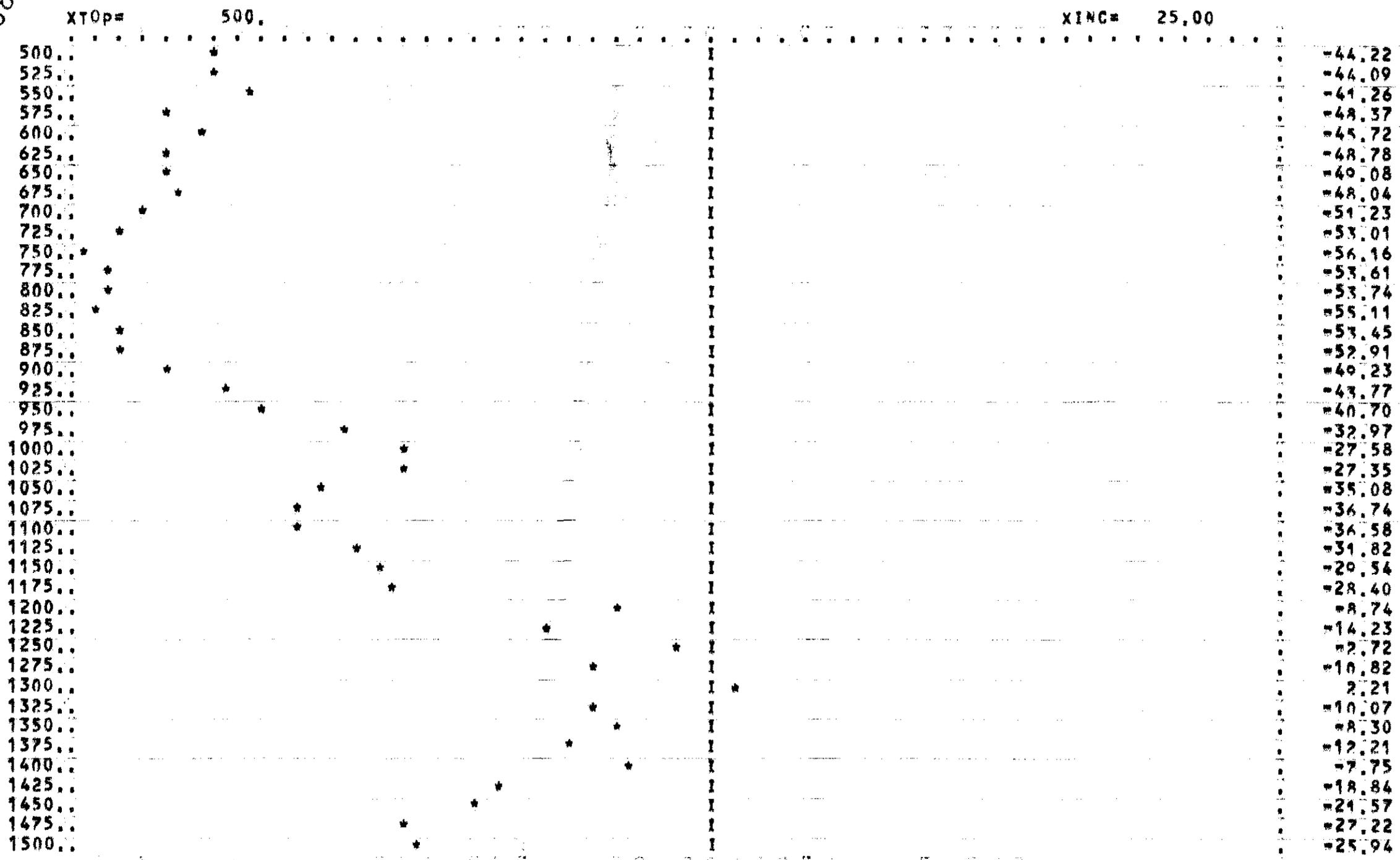
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XBOT# 1500.
YMIN# -10.00

YINC# 0.2000
YMAX# 10.00

LINE 2000.S SECONDARY FIELD QUADRATURE MSQ/I

084



XBOT= 1500.
YMIN= 56.16

YINC= 1.062
YMAX= 50.00

LINE 2000.S MAGNETOMETRIC RESISTIVITY MMR

085

201087

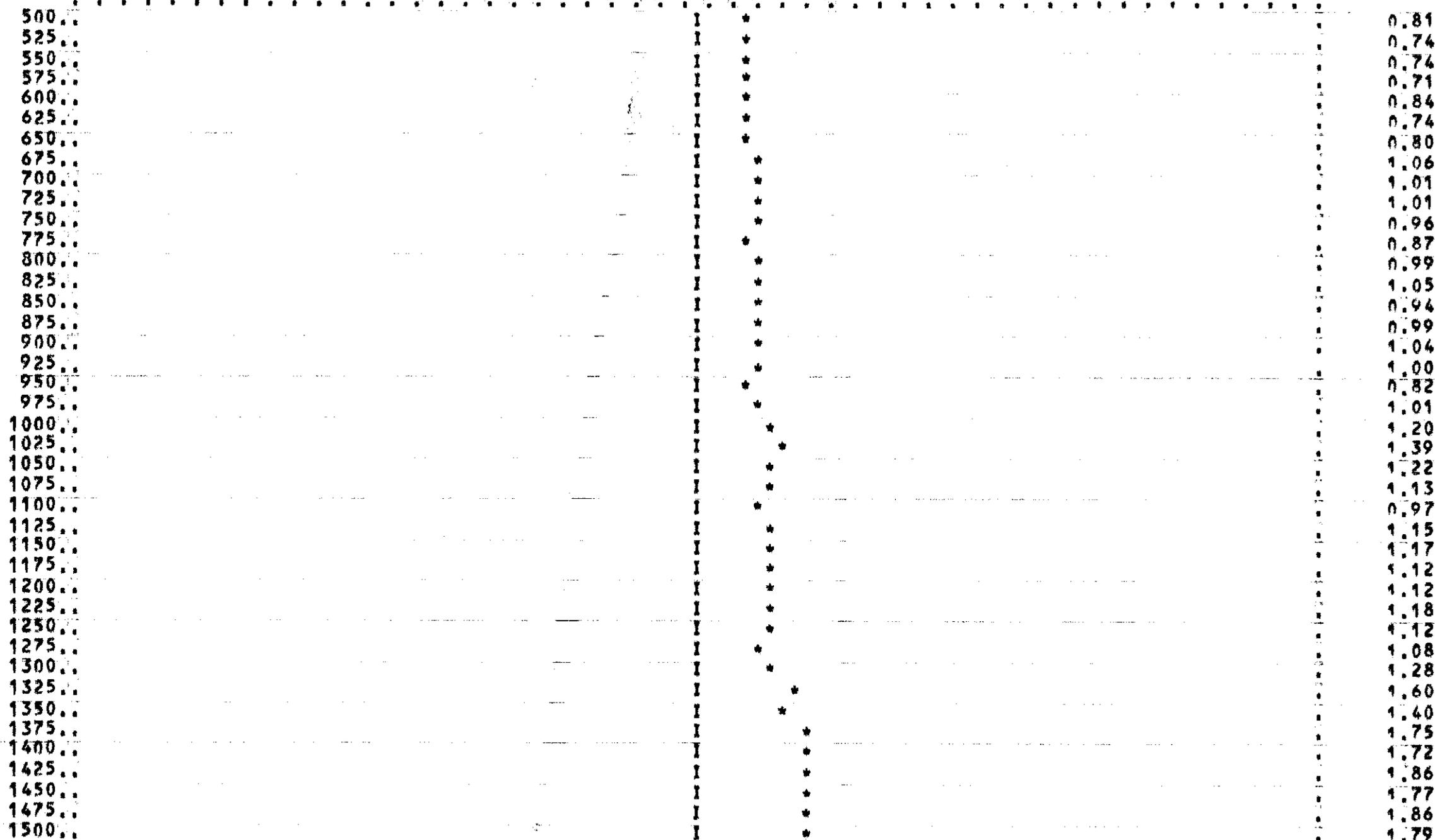
LINE# 2000.S FREQUENCY=3HZ N001

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500.E	3.20	0.22	-1.10	0.70	0.45	-0.15	0.17	41.17	-44.22	-1.35	0.85	0.51	-1.07	500.E
525.E	3.20	0.24	-1.20	0.80	0.45	-0.15	0.17	43.36	-44.09	-1.65	0.95	0.62	-1.24	525.E
550.E	3.20	0.28	-1.00	1.00	0.45	-0.15	0.18	48.83	-41.26	-1.45	1.15	0.88	-1.27	550.E
575.E	3.20	0.25	-1.30	1.00	0.45	-0.15	0.19	42.09	-48.37	-1.75	1.15	0.78	-1.37	575.E
600.E	3.20	0.29	-1.00	0.80	0.45	-0.15	0.19	47.15	-45.72	-1.45	0.95	0.75	-1.31	600.E
625.E	3.20	0.29	-1.00	0.80	0.45	-0.15	0.20	45.54	-48.78	-1.45	0.95	0.75	-1.31	625.E
650.E	3.20	0.31	-0.90	0.90	0.45	-0.15	0.21	47.04	-49.08	-1.35	1.05	0.89	-1.31	650.E
675.E	3.20	0.34	-0.70	0.50	0.45	-0.15	0.21	49.88	-48.04	-1.15	0.65	0.60	-1.22	675.E
700.E	3.20	0.34	-1.00	0.70	0.45	-0.15	0.22	48.28	-51.23	-1.45	0.85	0.79	-1.54	700.E
725.E	3.20	0.35	-0.80	0.70	0.45	-0.15	0.23	48.14	-53.01	-1.25	0.85	0.81	-1.37	725.E
750.E	3.20	0.35	-1.00	0.90	0.45	-0.20	0.23	46.71	-56.16	-1.45	1.10	1.05	-1.59	750.E
775.E	3.20	0.39	-0.80	0.70	0.45	-0.20	0.24	50.57	-53.61	-1.25	0.90	0.96	-1.52	775.E
800.E	3.20	0.41	-0.90	0.70	0.45	-0.20	0.25	51.76	-53.74	-1.35	0.90	1.01	-1.73	800.E
825.E	3.20	0.42	-0.70	0.60	0.45	-0.20	0.25	51.73	-53.11	-1.15	0.80	0.92	-1.51	825.E
850.E	3.20	0.45	-0.70	0.50	0.45	-0.20	0.26	54.21	-53.45	-1.15	0.70	0.86	-1.62	850.E
875.E	3.20	0.47	-0.50	0.30	0.45	-0.20	0.26	55.54	-52.91	-0.95	0.50	0.64	-1.40	875.E
900.E	3.20	0.51	-0.50	0.10	0.45	-0.20	0.27	59.30	-49.23	-0.95	0.30	0.42	-1.51	900.E
925.E	3.20	0.56	-0.50	0.20	0.45	-0.20	0.27	64.28	-43.77	-0.95	0.40	0.61	-1.66	925.E
950.E	3.20	0.59	-0.60	0.10	0.45	-0.20	0.27	67.09	-40.70	-1.05	0.30	0.48	-1.94	950.E
975.E	3.20	0.65	-0.60	0.10	0.45	-0.20	0.28	73.49	-32.97	-1.05	0.30	0.53	-2.13	975.E
1000.E	3.20	0.69	-0.50	0.20	0.40	-0.25	0.28	77.86	-27.58	-0.90	0.45	0.85	-1.94	1000.E
1025.E	3.20	0.69	-0.60	0.10	0.40	-0.25	0.28	78.01	-27.35	-1.00	0.35	0.66	-2.16	1025.E
1050.E	3.20	0.63	-0.50	0.10	0.40	-0.25	0.27	71.64	-35.08	-0.90	0.35	0.60	-1.77	1050.E
1075.E	3.20	0.61	-0.80	0.20	0.40	-0.25	0.27	70.01	-36.74	-1.20	0.45	0.75	-2.29	1075.E
1100.E	3.20	0.60	-0.70	0.20	0.40	-0.25	0.27	69.76	-36.58	-1.10	0.45	0.74	-2.06	1100.E
1125.E	3.20	0.62	-0.70	0.20	0.40	-0.25	0.26	73.26	-31.82	-1.10	0.45	0.76	-2.13	1125.E
1150.E	3.20	0.62	-0.60	0.10	0.40	-0.25	0.26	74.69	-29.54	-1.00	0.35	0.59	-1.94	1150.E
1175.E	3.20	0.61	-0.70	0.00	0.40	-0.25	0.25	75.13	-28.40	-1.10	0.25	0.42	-2.10	1175.E
1200.E	3.20	0.73	-0.90	-0.10	0.40	-0.25	0.25	92.15	-8.74	-1.30	0.15	0.30	-2.97	1200.E
1225.E	3.20	0.67	-0.70	0.10	0.40	-0.25	0.24	86.88	-14.23	-1.10	0.35	0.64	-2.30	1225.E
1250.E	3.20	0.73	-0.80	0.10	0.40	-0.30	0.23	97.41	-2.72	-1.20	0.40	0.80	-2.74	1250.E
1275.E	3.20	0.65	-0.90	0.10	0.40	-0.30	0.23	89.41	-10.82	-1.30	0.40	0.71	-2.64	1275.E
1300.E	3.20	0.72	-0.90	0.10	0.40	-0.30	0.22	102.23	2.21	-1.30	0.40	0.79	-2.93	1300.E
1325.E	3.20	0.61	-0.90	0.20	0.40	-0.30	0.21	89.50	-10.07	-1.30	0.50	0.83	-2.48	1325.E
1350.E	3.20	0.60	-0.90	0.10	0.40	-0.30	0.21	91.04	-8.30	-1.30	0.40	0.65	-2.44	1350.E
1375.E	3.20	0.55	-1.00	0.10	0.40	-0.30	0.20	86.36	-12.21	-1.40	0.40	0.60	-2.41	1375.E
1400.E	3.20	0.56	-0.90	0.20	0.40	-0.30	0.19	91.04	-7.75	-1.30	0.50	0.76	-2.27	1400.E
1425.E	3.20	0.46	-1.00	0.40	0.40	-0.30	0.19	77.45	-18.84	-1.40	0.70	0.88	-2.01	1425.E
1450.E	3.20	0.42	-1.20	0.60	0.40	-0.30	0.18	73.25	-21.57	-1.60	0.90	1.03	-2.10	1450.E
1475.E	3.20	0.36	-1.70	0.70	0.40	-0.30	0.17	65.03	-27.22	-2.10	1.00	0.98	-2.36	1475.E
1500.E	3.20	0.35	-2.10	0.90	0.40	-0.30	0.17	65.49	-25.94	-2.50	1.20	1.15	-2.73	1500.E

086

XTOP= 500.

XINC= 25.00



0.81
0.74
0.74
0.71
0.84
0.74
0.80
1.06
1.01
1.01
0.96
0.87
0.99
1.05
0.94
0.99
1.04
1.00
0.82
1.01
1.20
1.39
1.22
1.13
0.97
1.15
1.17
1.12
1.12
1.18
1.12
1.08
1.28
1.60
1.40
1.75
1.72
1.86
1.77
1.86
1.79

XBOT= 1500.
YMIN= -10.00

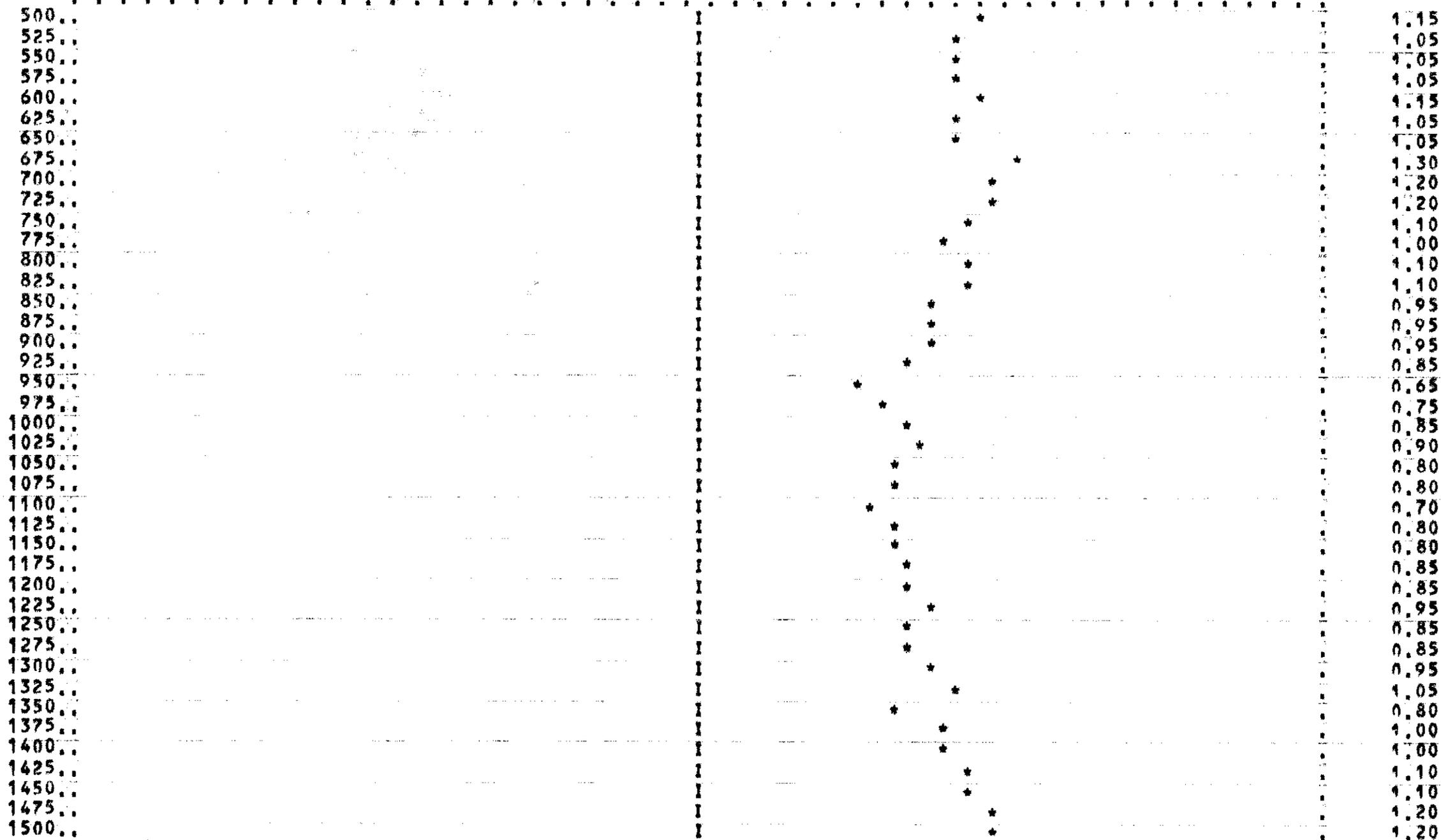
YINC= 0.2000
YMAX= 10.00

LINE 1800.S SECONDARY FIELD QUADRATURE HSQ/I

087

XTOP= 500.

XINC= 25.00



XBOT= 1500.
YMIN= -2.500

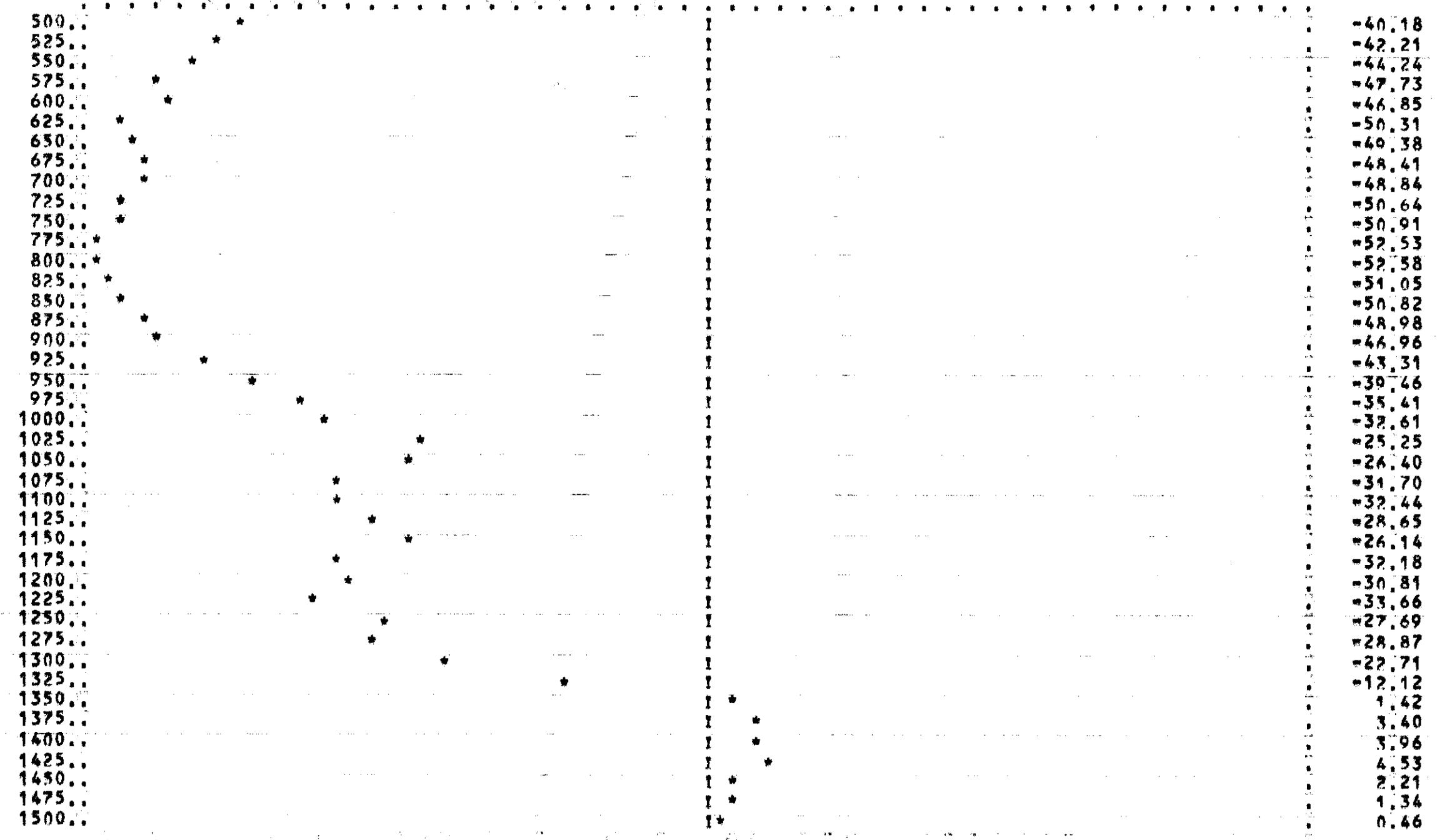
YINC= 0.5000E-01
YMAX= 2.500

LINE 1800.S RELATIVE PHASE SHIFT RPS

088

XTOP= 500.

XINC= 25.00



XBOT= 1500.
YMIN= 52.58

YINC= 1.026
YMAX= 50.00

LINE 1800.S MAGNETOMETRIC RESESTIVITY MMR

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8111

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LINE# 1800.S FREQUENCY=3HZ N001

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500.E	3.10	0.25	-1.70	0.70	0.35	-0.45	0.17	47.46	-40.18	-2.05	1.15	0.81	-1.65	500.E
525.E	3.10	0.25	-1.70	0.60	0.35	-0.45	0.17	46.23	-42.21	-2.05	1.05	0.74	-1.65	525.E
550.E	3.10	0.25	-1.60	0.60	0.35	-0.45	0.18	45.06	-44.24	-1.95	1.05	0.74	-1.57	550.E
575.E	3.10	0.24	-1.50	0.60	0.35	-0.45	0.18	42.19	-47.73	-1.85	1.05	0.71	-1.43	575.E
600.E	3.10	0.26	-1.50	0.70	0.35	-0.45	0.19	44.62	-46.85	-1.85	1.15	0.84	-1.55	600.E
625.E	3.10	0.25	-1.60	0.60	0.35	-0.45	0.19	41.91	-50.31	-1.95	1.05	0.74	-1.57	625.E
650.E	3.10	0.27	-1.10	0.60	0.35	-0.45	0.20	44.25	-49.38	-1.45	1.05	0.80	-1.26	650.E
675.E	3.10	0.29	-1.20	0.90	0.35	-0.40	0.20	46.51	-48.41	-1.55	1.30	1.06	-1.45	675.E
700.E	3.10	0.30	-1.10	0.80	0.35	-0.40	0.21	47.14	-48.84	-1.45	1.20	1.01	-1.40	700.E
725.E	3.10	0.30	-1.10	0.80	0.35	-0.40	0.21	46.23	-50.64	-1.45	1.20	1.01	-1.40	725.E
750.E	3.10	0.31	-1.00	0.70	0.35	-0.40	0.21	46.92	-50.91	-1.35	1.10	0.96	-1.35	750.E
775.E	3.10	0.31	-1.10	0.60	0.35	-0.40	0.22	46.14	-52.53	-1.45	1.00	0.87	-1.43	775.E
800.E	3.10	0.32	-1.00	0.70	0.35	-0.40	0.22	46.90	-52.58	-1.35	1.10	0.99	-1.39	800.E
825.E	3.10	0.34	-0.90	0.70	0.40	-0.40	0.22	49.16	-51.05	-1.30	1.10	1.05	-1.43	825.E
850.E	3.10	0.35	-1.00	0.60	0.40	-0.35	0.23	49.99	-50.82	-1.40	0.95	0.94	-1.58	850.E
875.E	3.10	0.37	-0.80	0.60	0.40	-0.35	0.23	52.30	-48.98	-1.20	0.95	0.99	-1.43	875.E
900.E	3.10	0.39	-0.80	0.60	0.40	-0.35	0.23	54.66	-46.96	-1.20	0.95	1.04	-1.51	900.E
925.E	3.10	0.42	-0.70	0.50	0.40	-0.35	0.23	58.47	-43.31	-1.10	0.85	1.00	-1.49	925.E
950.E	3.10	0.45	-0.80	0.30	0.40	-0.35	0.23	62.34	-39.46	-1.20	0.65	0.82	-1.74	950.E
975.E	3.10	0.48	-0.80	0.40	0.40	-0.35	0.23	66.30	-35.41	-1.20	0.75	1.01	-1.86	975.E
1000.E	3.10	0.50	-0.80	0.50	0.40	-0.35	0.23	69.00	-32.61	-1.20	0.85	1.20	-1.94	1000.E
1025.E	3.10	0.55	-0.80	0.60	0.40	-0.30	0.23	75.97	-25.25	-1.20	0.90	1.39	-2.13	1025.E
1050.E	3.10	0.54	-1.00	0.50	0.40	-0.30	0.23	74.81	-26.40	-1.40	0.80	1.22	-2.44	1050.E
1075.E	3.10	0.50	-0.90	0.50	0.40	-0.30	0.23	69.60	-31.70	-1.30	0.80	1.13	-2.10	1075.E
1100.E	3.10	0.49	-0.80	0.40	0.40	-0.30	0.23	68.67	-32.44	-1.20	0.70	0.97	-1.90	1100.E
1125.E	3.10	0.51	-0.80	0.50	0.40	-0.30	0.23	72.10	-28.65	-1.20	0.80	1.15	-1.97	1125.E
1150.E	3.10	0.52	-0.80	0.50	0.40	-0.30	0.23	74.28	-26.14	-1.20	0.80	1.17	-2.01	1150.E
1175.E	3.10	0.47	-0.90	0.60	0.45	-0.25	0.22	67.95	-32.18	-1.35	0.85	1.12	-2.05	1175.E
1200.E	3.10	0.47	-1.00	0.60	0.45	-0.25	0.22	68.89	-30.81	-1.45	0.85	1.12	-2.20	1200.E
1225.E	3.10	0.44	-1.00	0.70	0.45	-0.25	0.22	65.49	-33.66	-1.45	0.95	1.18	-2.06	1225.E
1250.E	3.10	0.47	-1.00	0.60	0.45	-0.25	0.21	71.13	-27.69	-1.45	0.85	1.12	-2.20	1250.E
1275.E	3.10	0.45	-1.00	0.60	0.45	-0.25	0.21	69.35	-28.87	-1.45	0.85	1.08	-2.10	1275.E
1300.E	3.10	0.48	-1.10	0.70	0.45	-0.25	0.21	75.42	-22.71	-1.55	0.95	1.28	-2.40	1300.E
1325.E	3.10	0.54	-1.20	0.80	0.45	-0.25	0.20	86.61	-12.12	-1.65	1.05	1.60	-2.87	1325.E
1350.E	3.10	0.62	-1.20	0.60	0.45	-0.20	0.20	101.61	1.42	-1.65	0.80	1.40	-3.30	1350.E
1375.E	3.10	0.62	-1.40	0.80	0.45	-0.20	0.19	103.93	3.40	-1.85	1.00	1.75	-3.70	1375.E
1400.E	3.10	0.61	-1.50	0.80	0.45	-0.20	0.19	104.68	3.96	-1.95	1.00	1.72	-3.84	1400.E
1425.E	3.10	0.60	-1.50	0.90	0.45	-0.20	0.18	105.49	4.53	-1.95	1.10	1.86	-3.77	1425.E
1450.E	3.10	0.57	-1.70	0.90	0.45	-0.20	0.18	102.74	2.21	-2.15	1.10	1.77	-3.95	1450.E
1475.E	3.10	0.55	-1.70	1.00	0.45	-0.20	0.17	101.71	1.34	-2.15	1.20	1.86	-3.81	1475.E
1500.E	3.10	0.53	-1.80	1.00	0.45	-0.20	0.17	100.61	0.46	-2.25	1.20	1.79	-3.85	1500.E

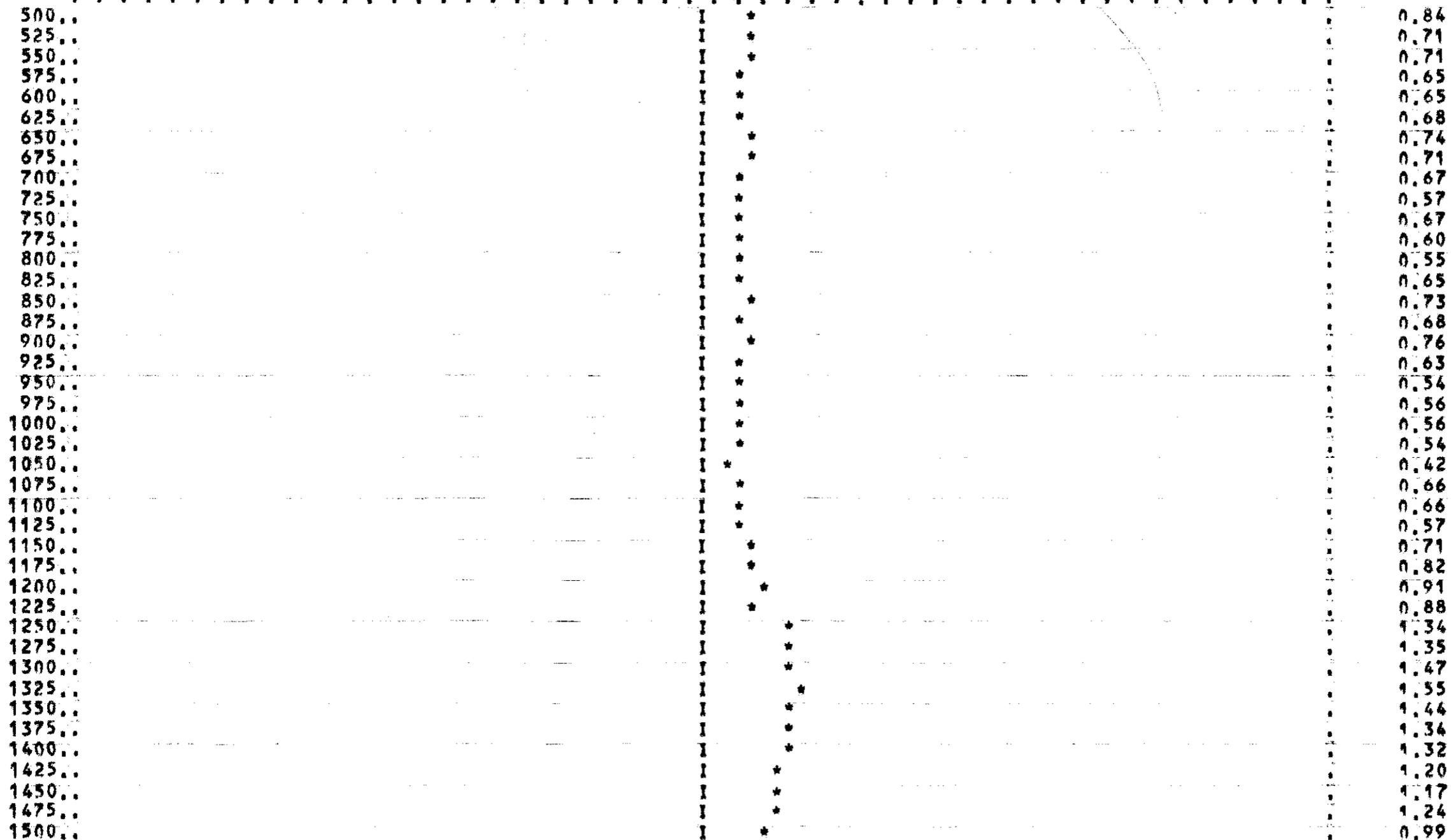
XTOP#

090

500.

XINC#

25.00



XBOT#

1500.

YINC#

0.2000

YMIN#

-10.00

YMAX#

10.00

LINE

1600.S

SECONDARY FIELD QUADRATURE

MSQ/I

093

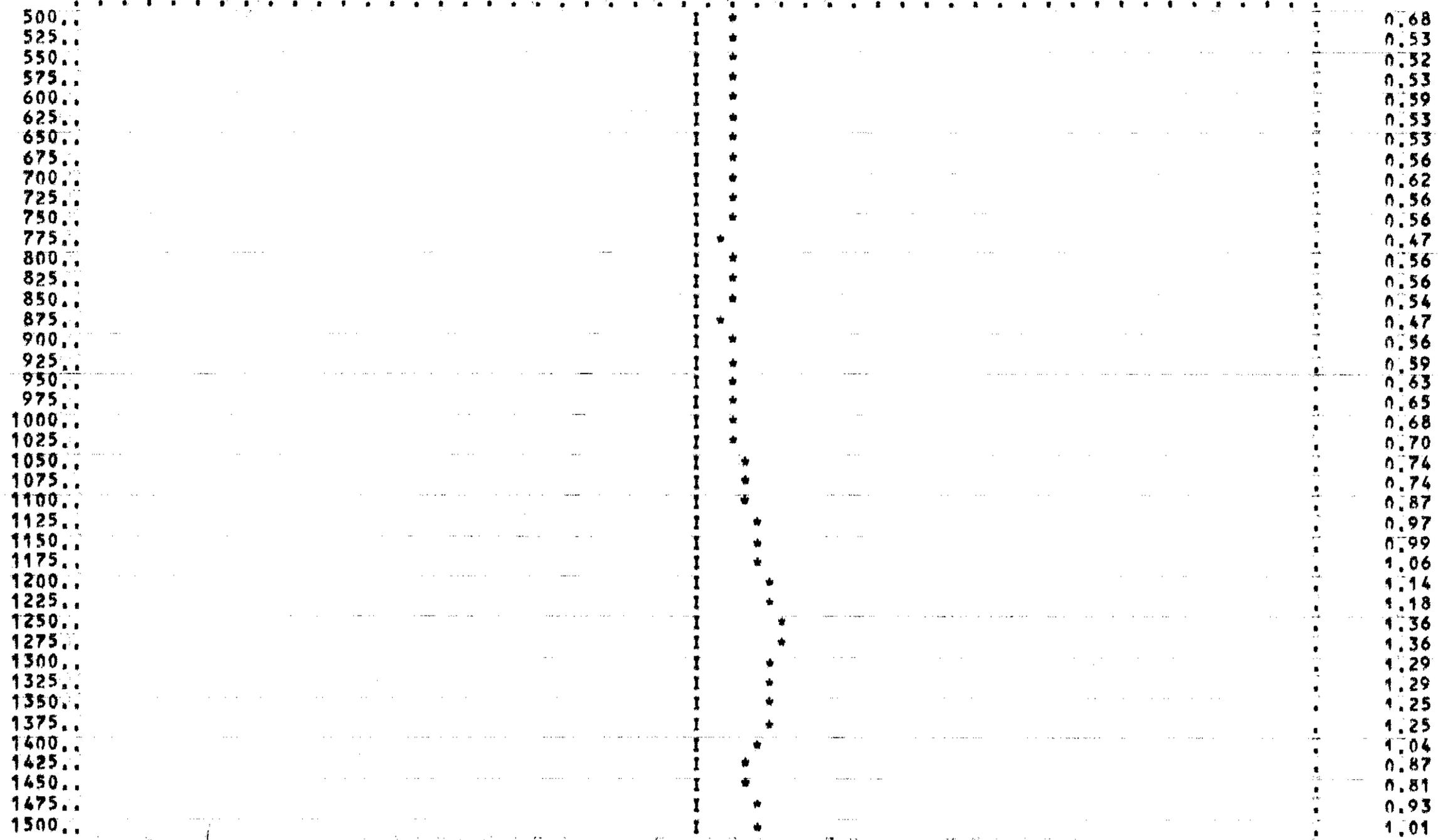
1600.S FREQUENCY=3HZ N001

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500.E	3.10	0.23	-1.70	0.80	0.30	-0.50	0.17	43.69	-43.03	-2.00	1.30	0.84	-1.48	500.E
525.E	3.10	0.23	-1.70	0.60	0.30	-0.50	0.17	42.69	-44.83	-2.00	1.10	0.71	-1.48	525.E
550.E	3.10	0.23	-1.80	0.60	0.30	-0.50	0.18	41.73	-46.61	-2.10	1.10	0.71	-1.56	550.E
575.E	3.10	0.23	-1.70	0.50	0.30	-0.50	0.18	40.83	-48.38	-2.00	1.00	0.65	-1.48	575.E
600.E	3.10	0.23	-1.80	0.50	0.30	-0.50	0.19	39.98	-50.12	-2.10	1.00	0.65	-1.56	600.E
625.E	3.10	0.24	-1.70	0.50	0.30	-0.50	0.19	40.89	-50.37	-2.00	1.00	0.68	-1.55	625.E
650.E	3.10	0.24	-1.60	0.60	0.30	-0.50	0.19	40.11	-52.02	-1.90	1.10	0.74	-1.47	650.E
675.E	3.10	0.24	-1.70	0.50	0.30	-0.55	0.20	39.38	-53.63	-2.00	1.05	0.71	-1.55	675.E
700.E	3.10	0.25	-1.80	0.40	0.30	-0.55	0.20	40.32	-53.71	-2.10	0.95	0.67	-1.60	700.E
725.E	3.10	0.24	-1.70	0.30	0.30	-0.55	0.20	38.09	-56.62	-2.00	0.85	0.57	-1.55	725.E
750.E	3.10	0.25	-1.70	0.40	0.25	-0.55	0.21	39.09	-56.55	-1.95	0.95	0.67	-1.57	750.E
775.E	3.10	0.25	-1.70	0.30	0.25	-0.55	0.21	38.56	-57.83	-1.95	0.85	0.60	-1.57	775.E
800.E	3.10	0.26	-1.80	0.20	0.25	-0.55	0.21	39.61	-57.55	-2.05	0.75	0.55	-1.72	800.E
825.E	3.10	0.27	-1.70	0.30	0.25	-0.55	0.21	40.68	-57.16	-1.95	0.85	0.65	-1.70	825.E
850.E	3.10	0.29	-1.50	0.30	0.25	-0.60	0.22	43.27	-55.20	-1.75	0.90	0.73	-1.64	850.E
875.E	3.10	0.30	-1.40	0.20	0.25	-0.60	0.22	44.39	-54.56	-1.65	0.80	0.68	-1.60	875.E
900.E	3.10	0.30	-1.40	0.30	0.25	-0.60	0.22	44.09	-55.23	-1.65	0.90	0.76	-1.60	900.E
925.E	3.10	0.32	-1.40	0.10	0.25	-0.60	0.22	46.77	-52.86	-1.65	0.70	0.63	-1.70	925.E
950.E	3.10	0.32	-1.30	0.00	0.25	-0.60	0.22	46.59	-53.24	-1.55	0.60	0.54	-1.60	950.E
975.E	3.10	0.33	-1.20	0.00	0.25	-0.60	0.22	47.94	-52.02	-1.45	0.60	0.56	-1.54	975.E
1000.E	3.10	0.33	-1.30	0.00	0.25	-0.60	0.22	47.90	-52.10	-1.55	0.60	0.56	-1.65	1000.E
1025.E	3.10	0.35	-1.10	-0.10	0.20	-0.65	0.22	50.85	-49.12	-1.30	0.55	0.54	-1.47	1025.E
1050.E	3.10	0.33	-1.00	-0.20	0.20	-0.65	0.22	48.05	-51.79	-1.20	0.45	0.42	-1.28	1050.E
1075.E	3.10	0.36	-1.10	0.00	0.20	-0.65	0.22	52.62	-47.05	-1.30	0.65	0.66	-1.51	1075.E
1100.E	3.10	0.36	-1.10	0.00	0.20	-0.65	0.22	52.90	-46.52	-1.30	0.65	0.66	-1.51	1100.E
1125.E	3.10	0.37	-1.20	-0.10	0.20	-0.65	0.22	54.75	-44.40	-1.40	0.55	0.57	-1.67	1125.E
1150.E	3.10	0.46	-1.20	-0.10	0.20	-0.65	0.22	68.63	-30.52	-1.40	0.55	0.71	-2.08	1150.E
1175.E	3.10	0.58	-1.20	-0.20	0.20	-0.70	0.21	87.38	-12.16	-1.40	0.50	0.82	-2.62	1175.E
1200.E	3.10	0.54	-1.50	-0.10	0.20	-0.70	0.21	82.26	-16.91	-1.70	0.60	0.91	-2.96	1200.E
1225.E	3.10	0.52	-1.50	-0.10	0.20	-0.70	0.21	80.20	-18.63	-1.70	0.60	0.88	-2.85	1225.E
1250.E	3.10	0.53	-1.50	0.20	0.20	-0.70	0.21	82.87	-15.90	-1.70	0.90	1.34	-2.91	1250.E
1275.E	3.10	0.60	-1.50	0.10	0.15	-0.70	0.20	95.23	-4.36	-1.65	0.80	1.35	-3.10	1275.E
1300.E	3.10	0.58	-1.40	0.20	0.15	-0.70	0.20	93.55	-5.81	-1.55	0.90	1.47	-2.90	1300.E
1325.E	3.10	0.61	-1.40	0.20	0.15	-0.70	0.20	100.10	0.08	-1.55	0.90	1.55	-3.05	1325.E
1350.E	3.10	0.60	-1.20	0.10	0.15	-0.75	0.19	100.27	0.23	-1.35	0.85	1.44	-2.61	1350.E
1375.E	3.10	0.56	-1.30	0.10	0.15	-0.75	0.19	95.40	-3.92	-1.45	0.85	1.34	-2.62	1375.E
1400.E	3.10	0.55	-1.40	0.10	0.15	-0.75	0.19	95.61	-3.67	-1.55	0.85	1.32	-2.75	1400.E
1425.E	3.10	0.50	-1.30	0.10	0.15	-0.75	0.18	88.77	-9.19	-1.45	0.85	1.20	-2.34	1425.E
1450.E	3.10	0.49	-1.70	0.10	0.15	-0.75	0.18	88.91	-8.87	-1.85	0.85	1.17	-2.92	1450.E
1475.E	3.10	0.52	-1.70	0.10	0.15	-0.75	0.17	96.51	-2.73	-1.85	0.85	1.24	-3.10	1475.E
1500.E	3.10	0.47	-1.80	0.00	0.15	-0.75	0.17	89.28	-8.19	-1.95	0.75	0.99	-2.96	1500.E

094

XTOP# 500.

XINC# 25.00



XBOT# 1500.
YMIN# -10.00

YINC# 0.2000
YMAX# 10.00

LINE 1400.S SECONDARY FIELD QUADRATURE MSQ/I

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095

XTOP= 500.

XINC= 25.00

500.
525.
550.
575.
600.
625.
650.
675.
700.
725.
750.
775.
800.
825.
850.
875.
900.
925.
950.
975.
1000.
1025.
1050.
1075.
1100.
1125.
1150.
1175.
1200.
1225.
1250.
1275.
1300.
1325.
1350.
1375.
1400.
1425.
1450.
1475.
1500.

1.15
0.90
0.80
0.90
1.00
0.90
0.90
0.90
1.00
0.90
0.90
0.80
0.90
0.80
0.70
0.80
0.80
0.80
0.80
0.75
0.75
0.75
0.75
0.75
0.75
0.75
0.75
0.75
0.75
0.85
0.85
0.75
0.75
0.75
0.75
0.65
0.55
0.55
0.65
0.75

XBOT= 1500.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 1400.S RELATIVE PHASE SHIFT RPS

096

XTOP#

500.

XINC# 25.00

500.
525.
550.
575.
600.
625.
650.
675.
700.
725.
750.
775.
800.
825.
850.
875.
900.
925.
950.
975.
1000.
1025.
1050.
1075.
1100.
1125.
1150.
1175.
1200.
1225.
1250.
1275.
1300.
1325.
1350.
1375.
1400.
1425.
1450.
1475.
1500.

=45.99
=48.01
=47.14
=52.08
=54.11
=56.12
=58.09
=58.57
=60.45
=62.26
=63.98
=67.05
=67.10
=68.47
=66.79
=67.85
=67.28
=66.53
=64.14
=63.00
=61.65
=57.19
=53.98
=53.47
=44.06
=35.91
=33.40
=27.82
=20.65
=16.24
=13.17
=11.45
=3.84
=1.96
=2.93
=0.95
=1.85
=1.28
=5.05
=4.46
=6.79

XBOT#

1500.

YINC# 1.185

YMIN# -68.47

YMAX# 50.00

LINE

1400.S

MAGNETOMETRIC RESESTIVITY MMR

097

LINE# 1400.5 FREQUENCY=3HZ N001

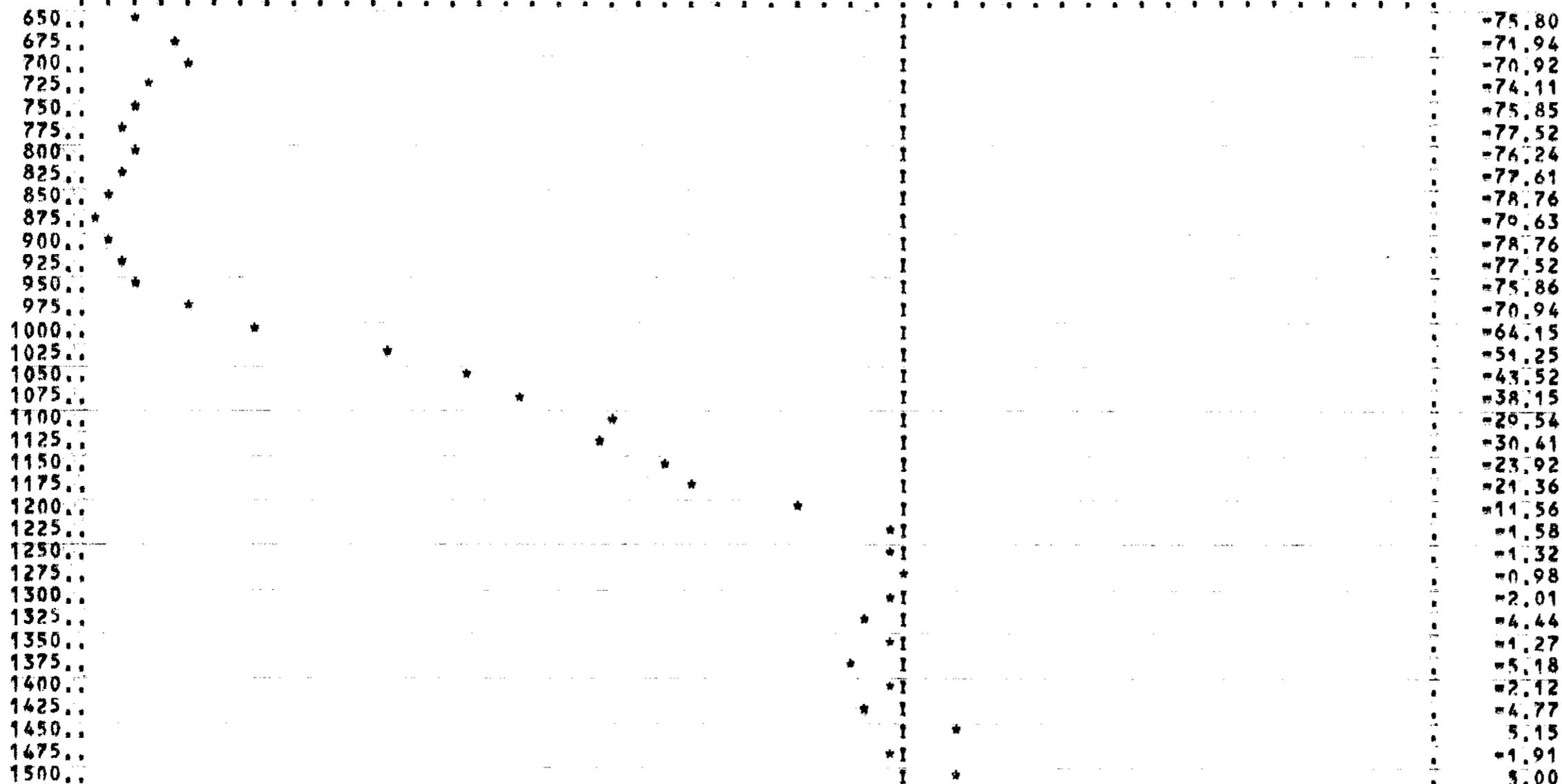
STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
500.E	3.10	0.21	-3.00	2.30	-0.85	1.15	0.17	39.86	-45.99	-2.15	1.15	0.68	-1.46	500.E
525.E	3.10	0.21	-2.60	2.00	-0.85	1.10	0.17	38.83	-48.01	-1.75	0.90	0.53	-1.10	525.E
550.E	3.10	0.23	-2.80	1.90	-0.85	1.10	0.18	41.46	-47.14	-1.95	0.80	0.52	-1.45	550.E
575.E	3.10	0.21	-3.20	2.00	-0.85	1.10	0.18	36.92	-52.08	-2.35	0.90	0.53	-1.59	575.E
600.E	3.10	0.21	-3.00	2.10	-0.85	1.10	0.19	36.04	-54.11	-2.15	1.00	0.59	-1.44	600.E
625.E	3.10	0.21	-3.00	2.00	-0.85	1.10	0.19	35.20	-56.12	-2.15	0.90	0.53	-1.46	625.E
650.E	3.10	0.21	-3.00	2.00	-0.85	1.10	0.20	34.42	-58.09	-2.15	0.90	0.53	-1.44	650.E
675.E	3.10	0.22	-2.90	2.00	-0.85	1.10	0.20	35.28	-58.57	-2.05	0.90	0.56	-1.45	675.E
700.E	3.10	0.22	-2.80	2.10	-0.85	1.10	0.21	34.57	-60.45	-1.95	1.00	0.62	-1.38	700.E
725.E	3.10	0.22	-2.80	2.00	-0.85	1.10	0.21	33.90	-62.26	-1.95	0.90	0.56	-1.38	725.E
750.E	3.10	0.22	-2.80	2.00	-0.85	1.10	0.21	33.30	-63.98	-1.95	0.90	0.56	-1.38	750.E
775.E	3.10	0.21	-2.60	1.90	-0.85	1.10	0.22	31.26	-67.05	-1.75	0.80	0.47	-1.10	775.E
800.E	3.10	0.22	-3.20	2.00	-0.85	1.10	0.22	32.25	-67.10	-2.35	0.90	0.56	-1.67	800.E
825.E	3.10	0.22	-3.00	2.00	-0.85	1.10	0.22	31.81	-68.47	-2.15	0.90	0.56	-1.53	825.E
850.E	3.10	0.24	-2.40	1.90	-0.85	1.10	0.23	34.28	-66.79	-1.55	0.80	0.54	-1.20	850.E
875.E	3.10	0.24	-2.60	1.80	-0.85	1.10	0.23	33.93	-67.85	-1.75	0.70	0.47	-1.35	875.E
900.E	3.10	0.25	-2.40	1.90	-0.85	1.10	0.23	35.04	-67.28	-1.55	0.80	0.56	-1.25	900.E
925.E	3.10	0.26	-2.40	1.90	-0.85	1.10	0.23	36.19	-66.53	-1.55	0.80	0.59	-1.30	925.E
950.E	3.10	0.28	-2.20	1.90	-0.85	1.10	0.23	38.79	-64.14	-1.35	0.80	0.63	-1.22	950.E
975.E	3.10	0.29	-2.30	1.90	-0.85	1.10	0.23	40.06	-63.00	-1.45	0.80	0.65	-1.36	975.E
1000.E	3.10	0.30	-2.20	1.90	-0.85	1.10	0.23	41.40	-61.65	-1.35	0.80	0.68	-1.31	1000.E
1025.E	3.10	0.33	-2.10	1.80	-0.85	1.05	0.23	45.58	-57.19	-1.25	0.75	0.70	-1.33	1025.E
1050.E	3.10	0.35	-2.10	1.80	-0.85	1.05	0.23	48.49	-53.98	-1.25	0.75	0.74	-1.41	1050.E
1075.E	3.10	0.35	-2.20	1.80	-0.85	1.05	0.23	48.72	-53.47	-1.35	0.75	0.74	-1.52	1075.E
1100.E	3.10	0.41	-2.20	1.80	-0.85	1.05	0.23	57.46	-44.06	-1.35	0.75	0.87	-1.79	1100.E
1125.E	3.10	0.46	-2.30	1.80	-0.85	1.05	0.23	65.03	-35.91	-1.45	0.75	0.97	-2.15	1125.E
1150.E	3.10	0.47	-2.40	1.80	-0.85	1.05	0.23	67.13	-33.40	-1.55	0.75	0.99	-2.35	1150.E
1175.E	3.10	0.50	-2.40	1.80	-0.85	1.05	0.22	72.29	-27.82	-1.55	0.75	1.06	-2.50	1175.E
1200.E	3.10	0.54	-2.40	1.80	-0.85	1.05	0.22	79.15	-20.65	-1.55	0.75	1.14	-2.70	1200.E
1225.E	3.10	0.56	-2.50	1.80	-0.85	1.05	0.22	83.35	-16.24	-1.65	0.75	1.18	-2.98	1225.E
1250.E	3.10	0.57	-2.60	1.90	-0.85	1.05	0.21	86.27	-13.17	-1.75	0.85	1.36	-3.22	1250.E
1275.E	3.10	0.57	-2.60	1.90	-0.85	1.05	0.21	87.84	-11.45	-1.75	0.85	1.36	-3.22	1275.E
1300.E	3.10	0.61	-2.60	1.80	-0.85	1.05	0.21	95.84	-3.84	-1.75	0.75	1.29	-3.44	1300.E
1325.E	3.10	0.61	-2.60	1.80	-0.85	1.05	0.20	97.83	-1.96	-1.75	0.75	1.29	-3.44	1325.E
1350.E	3.10	0.59	-2.50	1.80	-0.85	1.05	0.20	96.69	-2.93	-1.65	0.75	1.25	-3.14	1350.E
1375.E	3.10	0.59	-2.40	1.80	-0.85	1.05	0.19	98.90	-0.95	-1.55	0.75	1.25	-2.95	1375.E
1400.E	3.10	0.57	-2.50	1.70	-0.85	1.05	0.19	97.81	-1.85	-1.65	0.65	1.04	-3.03	1400.E
1425.E	3.10	0.56	-2.60	1.60	-0.85	1.05	0.18	98.45	-1.28	-1.75	0.55	0.87	-3.16	1425.E
1450.E	3.10	0.52	-2.60	1.60	-0.85	1.05	0.18	93.73	-5.05	-1.75	0.55	0.81	-2.94	1450.E
1475.E	3.10	0.51	-2.70	1.70	-0.85	1.05	0.17	94.31	-4.46	-1.85	0.65	0.93	-3.04	1475.E
1500.E	3.10	0.48	-2.60	1.80	-0.85	1.05	0.17	91.12	-6.79	-1.75	0.75	1.01	-2.71	1500.E

100

XTOP=

650.

XINC= 25.00



XBOT=

1500.

VINC= 1.296

YMIN= -79.63

YMAX= 50.00

LINE 1200.S MAGNETOMETRIC RESESTIVITY MMR

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LINE= 1200.S FREQUENCY=3HZ N001

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
650.E	3.20	0.12	-3.00	2.40	-0.95	1.10	0.21	18.21	-75.80	-2.05	1.30	0.43	-0.77	650.E
675.E	3.20	0.17	-3.00	2.40	-0.95	1.10	0.21	24.94	-71.94	-2.05	1.30	0.60	-1.00	675.E
700.E	3.20	0.20	-2.90	2.30	-0.95	1.10	0.22	28.40	-70.92	-1.95	1.20	0.65	-1.22	700.E
725.E	3.20	0.20	-2.80	2.20	-0.95	1.10	0.23	27.51	-74.11	-1.85	1.10	0.60	-1.16	725.E
750.E	3.20	0.21	-2.70	2.20	-0.95	1.10	0.23	28.02	-75.85	-1.75	1.10	0.63	-1.15	750.E
775.E	3.20	0.22	-2.50	2.00	-0.95	1.10	0.24	28.53	-77.52	-1.55	0.90	0.54	-1.07	775.E
800.E	3.20	0.25	-2.50	1.90	-0.95	1.10	0.25	31.56	-76.24	-1.55	0.80	0.55	-1.21	800.E
825.E	3.20	0.26	-2.40	1.90	-0.95	1.10	0.25	32.02	-77.61	-1.45	0.80	0.57	-1.18	825.E
850.E	3.20	0.27	-2.30	1.90	-0.95	1.10	0.26	32.53	-78.76	-1.35	0.80	0.59	-1.14	850.E
875.E	3.20	0.28	-2.30	1.80	-0.95	1.10	0.26	33.09	-79.63	-1.35	0.70	0.53	-1.18	875.E
900.E	3.20	0.30	-2.20	1.80	-0.95	1.10	0.27	34.88	-78.76	-1.25	0.70	0.57	-1.17	900.E
925.E	3.20	0.32	-2.30	1.80	-0.95	1.10	0.27	36.73	-77.52	-1.35	0.70	0.61	-1.35	925.E
950.E	3.20	0.34	-2.20	1.80	-0.95	1.10	0.27	38.66	-75.86	-1.25	0.70	0.65	-1.33	950.E
975.E	3.20	0.38	-2.10	1.80	-0.95	1.10	0.28	42.96	-70.94	-1.15	0.70	0.73	-1.37	975.E
1000.E	3.20	0.43	-2.00	1.70	-0.95	1.10	0.28	48.52	-64.15	-1.05	0.60	0.70	-1.41	1000.E
1025.E	3.20	0.52	-2.00	1.70	-0.95	1.05	0.28	58.79	-51.25	-1.05	0.65	0.92	-1.71	1025.E
1050.E	3.20	0.57	-2.00	1.70	-0.95	1.05	0.27	64.81	-43.52	-1.05	0.65	1.01	-1.87	1050.E
1075.E	3.20	0.60	-2.10	1.70	-0.95	1.05	0.27	68.87	-38.15	-1.15	0.65	1.06	-2.16	1075.E
1100.E	3.20	0.65	-2.00	1.70	-0.95	1.05	0.27	75.57	-29.54	-1.05	0.65	1.15	-2.13	1100.E
1125.E	3.20	0.63	-2.00	1.70	-0.95	1.05	0.26	74.45	-30.41	-1.05	0.65	1.12	-2.07	1125.E
1150.E	3.20	0.66	-2.10	1.60	-0.95	1.05	0.26	79.51	-23.92	-1.15	0.55	0.99	-2.37	1150.E
1175.E	3.20	0.66	-2.10	1.50	-0.95	1.05	0.25	81.29	-21.36	-1.15	0.45	0.81	-2.37	1175.E
1200.E	3.20	0.71	-2.10	1.60	-0.95	1.05	0.25	89.63	-11.56	-1.15	0.55	1.06	-2.55	1200.E
1225.E	3.20	0.76	-2.10	1.60	-0.95	1.05	0.24	98.55	-1.58	-1.15	0.55	1.14	-2.73	1225.E
1250.E	3.20	0.74	-2.10	1.60	-0.95	1.05	0.23	98.75	-1.32	-1.15	0.55	1.11	-2.66	1250.E
1275.E	3.20	0.72	-2.10	1.70	-0.95	1.05	0.23	99.04	-0.98	-1.15	0.65	1.28	-2.50	1275.E
1300.E	3.20	0.69	-2.20	1.60	-0.95	1.05	0.22	97.97	-2.01	-1.25	0.55	1.03	-2.70	1300.E
1325.E	3.20	0.65	-2.40	1.50	-0.95	1.05	0.21	95.37	-4.44	-1.45	0.45	0.80	-2.95	1325.E
1350.E	3.20	0.65	-2.50	1.60	-0.95	1.05	0.21	98.63	-1.27	-1.55	0.55	0.97	-3.15	1350.E
1375.E	3.20	0.60	-2.60	1.60	-0.95	1.05	0.20	94.21	-5.18	-1.65	0.55	0.90	-3.00	1375.E
1400.E	3.20	0.60	-2.50	1.60	-0.95	1.05	0.19	97.54	-2.12	-1.55	0.55	0.90	-2.91	1400.E
1425.E	3.20	0.56	-2.60	1.60	-0.95	1.05	0.19	94.29	-4.77	-1.65	0.55	0.84	-2.80	1425.E
1450.E	3.20	0.61	-2.60	1.50	-0.95	1.05	0.18	106.38	5.15	-1.65	0.45	0.75	-3.15	1450.E
1475.E	3.20	0.54	-2.70	1.60	-0.95	1.05	0.17	97.55	-1.91	-1.75	0.55	0.81	-2.95	1475.E
1500.E	3.20	0.57	-2.70	1.50	-0.95	1.05	0.17	106.66	5.00	-1.75	0.45	0.70	-3.12	1500.E

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201104

UNITS FLAG= 0 CURRENT ELECTRODE CO-ORDS= 1000.E 700.S 1000.E 2500.S
 PLOT SCALE= 2500. HN SCALE 10. PFE & RPS SCALE= 1. HSQ & HSP SCALE= 1.
 ORIGIN CO-ORDS= 500.E 2400.S ARRAY IDENTIFIER= LN01 ANNOTATION SUPPRESSION FLAG= 0
 SPLINE INTERVAL= 0.
 PLOT BASE LEVELS FOR PFE,RPS,HSQ,HSP ARE 0.00 0.00 0.00 0.00

PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

HN = 0
 MMR = 1
 PFE = 0
 RPS = 1
 HSQ = 1
 HSP = 0

FOR HN , MMR 100.00 0.00

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Q36/29

201105

1104

DOCUMENT LISTMIP2 , NORMC001AMIP2RUNP: LPOO ON 15/05/79 AT 12.38

PROGRAM MIP2.CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS
3HZ RRMIP SURVEY LOONGANA AREA TAS 068R ARRAYN001

103

201106

INTERP TAPE FLAG# 0 GRIDDATA TAPE FLAG# 0

LINE POSITIONING MULTIPLYING FACTOR# 1.0

P CON PART U

