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vol 1/2

REPORT ON EXPLORATION PROGRESS

PERIOD ENDING APRIL 1979

MT. PEARSE E.L. 10/77.

MICROFILMED

J.R. CHAPMAN
ADVANCED GEOLOGIST

SEPTEMBER 1979

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1. INTRODUCTION

In 1977 Pennzoil was granted Exploration Licence 10/77 at Mt. Pearse in Western Tasmania. The licence area is immediately east of two major tin deposits - Mt. Bischoff (now depleted) and Cleveland (currently in production).

The licence has never been effectively explored in the past due to almost complete cover of the Precambrian and Palaeozoic geology by Tertiary basalts. Pennzoil planned to utilise the recently developed Rapid Reconnaissance Magnetic Induced Polarisation method (R.R.M.I.P.) to locate sulphide accumulations beneath the basalt cover. The principle conceptual target was, and remains, stanniferous massive pyrrhotite replacement deposits of the Mt. Bischoff type.

During the 1977/78 field season a reconnaissance survey program was designed to test the area of greatest potential. Technical problems caused this initial attempt to abort, but the problems were subsequently overcome and the program was completed in late 1978.

This report follows on from the Progress Report to April 1978 and covers all exploration during the 1978/79 field season, and proposes a continuing program for the coming field season.

2. SUMMARY OF WORK COMPLETED

1. The reconnaissance grids previously prepared were surveyed using the RRMIP system. This totalled approximately 24 line kilometres of survey.
2. A detailed "follow-up" survey was carried out over two anomalies generated by the above program. A 800 x 2000 metre grid was prepared and surveyed at varying electrode spacing and transmission frequency. This phase totalled 13.6 line kilometres of survey.

3. EXPENDITURE

A total of \$52,887.16 has been spent on E.L. 10/77. A breakdown of the expenditure is given in Appendix A.

4. DESCRIPTION OF THE PROJECT AREA

Appendix B is a progress report for the period ending April, 1978. It includes a description of the location, general geology and geophysical results to April, 1978.

5. RECONNAISSANCE RRMIP SURVEY (Ref:Printographs,Map No 48196, Plates 2,3 & 4)

Introduction

All RRMIP surveys were carried out by Scintrex Pty.Limited with Pennzoil supervision and manpower support. Six arrays, each incorporating four 1,000 metre survey lines were completed,totalling 24 line kilometres. This combined with previous programs gives a total reconnaissance RRMIP survey coverage on the Mt. Pearse project

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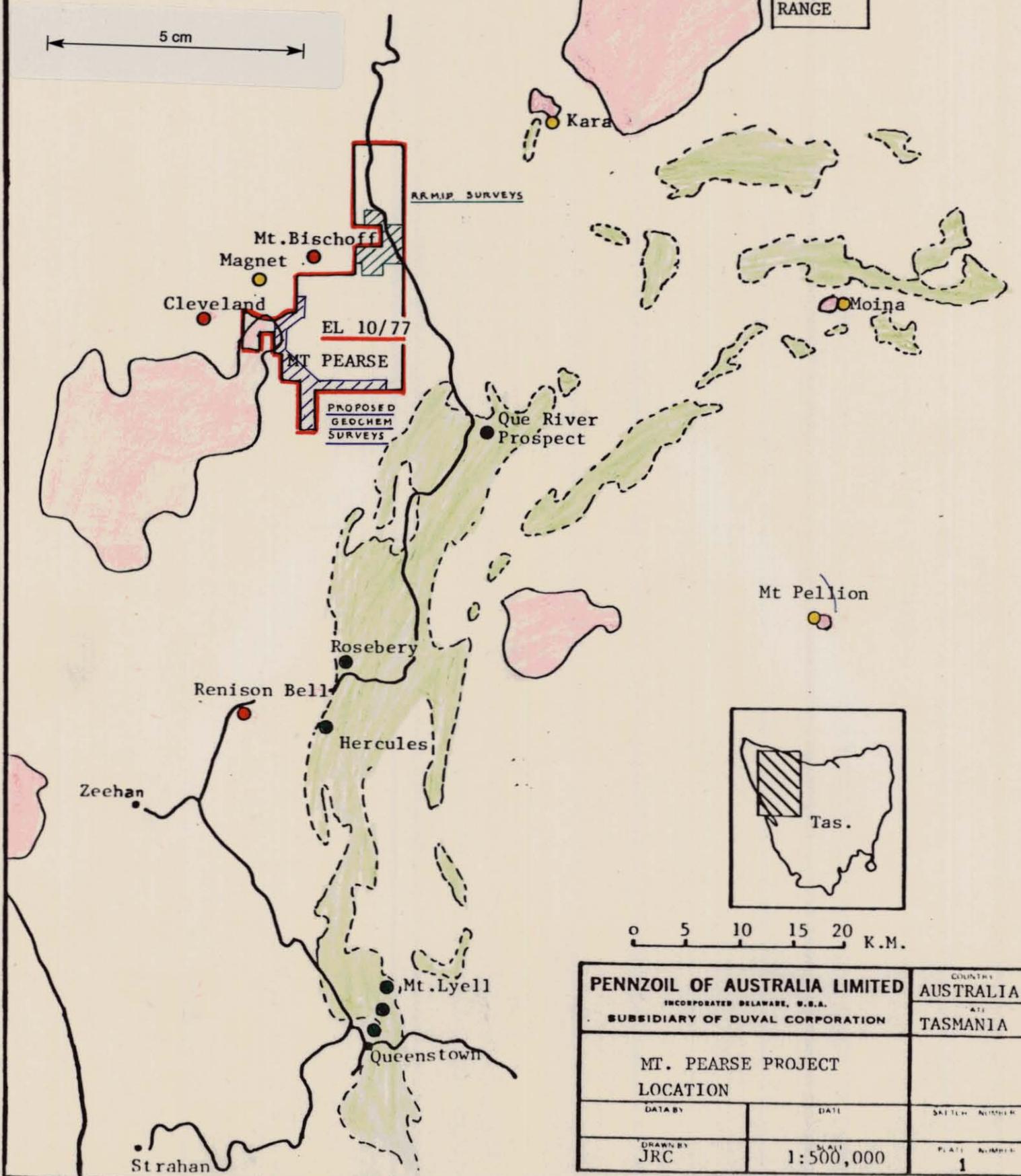
Ulverstone

- Volcanogenic Deposit
- Major Tin Deposit
- Hydrothermal/Metasomatic Mineralisation

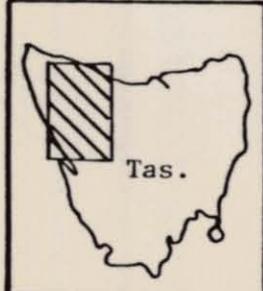
- Devonian Granite
- Mt. Read Volcanogenic Lithologies

5 cm

EL 24/73
DIAL RANGE



Mt Pellion



0 5 10 15 20 K.M.

PENNZOIL OF AUSTRALIA LIMITED INCORPORATED DELAWARE, U.S.A. SUBSIDIARY OF DUVAL CORPORATION		COUNTRY AUSTRALIA STATE TASMANIA
MT. PEARSE PROJECT LOCATION		
DATE BY	DATE	SHEET NUMBER
DRAWN BY JRC	SCALE 1:500,000	PLATE NUMBER 1

of 30 line kilometres. For array locations see Map No 48196. An electrode spacing of 2 kilometres and a transmission frequency of 3 hertz was utilised in the survey.

The data is presented as computer plotted line profiles (or printographs) of magnetometric resistivity (M.M.R.), relative phase shift (R.P.S.) and secondary field quadrature (H.S.Q.). The printographs are incorporated in this report and labled 063R, Array Nos 1 to 6. In addition Anomalies I,II and III are presented in Plates 2,3 and 4 respectively.

The parameters M.M.R. and R.P.S. represent bedrock conductivity and chargeability respectively. The parameter H.S.Q. is analogous to M.M.R. but represents the secondary current flow due to induced polarisation. Appendix C is an explanation of the M.I.P. method and parameters used.

Results

The basalts at Mt. Pearse are in general resistive and somewhat chargeable. Although there is a relatively high noise level due to shallow features 3 survey lines have well defined anomalies that were considered to have deep sources. The following descriptions of the anomalies were written prior to the "follow-up" detailed surveys.

Anomaly I - Line 2800N, 1450E (Refer Plate 2)

A good 0.5 degree RPS anomaly at 1450E is on the edge of a +42 percent MMR feature centred just east of 1300N. The RPS anomaly represents a moderately chargeable source some 100 metres below surface. The RPS anomaly is not conductive.

Anomaly II - Line 2500E, 1500N and 1325N (Refer Plate 3)

Superimposed on an artificial gradient on the RPS profile due to "wire effects" are RPS anomalies at 1500N and 1325N. The anomalies have RPS amplitudes of approximately 0.60 degrees (above background). Adjacent to the 1325N feature the MMR response is increasing, possibly, due to the same conductivity source as at Anomaly I. The sources are some 50 metres below surface.

Anomaly III - Line 4300E, 3075N (Refer Plate 4)

A 0.4 - 0.5 degree RPS anomaly at 3075N indicates a chargeable zone some 50-75 metres below surface. The anomaly coincides with a relatively resistive zone on the MMR profile. This could indicate a high in the pre-basalt topography.

Generally the M.M.R. results are of little interperative value beyond predicting local pre-basalt topographic highs identified by anomalously low conductivities.

Conclusions

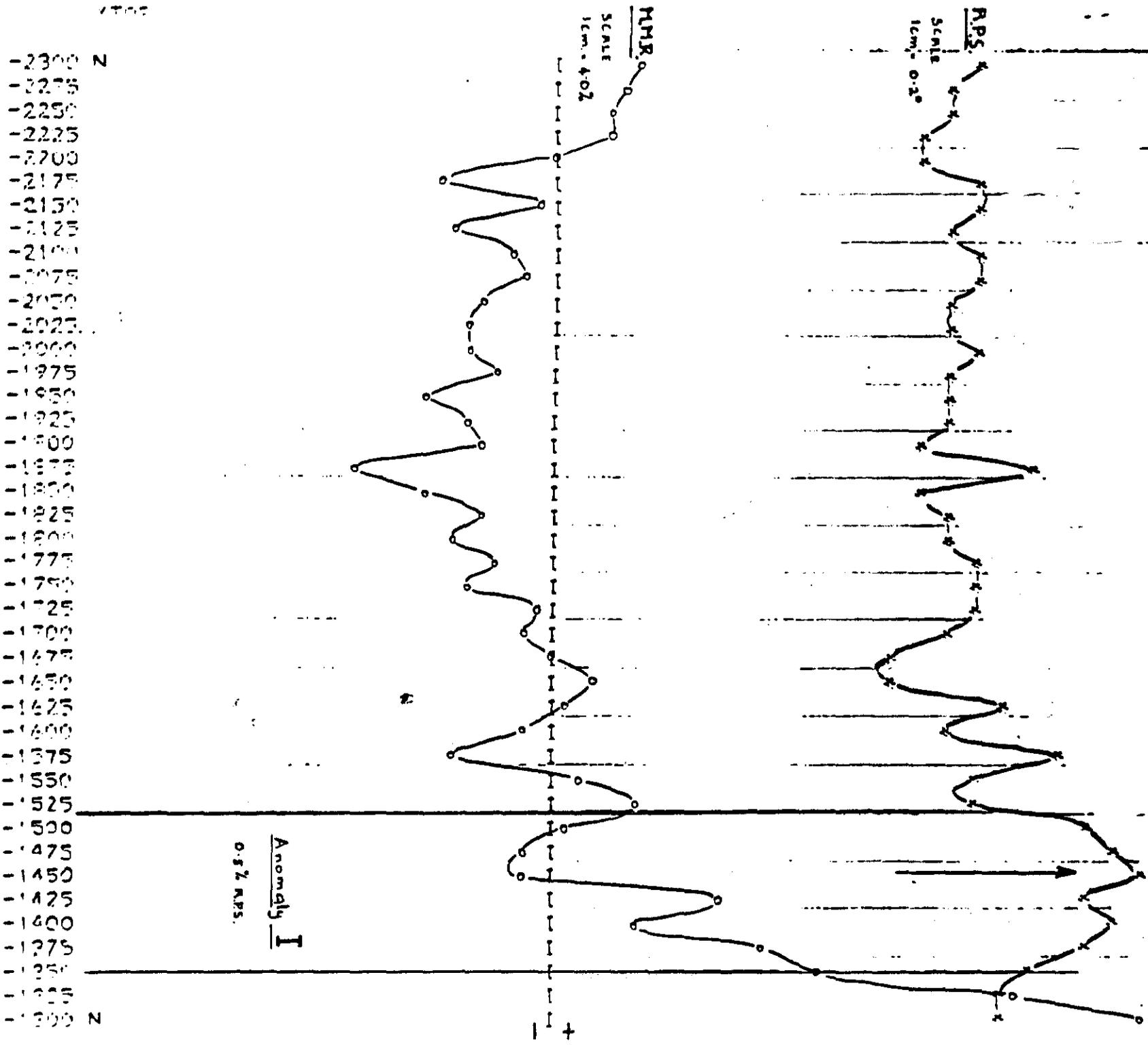
Although the results are generally noisy and "wire effects" at the end of lines are in some cases substantial there was a high level of confidence in the effectiveness of the survey. Features that only became apparent after the detailed survey will be discussed later.

Anomaly I at 2800E, 1450N is the most significant RRMIP feature. It is also coincident with a previously identified magnetic trend. (See Map No. 48196). As it was located by a reconnaissance program it was decided that it must be more closely defined by a detailed survey before drill testing. A new array centred on the anomaly was therefore planned and surveyed in a "follow-up" program.

LINE 2800 E

128006

Plate 2



Anomaly I
0.5% MPS

-2300 N
 -2275
 -2250
 -2225
 -2200
 -2175
 -2150
 -2125
 -2100
 -2075
 -2050
 -2025
 -2000
 -1975
 -1950
 -1925
 -1900
 -1875
 -1850
 -1825
 -1800
 -1775
 -1750
 -1725
 -1700
 -1675
 -1650
 -1625
 -1600
 -1575
 -1550
 -1525
 -1500
 -1475
 -1450
 -1425
 -1400
 -1375
 -1350
 -1325
 -1300 N

LINE 2500 E

128007

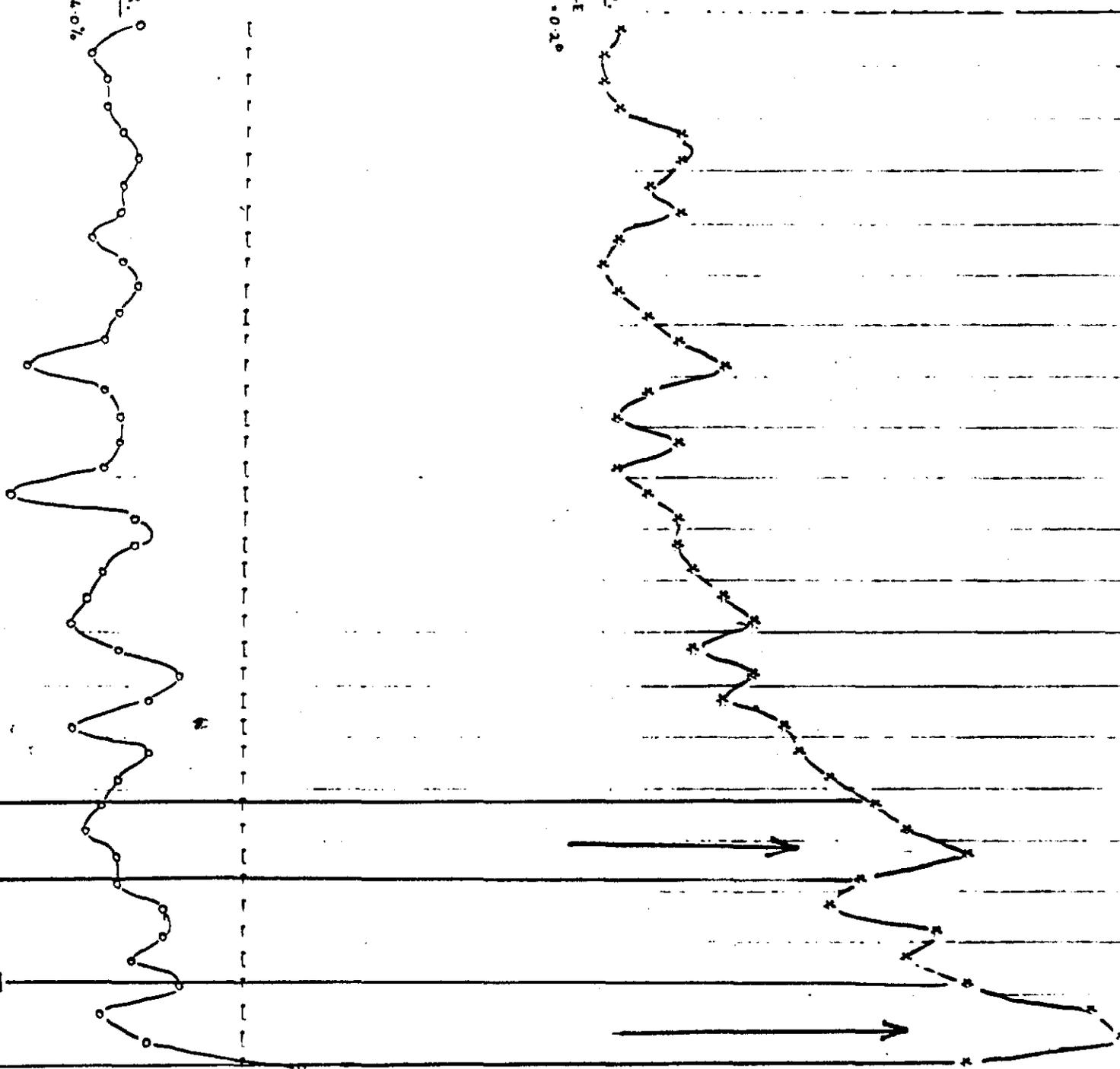
Plate 3

RPS
SCALE
1cm = 0.2°

MJR.
SCALE
1cm = 4.0%

-2300 N
-2275
-2250
-2225
-2200
-2175
-2150
-2125
-2100
-2075
-2050
-2025
-2000
-1975
-1950
-1925
-1900
-1875
-1850
-1825
-1800
-1775
-1750
-1725
-1700
-1675
-1650
-1625
-1600
-1575
-1550
-1525
-1500
-1475
-1450
-1425
-1400
-1375
-1350
-1325
-1300 N

(0.5% RPS)
Anomaly I
(0.4 RPS)
Anomaly II

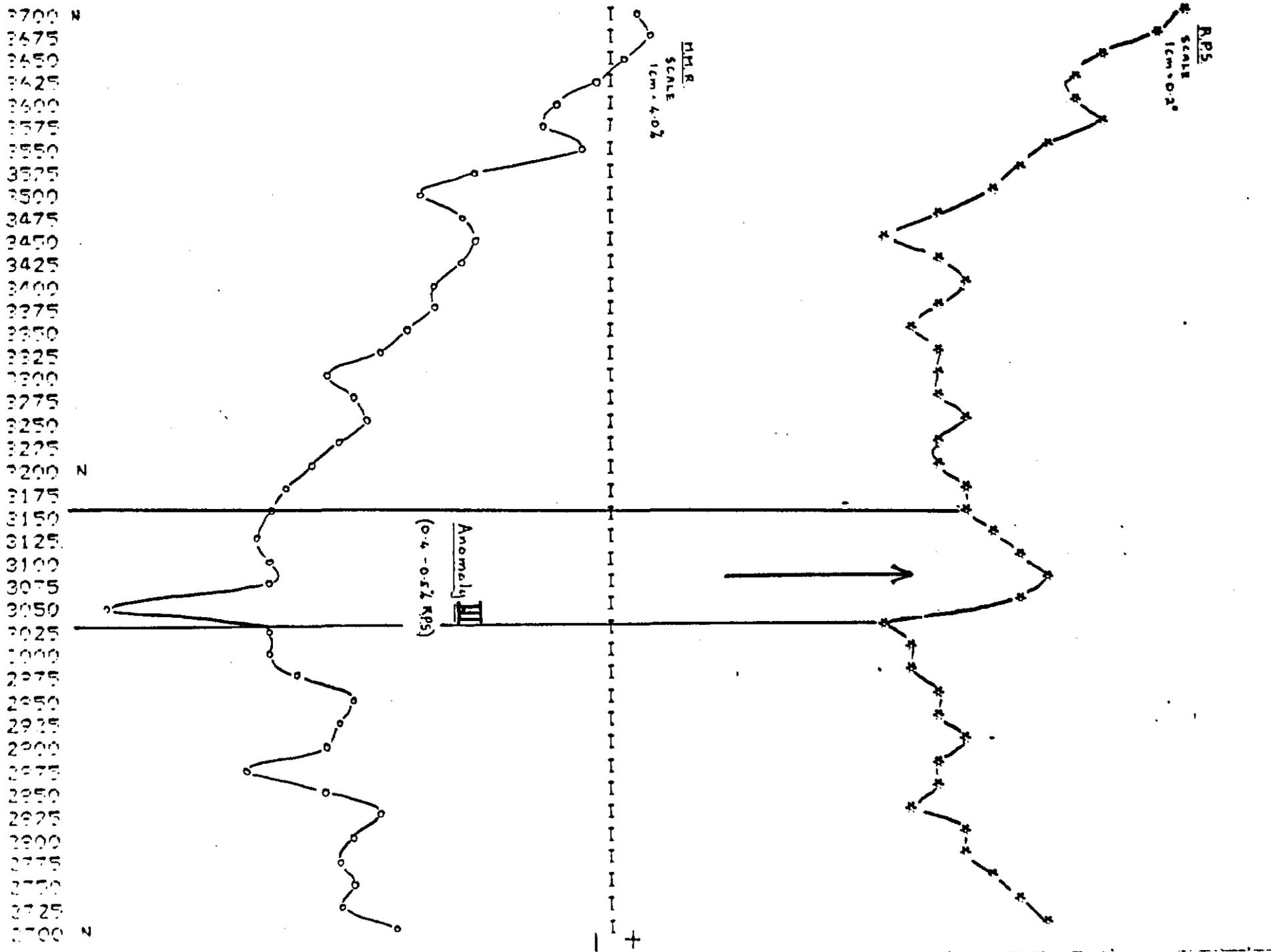


+

LINE 4300 E

128008

Plate 4



3700 N
 3675
 3650
 3625
 3600
 3575
 3550
 3525
 3500
 3475
 3450
 3425
 3400
 3375
 3350
 3325
 3300
 3275
 3250
 3225
 3200 N
 3175
 3150
 3125
 3100
 3075
 3050
 3025
 3000
 2975
 2950
 2925
 2900
 2875
 2850
 2825
 2800
 2775
 2750
 2725
 2700 N

H.M.R.
 SCALE
 1cm. 4.0%

R.P.S.
 SCALE
 1cm. 0.2°

Anomaly

(0.4 - 0.5% RPS)

800

6. DETAILED R.R.M.I.P. SURVEY (Ref: Printographs, Plate 5)

Introduction

The new array was planned to cover both anomalies I and II. One hundred metre spaced grid lines were cut and numbered to conform with the existing grid system. (See Plate 5).

Initially the area was surveyed using a 2 kilometre electrode spacing and 3 hertz frequency as in the original survey. The results are presented in printographs 070R, Array No.1.

The electrode spacing was then reduced to 1 kilometre and the central seven lines resurveyed. This was to give better definition by increasing the current in the circuit and improved "focussing" if the source was of limited strike length. It was recognised that the pre-basalt topography could have a substantial effect on the configuration and near surface extent of a potential sulphide body. Line 2800E was resurveyed at 1 hertz to confirm that 3 hertz is the most effective frequency in this terrain. The results of the 1 kilometre, 3 hertz and 1 hertz surveys are presented in Printographs 070R, Array No 2.

A fourth parameter, percentage frequency effect (PFE) is also presented in these data. As with RPS this represents chargeability but is derived from separate readings and so acts as a check on RPS results suspected of being spurious. Note a reversed sign convention with the PFE printographs. An increase in PFE (increase in chargeability) is represented by a drop in the line profiles.

Results

The original anomaly II was not repeated during this survey. Line 2500E has no anomalous RPS results except an increase at the northern end of the line that is attributed to "wire effect". The adjacent line 2600E exhibits small RPS (0.3^o) and PFE (0.5%) anomalies centred on 1525N, but this feature does not continue onto line 2700E.

On line 2800E erratic RPS results over the same location as Anomaly I indicates the anomaly could still be there. However the PFE response is flat suggesting a "pseudo" RPS anomaly.

The survey produced no other MIP features that could be validly considered as having a massive sulphide source. Numerous erratic results are attributed to local cultural features including powerlines an old railway and a buried telephone cable.

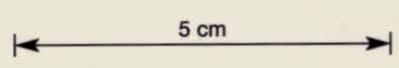
The electrode spacing was then reduced to 1 kilometre and lines 2500E to 3100E were resurveyed. This increased the current through the circuit from 3.5 amps previously to 4.5 amps. The effect was that "noise" levels in the readings were reduced substantially giving flatter profiles. The possible anomalies on lines 2600E and 2800E disappeared. Portion of line 2800E was rerun at 1 hertz frequency and this confirmed that no valid bedrock source exists in the vicinity of Anomaly I.

7. GENERAL DISCUSSION OF RRMIP RESULTS

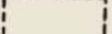
The RRMIP results from the Mt. Pearse surveys, and from surveys elsewhere in Tasmania where there was good geological control across the perimeter of basalt cover, has led to some general observations.

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128010



-  - Reconnaissance Survey R.P.S. Anomaly
-  - Detailed Survey R.P.S. Anomaly

-  - Array 1 electrodes
-  - Array 2 electrodes
-  - Circuit loop

NOTE Location 28E 18N on this map refers to location 2800E 1800N on line printographs

PENNZOIL OF AUSTRALIA LIMITED <small>INCORPORATED DELAWARE, U.S.A.</small>		COUNTRY Australia
SUBSIDIARY OF DUVAL CORPORATION		STATE Tasmania
MT. PEARSE DETAILED R.R.M.I.P.		LATITUDE
		LONGITUDE
DATA BY PZL. SCINTREX	DATE SEPT 1979	SKETCH NUMBER
DRAWN BY JRC	SCALE 1:20000	PLATE NUMBER 5

01C

The following comments are from a final report on E.L. 2/76 but refer to the Mt. Pearse Project as well.

"The reliability of the Relative Phase Shaft (R.P.S. - represents chargeability) results appear to be dependant on the intensity of current flow within the circuit. With approximately 2km electrode spacing, a low current e.g. 3 amps tend to give high but variable R.P.S. readings. In this situation it is suspected that "noise" is substantially affecting the readings inevitably giving rise to false or pseudo anomalies. With a higher current flow e.g. 4 amps the R.P.S. values are lower but profiles are smoother reflecting less "noise" contamination. This phenomenon gives rise to two distinctive features.

1. With a low current circuit the low current densities occurring at the end of lines, mainly the lines closest to the electrodes, results in an increase in the R.P.S. levels giving "valley" shaped profiles.
2. With a low current, cultural features and specifically the magnetic field generated by the circuit loop ("wire effect") can contaminate to the extent of obscuring meaningful results in portions of the array."

These effects were prominent in the Mt. Pearse surveys where 2 kilometre electrode spacing was used. It therefore appears crucial, with the present instrumentation, to get adequate current into the ground wherever the basalt cover is substantial. The surveys within E.L. 2/76 showed that the basalt does not give spurious chargeability results when the current flow is adequate, and so Pennzoil is confident of the effectiveness of the system given the right conditions.

8. CONCLUSIONS

The RRMIP exploration program within E.L. 10/77 has failed to locate targets worthy of drill testing. Two anomalies produced during the reconnaissance surveys were shown to have no valid bedrock source by subsequent detailed surveys. This negated the rationale of testing other lesser anomalies.

It is evident that blanket RRMIP surveys, with no geological control, are unfeasible. Excessively thick basalt cover (e.g. plus 100 metres) causes attenuation of results that can only be remedied by smaller arrays, thus defeating the rapid reconnaissance nature of the programs.

However if other approaches can be used to focus on target areas beneath basalt cover, RRMIP remains the most suited geophysical system for this environment.

9. PROPOSAL FOR CONTINUING EXPLORATION

As E.L. 10/77 remains highly prospective for buried stanniferous massive pyrrhotite deposits, it is proposed that geochemical methods be used to continue the search for favourable environments.

1. Pan concentrates from stream draining the basalt contact should be tested for tin and tungsten to locate sub-basaltic fluvial sediments anomalous in these metals.
2. Minus 80 mesh stream sediment and water analyses could help locate sub-basaltic water seepage anomalous in base metals and flourine. The substantial flourine and copper, lead and zinc halos to the Cleveland and Mt. Bischoff tin deposits provide the basis of this approach.

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Sampling is proposed in the areas indicated on Plate 1, chosen for the proximity of the Meredith granite and the prospective carbonate bearing Cambrian sequences trending beneath the basalt.

This program involves the collection of ± 120 samples (40 each of pan concentrates, -80 mesh sediment and water), and would take approximately 2 weeks.

Identification of a sub-basaltic geochemically anomalous environment would lead to geophysical testing using the RRMIP, and diamond drilling if warranted.

012

ENCLOSURES

- Appendix A Expenditure Sheet
- Appendix B Progress Report to April 1978
- Appendix C Explanation of the RRMIP System.
- Map No. 48196 - Geophysics
- Printographs 063R Arrays 1 to 6 - Reconnaissance RRMIP Surveys
- Printographs 070R Arrays 1 & 2 - Detailed RRMIP Surveys.

Period INCEPTION TO AUGUST 1979

The following are transcribed from the Pennzoil of Australia Limited expenditure records.

Project..... MT. PEARSE

Expenses

001	Surface Rights34.73.....
002	Mineral Rights829.52.....
003	Annual Rentals121.50.....
101	Geological Surveys	..8,941.31.....
102	Geophysical/Geochemical	..36,691.83.....
103	Site Prep. for Drilling
104	Diamond Drilling
105	Assays, Augering
106	Travel, General
107	Administration Expense	..4,781.77.....
108	Vehicle & Equipment	..1,486.00.....
	
		52,887.16

TOTAL EXPENDITURE THIS PERIOD

TOTAL PREVIOUSLY REPORTED

52,887.16

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PENNZOIL OF AUSTRALIA LIMITED

REPORT ON EXPLORATION PROGRESS
PERIOD ENDING APRIL, 1978

MOUNT PEARSE - E.L. 10/77

J.R. Chapman
Project Geologist
APRIL, 1978

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INTRODUCTION

In 1977 Pennzoil became financially involved in the development of a low noise magnetic I.P. system by Scintrex Pty. Ltd. called the R.R.M.I.P. (Rapid Reconnaissance Magnetic Induced Polarization). With access to this potential geophysical quantum jump Pennzoil reviewed areas that hold strong mineral potential but have been insufficiently explored due to adverse ground cover conditions. Mt Pearse was selected as the highly prospective Precambrian and Palaeozoic geology here was previously unexplored due to a plus 100 metre thick basalt cover. The R.R.M.I.P. system was to be used to attempt penetration of the basalt.

The project area is situated within the extremely productive west Tasmania portion of the Tasman Geosyncline and is located immediately east of two major tin occurrences, (i) Mt Bischoff, a worked out but once world famous tin mine, and (ii) the producing Cleveland mine. Other nearby mineral occurrences include the exhausted Magnet lead-silver-zinc mine and the recently discovered Que River massive lead-zinc-copper bodies.

Exploration Licence 10/77 was granted to Pennzoil in 1977. This report describes all exploration activity carried out since that date.

SUMMARY OF WORK COMPLETED

Phase 1 of the program involved a review of all published data and reconnaissance geology to estimate the basalt thickness within the E.L. and to identify prospective geology that trends beneath the basalt cover.

Phase 2 involved systematic wide spaced gridding (35 line kilometres) and an attempted R.R.M.I.P. survey. The R.R.M.I.P. was unsuccessful and the gridded lines were surveyed by proton magnetometer.

ACCESS AND PHYSIOGRAPHY

The area consists of a moderately flat plateau with deeply incised drainage occurring off the edge of the basalt capping. Excellent access is provided by the conveniently located Murchison Highway and Savage River Road. Logging tracks service most areas not traversed by the main roads. Vegetation within the E.L. includes dense myrtle forest with interspaced button grass plains and open and closed eucalypt forest.

PREVIOUS WORK

As the E.L. is adjacent to Mt Bischoff surface prospecting by the old timers would have been comprehensive. However the only remote sensing effort to date that would have penetrated the basalt cover was an Aero-magnetic survey flown by CRA in the 1950's. This was part of a regional survey and flight lines were too widely spaced to be of any detailed use.

GENERAL GEOLOGY (Refer Map No. 48194, 48178)

E.L. 10/77 is nearly entirely underlain by Tertiary deposits of basalt lava flows with minor basal and interflow sediments. Descriptions of the pre-Tertiary geology are derived from surrounding exposures and are extrapolated to represent the rocks immediately underlying the Tertiary sequence.

The oldest rocks are Precambrian slates and quartzites that form an east-west trending anticlinorial inlier penetrating a Cambrian sequence. The Precambrian also contains minor dolomites and limestones that have acted as hosts to the Mt Bischoff stanniferous pyrrhotite bodies.

The Cambrian sequence trends north east and consists predominantly of poorly sorted marine greywackes, siltstone and mudstone. Other lithologies include basic to ultra-basic intrusives, basic volcanics, chert and conglomerate. An atypical massive conglomerate containing prominent limestone clasts outcrops to the immediate south of the E.L.

Overlying the Cambrian are well sorted Ordovician sedimentary rocks. These outcrop in the south east extremity of the E.L. forming the resistant Mt Pearse.

The Devonian Meredith granite intrudes the Cambrian sequence and is the source of the district's tin mineralization. Alluvial workings over the granite reflect mineralization within shears, intrusive phases and greisens. Related quartz feldspar porphyry dykes containing cassiterite occur at Mt Bischoff.

The only other pre-Tertiary rocks are Permian glacio-marine sediments occurring to the north of the E.L.

BASALT THICKNESS (Refer Maps No. 48195, 48179)

To determine the basalt thickness within the E.L. an understanding of the pre-basalt Tertiary topography was required. Elevations of the base of the basalt were obtained from published data and results of drilling by Tasmania Mines Department at Fooks Lode

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Waratah, and by North Prospecting Pty. Ltd. to the east of E.L. 10/77. Field measurements were also made using an altimeter. Unfortunately the basal contact is usually masked by scree slopes.

From the available data it appears that the pre-basalt Tertiary drainage was principally to the north east with hills formed by porphyry intruded quartzites of Mt Bischoff, the Meredith granite and Mt Pearse acting as an arcuate water shed to the west and south. Relief and drainage slope within the central portion of E.L. 10/77 were probably relatively gentle.

The average thickness of the basalt within the subsequently gridded area is estimated to be approximately 100 metres.

GEOPHYSICS

1. Location

It was decided that the most prospective conceptual target that would be detectable is a tin bearing massive pyrrhotite replacement body after carbonates.

Within this concept, factors examined to determine the location of the first R.R.M.I.P. survey included the following:

- a) The easterly trend of the Precambrian inlier that contains dolomite.
- b) The porphyry dyke trend at Mt Bischoff.
- c) The trend connecting the Meredith granite and the Mt Housetop granite to the north east.
- d) The carbonate bearing potential of the Cambrian sequence.

The area chosen was to cover the extrapolated limits of the pre-Cambrian inlier (Refer Map No. 48194).

2. Gridding (Refer Map No. 48196)

Eleven 1 km arrays each incorporating three 1 km survey lines were planned. Grid preparation proceeded slower than anticipated due to dense undergrowth, resulting in 9 arrays being available at the start of the survey. With commencement of the survey the arrays had to be altered to allow for 500 metre survey lines.

3. R.R.M.I.P. Survey

Scintrex started the survey in early February. Initial progress was slow due to rain and variable magnetic noise. At the completion of three set ups increased magnetic noise prevented further surveying. Intense efforts were made to eliminate the noise, all to no avail, and so personnel and equipment were demobilised.

Scintrex are uncertain as to the cause of the problem but subsequent instrument performance has indicated that instrument malfunction could have played a substantial role.

019

The lines that were assayed gave flat responses that are of little interest.

4. Soundings

A Schlumberger expander was used to obtain vertical electrical property information.

Results indicate that a conductive zone (80 ohm-metre), probably representing the basalt, extends to a depth of at least 100 to 150 metres. Scintrex estimates that enough current penetrates this zone to justify the effectiveness of the R.R.M.I.P.

5. Magnetics (Refer Map No. 68196)

In the absence of R.R.M.I.P. coverage it was decided to survey the prepared lines with a proton magnetometer.

Results were predictably noisy and little useful information could be gleaned from the profiles. However magnetic property trends were identified in places, especially on the eastern lines traversing base line 18N. Two parallel magnetic high zones with associated lows are identifiable.

SUMMARY AND RECOMMENDATIONS

The initial attempt to penetrate the basalt with R.R.M.I.P. was unsuccessful. As instrument malfunction is suspected as being the probable cause of failure, it is recommended that a further trial be carried out during the next summer field season.

If progress is too slow to make the entire survey feasible, the magnetic high zone, identified by the proton magnetometer survey, should at least be tested.

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APPENDIX C

Enclosed is some Scintrex derived information on the R.R.M.I.P. system, the parameters used and some typical anomaly forms.

128022

**Frequency Domain
IP Measurements using
Harmonically Related Components**
Application Brief 76-1

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020
FREQUENCY DOMAIN
IP MEASUREMENTS USING
HARMONICALLY RELATED
COMPONENTS

INTRODUCTION

The earliest and still most prevalent method of IP measurement in the frequency domain entails the comparison of earth resistivities at two widely spaced frequencies, often a decade apart. Such comparisons require, in fact, four measurements, two of current and two of voltage, using sequential transmission of current at the two frequencies. Usually a constant current source is employed which, within certain limits of load variation, keeps the ground current constant.

In any event, the traditional frequency domain method, producing the so-called PFE or Percent Frequency Effect, requires at least two measurements of voltage, a constant current source and, for greater accuracy, a measurement of the deviation of the primary current between the two measurements. The errors entailed in these measurements are additive, of course.

More recently, a second method of IP measurement in the frequency domain has come into use, in the form of the phase angle between measured voltages in the ground and the primary current. Publications by Katsube and Collett (1973), Zonge (1975) and Wynn (1975), Hallof (1974), Van Voorhis (1973), Hohmann (1975) and Seigel (1974) show the general equivalence of the measurement of the phase angle θ , at a specific frequency in the IP range, with the P.F.E. over two frequencies spanning this range.

One of the obvious advantages of phase angle measurement is that only a single frequency need be transmitted, not two frequencies sequentially, as in the older PFE measurement. Also the necessity of rigid current stabilization is eliminated. Less obvious are its disadvantages. Firstly there is the necessity of providing a phase, or time reference. This has usually been accomplished by one of two schemes, firstly radio transmission of a reference phase and, more popularly, through the use of two matched and synchronized crystal clocks. The first suffers from the usual problems of radio links, viz. blind spots and licensing problems. The latter is more successful, although requiring additional instrumentation and periodic synchronization from time to time for high accuracy.

026

The second problem with phase angle measurements is that they are rather more susceptible to E.M. Induction effects than are the equivalent PFE measurements, because they are quadrature measurements and PFE's are amplitude (mainly in-phase) measurements. Most IP workers who have the common misfortune to work in geologic environments which include moderate-to-highly conducting near-surface formations, have found that electromagnetic induction effects are particularly troublesome. In order to attempt the removal of these E.M. effects from the observed phase angles and thereby reveal the true IP contribution, various workers have proposed the measurement of phase angles at two or more frequencies; (eg. Hall of (1974) and Wynn and Zonge (1975)). In general, it is clear, that it would be foolhardy to measure phase angles at only one frequency in such an environment. To yield interpretable phase angle results, one must, therefore transmit currents with at least two widely spaced frequencies, bringing us back to the old PFE requirement.

Once one returns to a multi-frequency approach one might as well measure complex resistivities at each frequency. The totality of this information may be employed in an attempt to strip the EM coupling effects (eg. Hall of (1974) and Wynn and Zonge (1975) and to differentiate between IP sources of differing natures (eg. Zonge (1975)).

THE IPRF-2 APPROACH

The current wave form commonly employed in frequency domain IP is a square wave, simply because it is easy to create by solid state switching. It is well known that a square wave contains the fundamental and its odd harmonics, each harmonic having an amplitude inversely proportional to its order. It has always been theoretically possible to use any of these various frequency components, transmitted simultaneously, in order to obtain the desired IP information. In practice this has been rather difficult to achieve instrumentally until the advent of active filters and phase locking.

The subject of this paper is a frequency domain IP receiver, the IPRF-2, which works on the principle of the simultaneous comparison of amplitude and phase of two or more harmonically related components transmitted simultaneously in a single square wave.

Figure 1 shows, in block diagram form, the basic operation of this receiver. The input is coupled to the preamplifier by a band pass filter which eliminates any D.C. component and attenuates harmonics of order higher than three, as well as higher frequency interferences such as power lines etc.

Two additional band pass filters separate the fundamental and the third harmonic components and feed them into separate phase lock loop circuits.

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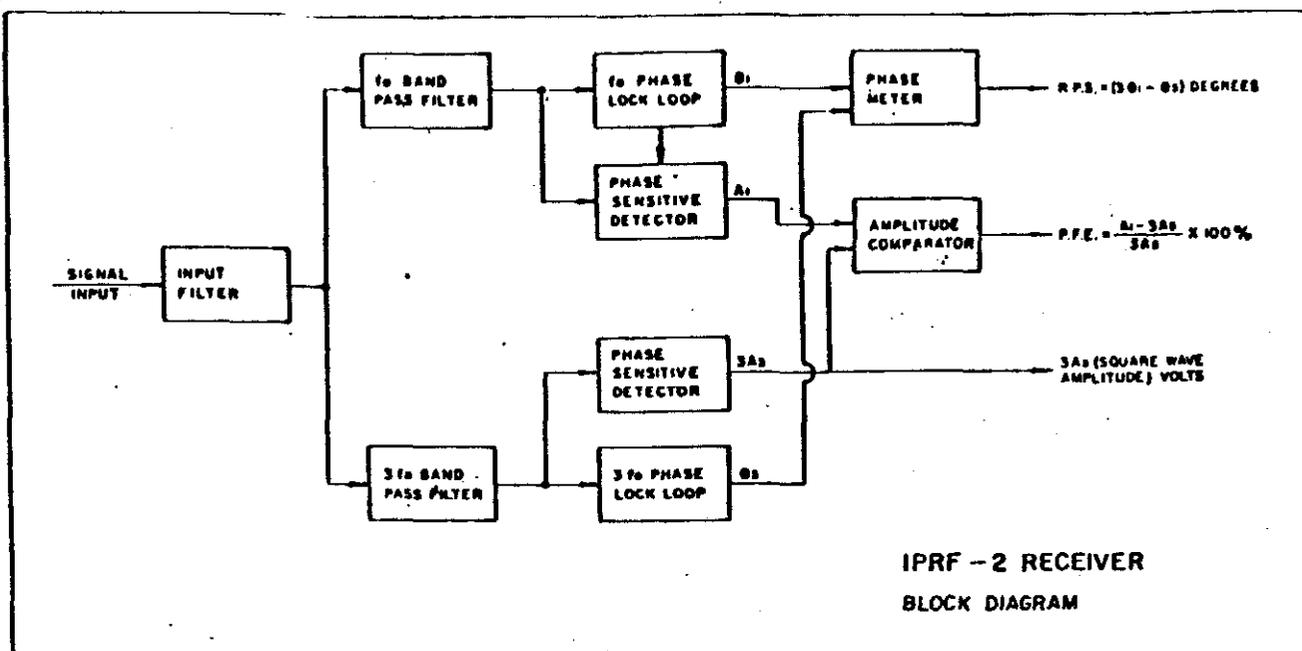


Figure 1

Phase sensitive detectors produce D.C. output voltages which are proportional to the amplitude A_1 of the fundamental and A_3 of the third harmonic of the input waveform. These two quantities are fed into an amplitude comparator, to produce the PFE (see below). The quantity A_3 is taken out separately, to be used as a measure of the square wave amplitude.

The relative phase (time shift) between the fundamental and third harmonic signals is compared on a phase meter which produces the RPS quantity (see also below).

QUANTITIES MEASURED

The quantities actually measured by the IPRF-2 are

a) The amplitude (A_3) of the square wave signal

b) The PFE defined as $\frac{A_1 - 3A_3}{3A_3} \times 100\%$ where A_1 and A_3 are the

amplitudes of the fundamental and third harmonic ground signal respectively, and

c) The Relative Phase Shift or RPS, defined as $3\theta_1 - \theta_3$ where θ_1 is the phase lag of the measured voltage of the fundamental and θ_3 is the phase lag of the measured voltage of the third harmonic relative to the transmitted components of the current.

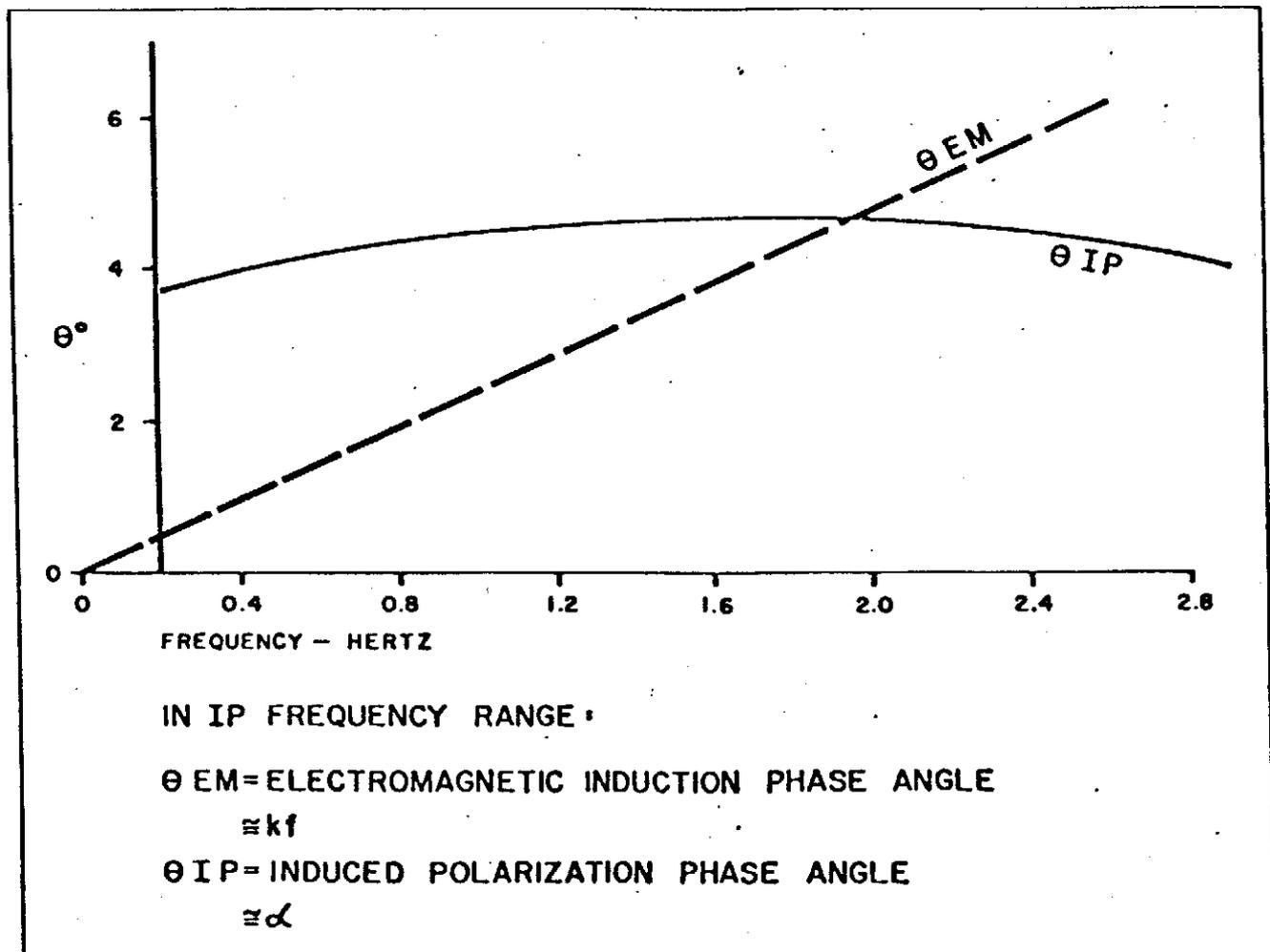
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The significance of the PFE measurement needs no comment. It is the classical frequency domain IP measurement, albeit only over a frequency difference of a factor of three rather than the more typical factor of 10. The resultant PFE's are therefore about one half of those observed over a decade change in frequency. This decrease in amplitude is more than compensated by the facts that a) the basic instrumental noise levels are less than 0.05% PFE and 0.05° RPS and b) the measurements are made simultaneously on the components of one square wave. These components will largely increase or decrease in the same proportion when the ground load changes (resistively). Measurements of PFE are thus largely unaffected by moderate ground load changes and, in fact, accuracies of 0.1% PFE are attainable with transmitters that are not current stabilized.

The significance of the RPS measurement is illustrated by Figure 2. All the field experimental evidence to date suggests that the IP phase lag θ is a slowly varying function of frequency and is, in effect, relatively constant over a factor of (say) three in frequency. Thus the RPS, as expressed by the IPRF-2, is very nearly $2\theta_1$. On the other hand, the phase shift due to

Figure 2



EM induction in the earth is almost proportional to the frequency employed, at least at very low frequencies. This fact has been remarked upon by other workers in this field, such as Hall of (1974). - For phase angles of EM origin, within the limits of the validity of the proportionality of these angles with frequency, the RPS will therefore vanish, since $\theta_3 = 3\theta_1$.

We thus come to the interesting conclusion that the IPRF-2 automatically eliminates EM coupling effects, at least at a first approximation. Field results shown by Hall of (1974) and Wynn and Zonge (1975) from actual field cases in the western U.S.A. demonstrate that EM coupling is effectively removed by this means.

EM coupling is still present in the PFE measurement and divergence between the PFE and RPS values could reflect the influence of EM effects and indicate its presence.

So far, we have mentioned only the operation of the IPRF-2 on the fundamental and third harmonic, and the information that can thereby be determined. Since the primary current wave form has many more harmonics than these, other measurements are possible, providing that the signal strength is adequate. For example, the third harmonic may be used as a false fundamental, in which case the ninth harmonic becomes the false third.

If PFE and RPS measurements are also made using the third and ninth harmonic, then additional information becomes available for use in EM coupling elimination and in discrimination between different sources of IP response.

For example it can be shown that the quadratic frequency terms in the EM coupling in the PFE and RPS may be removed, using their values obtained by employing the original fundamental and then the third harmonic as a second fundamental. To be specific, if $(PFE)_1$ and $(PFE)_3$ and $(RPS)_1$ and $(RPS)_3$ are the respective values, then the EM quadratic-stripped values become

$$\begin{aligned} PFE &= (9(PFE)_1 - (PFE)_3)/8 \\ RPS &= (9(RPS)_1 - (RPS)_3)/8 \end{aligned}$$

When measurements are made using more than one fundamental frequency, then one can use the results thereof to obtain a better approximation to actual phase angles θ rather than the RPS. For example, if f and $3f$ are used sequentially as fundamental frequencies, then

$$(RPS)_1 = 3\theta_1 - \theta_3 \text{ and } (RPS)_2 = 3\theta_3 - \theta_9$$

$$\text{Thus } (RPS)_1 + \frac{1}{3}(RPS)_2 = 3\theta_1 - \frac{\theta_9}{3} \approx \frac{8\theta_1}{3} \text{ (stripped of Induction effects)}$$

Based upon a large number of field experimental results, (eg. Scott, 1971) the normal equivalence between the two quantities measured by the IPRF-2 should be approximately given by

$$\text{RPS (degrees)} = 1.6 \text{ PFE (percent)} (\pm 10\%)$$

Any major departure from this equivalence would signify an anomalous ground response, EM coupling, measuring error, etc.

FIELD RESULTS

Figure 3 shows the IPRF-2 at work in the field.

Figure 4 shows a typical 2.5 kw transmitter being used in the field in conjunction with it.

Figure 5 shows PFE and RPS profiles over a small lead-zinc body in carbonate rocks, in the Pine Point area, Northwest Territories, Canada, together with the corresponding time domain chargeability and resistivity profiles. The similarity of all IP profiles may be noted. No attempt has been made to make the scales comparable on the various IP profiles. It can be deduced, from the regularity of the IPRF-2 field profiles that the noise level from all sources is less than 0.1% PFE and 0.1° RPS.

Figure 6 shows a 200' dipole-dipole profile over a standard test line in the Cavendish test range, Ontario. Two sulphide zones are known on this line, of which the one near 15W is more massive than the one near 9W. An operating frequency of 0.3 Hz was employed.

It is interesting to note that the westerly conductor is not as clearly indicated on the PFE values as on the RPS values. This may reflect the fact that EM induction effects are present.

SUMMARY

In summary, the IPRF-2 frequency domain IP receiver has the following novel features.

1. It operates on a single square wave, thus potentially speeding up the field procedure.
2. It is insensitive to slow changes in ground voltages, thus reducing the dependence on the primary current stabilization.

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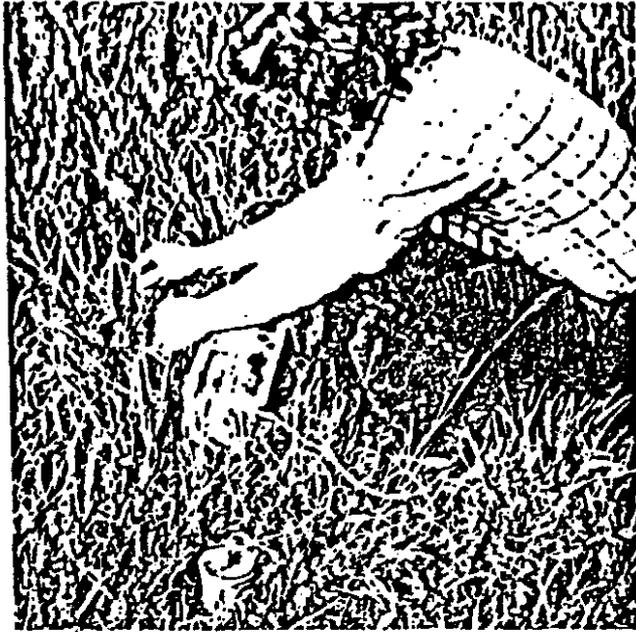


Figure 3

Figure 4

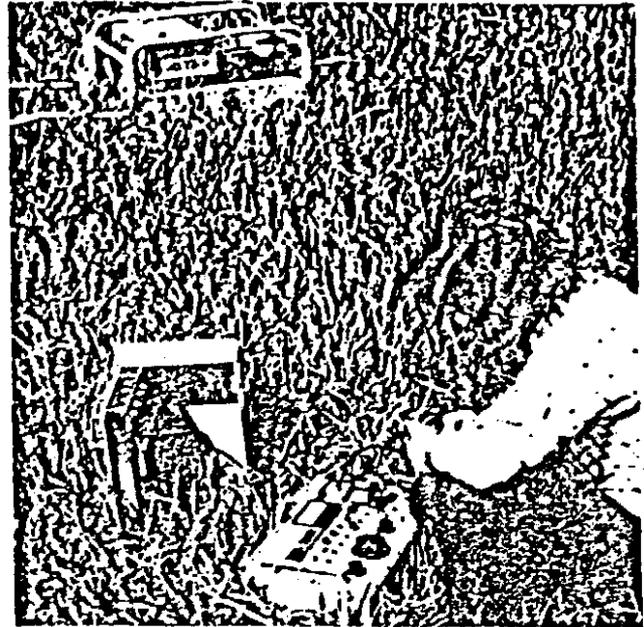


Figure 5

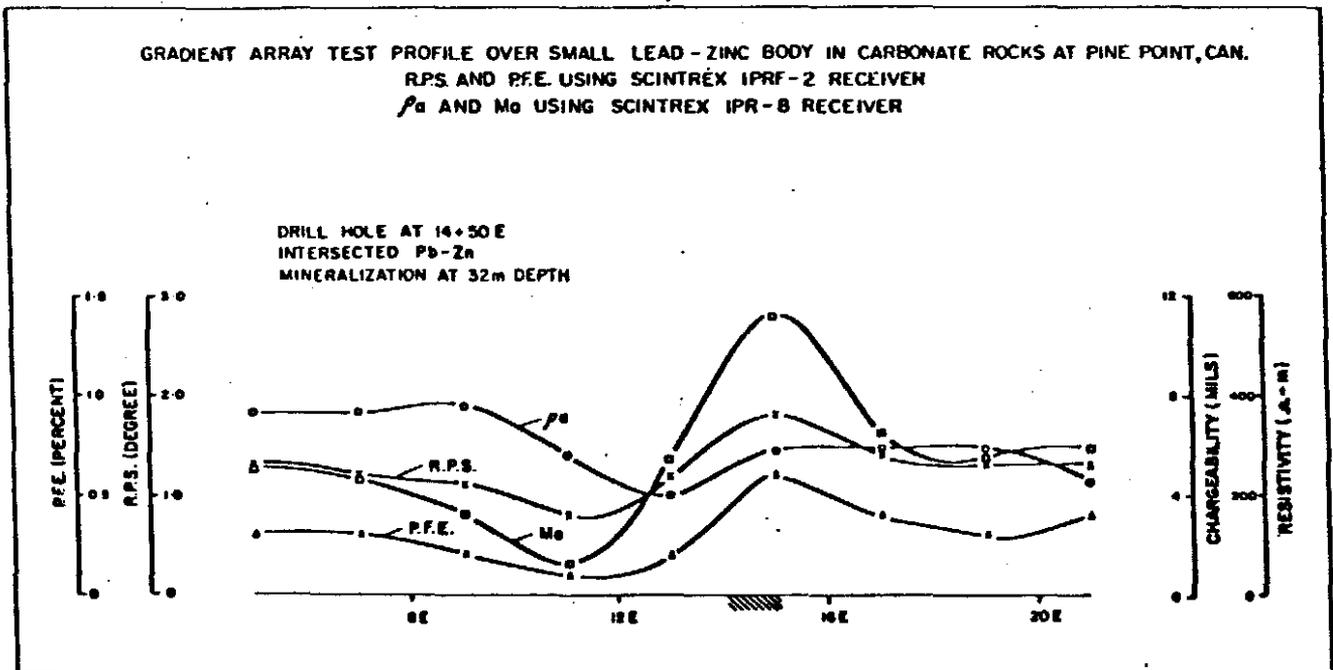
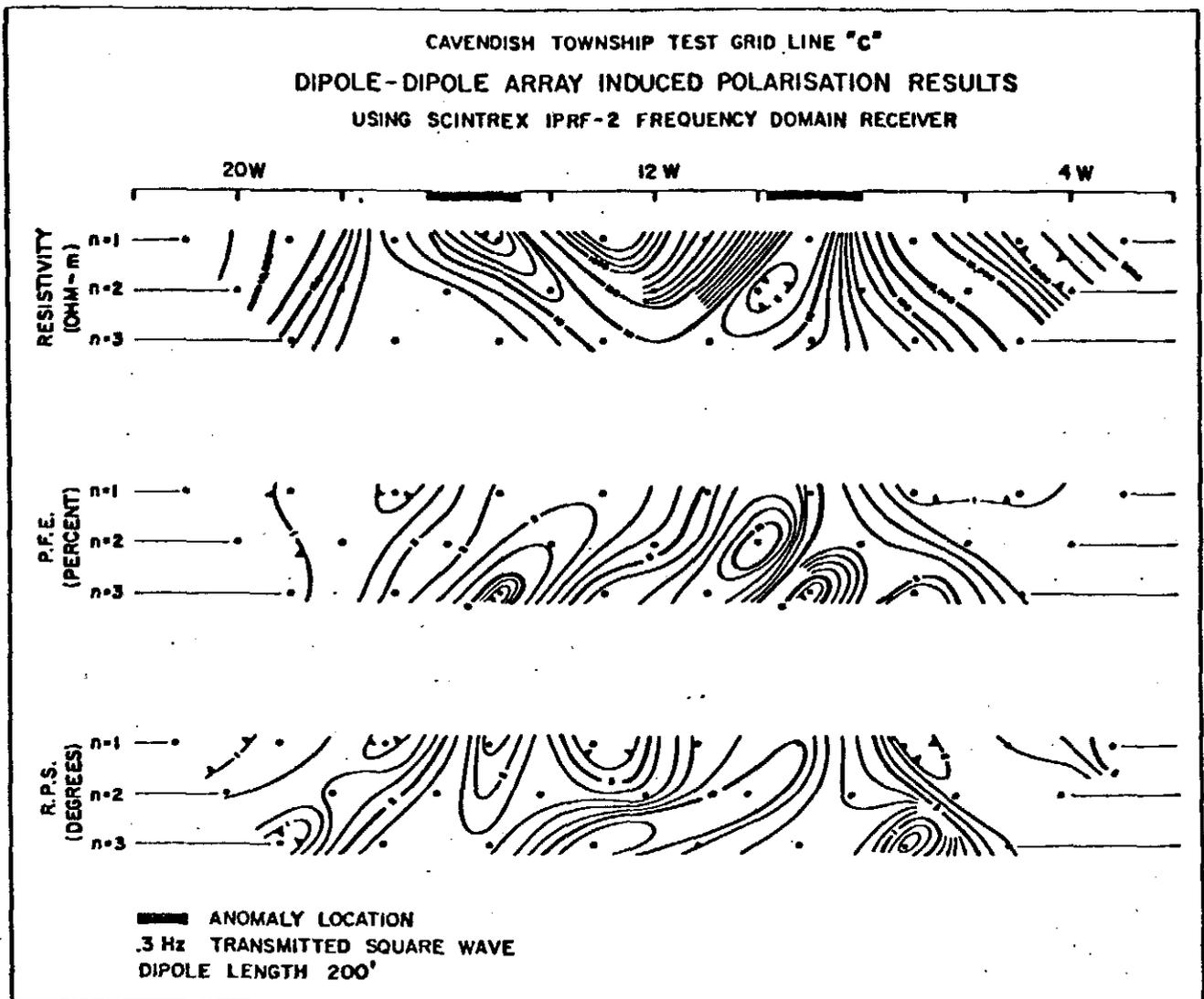


Figure 6



3. It provides the classical PFE measurement as well as a Relative Phase Measurement (RPS).

4. The RPS is achieved without the necessity of providing a time reference by radio or synchronized crystal clocks, etc., to the transmitter.

and 5. The RPS measurement is automatically largely stripped of EM Induction effects, at least to a first approximation and can be stripped to a second approximation through measurements at two fundamental frequencies.

ACKNOWLEDGEMENT

We gratefully acknowledge the permission of Pine Point Mines Limited, to present the field information shown on Figure 5.

030

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19 AUG 1977

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SCINTREX LIMITED

August 4, 1977

Dr. Graham Linford
Scintrex Pty. Limited
1031 Wellington Street
West Perth, W. Australia 6005

Dear Graham:

In reply to your telex of August 1, 1977, I would like to summarize the various frequency domain MIP parameters which are presented.

The quantities measured by the IPRF-2 are H_p , RPS and PFE. From these parameters, other fields may be calculated to emphasize anomalous zones of high conductivity or high chargeability.

The first quantity, H_p is generated by the primary current flow in the ground. Since the distribution of the primary current flow is very much dependent on electrode location, it is useful to calculate H_N , as follows:

$$H_N = \frac{H_p}{H_{pNormal}} \times 100\% \quad \text{---- (1)}$$

The normalized magnetic field, H_N is calculated from the primary field, H_p by dividing it by the magnetic field that would be observed for the current distribution in a horizontally stratified earth, that is, if the earth were made up of a number of horizontal layers of the same or varying conductivities. It should be noted that the primary magnetic field is independent of the horizontal layering. Hence, H_N is a good indicator of zones of lateral inhomogeneities and detects anomalous conductors in the ground.

A different parameter is presented in the magnetometric resistivity (MMR) method and is termed MMR anomaly.

$$\text{MMR anomaly} = \frac{(H_p - H_{pNormal}) \times 100\%}{\left(\frac{200 I}{l} \right)} \quad \text{---- (2)}$$

.. . . 2

Page Two.

Hence, the normal primary field is subtracted from the observed primary field which is then normalized by the normal field midway between the current electrodes, $200 I$. This parameter is really a normalized secondary field component associated with anomalous current flow in the ground. Nigel Edwards claims that it is a more useful parameter than H_N to interpret by comparing it with theoretical curves. One problem, however, with this presentation is that conductors in regions of high current density are emphasized.

The next parameter is associated with the polarization characteristics of the ground and is termed relative phase shift, RPS. It is defined by

$$RPS = 3 \theta_1 - \theta_3 \quad \text{-----(3)}$$

where θ_1 = Phase shift of first harmonic relative to the transmitted waveform

θ_3 = Phase shift of third harmonic relative to the transmitted waveform

For a pure square wave, $3 \theta_1 = \theta_3$ and $RPS = 0$. It, of course, provides a first order correction for electromagnetic induction effects. Also, since there is little change in phase shift due to polarizability with change in frequency, the RPS is given approximately by 2θ , twice the IP phase shift.

The sign convention for the IPRF-2 is to represent the phase shift between the primary current, I_p and the secondary current, I_s within a polarizable body as positive so that directly over such a body where the interior current dominates, a positive RPS is observed and off to the sides of the body where the exterior current dominates a negative RPS is observed.

An alternate presentation to the RPS is the quadrature magnetic field H_{SQ} divided by the primary current level I defined by

$$\frac{H_{SQ}}{I} \sim \frac{H_p}{I} \sin \phi/2 \text{ where } \phi = RPS \sim 2 \theta$$

$\frac{H_{SQ}}{I}$ is usually expressed in milligammas per amp.

$$i.e. \frac{H_{SQ}}{I} = \frac{H_p}{I} \times 1000 \sin \left(\frac{RPS}{2} \right) \quad \text{-----4.} \quad [m\gamma/r]$$

Dr. Linford

August 4, 1977

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Page Three.

H_{SQ} is analogous to the MMR anomaly parameter defined by equation (2). It is the secondary field produced by quadrature current flow in the ground due to induced polarization. The H_{SQ} field emphasizes chargeable media in the central region where the current density is higher. The RPS, however, tends to enhance anomalies on the flanks. Clearly, there is an equivalence between H_{SQ} or RPS with H_S or M in the time domain.

The percent frequency effect, PFE is defined by

$$PFE = \frac{A_1 - 3A_3}{3A_3} \times 100\% \quad \text{----(5)}$$

where A_1 = Amplitude of first harmonic

A_3 = Amplitude of third harmonic

For a pure square wave, $3A_3 = A_1$ and $PFE = 0$. The sign convention is chosen so that a negative PFE is observed directly over a polarizable body and positive off to the sides.

There is also an alternate presentation to the PFE which is termed the in phase change H_{sp} , defined by

$$\frac{H_{sp}}{I} \approx \frac{H_p \times PFE \times 1000}{100 I} \quad [m\delta/I] \quad \text{----(6)}$$

Again, H_{sp} is a secondary field associated with polarization characteristics and emphasizes anomalies in higher current density regions.

We present H_N together with the RPS and PFE or $\frac{H_{SQ}}{I}$ and $\frac{H_{sp}}{I}$.

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Dr. Linford

August 4, 1977

Page Four.

I hope this summary will help you decide which presentation is most satisfactory for your surveys in the future.

Please let us know if you have any further questions about MIP presentation.

Best regards,

SCINTREX LIMITED

Doug
Douglas H. Pitcher, M.Sc.,
Research & Development

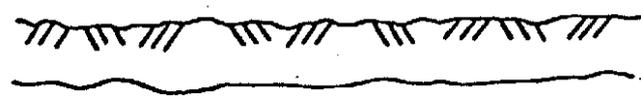
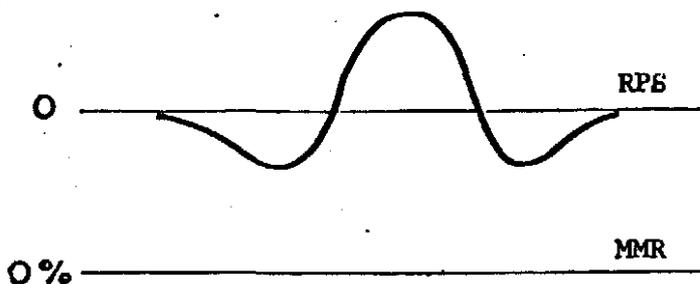
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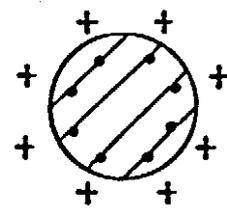
TYPICAL M.I.P. ANOMALY FORMS

THEORETICAL MODEL

CHARGEABLE SOURCE
NO RESISTIVITY
CONTRAST

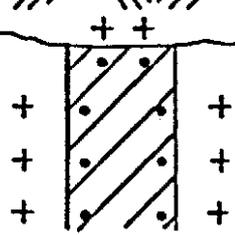
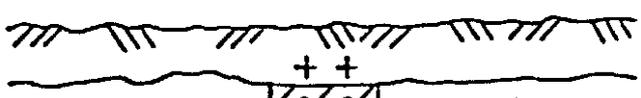
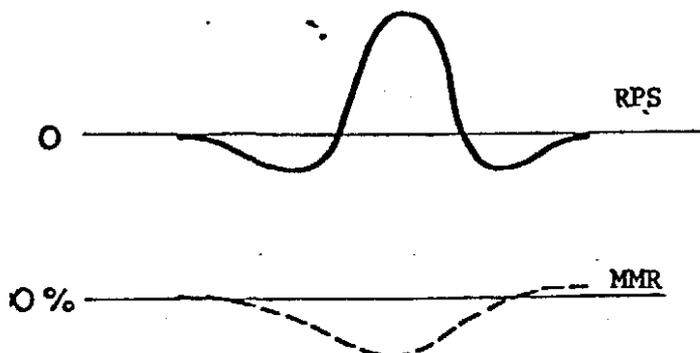


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TYPE A

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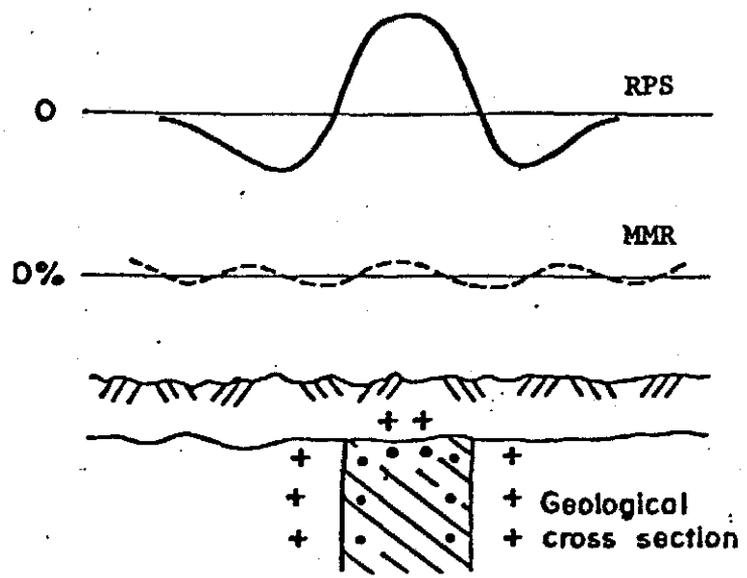


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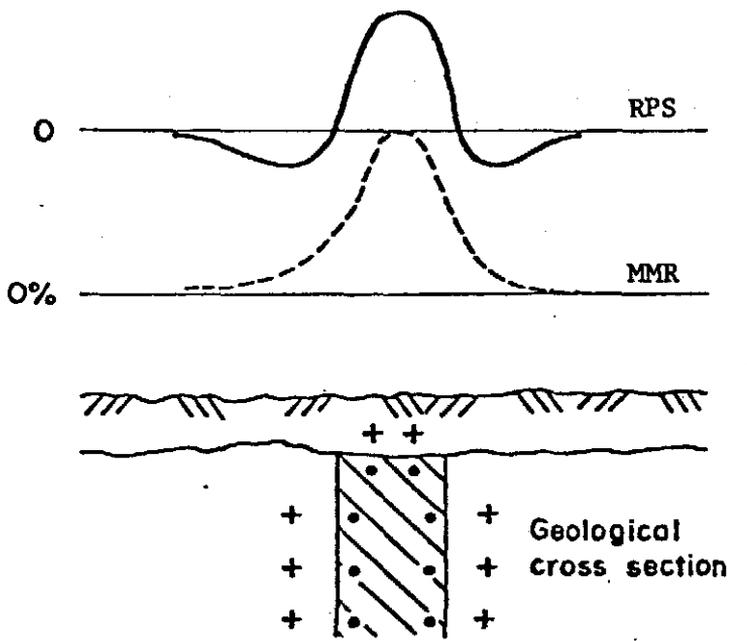
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TYPE C

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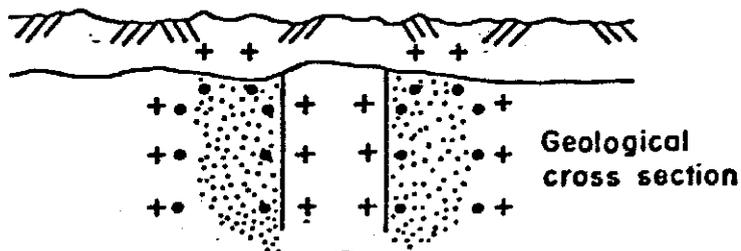
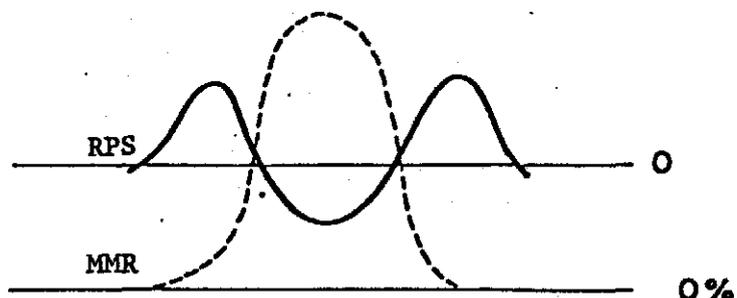
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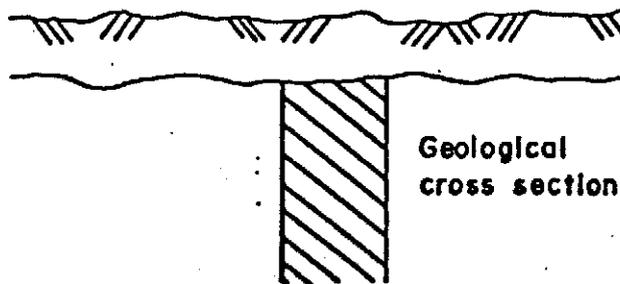
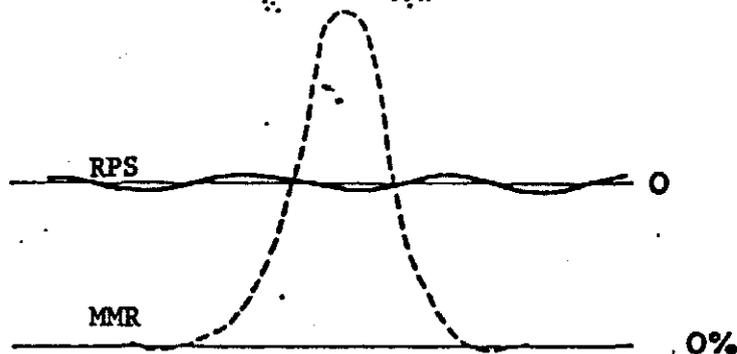
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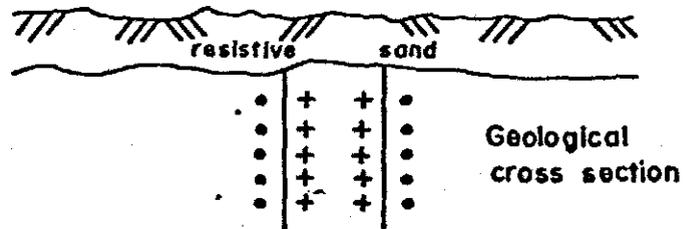
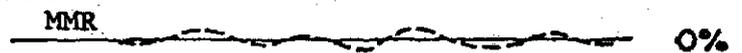
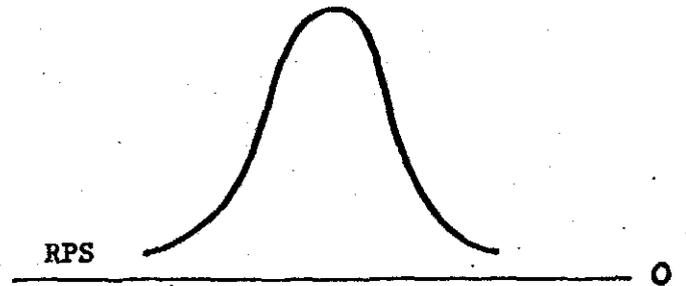
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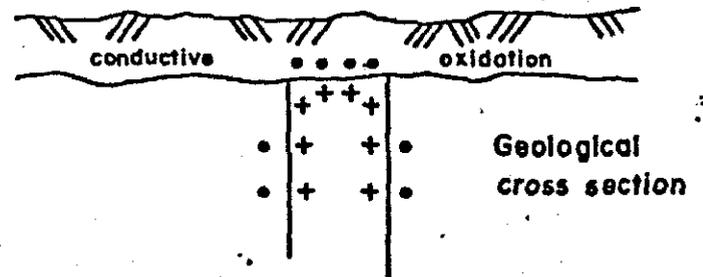
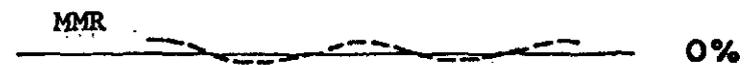
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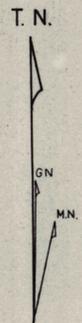
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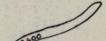
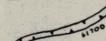
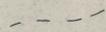
TYPE G

CHARGEABLE SOURCE HOMOGENEOUS
(AS C) UNDER HIGHLY
CONDUCTIVE COVER





MAGNETICS

-  Zone of high magnetic susceptibility with peak values in gammas.
-  Zone of low magnetic susceptibility with minimum values in gammas.
-  Possible magnetic property trend.

RR.M.I.P

-  Chargeable anomaly (> 0.40% R.P.S.)



▲ MT. BISCHOFF

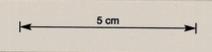
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To Savage River

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PROGRAM MIP? . CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

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128043

1 PLOT SCALE= 2500. HN SCALE 10. PFF & RPS SCALE= 1. HSO & HSP SCALE= 1.

3 ORIGIN CO-ORDS= 500. E -1300. N ARRAY IDENTIFIER= MP01 ANNOTATION SUPPRESSION FLAG= 0

5 SPLINE INTERVAL = 0.

7 PLOT BASE LEVELS FOR PFF, RPS, HSO, HSP ARE 0.00 0.00 0.00 0.00

10 PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

12	HN	=	0
13	MMR	=	1
14	PFF	=	0
15	RPS	=	1
16	HSO	=	1
17	HSP	=	0

20 FOR HN , MMR 100.00 0.00

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARADO

FORM No 11 15

LINE 003 500. F FREQUENCY=3HZ N001

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

STATION	CURRENT	HP	FIELD				OFFSET				HSP/I	STATION		
			PFE	RPS	FFF	RPS	HU	HN	MMR	FFF			RPS	HSQ/I
-2300. N	3.27	0.49	-2.50	3.10	-1.70	2.20	0.16	95.11	-3.91	-1.30	0.90	1.20	-1.98	-2300. N
-2275. N	3.22	0.54	-2.60	3.00	-1.70	2.20	0.17	101.70	0.99	-1.40	0.80	1.17	-2.35	-2275. N
-2250. N	3.22	0.48	-2.40	3.00	-1.20	2.20	0.17	86.84	-11.30	-1.20	0.80	1.04	-1.79	-2250. N
-2225. N	3.22	0.59	-2.40	3.20	-1.70	2.70	0.18	103.04	2.70	-1.20	1.00	1.60	-2.20	-2225. N
-2200. N	3.27	0.59	-2.50	3.10	-1.20	2.20	0.18	99.48	-0.48	-1.30	0.90	1.44	-2.38	-2200. N
-2175. N	3.22	0.61	-2.70	3.00	-1.20	2.70	0.19	99.37	0.65	-1.50	0.80	1.32	-2.84	-2175. N
-2150. N	3.27	0.58	-2.60	3.00	-1.20	2.70	0.20	91.72	-8.66	-1.40	0.80	1.26	-2.52	-2150. N
-2125. N	3.22	0.65	-2.60	2.90	-1.70	2.20	0.20	98.82	-1.21	-1.40	0.70	1.23	-2.83	-2125. N
-2100. N	3.22	0.65	-2.50	3.00	-1.70	2.70	0.21	95.60	-4.65	-1.30	0.80	1.41	-2.62	-2100. N
-2075. N	3.22	0.59	-2.40	3.00	-1.70	2.20	0.22	84.03	-17.41	-1.20	0.80	1.28	-2.20	-2075. N
-2050. N	3.27	0.74	-2.30	2.90	-1.70	2.15	0.22	102.70	2.47	-1.10	0.75	1.50	-2.53	-2050. N
-2025. N	3.27	0.77	-2.40	3.00	-1.70	2.15	0.23	103.79	3.81	-1.20	0.85	1.77	-2.87	-2025. N
-2000. N	3.22	0.75	-2.30	2.90	-1.20	2.15	0.24	97.90	-2.50	-1.10	0.75	1.52	-2.56	-2000. N
-1975. N	3.22	0.78	-2.30	3.00	-1.20	2.15	0.24	99.30	-0.85	-1.10	0.85	1.80	-2.66	-1975. N
-1950. N	3.21	0.82	-2.40	3.00	-1.20	2.15	0.25	102.39	2.98	-1.20	0.85	1.89	-3.07	-1950. N
-1925. N	3.21	0.82	-2.50	3.10	-1.70	2.15	0.25	100.40	0.50	-1.30	0.95	2.12	-3.32	-1925. N
-1900. N	3.21	0.84	-2.60	3.00	-1.20	2.15	0.26	101.16	1.50	-1.40	0.85	1.94	-3.66	-1900. N
-1875. N	3.21	0.85	-2.50	2.80	-1.20	2.15	0.26	101.03	1.35	-1.30	0.65	1.50	-3.44	-1875. N
-1850. N	3.21	0.85	-2.50	2.90	-1.20	2.15	0.26	100.07	0.09	-1.30	0.75	1.73	-3.44	-1850. N
-1825. N	3.21	0.83	-2.60	2.90	-1.20	2.15	0.27	97.15	-3.79	-1.40	0.75	1.69	-3.62	-1825. N
-1800. N	3.21	0.85	-2.50	3.00	-1.20	2.10	0.27	99.30	-0.93	-1.30	0.90	2.08	-3.44	-1800. N
-1775. N	3.21	0.86	-2.60	3.00	-1.15	2.10	0.27	100.66	0.88	-1.45	0.90	2.10	-3.88	-1775. N
-1750. N	3.21	0.85	-2.80	3.10	-1.15	2.10	0.26	100.07	0.09	-1.65	1.00	2.31	-4.37	-1750. N
-1725. N	3.21	0.82	-2.80	3.00	-1.15	2.10	0.26	97.46	-3.32	-1.65	0.90	2.01	-4.21	-1725. N
-1700. N	3.21	0.84	-2.90	3.00	-1.15	2.10	0.26	101.16	1.50	-1.75	0.90	2.06	-4.58	-1700. N
-1675. N	3.21	0.86	-2.90	3.00	-1.15	2.10	0.25	105.29	6.74	-1.75	0.90	2.10	-4.69	-1675. N
-1650. N	3.21	0.84	-3.00	3.20	-1.15	2.10	0.25	104.89	6.09	-1.85	1.10	2.51	-4.84	-1650. N
-1625. N	3.20	0.86	-3.00	3.20	-1.15	2.10	0.24	110.17	12.40	-1.85	1.10	2.58	-4.97	-1625. N
-1600. N	3.20	0.74	-3.40	3.40	-1.15	2.10	0.24	97.70	-3.33	-2.25	1.30	2.62	-5.20	-1600. N
-1575. N	3.20	0.77	-3.90	3.40	-1.15	2.10	0.23	97.10	-3.26	-2.75	1.30	2.55	-6.19	-1575. N
-1550. N	3.20	0.70	-4.30	3.30	-1.15	2.05	0.22	97.28	-3.06	-3.15	1.25	2.39	-6.89	-1550. N
-1525. N	3.20	0.71	-4.40	3.20	-1.15	2.05	0.22	101.75	1.91	-3.25	1.15	2.23	-7.21	-1525. N
-1500. N	3.20	0.65	-4.80	3.30	-1.15	2.05	0.21	96.19	-4.02	-3.65	1.25	2.27	-7.41	-1500. N
-1475. N	3.20	0.65	-4.70	3.20	-1.15	2.05	0.20	99.44	-0.57	-3.55	1.15	2.04	-7.21	-1475. N
-1450. N	3.20	0.75	-4.50	3.10	-1.15	2.05	0.20	118.70	18.46	-3.35	1.05	2.15	-7.85	-1450. N
-1425. N	3.20	0.77	-4.70	3.10	-1.15	2.05	0.19	117.96	17.13	-3.55	1.05	2.06	-7.99	-1425. N
-1400. N	3.20	0.66	-5.20	3.50	-1.15	2.05	0.18	111.98	11.03	-4.05	1.45	2.61	-8.35	-1400. N
-1375. N	3.20	0.00	0.00	0.00	-1.15	2.05	0.18	0.00	88.91	1.15	-2.05	0.00	0.00	-1375. N
-1350. N	3.20	0.00	0.00	0.00	-1.15	2.05	0.17	0.00	-85.83	1.15	-2.05	0.00	0.00	-1350. N
-1325. N	3.20	0.00	0.00	0.00	-1.15	2.05	0.17	0.00	-82.86	1.15	-2.05	0.00	0.00	-1325. N
-1300. N	3.20	0.56	-6.60	4.20	-1.15	2.05	0.16	109.37	7.50	-5.45	2.15	3.28	-9.54	-1300. N

FORM No. 11 15 010345

SOP=-2300.

XINC= 25.00

128046

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-2300.	I	*	0.90	1
2	-2275.	I	*	0.80	2
3	-2250.	I	*	0.80	3
4	-2225.	I	*	1.00	4
5	-2200.	I	*	0.90	5
6	-2175.	I	*	0.80	6
7	-2150.	I	*	0.80	7
8	-2125.	I	*	0.70	8
9	-2100.	I	*	0.80	9
10	-2075.	I	*	0.80	10
11	-2050.	I	*	0.75	11
12	-2025.	I	*	0.85	12
13	-2000.	I	*	0.75	13
14	-1975.	I	*	0.85	14
15	-1950.	I	*	0.85	15
16	-1925.	I	*	0.95	16
17	-1900.	I	*	0.85	17
18	-1875.	I	*	0.65	18
19	-1850.	I	*	0.75	19
20	-1825.	I	*	0.75	20
21	-1800.	I	*	0.90	21
22	-1775.	I	*	0.90	22
23	-1750.	I	*	1.00	23
24	-1725.	I	*	0.90	24
25	-1700.	I	*	0.90	25
26	-1675.	I	*	0.90	26
27	-1650.	I	*	1.10	27
28	-1625.	I	*	1.10	28
29	-1600.	I	*	1.30	29
30	-1575.	I	*	1.30	30
31	-1550.	I	*	1.25	31
32	-1525.	I	*	1.15	32
33	-1500.	I	*	1.25	33
34	-1475.	I	*	1.15	34
35	-1450.	I	*	1.05	35
36	-1425.	I	*	1.05	36
37	-1400.	I	*	1.45	37
38	-1375.	I	*	-2.05	38
39	-1350.	I	*	-2.05	39
40	-1325.	I	*	-2.05	40
41	-1300.	I	*	2.15	41

XBOT=-1300.
YMIN=-2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 500. E RELATIVE PHASE SHIFT RPS

FORM No. 115
01347

42					42
43					43
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60					60

XTOP= -2300.

XINC= 25.00

128049

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

048

1	-2300.	*	I			-9.02	1
2	-2275.		* I			-3.04	2
3	-2250.		*			-0.16	3
4	-2225.		* I			-3.47	4
5	-2200.		I*			1.01	5
6	-2175.		* I			-0.69	6
7	-2150.		* I			-3.90	7
8	-2125.		* I			-3.96	8
9	-2100.		* I			-2.40	9
10	-2075.		* I			-3.87	10
11	-2050.	*	I			-11.47	11
12	-2025.		* I			-5.00	12
13	-2000.		* I			-3.09	13
14	-1975.		* I			-5.72	14
15	-1950.		* I			-3.27	15
16	-1925.		* I			-4.10	16
17	-1900.		* I			-6.34	17
18	-1875.		* I			-5.33	18
19	-1850.		* I			-5.72	19
20	-1825.		* I			-5.96	20
21	-1800.		* I			-4.48	21
22	-1775.		* I			-2.84	22
23	-1750.		* I			-4.16	23
24	-1725.	*	I			-6.89	24
25	-1700.		* I			-3.23	25
26	-1675.		* I			-2.54	26
27	-1650.		*			-0.16	27
28	-1625.		I*			1.12	28
29	-1600.		I*			2.20	29
30	-1575.		I *			4.95	30
31	-1550.	*	I			-96.87	31
32	-1525.	*	I			-95.48	32
33	-1500.	*	I			-94.01	33
34	-1475.		I *			7.53	34
35	-1450.		I *			7.58	35
36	-1425.		I *			2.99	36
37	-1400.		I *			4.69	37
38	-1375.		I *			4.86	38
39	-1350.		I *			6.62	39
40	-1325.		I *			5.27	40
41	-1300.		I *			8.62	41

XBOT= 1300.
YMIN= -96.87

YINC= 1.469
YMAX= 50.00

LINE 800. F MAGNETOMETRIC RESISTIVITY MMR

FORM No 111

42							42
43							43
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59							59
60							60

XTOP= -2300.

XINC= 25.00

128050

049

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	-2300.		I	*		1.00	1
2	-2275.		I	*		1.00	2
3	-2250.		I	*		1.00	3
4	-2225.		I		*	1.20	4
5	-2200.		I		*	1.20	5
6	-2175.		I	*		1.00	6
7	-2150.		I	*		1.00	7
8	-2125.		I	*		1.00	8
9	-2100.		I		*	1.10	9
10	-2075.		I		*	1.15	10
11	-2050.		I	*		0.95	11
12	-2025.		I		*	1.15	12
13	-2000.		I	*		0.95	13
14	-1975.		I	*		0.95	14
15	-1950.		I		*	1.05	15
16	-1925.		I		*	1.15	16
17	-1900.		I		*	1.15	17
18	-1875.		I	*		0.90	18
19	-1850.		I	*		0.90	19
20	-1825.		I		*	1.10	20
21	-1800.		I		*	1.10	21
22	-1775.		I		*	1.10	22
23	-1750.		I	*		1.00	23
24	-1725.		I	*		0.90	24
25	-1700.		I	*		0.80	25
26	-1675.		I	*		0.85	26
27	-1650.		I	*		0.95	27
28	-1625.		I	*		0.95	28
29	-1600.		I		*	1.05	29
30	-1575.		I		*	1.05	30
31	-1550.	*	I			2.15	31
32	-1525.	*	I			-2.15	32
33	-1500.	*	I			-2.15	33
34	-1475.		I	*		1.00	34
35	-1450.		I	*		1.00	35
36	-1425.		I		*	1.60	36
37	-1400.		I		*	1.60	37
38	-1375.		I		*	1.80	38
39	-1350.		I		*	2.00	39
40	-1325.		I		*	2.30	40
41	-1300.		I		*	2.20	41

XBOT= -1300.

YINC= 0.5000E-01

YMIN= -2.500

YMAX= 2.500

LINE 800. F RELATIVE PHASE SHIFT RPS

FORM NO. 11 55 013451

XTOP= -2300.

XINC= 25.00

128051

050

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARA FLO

1	2300.	I	*		1.25	1
2	-2275.	I	*		1.38	2
3	-2250.	I	*		1.46	3
4	-2225.	I	*		1.72	4
5	-2200.	I	*		1.85	5
6	-2175.	I	*		1.54	6
7	-2150.	I	*		1.52	7
8	-2125.	I	*		1.54	8
9	-2100.	I	*		1.76	9
10	-2075.	I	*		1.84	10
11	-2050.	I	*		1.42	11
12	-2025.	I	*		1.87	12
13	-2000.	I	*		1.60	13
14	-1975.	I	*		1.57	14
15	-1950.	I	*		1.80	15
16	-1925.	I	*		1.97	16
17	-1900.	I	*		1.94	17
18	-1875.	I	*		1.54	18
19	-1850.	I	*		1.54	19
20	-1825.	I	*		1.88	20
21	-1800.	I	*		1.91	21
22	-1775.	I	*		1.94	22
23	-1750.	I	*		1.74	23
24	-1725.	I	*		1.52	24
25	-1700.	I	*		1.99	25
26	-1675.	I	*		1.48	26
27	-1650.	I	*		1.68	27
28	-1625.	I	*		1.68	28
29	-1600.	I	*		1.86	29
30	-1575.	I	*		1.89	30
31	-1550.	*			0.00	31
32	-1525.	*			0.00	32
33	-1500.	*			0.00	33
34	-1475.	I	*		1.75	34
35	-1450.	I	*		1.72	35
36	-1425.	I	*	*	2.57	36
37	-1400.	I	*	*	2.57	37
38	-1375.	I	*	*	2.85	38
39	-1350.	I	*	*	3.16	39
40	-1325.	I	*	*	3.51	40
41	-1300.	I	*	*	3.42	41

XBOT= -1300.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINF 800. F SECONDARY FIELD QUADRATURE HSQ/I

FORM No 11 15

43						43
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MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No. 11 013453

---FIELD--- ---OFFSET---

STATION	CURRENT	HP	PFF	RPS	PFF	RPS	HU	HN	MMR	PFF	RPS	HSQ/I	HSP/I	STATION
-2300. N	3.18	0.50	-2.40	3.30	-1.70	2.60	0.16	97.72	-1.83	-1.20	0.70	0.96	-1.89	-2300. N
-2275. N	3.18	0.49	-2.30	3.40	-1.70	2.60	0.16	93.69	-5.19	-1.10	0.80	1.08	-1.69	-2275. N
-2250. N	3.18	0.51	-2.60	3.40	-1.20	2.60	0.17	95.45	-3.82	-1.40	0.80	1.12	-2.25	-2250. N
-2225. N	3.18	0.52	-2.70	3.50	-1.20	2.60	0.17	95.33	-4.01	-1.50	0.90	1.28	-2.45	-2225. N
-2200. N	3.18	0.52	-2.70	3.60	-1.70	2.60	0.18	93.44	-5.74	-1.50	1.00	1.43	-2.45	-2200. N
-2175. N	3.18	0.51	-3.00	3.60	-1.20	2.60	0.18	89.90	-9.01	-1.80	1.00	1.40	-2.89	-2175. N
-2150. N	3.18	0.55	-2.60	3.60	-1.20	2.60	0.18	95.18	-4.38	-1.40	1.00	1.51	-2.42	-2150. N
-2125. N	3.18	0.54	-2.60	3.60	-1.70	2.60	0.18	95.23	-4.42	-1.40	1.00	1.54	-2.47	-2125. N
-2100. N	3.18	0.56	-2.40	3.60	-1.20	2.60	0.19	93.66	-5.96	-1.20	1.00	1.54	-2.11	-2100. N
-2075. N	3.18	0.57	-2.60	3.40	-1.20	2.60	0.19	93.86	-5.86	-1.40	0.80	1.25	-2.51	-2075. N
-2050. N	3.18	0.59	-2.80	3.60	-1.20	2.60	0.19	95.76	-4.11	-1.60	1.00	1.62	-2.97	-2050. N
-2025. N	3.18	0.58	-2.80	3.60	-1.20	2.60	0.20	92.89	-6.98	-1.60	1.00	1.59	-2.92	-2025. N
-2000. N	3.18	0.60	-2.80	3.60	-1.70	2.60	0.20	94.94	-5.02	-1.60	1.00	1.65	-3.02	-2000. N
-1975. N	3.18	0.60	-2.90	3.60	-1.70	2.60	0.20	93.92	-6.11	-1.70	1.00	1.65	-3.21	-1975. N
-1950. N	3.18	0.60	-3.00	3.60	-1.70	2.60	0.20	93.03	-7.06	-1.80	1.00	1.65	-3.40	-1950. N
-1925. N	3.18	0.61	-3.00	3.60	-1.20	2.60	0.20	93.82	-6.32	-1.80	1.00	1.67	-3.45	-1925. N
-1900. N	3.18	0.62	-3.00	3.60	-1.70	2.60	0.21	94.72	-5.43	-1.80	1.00	1.70	-3.51	-1900. N
-1875. N	3.18	0.62	-2.90	3.60	-1.20	2.60	0.21	94.22	-5.98	-1.70	1.00	1.70	-3.31	-1875. N
-1850. N	3.18	0.62	-3.00	3.60	-1.20	2.60	0.21	93.87	-6.37	-1.80	1.00	1.70	-3.51	-1850. N
-1825. N	3.18	0.00	0.00	0.00	-1.20	2.60	0.21	0.00	-104.09	1.20	-2.60	0.00	0.00	-1825. N
-1800. N	3.18	0.00	0.00	0.00	-1.20	2.60	0.21	0.00	-104.17	1.20	-2.60	0.00	0.00	-1800. N
-1775. N	3.17	0.64	-3.20	3.60	-1.70	2.60	0.21	96.98	-3.14	-2.00	1.00	1.76	-4.04	-1775. N
-1750. N	3.17	0.63	-3.20	3.80	-1.20	2.60	0.21	95.68	-4.48	-2.00	1.20	2.08	-3.97	-1750. N
-1725. N	3.17	0.63	-3.90	3.80	-1.70	2.60	0.21	96.05	-4.09	-2.70	1.20	2.08	-5.37	-1725. N
-1700. N	3.17	0.65	-3.60	3.80	-1.20	2.60	0.21	99.67	-0.39	-2.40	1.20	2.15	-4.92	-1700. N
-1675. N	3.17	0.65	-4.00	3.80	-1.20	2.60	0.20	100.29	0.29	-2.80	1.20	2.15	-5.74	-1675. N
-1650. N	3.17	0.64	-4.00	4.00	-1.20	2.60	0.20	99.55	-0.46	-2.80	1.40	2.47	-5.65	-1650. N
-1625. N	3.17	0.64	-4.40	4.00	-1.70	2.60	0.20	100.50	0.50	-3.20	1.40	2.47	-6.46	-1625. N
-1600. N	3.17	0.62	-4.20	3.80	-1.20	2.60	0.20	98.42	-1.57	-3.00	1.20	2.05	-5.87	-1600. N
-1575. N	3.17	0.64	-5.00	4.20	-1.20	2.60	0.20	102.83	2.78	-3.80	1.60	2.82	-7.67	-1575. N
-1550. N	3.17	0.63	-5.00	4.20	-1.70	2.60	0.19	102.58	2.50	-3.80	1.60	2.77	-7.55	-1550. N
-1525. N	3.17	0.63	-5.00	4.20	-1.20	2.60	0.19	104.07	3.89	-3.80	1.60	2.77	-7.55	-1525. N
-1500. N	3.17	0.62	-5.00	4.40	-1.70	2.60	0.19	104.02	3.78	-3.80	1.80	3.07	-7.43	-1500. N
-1475. N	3.17	0.64	-5.50	4.40	-1.70	2.60	0.18	109.17	8.48	-4.30	1.80	3.17	-8.68	-1475. N
-1450. N	3.17	0.62	-6.00	4.40	-1.20	2.60	0.18	107.63	6.93	-4.80	1.80	3.07	-9.39	-1450. N
-1425. N	3.17	0.56	-6.00	4.60	-1.20	2.60	0.18	99.02	-0.87	-4.80	2.00	3.08	-8.48	-1425. N
-1400. N	3.17	0.59	-6.50	4.80	-1.20	2.60	0.18	106.35	5.56	-5.30	2.20	3.57	-9.86	-1400. N
-1375. N	3.17	0.62	-6.50	5.00	-1.70	2.60	0.17	114.02	12.03	-5.30	2.40	4.10	-10.37	-1375. N
-1350. N	3.17	0.56	-7.20	5.00	-1.70	2.60	0.17	105.14	4.32	-6.00	2.40	3.70	-10.60	-1350. N
-1325. N	3.17	0.55	-8.00	5.50	-1.20	2.60	0.16	105.50	4.52	-6.00	2.90	4.39	-11.80	-1325. N
-1300. N	3.17	0.55	-8.50	5.50	-1.20	2.60	0.16	107.84	6.30	-7.30	2.90	4.39	-12.67	-1300. N

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

053

XTOP= -2300.

XINC= 25.00

128054

MOORE PARSONS (WA) LIMITED - FORMALINER PARAFLO

1	-2300.	I	*		0.70
2	-2275.	I	*		0.80
3	-2250.	I	*		0.80
4	-2225.	I	*		0.90
5	-2200.	I	*		1.00
6	-2175.	I	*		1.00
7	-2150.	I	*		1.00
8	-2125.	I	*		1.00
9	-2100.	I	*		1.00
10	-2075.	I	*		0.80
11	-2050.	I	*		1.00
12	-2025.	I	*		1.00
13	-2000.	I	*		1.00
14	-1975.	I	*		1.00
15	-1950.	I	*		1.00
16	-1925.	I	*		1.00
17	-1900.	I	*		1.00
18	-1875.	I	*		1.00
19	-1850.	I	*		1.00
20	-1825. *	I			-2.60
21	-1800. *	I			-2.60
22	-1775.	I	*		1.00
23	-1750.	I		*	1.20
24	-1725.	I		*	1.20
25	-1700.	I		*	1.20
26	-1675.	I		*	1.20
27	-1650.	I		*	1.40
28	-1625.	I		*	1.40
29	-1600.	I		*	1.20
30	-1575.	I		*	1.60
31	-1550.	I		*	1.60
32	-1525.	I		*	1.60
33	-1500.	I		*	1.80
34	-1475.	I		*	1.80
35	-1450.	I		*	1.80
36	-1425.	I		*	2.00
37	-1400.	I		*	2.20
38	-1375.	I		*	2.40
39	-1350.	I		*	2.40
40	-1325.	I		*	2.90
41	-1300.	I		*	2.90

XBOT= 1300.

YINC= 0.5500E-01

YMIN= -2.600

YMAX= 2.900

LINE 1200. E RELATIVE PHASE SHIFT RPS

FORM No. 11-15 0143455

051

XTOP= -2300.

XINC= 25.00

128055

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-2300.	I	*			0.96	1
2	-2275.	I	*			1.08	2
3	-2250.	I	*			1.12	3
4	-2225.	I	*			1.28	4
5	-2200.	I	*			1.43	5
6	-2175.	I	*			1.40	6
7	-2150.	I	*			1.51	7
8	-2125.	I	*			1.54	8
9	-2100.	I	*			1.54	9
10	-2075.	I	*			1.25	10
11	-2050.	I	*			1.62	11
12	-2025.	I	*			1.59	12
13	-2000.	I	*			1.65	13
14	-1975.	I	*			1.65	14
15	-1950.	I	*			1.65	15
16	-1925.	I	*			1.67	16
17	-1900.	I	*			1.70	17
18	-1875.	I	*			1.70	18
19	-1850.	I	*			1.70	19
20	-1825.	*				0.00	20
21	-1800.	*				0.00	21
22	-1775.	I	*			1.76	22
23	-1750.	I	*			2.08	23
24	-1725.	I	*			2.08	24
25	-1700.	I	*			2.15	25
26	-1675.	I	*			2.15	26
27	-1650.	I	*			2.47	27
28	-1625.	I	*			2.47	28
29	-1600.	I	*			2.05	29
30	-1575.	I	*	*		2.82	30
31	-1550.	I	*	*		2.77	31
32	-1525.	I	*	*		2.77	32
33	-1500.	I	*	*		3.07	33
34	-1475.	I	*	*		3.17	34
35	-1450.	I	*	*		3.07	35
36	-1425.	I	*	*		3.08	36
37	-1400.	I	*	*	*	3.57	37
38	-1375.	I	*	*	*	4.10	38
39	-1350.	I	*	*	*	3.70	39
40	-1325.	I	*	*	*	4.39	40
41	-1300.	I	*	*	*	4.39	41

XBOT= 1300.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINF 1200. E SECONDARY FIELD QUADRATURE HSQ/I

FORM No. 11 15

1500. F FRFQUENCY=3HZ N001

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

FORM No. 11-15 0103457

STATION	CURRENT	HP	FIELD		OFFSET		HU	HN	MMR	PFF	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFF	RPS								
-2300. N	3.17	0.49	-3.10	2.60	-1.60	1.80	0.16	96.61	-2.71	-1.50	0.80	1.08	-2.32	-2300. N
-2275. N	3.17	0.52	-2.70	2.70	-1.60	1.80	0.17	98.99	-0.84	-1.10	0.90	1.29	-1.80	-2275. N
-2250. N	3.17	0.52	-2.80	2.80	-1.60	1.80	0.17	95.56	-3.81	-1.20	1.00	1.43	-1.97	-2250. N
-2225. N	3.17	0.57	-3.00	2.60	-1.60	1.80	0.18	101.12	0.99	-1.40	0.80	1.26	-2.52	-2225. N
-2200. N	3.17	0.55	-3.30	2.70	-1.60	1.80	0.18	94.20	-5.35	-1.70	0.90	1.36	-2.95	-2200. N
-2175. N	3.17	0.46	-3.70	3.00	-1.60	1.80	0.19	76.08	-27.82	-2.10	1.20	1.52	-3.05	-2175. N
-2150. N	3.17	0.64	-3.30	2.60	-1.60	1.80	0.20	102.25	2.22	-1.70	0.80	1.41	-3.43	-2150. N
-2125. N	3.17	0.62	-3.20	2.70	-1.60	1.80	0.20	95.75	-4.35	-1.60	0.90	1.54	-3.13	-2125. N
-2100. N	3.17	0.58	-3.20	2.80	-1.60	1.80	0.21	86.65	-14.10	-1.60	1.00	1.60	-2.93	-2100. N
-2075. N	3.17	0.65	-3.00	2.70	-1.60	1.80	0.22	94.04	-6.50	-1.40	0.90	1.61	-2.67	-2075. N
-2050. N	3.17	0.72	-2.90	2.60	-1.60	1.80	0.22	101.01	1.13	-1.30	0.80	1.59	-2.95	-2050. N
-2025. N	3.17	0.00	0.00	0.00	-1.60	1.80	0.23	0.00	-115.76	1.60	-1.80	0.00	0.00	-2025. N
-2000. N	3.17	0.00	0.00	0.00	-1.60	1.80	0.24	0.00	-118.96	1.60	-1.80	0.00	0.00	-2000. N
-1975. N	3.17	0.00	0.00	0.00	-1.60	1.80	0.24	0.00	-121.97	1.60	-1.80	0.00	0.00	-1975. N
-1950. N	3.17	0.65	-4.00	3.10	-1.60	1.80	0.25	82.19	-22.22	-2.40	1.30	2.33	-4.92	-1950. N
-1925. N	3.17	0.82	-3.40	2.60	-1.60	1.80	0.25	101.66	2.12	-1.80	0.80	1.81	-4.66	-1925. N
-1900. N	3.17	0.80	-3.70	2.70	-1.60	1.80	0.26	97.56	-3.16	-2.10	0.90	1.98	-5.30	-1900. N
-1875. N	3.17	0.82	-3.50	2.70	-1.60	1.80	0.26	98.69	-1.71	-1.90	0.90	2.03	-4.91	-1875. N
-1850. N	3.17	0.85	-3.40	2.60	-1.60	1.80	0.26	101.33	1.76	-1.80	0.80	1.87	-4.83	-1850. N
-1825. N	3.17	0.87	-3.40	2.60	-1.60	1.80	0.27	103.12	4.15	-1.80	0.80	1.92	-4.94	-1825. N
-1800. N	3.16	0.83	-3.50	2.70	-1.55	1.75	0.27	98.50	-2.00	-1.95	0.95	2.18	-5.12	-1800. N
-1775. N	3.16	0.85	-3.60	2.70	-1.55	1.75	0.27	101.07	1.42	-2.05	0.95	2.23	-5.51	-1775. N
-1750. N	3.16	0.83	-3.70	2.80	-1.55	1.75	0.26	99.26	-0.98	-2.15	1.05	2.41	-5.65	-1750. N
-1725. N	3.16	0.84	-3.90	2.80	-1.55	1.75	0.26	101.42	1.86	-2.35	1.05	2.44	-6.25	-1725. N
-1700. N	3.16	0.84	-4.20	2.90	-1.55	1.75	0.26	102.76	3.57	-2.65	1.15	2.67	-7.04	-1700. N
-1675. N	3.16	0.85	-4.20	3.00	-1.55	1.75	0.25	105.72	7.27	-2.65	1.25	2.93	-7.13	-1675. N
-1650. N	3.16	0.86	-4.10	3.10	-1.55	1.75	0.25	109.08	11.33	-2.55	1.35	3.21	-6.94	-1650. N
-1625. N	3.16	0.82	-3.90	3.00	-1.55	1.75	0.24	106.37	7.77	-2.35	1.25	2.83	-6.10	-1625. N
-1600. N	3.16	0.79	-4.30	3.00	-1.55	1.75	0.24	105.08	6.04	-2.75	1.25	2.73	-6.87	-1600. N
-1575. N	3.16	0.85	-4.70	3.00	-1.55	1.75	0.23	116.18	18.73	-3.15	1.25	2.93	-8.47	-1575. N
-1550. N	3.16	0.82	-5.10	3.10	-1.55	1.75	0.22	115.40	17.31	-3.55	1.35	3.06	-9.21	-1550. N
-1525. N	3.16	0.77	-5.50	3.20	-1.55	1.75	0.22	111.75	12.81	-3.95	1.45	3.08	-9.62	-1525. N
-1500. N	3.16	0.69	-5.60	3.30	-1.55	1.75	0.21	103.41	3.60	-4.05	1.55	2.95	-8.84	-1500. N
-1475. N	3.16	0.58	-5.70	3.20	-1.55	1.75	0.20	89.85	-10.37	-4.15	1.45	2.32	-7.62	-1475. N
-1450. N	3.16	0.62	-6.10	3.10	-1.55	1.75	0.20	99.37	-0.63	-4.55	1.35	2.31	-8.93	-1450. N
-1425. N	3.16	0.60	-6.30	3.20	-1.55	1.75	0.19	99.54	-0.44	-4.75	1.45	2.40	-9.02	-1425. N
-1400. N	3.16	0.65	-6.90	3.40	-1.55	1.75	0.18	111.67	10.75	-5.35	1.65	2.96	-11.00	-1400. N
-1375. N	3.16	0.63	-7.30	3.60	-1.55	1.75	0.18	112.12	10.77	-5.75	1.85	3.22	-11.46	-1375. N
-1350. N	3.16	0.55	-7.90	3.80	-1.55	1.75	0.17	101.39	1.20	-6.35	2.05	3.11	-11.05	-1350. N
-1325. N	3.16	0.50	-8.20	4.20	-1.55	1.75	0.17	95.48	-3.74	-6.65	2.45	3.38	-10.52	-1325. N
-1300. N	3.16	0.49	-8.40	4.40	-1.55	1.75	0.16	96.91	-2.47	-6.85	2.65	3.59	-10.62	-1300. N

057

XTOP= -2300.

XINC= 25.00

128058

MOORE PARSONS (WA) LIMITED - FORMALINER PARAFLO

1	-2300.		I	*		0.80	1
2	-2275.		I	*		0.90	2
3	-2250.		I	*	*	1.00	3
4	-2225.		I	*		0.80	4
5	-2200.		I	*		0.90	5
6	-2175.		I	*	*	1.20	6
7	-2150.		I	*		0.80	7
8	-2125.		I	*		0.90	8
9	-2100.		I	*	*	1.00	9
10	-2075.		I	*		0.90	10
11	-2050.		I	*		0.80	11
12	-2025.	*	I			-1.80	12
13	-2000.	*	I			-1.80	13
14	-1975.	*	I			-1.80	14
15	-1950.		I	*	*	1.30	15
16	-1925.		I	*		0.80	16
17	-1900.		I	*	*	0.90	17
18	-1875.		I	*	*	0.90	18
19	-1850.		I	*		0.80	19
20	-1825.		I	*	*	0.80	20
21	-1800.		I	*	*	0.95	21
22	-1775.		I	*	*	0.95	22
23	-1750.		I	*	*	1.05	23
24	-1725.		I	*	*	1.05	24
25	-1700.		I	*	*	1.15	25
26	-1675.		I	*	*	1.25	26
27	-1650.		I	*	*	1.35	27
28	-1625.		I	*	*	1.25	28
29	-1600.		I	*	*	1.25	29
30	-1575.		I	*	*	1.25	30
31	-1550.		I	*	*	1.35	31
32	-1525.		I	*	*	1.45	32
33	-1500.		I	*	*	1.55	33
34	-1475.		I	*	*	1.45	34
35	-1450.		I	*	*	1.35	35
36	-1425.		I	*	*	1.45	36
37	-1400.		I	*	*	1.65	37
38	-1375.		I	*	*	1.85	38
39	-1350.		I	*	*	2.05	39
40	-1325.		I	*	*	2.45	40
41	-1300.		I	*	*	2.65	41

XDBT= -1300.
YMIN= -2.500

YINC= 0.5150E-01
YMAX= 2.650

LINE 1500. F RELATIVE PHASE SHIFT RPS

013459

QIM No. 11 15

059

128060

MOORE PARAGON (WA) LIMITED - POKMALINER PARAFLO

FORM No. 11 15

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PROGRAM MIP2. CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

3HZ RRMIP SURVEY MT PEARSE AREA TASMANIA 063R ARRAY NO2

79-1593 Vol 2/2

060

XTOP= -2300.

XINC= 25.00

128061

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

FORM No 11-15

1	-2300.	I	*	2.27	1
2	-2275.	I	*	2.16	2
3	-2250.	I	*	2.19	3
4	-2225.	I	*	2.10	4
5	-2200.	I	*	2.07	5
6	-2175.	I	*	2.24	6
7	-2150.	I	*	2.49	7
8	-2125.	I	*	2.27	8
9	-2100.	I	*	2.57	9
10	-2075.	I	*	2.64	10
11	-2050.	I	*	2.46	11
12	-2025.	I	*	2.50	12
13	-2000.	I	*	2.71	13
14	-1975.	I	*	2.64	14
15	-1950.	I	*	2.57	15
16	-1925.	I	*	2.67	16
17	-1900.	I	*	2.54	17
18	-1875.	I	*	3.07	18
19	-1850.	I	*	2.48	19
20	-1825.	I	*	2.77	20
21	-1800.	I	*	2.74	21
22	-1775.	I	*	3.01	22
23	-1750.	I	*	2.93	23
24	-1725.	I	*	3.04	24
25	-1700.	I	*	2.81	25
26	-1675.	I	*	2.41	26
27	-1650.	I	*	2.43	27
28	-1625.	I	*	3.17	28
29	-1600.	I	*	2.64	29
30	-1575.	I	*	3.17	30
31	-1550.	I	*	2.82	31
32	-1525.	I	*	2.86	32
33	-1500.	I	*	3.39	33
34	-1475.	I	*	3.37	34
35	-1450.	I	*	3.44	35
36	-1425.	I	*	3.48	36
37	-1400.	I	*	3.37	37
38	-1375.	I	*	3.44	38
39	-1350.	I	*	3.12	39
40	-1325.	I	*	3.25	40
41	-1300.	I	*	3.44	41

XBOT= -1300.

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 2800. E SECONDARY FIELD QUADRATURE HSG/I

42					42
43					43
44					44
45					45
46					46
47					47
48					48
49					49
50					50
51					51
52					52
53					53
54					54
55					55
56					56
57					57
58					58
59					59
60					60

XTOP= -2300.

XINC= 25.00

128062

0061

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

1	000.	I	*	1.50	1
2	-2275.	I	*	1.40	2
3	-2250.	I	*	1.40	3
4	-2225.	I	*	1.30	4
5	-2200.	I	*	1.30	5
6	-2175.	I	*	1.50	6
7	-2150.	I	*	1.50	7
8	-2125.	I	*	1.40	8
9	-2100.	I	*	1.50	9
10	-2075.	I	*	1.50	10
11	-2050.	I	*	1.40	11
12	-2025.	I	*	1.40	12
13	-2000.	I	*	1.50	13
14	-1975.	I	*	1.40	14
15	-1950.	I	*	1.40	15
16	-1925.	I	*	1.40	16
17	-1900.	I	*	1.30	17
18	-1875.	I	*	1.70	18
19	-1850.	I	*	1.30	19
20	-1825.	I	*	1.40	20
21	-1800.	I	*	1.40	21
22	-1775.	I	*	1.50	22
23	-1750.	I	*	1.50	23
24	-1725.	I	*	1.50	24
25	-1700.	I	*	1.40	25
26	-1675.	I	*	1.20	26
27	-1650.	I	*	1.20	27
28	-1625.	I	*	1.60	28
29	-1600.	I	*	1.40	29
30	-1575.	I	*	1.80	30
31	-1550.	I	*	1.50	31
32	-1525.	I	*	1.50	32
33	-1500.	I	*	1.90	33
34	-1475.	I	*	2.00	34
35	-1450.	I	*	2.10	35
36	-1425.	I	*	1.90	36
37	-1400.	I	*	2.00	37
38	-1375.	I	*	1.90	38
39	-1350.	I	*	1.70	39
40	-1325.	I	*	1.60	40
41	-1300.	I	*	1.60	41

XBOT= -1300.

YINC= 0.5000E-01

YMIN= -7.500

YMAX= 7.500

LINE 2800. F RELATIVE PHASE SHIFT RPS

FORM No. 1115 0143307

50 51 52 53 54 55 56 57 58 59 60

XTOP= -2300.

XINC= 25.00

128063

062

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-2300.			I	*			5.98	1
2	-2275.			I	*			4.98	2
3	-2250.			I	*			3.93	3
4	-2225.			I	*			4.24	4
5	-2200.			*				0.33	5
6	-2175.	*		I				-7.81	6
7	-2150.			*I				-0.55	7
8	-2125.	*		I				-7.28	8
9	-2100.		*	I				-2.77	9
10	-2075.		*	I				-2.41	10
11	-2050.		*	I				-4.78	11
12	-2025.		*	I				-5.63	12
13	-2000.		*	I				-6.36	13
14	-1975.		*	I				-4.12	14
15	-1950.	*		I				-8.70	15
16	-1925.		*	I				-6.06	16
17	-1900.		*	I				-4.57	17
18	-1875.	*		I				-14.02	18
19	-1850.		*	I				-9.18	19
20	-1825.		*	I				-5.45	20
21	-1800.		*	I				-7.00	21
22	-1775.		*	I				-4.05	22
23	-1750.		*	I				-6.38	23
24	-1725.			*I				-1.42	24
25	-1700.			*I				-1.77	25
26	-1675.			*				-0.45	26
27	-1650.			I	*			2.51	27
28	-1625.			I*				1.48	28
29	-1600.		*	I				-2.16	29
30	-1575.	*		I				-7.03	30
31	-1550.			I	*			2.23	31
32	-1525.			I	*			5.99	32
33	-1500.			I*				1.43	33
34	-1475.		*	I				-1.68	34
35	-1450.		*	I				-1.95	35
36	-1425.			I		*		11.79	36
37	-1400.			I	*			5.93	37
38	-1375.			I		*		15.45	38
39	-1350.			I		*		19.34	39
40	-1325.			I		*		32.99	40
41	-1300.			I		*		42.39	41

XBOT= -1300.

YINC= 1.000

YMIN= -50.00

YMAX= 50.00

LINE 2800. E MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-15

MOORE PARAGON (MA) LIMITED - FORMALINER PARAFLO

FORM No. 11-15 0143305

---FIELD--- ---OFFSET---

STATION	CURRENT	HP	PFF	RPS	PFF	RPS	HU	HN	MMR	PFF	RPS	HSP/I	HSP/I	STATION
-2300. N	3.57	0.62	-5.30	3.60	-2.30	2.10	0.16	107.40	5.98	-3.00	1.50	2.27	-5.21	-2300. N
-2275. N	3.57	0.63	-5.40	3.50	-2.30	2.10	0.17	105.98	4.98	-3.10	1.40	2.16	-5.47	-2275. N
-2250. N	3.57	0.64	-5.30	3.50	-2.30	2.10	0.17	104.59	3.93	-3.00	1.40	2.19	-5.38	-2250. N
-2225. N	3.57	0.66	-5.50	3.40	-2.30	2.10	0.18	104.81	4.24	-3.20	1.30	2.10	-5.92	-2225. N
-2200. N	3.57	0.65	-5.40	3.40	-2.30	2.10	0.18	100.36	0.33	-3.10	1.30	2.07	-5.64	-2200. N
-2175. N	3.57	0.61	-5.50	3.60	-2.30	2.10	0.19	91.62	-7.81	-3.20	1.50	2.24	-5.47	-2175. N
-2150. N	3.57	0.68	-5.30	3.60	-2.30	2.10	0.19	99.42	-0.55	-3.00	1.50	2.49	-5.71	-2150. N
-2125. N	3.57	0.65	-5.50	3.50	-2.30	2.10	0.20	92.59	-7.28	-3.20	1.40	2.22	-5.83	-2125. N
-2100. N	3.57	0.70	-5.40	3.60	-2.30	2.10	0.20	97.25	-2.77	-3.10	1.50	2.57	-6.08	-2100. N
-2075. N	3.57	0.72	-5.40	3.60	-2.30	2.10	0.21	97.66	-2.41	-3.10	1.50	2.64	-6.25	-2075. N
-2050. N	3.57	0.72	-5.50	3.50	-2.30	2.10	0.21	95.48	-4.78	-3.20	1.40	2.46	-6.45	-2050. N
-2025. N	3.57	0.73	-5.40	3.50	-2.30	2.10	0.22	94.78	-5.63	-3.10	1.40	2.50	-6.34	-2025. N
-2000. N	3.57	0.74	-5.50	3.60	-2.30	2.10	0.22	94.22	-6.36	-3.20	1.50	2.71	-6.63	-2000. N
-1975. N	3.57	0.77	-5.60	3.50	-2.30	2.10	0.22	96.32	-4.12	-3.30	1.40	2.64	-7.12	-1975. N
-1950. N	3.57	0.75	-5.60	3.50	-2.25	2.10	0.23	92.35	-8.70	-3.35	1.40	2.57	-7.04	-1950. N
-1925. N	3.57	0.78	-5.70	3.50	-2.25	2.10	0.23	94.75	-6.06	-3.45	1.40	2.67	-7.54	-1925. N
-1900. N	3.57	0.80	-5.80	3.40	-2.25	2.10	0.23	96.08	-4.57	-3.55	1.30	2.54	-7.96	-1900. N
-1875. N	3.57	0.74	-5.80	3.80	-2.25	2.10	0.24	88.08	-14.02	-3.55	1.70	3.07	-7.36	-1875. N
-1850. N	3.57	0.78	-5.70	3.40	-2.25	2.10	0.24	92.25	-9.18	-3.45	1.30	2.48	-7.54	-1850. N
-1825. N	3.57	0.81	-5.50	3.50	-2.25	2.10	0.24	95.42	-5.45	-3.25	1.40	2.77	-7.37	-1825. N
-1800. N	3.57	0.80	-5.80	3.50	-2.25	2.10	0.24	94.12	-7.00	-3.55	1.40	2.74	-7.96	-1800. N
-1775. N	3.57	0.82	-5.90	3.60	-2.25	2.10	0.24	96.60	-4.05	-3.65	1.50	3.01	-8.38	-1775. N
-1750. N	3.57	0.80	-6.30	3.60	-2.25	2.10	0.24	94.61	-6.38	-4.05	1.50	2.93	-9.08	-1750. N
-1725. N	3.57	0.83	-6.20	3.60	-2.25	2.10	0.24	98.80	-1.42	-3.95	1.50	3.04	-9.18	-1725. N
-1700. N	3.57	0.82	-6.20	3.50	-2.25	2.10	0.23	98.48	-1.77	-3.95	1.40	2.81	-9.07	-1700. N
-1675. N	3.57	0.82	-6.40	3.30	-2.25	2.10	0.23	99.61	-0.45	-4.15	1.20	2.41	-9.53	-1675. N
-1650. N	3.57	0.83	-6.40	3.30	-2.25	2.10	0.23	102.20	2.51	-4.15	1.20	2.43	-9.65	-1650. N
-1625. N	3.57	0.81	-6.70	3.70	-2.25	2.10	0.22	101.32	1.48	-4.45	1.60	3.17	-10.10	-1625. N
-1600. N	3.57	0.77	-7.20	3.50	-2.25	2.10	0.22	98.04	-2.16	-4.95	1.40	2.64	-10.68	-1600. N
-1575. N	3.57	0.72	-7.00	3.90	-2.25	2.10	0.22	93.48	-7.03	-4.75	1.80	3.17	-9.58	-1575. N
-1550. N	3.57	0.77	-7.30	3.60	-2.25	2.10	0.21	102.11	2.23	-5.05	1.50	2.82	-10.89	-1550. N
-1525. N	3.57	0.78	-7.40	3.60	-2.25	2.10	0.21	105.80	5.99	-5.15	1.50	2.86	-11.25	-1525. N
-1500. N	3.57	0.73	-7.80	4.00	-2.25	2.10	0.20	101.42	1.43	-5.55	1.90	3.39	-11.35	-1500. N
-1475. N	3.57	0.69	-8.00	4.10	-2.25	2.10	0.20	98.29	-1.68	-5.75	2.00	3.37	-11.11	-1475. N
-1450. N	3.57	0.67	-8.20	4.20	-2.25	2.10	0.19	97.96	-1.95	-5.95	2.10	3.44	-11.17	-1450. N
-1425. N	3.57	0.75	-7.80	4.00	-2.25	2.10	0.19	112.65	11.79	-5.55	1.90	3.48	-11.66	-1425. N
-1400. N	3.57	0.69	-7.70	4.10	-2.25	2.10	0.18	106.53	5.93	-5.45	2.00	3.37	-10.53	-1400. N
-1375. N	3.57	0.74	-7.70	4.00	-2.25	2.10	0.18	117.52	15.45	-5.45	1.90	3.44	-11.30	-1375. N
-1350. N	3.57	0.75	-7.60	3.80	-2.25	2.10	0.17	122.56	19.34	-5.35	1.70	3.12	-11.24	-1350. N
-1325. N	3.57	0.83	-7.40	3.70	-2.25	2.10	0.17	139.63	32.99	-5.15	1.60	3.25	-11.97	-1325. N
-1300. N	3.57	0.88	-7.30	3.70	-2.25	2.10	0.16	152.43	42.39	-5.05	1.60	3.44	-12.45	-1300. N

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

084

XTOP= -2300.

XINC= 25.00

128065

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

1	-2300.	I	*	1.78	1
2	-2275.	I	*	1.62	2
3	-2250.	I	*	1.68	3
4	-2225.	I	*	1.65	4
5	-2200.	I	*	2.19	5
6	-2175.	I	*	2.27	6
7	-2150.	I	*	2.13	7
8	-2125.	I	*	2.31	8
9	-2100.	I	*	2.07	9
10	-2075.	I	*	1.94	10
11	-2050.	I	*	2.16	11
12	-2025.	I	*	2.31	12
13	-2000.	I	*	2.46	13
14	-1975.	I	*	2.64	14
15	-1950.	I	*	2.35	15
16	-1925.	I	*	2.22	16
17	-1900.	I	*	2.58	17
18	-1875.	I	*	2.22	18
19	-1850.	I	*	2.24	19
20	-1825.	I	*	2.62	20
21	-1800.	I	*	2.62	21
22	-1775.	I	*	2.74	22
23	-1750.	I	*	2.86	23
24	-1725.	I	*	2.97	24
25	-1700.	I	*	2.74	25
26	-1675.	I	*	3.16	26
27	-1650.	I	*	2.90	27
28	-1625.	I	*	3.03	28
29	-1600.	I	*	3.34	29
30	-1575.	I	*	3.39	30
31	-1550.	I	*	3.58	31
32	-1525.	I	*	3.67	32
33	-1500.	I	*	3.96	33
34	-1475.	I	*	3.32	34
35	-1450.	I	*	3.23	35
36	-1425.	I	*	3.75	36
37	-1400.	I	*	3.48	37
38	-1375.	I	*	3.83	38
39	-1350.	I	*	4.15	39
40	-1325.	I	*	4.36	40
41	-1300.	I	*	3.96	41

XBOT= -1300.

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 2500. F SECONDARY FIELD QUADRATURE HS0/1

FORM No 11 15

42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

XTOP= -2300.

XINC= 75.00

128066

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

065

1	-2300.	I	*	1.40
2	-2275.	I	*	1.30
3	-2250.	I	*	1.30
4	-2225.	I	*	1.40
5	-2200.	I	*	1.60
6	-2175.	I	*	1.60
7	-2150.	I	*	1.50
8	-2125.	I	*	1.60
9	-2100.	I	*	1.40
10	-2075.	I	*	1.30
11	-2050.	I	*	1.40
12	-2025.	I	*	1.50
13	-2000.	I	*	1.60
14	-1975.	I	*	1.80
15	-1950.	I	*	1.50
16	-1925.	I	*	1.40
17	-1900.	I	*	1.60
18	-1875.	I	*	1.40
19	-1850.	I	*	1.50
20	-1825.	I	*	1.60
21	-1800.	I	*	1.60
22	-1775.	I	*	1.70
23	-1750.	I	*	1.80
24	-1725.	I	*	1.90
25	-1700.	I	*	1.70
26	-1675.	I	*	1.90
27	-1650.	I	*	1.80
28	-1625.	I	*	2.00
29	-1600.	I	*	2.10
30	-1575.	I	*	2.20
31	-1550.	I	*	2.40
32	-1525.	I	*	2.50
33	-1500.	I	*	2.70
34	-1475.	I	*	2.30
35	-1450.	I	*	2.20
36	-1425.	I	*	2.60
37	-1400.	I	*	2.50
38	-1375.	I	*	2.70
39	-1350.	I	*	3.20
40	-1325.	I	*	3.30
41	-1300.	I	*	2.70

XBOT= -1300.

YINC= 0.5800E-01

YMIN= -7.500

YMAX= 3.300

LINE 7500. F RELATIVE PHASE SHIFT RPS

FORM No. 11-15 0143303

XTOP= -2300.

XINC= 25.00

128067

066

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

1	-2300.		*	I		-7.29	1
2	-2275.		*	I		-10.33	2
3	-2250.		*	I		-9.15	3
4	-2225.		*	I		-9.35	4
5	-2200.		*	I		-8.11	5
6	-2175.		*	I		-6.83	6
7	-2150.		*	I		-8.30	7
8	-2125.		*	I		-8.32	8
9	-2100.		*	I		-9.67	9
10	-2075.		*	I		-8.16	10
11	-2050.		*	I		-6.56	11
12	-2025.		*	I		-7.68	12
13	-2000.		*	I		-8.71	13
14	-1975.	*		I		-13.83	14
15	-1950.		*	I		-9.04	15
16	-1925.		*	I		-8.34	16
17	-1900.		*	I		-7.52	17
18	-1875.		*	I		-9.38	18
19	-1850.	*		I		-15.31	19
20	-1825.		*	I		-7.11	20
21	-1800.		*	I		-7.17	21
22	-1775.		*	I		-8.51	22
23	-1750.		*	I		-9.71	23
24	-1725.	*		I		-10.78	24
25	-1700.		*	I		-7.52	25
26	-1675.		*	I	*	-4.14	26
27	-1650.		*	I	*	-6.24	27
28	-1625.	*		I	*	-11.03	28
29	-1600.		*	I	*	-5.90	29
30	-1575.		*	I	*	-7.68	30
31	-1550.		*	I	*	-9.36	31
32	-1525.	*		I	*	-9.56	32
33	-1500.		*	I	*	-8.27	33
34	-1475.		*	I	*	-8.32	34
35	-1450.		*	I	*	-5.50	35
36	-1425.		*	I	*	-5.43	36
37	-1400.		*	I	*	-6.71	37
38	-1375.		*	I	*	-3.74	38
39	-1350.	*		I	*	-9.15	39
40	-1325.		*	I	*	-6.13	40
41	-1300.			I	*	3.91	41

XBOT= -1300.

YINC= 1.000

YMIN= -50.00

YMAX= 50.00

LINE 2500. E MAGNETOMETRIC RESISTIVITY MMR

FORM No 11 13

50 51 52 53 54 55 56 57 58 59 60

LINE# 2500. F FREQUENCY=3HZ N002

087

MOORE PARAGON (WA) LIMITED - FORMALINER P.I. (A) LU

FORM No. 0143301

LINE#	STATION	CURRENT	HF	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RFS	HSP/T	HSP/I	STATION
				PFF	RFS	PFF	RFS								
1	-2300. N	3.57	0.52	-5.60	3.50	-7.30	2.10	0.16	90.90	-7.29	-3.30	1.40	1.78	-4.81	-2300. N
2	-2275. N	3.57	0.51	-5.50	3.40	-7.30	2.10	0.16	87.36	-10.33	-3.20	1.30	1.62	-4.57	-2275. N
3	-2250. N	3.57	0.53	-5.60	3.40	-7.30	2.10	0.17	89.02	-9.15	-3.30	1.30	1.60	-4.90	-2250. N
4	-2225. N	3.57	0.54	-5.70	3.50	-7.30	2.10	0.17	89.00	-9.35	-3.40	1.40	1.85	-5.14	-2225. N
5	-2200. N	3.57	0.56	-5.70	3.70	-7.30	2.10	0.17	90.63	-8.11	-3.40	1.60	2.19	-5.33	-2200. N
6	-2175. N	3.57	0.58	-5.80	3.70	-7.30	2.10	0.18	92.75	-6.83	-3.50	1.60	2.27	-5.69	-2175. N
7	-2150. N	3.57	0.58	-5.80	3.60	-7.30	2.10	0.18	90.73	-8.30	-3.50	1.50	2.13	-5.69	-2150. N
8	-2125. N	3.57	0.59	-5.90	3.70	-7.30	2.10	0.18	90.85	-8.32	-3.60	1.60	2.31	-5.95	-2125. N
9	-2100. N	3.57	0.59	-5.90	3.50	-7.30	2.10	0.18	89.52	-9.67	-3.60	1.40	2.02	-5.95	-2100. N
10	-2075. N	3.57	0.61	-6.00	3.40	-7.30	2.10	0.19	91.28	-8.16	-3.70	1.30	1.94	-6.32	-2075. N
11	-2050. N	3.57	0.63	-5.90	3.50	-7.30	2.10	0.19	93.08	-6.56	-3.60	1.40	2.16	-6.35	-2050. N
12	-2025. N	3.57	0.63	-6.10	3.60	-7.30	2.10	0.19	91.99	-7.68	-3.80	1.50	2.31	-6.71	-2025. N
13	-2000. N	3.57	0.63	-6.00	3.70	-7.30	2.10	0.19	91.02	-8.71	-3.70	1.60	2.46	-6.53	-2000. N
14	-1975. N	3.57	0.60	-5.80	3.90	-7.35	2.10	0.20	85.87	-13.83	-3.45	1.80	2.64	-5.80	-1975. N
15	-1950. N	3.57	0.64	-6.10	3.60	-7.35	2.10	0.20	90.84	-9.04	-3.75	1.50	2.35	-6.72	-1950. N
16	-1925. N	3.57	0.65	-6.30	3.50	-7.35	2.10	0.20	91.61	-8.34	-3.95	1.40	2.22	-7.19	-1925. N
17	-1900. N	3.57	0.66	-6.50	3.70	-7.35	2.10	0.20	92.47	-7.52	-4.15	1.60	2.58	-7.67	-1900. N
18	-1875. N	3.57	0.65	-6.60	3.50	-7.35	2.10	0.20	90.66	-9.38	-4.25	1.40	2.22	-7.74	-1875. N
19	-1850. N	3.57	0.61	-6.40	3.60	-7.35	2.10	0.20	84.80	-15.31	-4.05	1.50	2.24	-6.92	-1850. N
20	-1825. N	3.57	0.67	-6.60	3.70	-7.35	2.10	0.20	92.96	-7.11	-4.25	1.60	2.62	-7.98	-1825. N
21	-1800. N	3.57	0.67	-6.80	3.70	-7.35	2.10	0.20	92.90	-7.17	-4.45	1.60	2.62	-8.35	-1800. N
22	-1775. N	3.57	0.66	-6.70	3.80	-7.35	2.10	0.20	91.57	-8.51	-4.35	1.70	2.74	-8.04	-1775. N
23	-1750. N	3.57	0.65	-6.90	3.90	-7.35	2.10	0.20	90.36	-9.71	-4.55	1.80	2.86	-8.28	-1750. N
24	-1725. N	3.57	0.64	-6.70	4.00	-7.35	2.10	0.20	89.26	-10.78	-4.35	1.90	2.97	-7.80	-1725. N
25	-1700. N	3.57	0.66	-7.00	3.80	-7.35	2.10	0.20	92.47	-7.52	-4.65	1.70	2.74	-8.60	-1700. N
26	-1675. N	3.57	0.68	-7.10	4.00	-7.35	2.10	0.20	95.83	-4.14	-4.75	1.90	3.16	-9.05	-1675. N
27	-1650. N	3.57	0.66	-7.40	3.90	-7.35	2.10	0.20	93.67	-6.24	-5.05	1.80	2.90	-9.34	-1650. N
28	-1625. N	3.57	0.62	-7.60	4.10	-7.35	2.10	0.20	88.73	-11.03	-5.25	2.00	3.03	-9.12	-1625. N
29	-1600. N	3.57	0.65	-7.70	4.20	-7.35	2.10	0.19	93.91	-5.90	-5.35	2.10	3.34	-9.74	-1600. N
30	-1575. N	3.57	0.63	-8.10	4.30	-7.35	2.10	0.19	91.99	-7.68	-5.75	2.20	3.39	-10.15	-1575. N
31	-1550. N	3.57	0.61	-8.40	4.50	-7.35	2.10	0.19	90.12	-9.36	-6.05	2.40	3.58	-10.34	-1550. N
32	-1525. N	3.57	0.60	-8.70	4.60	-7.35	2.10	0.19	89.79	-9.56	-6.35	2.50	3.67	-10.67	-1525. N
33	-1500. N	3.57	0.60	-9.40	4.80	-7.35	2.10	0.18	91.04	-8.27	-7.05	2.70	3.96	-11.85	-1500. N
34	-1475. N	3.57	0.59	-9.00	4.40	-7.35	2.10	0.18	90.85	-8.32	-6.65	2.30	3.32	-10.99	-1475. N
35	-1450. N	3.57	0.60	-8.90	4.30	-7.35	2.10	0.18	93.86	-5.50	-6.55	2.20	3.23	-11.01	-1450. N
36	-1425. N	3.57	0.59	-9.20	4.70	-7.35	2.10	0.18	93.84	-5.43	-6.85	2.60	3.75	-11.32	-1425. N
37	-1400. N	3.57	0.57	-9.80	4.60	-7.35	2.10	0.17	92.25	-6.71	-7.45	2.50	3.48	-11.89	-1400. N
38	-1375. N	3.57	0.58	-10.00	4.80	-7.35	2.10	0.17	95.59	-3.74	-7.65	2.70	3.83	-12.43	-1375. N
39	-1350. N	3.57	0.53	-10.40	5.30	-7.35	2.10	0.17	89.02	-9.15	-8.05	3.20	4.15	-11.95	-1350. N
40	-1325. N	3.57	0.54	-10.60	5.40	-7.35	2.10	0.16	92.50	-6.13	-8.25	3.30	4.36	-12.48	-1325. N
41	-1300. N	3.57	0.60	-9.80	4.80	-7.35	2.10	0.16	104.88	3.91	-7.45	2.70	3.96	-12.52	-1300. N

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

XTOP= -2300.

XINC= 25.00

068

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-2300.	I	*	2.37	1
2	-2275.	I	*	2.41	2
3	-2250.	I	*	2.46	3
4	-2225.	I	*	2.46	4
5	-2200.	I	*	2.64	5
6	-2175.	I	*	1.99	6
7	-2150.	I	*	2.74	7
8	-2125.	I	*	2.78	8
9	-2100.	I	*	2.54	9
10	-2075.	I	*	2.67	10
11	-2050.	I	*	2.66	11
12	-2025.	I	*	3.07	12
13	-2000.	I	*	2.86	13
14	-1975.	I	*	3.13	14
15	-1950.	I	*	2.41	15
16	-1925.	I	*	2.41	16
17	-1900.	I	*	3.23	17
18	-1875.	I	*	3.27	18
19	-1850.	I	*	2.78	19
20	-1825.	I	*	2.82	20
21	-1800.	I	*	2.86	21
22	-1775.	I	*	2.87	22
23	-1750.	I	*	2.91	23
24	-1725.	I	*	3.42	24
25	-1700.	I	*	3.47	25
26	-1675.	I	*	3.42	26
27	-1650.	I	*	3.42	27
28	-1625.	I	*	3.28	28
29	-1600.	I	*	3.37	29
30	-1575.	I	*	3.42	30
31	-1550.	I	*	4.21	31
32	-1525.	I	*	4.08	32
33	-1500.	I	*	4.02	33
34	-1475.	I	*	4.08	34
35	-1450.	I	*	4.05	35
36	-1425.	I	*	3.99	36
37	-1400.	I	*	3.99	37
38	-1375.	I	*	3.93	38
39	-1350.	I	*	4.55	39
40	-1325.	I	*	4.47	40
41	-1300.	I	*	4.47	41

XBOT= -1300.

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 2200. E SECONDARY FIELD QUADRATURE HSG/I

FORM No 11 13

FORM No 11 13

069

XTOP= -2300.

XINC= 25.00

MOORE PARSON (WA) LIMITED - FORMA VER PARAFLO

1	-2300.	I	*	1.90	1
2	-2275.	I	*	1.90	2
3	-2250.	I	*	1.90	3
4	-2225.	I	*	1.90	4
5	-2200.	I	*	1.93	5
6	-2175.	I	*	1.43	6
7	-2150.	I	*	1.93	7
8	-2125.	I	*	1.93	8
9	-2100.	I	*	1.73	9
10	-2075.	I	*	1.73	10
11	-2050.	I	*	1.73	11
12	-2025.	I	*	1.93	12
13	-2000.	I	*	1.77	13
14	-1975.	I	*	1.97	14
15	-1950.	I	*	1.47	15
16	-1925.	I	*	1.47	16
17	-1900.	I	*	1.97	17
18	-1875.	I	*	1.97	18
19	-1850.	I	*	1.67	19
20	-1825.	I	*	1.67	20
21	-1800.	I	*	1.67	21
22	-1775.	I	*	1.70	22
23	-1750.	I	*	1.70	23
24	-1725.	I	*	2.00	24
25	-1700.	I	*	2.00	25
26	-1675.	I	*	2.00	26
27	-1650.	I	*	2.00	27
28	-1625.	I	*	2.00	28
29	-1600.	I	*	2.03	29
30	-1575.	I	*	2.03	30
31	-1550.	I	*	2.53	31
32	-1525.	I	*	2.53	32
33	-1500.	I	*	2.53	33
34	-1475.	I	*	2.53	34
35	-1450.	I	*	2.55	35
36	-1425.	I	*	2.55	36
37	-1400.	I	*	2.55	37
38	-1375.	I	*	2.55	38
39	-1350.	I	*	3.05	39
40	-1325.	I	*	3.05	40
41	-1300.	I	*	3.05	41

XBOT= -1300.

YINC= 0.5550E-01

YMIN= -2.500

YMAX= 3.050

LINE 2200.F RELATIVE PHASE SHIFT RPS

FORM No. 11.15 013309

42					42
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59					59
60					60

XTOP= -2300.

XINC= 25.00

128071

070

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-2300.	*	I	-9.02	1
2	-2275.	*	I	-9.40	2
3	-2250.	*	I	-9.78	3
4	-2225.	*	I	-11.54	4
5	-2200.	*	I	-9.07	5
6	-2175.	*	I	-9.37	6
7	-2150.	*	I	-9.63	7
8	-2125.	*	I	-9.83	8
9	-2100.	*	I	-9.98	9
10	-2075.	*	I	-8.65	10
11	-2050.	*	I	-8.64	11
12	-2025.	*	I	-7.13	12
13	-2000.	*	I	-6.93	13
14	-1975.	*	I	-9.41	14
15	-1950.	*	I	-7.57	15
16	-1925.	*	I	-8.39	16
17	-1900.	*	I	-9.08	17
18	-1875.	*	I	-8.22	18
19	-1850.	*	I	-8.61	19
20	-1825.	*	I	-7.45	20
21	-1800.	*	I	-6.13	21
22	-1775.	*	I	-7.45	22
23	-1750.	*	I	-5.81	23
24	-1725.	*	I	-5.42	24
25	-1700.	*	I	-3.48	25
26	-1675.	*	I	-4.19	26
27	-1650.	*	I	-3.36	27
28	-1625.	*	I	-6.61	28
29	-1600.	*	I	-4.13	29
30	-1575.	*	I	-1.53	30
31	-1550.	*	I	-1.63	31
32	-1525.	*	I	-3.05	32
33	-1500.	*	I	-2.97	33
34	-1475.	*	*	-0.03	34
35	-1450.	*	*	0.18	35
36	-1425.	*	*	0.44	36
37	-1400.		I *	2.14	37
38	-1375.		I *	2.47	38
39	-1350.		I *	1.43	39
40	-1325.		I *	1.80	40
41	-1300.		I *	3.59	41

XBOT= -1300.

YINC= 1.000

YMIN= -50.00

YMAX= 50.00

LINE 2700. F MAGNETOMETRIC RESISTIVITY MMR

FORM No 11 19

42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

XTOP= -2175.

XINC= 25.00

128073

072

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM No 11-13

1	-2175.	I	*	2.31	1
2	-2150.	I	*	2.55	2
3	-2125.	I	*	2.64	3
4	-2100.	I	*	2.88	4
5	-2075.	I	*	2.55	5
6	-2050.	I	*	2.97	6
7	-2025.	I	*	2.68	7
8	-2000.	I	*	2.40	8
9	-1975.	I	*	2.91	9
10	-1950.	I	*	2.62	10
11	-1925.	I	*	2.82	11
12	-1900.	I	*	2.82	12
13	-1875.	I	*	2.97	13
14	-1850.	I	*	2.97	14
15	-1825.	I	*	3.03	15
16	-1800.	I	*	3.40	16
17	-1775.	I	*	3.40	17
18	-1750.	I	*	3.61	18
19	-1725.	I	*	3.58	19
20	-1700.	I	*	3.36	20
21	-1675.	I	*	3.63	21
22	-1650.	I	*	3.42	22
23	-1625.	I	*	3.22	23
24	-1600.	I	*	3.70	24
25	-1575.	I	*	3.70	25
26	-1550.	I	*	3.72	26
27	-1525.	I	*	4.01	27
28	-1500.	I	*	3.63	28
29	-1475.	I	*	3.77	29
30	-1450.	I	*	3.82	30
31	-1425.	I	*	3.53	31
32	-1400.	I	*	4.23	32
33	-1375.	I	*	4.57	33
34	-1350.	I	*	4.35	34

XBOT= -1350.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 1800. F SECONDARY FIELD QUADRATURE HSQ/I

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60					60

XINC= 25.00

XTOP= -2175.

1	-2175.	I		*	1.70
2	-2150.	I		*	1.70
3	-2125.	I		*	1.70
4	-2100.	I		*	1.70
5	-2075.	I		*	1.50
6	-2050.	I		*	1.55
7	-2025.	I	*	*	1.35
8	-2000.	I	*	*	1.15
9	-1975.	I	*	*	1.35
10	-1950.	I	*	*	1.15
11	-1925.	I	*	*	1.20
12	-1900.	I	*	*	1.20
13	-1875.	I	*	*	1.20
14	-1850.	I	*	*	1.20
15	-1825.	I	*	*	1.20
16	-1800.	I	*	*	1.35
17	-1775.	I	*	*	1.35
18	-1750.	I	*	*	1.45
19	-1725.	I	*	*	1.45
20	-1700.	I	*	*	1.35
21	-1675.	I	*	*	1.50
22	-1650.	I	*	*	1.40
23	-1625.	I	*	*	1.40
24	-1600.	I	*	*	1.70
25	-1575.	I	*	*	1.70
26	-1550.	I	*	*	1.75
27	-1525.	I	*	*	1.95
28	-1500.	I	*	*	1.95
29	-1475.	I	*	*	1.95
30	-1450.	I	*	*	1.95
31	-1425.	I	*	*	2.00
32	-1400.	I	*	*	2.50
33	-1375.	I	*	*	3.00
34	-1350.	I	*	*	3.00

XBOT= -1350.
YMIN= -2.500

YINC= 0.5500E-01
YMAX= 3.000

LINE 1800. F RELATIVE PHASE SHIFT RPS

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM NO. 0143385

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

LINE	STATION	CURRENT	HP	---FIELD I---		---OFFSET---		HU	HN	MMR	PFF	RPS	HSQ/I	HSP/I	STATION
				PFF	RPS	PFF	RPS								
1															
2															
3															
4	-2175. N	3.60	0.56	-4.40	5.00	-1.35	3.30	0.19	80.89	-18.37	-3.05	1.70	2.31	-4.74	-2175. N
5	-2150. N	3.60	0.62	-4.40	5.00	-1.35	3.30	0.20	85.58	-14.51	-3.05	1.70	2.55	-5.25	-2150. N
6	-2125. N	3.60	0.64	-4.40	5.00	-1.35	3.30	0.21	84.41	-16.42	-3.05	1.70	2.64	-5.42	-2125. N
7	-2100. N	3.60	0.70	-4.40	5.00	-1.35	3.30	0.22	88.23	-12.97	-3.05	1.70	2.88	-5.93	-2100. N
8	-2075. N	3.60	0.70	-4.30	4.80	-1.35	3.30	0.23	84.37	-18.01	-2.95	1.50	2.55	-5.74	-2075. N
9	-2050. N	3.60	0.79	-4.00	4.80	-1.35	3.25	0.24	91.14	-10.67	-2.65	1.55	2.97	-5.82	-2050. N
10	-2025. N	3.60	0.82	-4.00	4.60	-1.35	3.25	0.25	90.68	-11.71	-2.65	1.35	2.68	-6.04	-2025. N
11	-2000. N	3.60	0.86	-3.80	4.40	-1.35	3.25	0.26	91.34	-11.32	-2.45	1.15	2.40	-5.85	-2000. N
12	-1975. N	3.60	0.89	-3.60	4.60	-1.35	3.25	0.27	91.03	-12.19	-2.75	1.35	2.91	-5.56	-1975. N
13	-1950. N	3.60	0.94	-3.60	4.40	-1.35	3.25	0.28	92.88	-10.01	-2.25	1.15	2.67	-5.87	-1950. N
14	-1925. N	3.60	0.97	-3.60	4.40	-1.35	3.20	0.29	92.95	-10.22	-2.25	1.20	2.82	-6.06	-1925. N
15	-1900. N	3.60	0.97	-3.60	4.40	-1.35	3.20	0.30	90.55	-14.05	-2.25	1.20	2.82	-6.06	-1900. N
16	-1875. N	3.60	1.07	-3.60	4.40	-1.35	3.20	0.30	93.24	-10.27	-2.25	1.20	2.97	-6.37	-1875. N
17	-1850. N	3.60	1.07	-3.60	4.40	-1.35	3.20	0.31	91.81	-12.63	-2.25	1.20	2.97	-6.37	-1850. N
18	-1825. N	3.60	1.04	-3.60	4.40	-1.35	3.20	0.31	92.74	-11.31	-2.25	1.20	3.03	-6.50	-1825. N
19	-1800. N	3.60	1.04	-3.80	4.50	-1.35	3.15	0.31	92.44	-11.81	-2.45	1.35	3.40	-7.08	-1800. N
20	-1775. N	3.60	1.04	-3.80	4.50	-1.35	3.15	0.31	92.74	-11.31	-2.45	1.35	3.40	-7.08	-1775. N
21	-1750. N	3.61	1.03	-4.00	4.60	-1.40	3.15	0.31	92.46	-11.64	-2.60	1.45	3.61	-7.42	-1750. N
22	-1725. N	3.61	1.02	-4.00	4.60	-1.40	3.15	0.30	92.98	-10.66	-2.60	1.45	3.58	-7.35	-1725. N
23	-1700. N	3.61	1.03	-4.20	4.50	-1.40	3.15	0.30	95.89	-6.12	-2.80	1.35	3.36	-7.99	-1700. N
24	-1675. N	3.61	1.00	-4.20	4.60	-1.40	3.10	0.29	95.56	-6.44	-2.80	1.50	3.63	-7.76	-1675. N
25	-1650. N	3.61	1.01	-4.40	4.50	-1.40	3.10	0.28	99.52	-0.68	-3.00	1.40	3.42	-8.39	-1650. N
26	-1625. N	3.61	0.95	-4.40	4.50	-1.40	3.10	0.27	96.89	-4.72	-3.00	1.40	3.77	-7.89	-1625. N
27	-1600. N	3.61	0.90	-4.60	4.80	-1.40	3.10	0.26	95.32	-6.12	-3.20	1.70	3.70	-7.98	-1600. N
28	-1575. N	3.61	0.90	-4.80	4.80	-1.40	3.10	0.25	99.25	-0.95	-3.40	1.70	3.70	-8.48	-1575. N
29	-1550. N	3.61	0.88	-5.00	4.80	-1.40	3.05	0.24	101.24	1.49	-3.60	1.75	3.72	-8.78	-1550. N
30	-1525. N	3.61	0.85	-5.50	5.00	-1.40	3.05	0.23	102.16	2.49	-4.10	1.95	4.01	-9.65	-1525. N
31	-1500. N	3.61	0.77	-5.50	5.00	-1.40	3.05	0.27	96.79	-3.54	-4.10	1.95	3.63	-8.75	-1500. N
32	-1475. N	3.61	0.80	-5.50	5.00	-1.40	3.05	0.21	105.22	5.50	-4.10	1.95	3.77	-9.09	-1475. N
33	-1450. N	3.61	0.81	-6.00	5.00	-1.40	3.05	0.20	111.50	11.57	-4.60	1.95	3.82	-10.32	-1450. N
34	-1425. N	3.61	0.73	-6.50	5.00	-1.40	3.00	0.19	105.16	4.96	-5.10	2.00	3.53	-10.31	-1425. N
35	-1400. N	3.61	0.70	-7.00	5.50	-1.40	3.00	0.18	105.48	5.04	-5.60	2.50	4.23	-10.86	-1400. N
36	-1375. N	3.61	0.63	-7.50	6.00	-1.40	3.00	0.18	99.26	-0.65	-6.10	3.00	4.57	-10.65	-1375. N
37	-1350. N	3.61	0.60	-8.50	6.00	-1.40	3.00	0.17	98.78	-1.03	-7.10	3.00	4.35	-11.80	-1350. N
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076

128077

UNITS FLAG= 0 CURRENT ELECTRODE CO-ORDS= 1400. E -1800. N 3400. E -1800. N

1 PLOT SCALE= 2500. HN SCALE 10. PFE & RPS SCALE= 1. HSG & HSP SCALE= 1.

3 ORIGIN CO-ORDS= 1800. E -1300. N ARRAY IDENTIFIER= MP02 ANNOTATION SUPPRESSION FLAG= 0

5 SPLINE INTERVAL= 0.

8 PLOT BASE LEVELS FOR PFE, RPS, HSG, HSP ARE 0.00 0.00 0.00 0.00

11 PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

12	HN	=	0
13	MMR	=	1
14	PFE	=	0
15	RPS	=	1
16	HSG	=	1
17	HSP	=	0

20 FOR HN , MMR 100.00 0.00

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No 11 15

077

INTERP TAPE FLAG= 0 GRIDDATA TAPE FLAG= 0

128078

1 LINE POSITIONING MULTIPLYING FACTOR= 1.0

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM No. 11-15
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078

128079

MOORE PARSON (WA) LIMITED FORMALINER PARAFLO

PROGRAM NIP2... CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

3HZ RRMJP SURVEY MT PEARSE AREA TAS 070R ARRAY N001

79-1393 Vol 2

0103279

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INTERP TAPE FLAG= 0 GRIDDATA TAPE FLAG= 0

128080

629
LINE POSITIONING MULTIPLYING FACTOR= 1.0

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM No. 11-13

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UNITS FLAG= 0 CURRENT ELECTRODE CO-ORDS= 1800. E -1400. N 3800. E -1400. N

128081

PLOT SCALE= 2500. HN SCALE 10. PFF & RPS SCALE= 1. HSG & HSP SCALE= 1.

ORIGIN CO-ORDS= 2100. E -1900. N ARRAY IDENTIFIER= MPO1 ANNOTATION SUPPRESSION FLAG= 0

SPLINE INTERVAL = 0.

PLOT BASE LEVELS FOR PFF, RPS, HSG, HSP ARE 0.00 0.00 0.00 0.00

PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

HN	=	0
MMR	=	1
PFF	=	1
RPS	=	1
HSG	=	1
HSP	=	0

FOR HN , MMR 100.00 0.00

FORMALINER PARAFLO

MOOI

0103201

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60

LINE#	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RPS	RSQ/I	HSP/I	STATION
				PFF	RPS	PFF	RPS								
1															
2															
3	-1800. N	3.50	0.58	-7.50	4.80	-7.00	2.00	0.18	90.15	-9.05	-5.50	2.80	4.05	-9.11	-1800. N
4	-1775. N	3.50	0.54	-8.00	4.80	-7.00	2.00	0.19	80.23	-19.01	-6.00	2.80	3.77	-9.26	-1775. N
5	-1750. N	3.50	0.62	-6.70	4.40	-2.00	2.00	0.20	88.03	-12.05	-4.70	2.40	3.71	-8.33	-1750. N
6	-1725. N	3.50	0.64	-6.60	4.40	-2.00	2.00	0.21	86.82	-13.88	-4.60	2.40	3.83	-8.41	-1725. N
7	-1700. N	3.50	0.69	-6.30	4.10	-2.00	2.00	0.22	89.46	-11.62	-4.30	2.10	3.61	-8.48	-1700. N
8	-1675. N	3.50	0.63	-6.20	4.20	-2.00	2.00	0.23	78.10	-25.23	-4.20	2.20	3.46	-7.56	-1675. N
9	-1650. N	3.50	0.71	-6.20	4.00	-2.00	2.00	0.24	84.25	-18.96	-4.20	2.00	3.54	-8.52	-1650. N
10	-1625. N	3.50	0.80	-5.70	3.60	-2.00	2.00	0.25	90.99	-11.31	-3.70	1.60	3.19	-8.46	-1625. N
11	-1600. N	3.50	0.82	-5.50	3.70	-2.00	2.00	0.26	89.58	-13.63	-3.50	1.70	3.48	-8.20	-1600. N
12	-1575. N	3.50	0.85	-5.40	3.60	-2.00	2.00	0.27	89.42	-14.37	-3.40	1.60	3.39	-8.26	-1575. N
13	-1550. N	3.50	0.87	-5.40	3.40	-2.00	2.00	0.28	88.42	-16.28	-3.40	1.40	3.04	-8.45	-1550. N
14	-1525. N	3.50	0.89	-5.20	3.50	-2.00	2.00	0.29	87.72	-17.80	-3.20	1.50	3.33	-8.14	-1525. N
15	-1500. N	3.50	0.91	-4.80	3.40	-2.00	2.00	0.30	87.38	-18.78	-2.80	1.40	3.18	-7.28	-1500. N
16	-1475. N	3.50	0.91	-4.50	3.40	-2.00	2.00	0.30	85.56	-21.94	-2.50	1.40	3.18	-6.50	-1475. N
17	-1450. N	3.50	0.92	-4.40	3.30	-2.00	2.00	0.31	85.18	-22.87	-2.40	1.30	2.98	-6.31	-1450. N
18	-1425. N	3.50	0.95	-4.40	3.40	-2.00	2.00	0.31	87.13	-20.04	-2.40	1.40	3.32	-6.51	-1425. N
19	-1400. N	3.50	0.94	-4.40	3.30	-1.95	2.00	0.31	85.94	-21.96	-2.45	1.30	3.05	-6.58	-1400. N
20	-1375. N	3.50	0.95	-4.40	3.40	-1.95	2.00	0.31	87.13	-20.04	-2.45	1.40	3.32	-6.65	-1375. N
21	-1350. N	3.50	0.92	-4.30	3.30	-1.95	2.00	0.31	85.18	-22.87	-2.35	1.30	2.98	-6.18	-1350. N
22	-1325. N	3.50	0.90	-4.20	3.30	-1.95	2.00	0.30	84.62	-23.36	-2.25	1.30	2.92	-5.79	-1325. N
23	-1300. N	3.50	0.90	-4.30	3.20	-1.95	2.00	0.30	86.42	-20.20	-2.35	1.20	2.69	-6.04	-1300. N
24	-1275. N	3.50	0.87	-4.40	3.30	-1.95	2.00	0.29	85.75	-20.65	-2.45	1.30	2.82	-6.09	-1275. N
25	-1250. N	3.50	0.84	-4.40	3.30	-1.95	2.00	0.28	85.37	-20.57	-2.45	1.30	2.72	-5.88	-1250. N
26	-1225. N	3.50	0.80	-4.50	3.40	-1.95	2.00	0.27	84.16	-21.51	-2.55	1.40	2.79	-5.83	-1225. N
27	-1200. N	3.50	0.76	-4.60	3.50	-1.95	2.00	0.26	83.03	-22.20	-2.65	1.50	2.84	-5.75	-1200. N
28	-1175. N	3.50	0.78	-4.40	3.60	-1.95	2.00	0.25	88.72	-14.17	-2.45	1.60	3.11	-5.46	-1175. N
29	-1150. N	3.50	0.72	-4.40	3.60	-1.95	2.00	0.24	85.43	-17.54	-2.45	1.60	2.87	-5.04	-1150. N
30	-1125. N	3.50	0.71	-4.30	3.60	-1.95	2.00	0.23	88.02	-13.81	-2.35	1.60	2.83	-4.77	-1125. N
31	-1100. N	3.50	0.67	-4.40	3.60	-1.95	2.00	0.22	86.86	-14.47	-2.45	1.60	2.67	-4.69	-1100. N
32	-1075. N	3.50	0.63	-5.50	4.00	-1.95	2.00	0.21	85.47	-15.31	-3.55	2.00	3.14	-6.39	-1075. N
33	-1050. N	3.50	0.60	-5.20	4.00	-1.95	2.00	0.20	85.19	-14.91	-3.25	2.00	2.99	-5.57	-1050. N
34	-1025. N	3.50	0.59	-4.80	4.00	-1.95	2.00	0.19	87.66	-11.87	-2.85	2.00	2.94	-4.80	-1025. N
35	-1000. N	3.50	0.61	-4.40	4.00	-1.95	2.00	0.18	94.81	-4.77	-2.45	2.00	3.04	-4.27	-1000. N
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MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No 11.1

XTOP= -1800.

XINC= 75.00

128083

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO.

1	-1800.			*	I	-9.05	1
2	-1775.	*			I	-19.01	2
3	-1750.		*		I	-12.05	3
4	-1725.		*		I	-13.88	4
5	-1700.		*		I	-11.62	5
6	-1675.	*			I	-25.23	6
7	-1650.		*		I	-18.96	7
8	-1625.		*		I	-11.31	8
9	-1600.		*		I	-13.63	9
10	-1575.		*		I	-14.37	10
11	-1550.		*		I	-16.28	11
12	-1525.		*		I	-17.80	12
13	-1500.		*		I	-18.78	13
14	-1475.	*			I	-21.94	14
15	-1450.	*			I	-22.87	15
16	-1425.	*	*		I	-20.04	16
17	-1400.	*			I	-21.96	17
18	-1375.	*	*		I	-20.04	18
19	-1350.	*			I	-22.87	19
20	-1325.	*			I	-23.36	20
21	-1300.	*	*		I	-20.20	21
22	-1275.	*			I	-20.65	22
23	-1250.	*	*		I	-20.57	23
24	-1225.	*			I	-21.51	24
25	-1200.	*			I	-22.20	25
26	-1175.		*	*	I	-14.17	26
27	-1150.		*		I	-17.54	27
28	-1125.		*	*	I	-13.81	28
29	-1100.		*	*	I	-14.47	29
30	-1075.		*	*	I	-15.31	30
31	-1050.		*	*	I	-14.91	31
32	-1025.		*	*	I	-11.87	32
33	-1000.		*	*	I	-4.77	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2200. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-15
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XTOP= -1800.

XINC= 25.00

128084

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	-1800.	*			I	-5.50	1
2	-1775.	*			I	-6.00	2
3	-1750.		*		I	-4.70	3
4	-1725.		*		I	-4.60	4
5	-1700.			*	I	-4.30	5
6	-1675.			*	I	-4.20	6
7	-1650.			*	I	-4.20	7
8	-1625.			*	I	-3.70	8
9	-1600.			*	I	-3.50	9
10	-1575.			*	I	-3.40	10
11	-1550.			*	I	-3.40	11
12	-1525.			*	I	-3.20	12
13	-1500.			*	I	-2.80	13
14	-1475.			*	I	-2.50	14
15	-1450.			*	I	-2.40	15
16	-1425.			*	I	-2.40	16
17	-1400.			*	I	-2.45	17
18	-1375.			*	I	-2.45	18
19	-1350.			*	I	-2.35	19
20	-1325.			*	I	-2.25	20
21	-1300.			*	I	-2.35	21
22	-1275.			*	I	-2.45	22
23	-1250.			*	I	-2.45	23
24	-1225.			*	I	-2.55	24
25	-1200.			*	I	-2.65	25
26	-1175.			*	I	-2.45	26
27	-1150.			*	I	-2.45	27
28	-1125.			*	I	-2.35	28
29	-1100.			*	I	-2.45	29
30	-1075.		*		I	-3.55	30
31	-1050.		*		I	-3.25	31
32	-1025.		*		I	-2.85	32
33	-1000.		*		I	-2.45	33

XBOT= -1000.
YMIN= -6.000

YINC= 0.8500E-01
YMAX= 2.500

LINE 2200. F PERCENT FREQUENCY EFFECT PFE

FORM No. 11 15

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XTOP= -1800.

XINC= 25.00

128085

MOORE PARSON (VA) LIMITED - FORMALINER PARAFLO

1	-1800.	I		*	2.80	1
2	-1775.	I		*	2.80	2
3	-1750.	I		*	2.40	3
4	-1725.	I		*	2.40	4
5	-1700.	I		*	2.10	5
6	-1675.	I		*	2.20	6
7	-1650.	I		*	2.00	7
8	-1625.	I	*		1.60	8
9	-1600.	I	*		1.70	9
10	-1575.	I	*		1.60	10
11	-1550.	I	*		1.40	11
12	-1525.	I	*		1.50	12
13	-1500.	I	*		1.40	13
14	-1475.	I	*		1.40	14
15	-1450.	I	*		1.30	15
16	-1425.	I	*		1.40	16
17	-1400.	I	*		1.30	17
18	-1375.	I	*		1.40	18
19	-1350.	I	*		1.30	19
20	-1325.	I	*		1.30	20
21	-1300.	I	*		1.20	21
22	-1275.	I	*		1.30	22
23	-1250.	I	*		1.30	23
24	-1225.	I	*		1.40	24
25	-1200.	I	*		1.50	25
26	-1175.	I	*		1.60	26
27	-1150.	I	*		1.60	27
28	-1125.	I	*		1.60	28
29	-1100.	I	*		1.60	29
30	-1075.	I		*	2.00	30
31	-1050.	I		*	2.00	31
32	-1025.	I		*	2.00	32
33	-1000.	I		*	2.00	33

XBOT= -1000.
YMIN= -2.500

YINC= 0.5300F-01
YMAX= 2.800

LINE 2200. E RELATIVE PHASE SHIFT RPS

FORM NO. 11-15
0103205

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

1	---FIFL II---		---OFFSE1---												1	
	STATION	CURRENT	HF	PFF	RPS	PFF	RPS	HU	HN	MNR	PFF	RPS	HSG/I	HSP/I		STATION
2																2
3	-1800. N	3.50	0.55	-8.00	4.80	-2.05	1.95	0.18	88.30	-10.41	-5.95	2.85	3.91	-9.35	-1800. N	3
4	-1775. N	3.50	0.58	-7.50	4.60	-2.05	1.95	0.18	91.04	-8.15	-5.45	2.65	3.83	-9.03	-1775. N	4
5	-1750. N	3.50	0.57	-7.60	4.80	-2.05	1.95	0.19	87.55	-11.58	-5.55	2.85	4.05	-9.04	-1750. N	5
6	-1725. N	3.50	0.58	-7.30	4.60	-2.05	1.95	0.19	87.25	-12.10	-5.25	2.65	3.83	-8.70	-1725. N	6
7	-1700. N	3.50	0.59	-7.20	4.60	-2.05	1.95	0.19	87.02	-12.58	-5.15	2.65	3.90	-8.68	-1700. N	7
8	-1675. N	3.50	0.62	-6.60	4.10	-2.05	1.95	0.20	89.74	-10.12	-4.55	2.15	3.32	-8.06	-1675. N	8
9	-1650. N	3.50	0.64	-6.50	4.20	-2.05	1.95	0.20	91.03	-9.01	-4.45	2.25	3.59	-8.14	-1650. N	9
10	-1625. N	3.50	0.60	-6.70	4.20	-2.05	1.95	0.20	83.97	-16.37	-4.65	2.25	3.37	-7.97	-1625. N	10
11	-1600. N	3.50	0.63	-6.40	4.10	-2.05	1.95	0.21	86.86	-13.61	-4.35	2.15	3.38	-7.83	-1600. N	11
12	-1575. N	3.50	0.66	-6.20	4.00	-2.05	1.95	0.21	89.79	-10.72	-4.15	2.05	3.37	-7.83	-1575. N	12
13	-1550. N	3.50	0.67	-6.10	4.10	-2.05	1.95	0.21	90.08	-10.53	-4.05	2.15	3.59	-7.75	-1550. N	13
14	-1525. N	3.50	0.69	-6.00	4.00	-2.05	1.95	0.21	91.84	-8.76	-3.95	2.05	3.53	-7.79	-1525. N	14
15	-1500. N	3.50	0.68	-6.00	4.10	-2.05	1.95	0.22	89.75	-11.09	-3.95	2.15	3.65	-7.67	-1500. N	15
16	-1475. N	3.50	0.66	-5.90	4.00	-2.05	1.95	0.22	86.54	-14.67	-3.85	2.05	3.37	-7.26	-1475. N	16
17	-1450. N	3.50	0.68	-5.80	4.00	-2.05	1.95	0.22	88.74	-12.33	-3.75	2.05	3.48	-7.29	-1450. N	17
18	-1425. N	3.50	0.69	-5.70	3.90	-2.05	1.95	0.22	89.79	-11.21	-3.65	1.95	3.35	-7.20	-1425. N	18
19	-1400. N	3.50	0.67	-5.70	3.80	-2.05	1.95	0.22	87.10	-14.18	-3.65	1.85	3.09	-6.99	-1400. N	19
20	-1375. N	3.50	0.66	-5.80	3.90	-2.10	1.95	0.22	85.88	-15.50	-3.70	1.95	3.21	-6.98	-1375. N	20
21	-1350. N	3.50	0.65	-5.70	4.00	-2.10	1.95	0.22	84.82	-16.61	-3.60	2.05	3.32	-6.69	-1350. N	21
22	-1325. N	3.50	0.66	-5.70	4.00	-2.10	1.95	0.22	86.54	-14.67	-3.60	2.05	3.37	-6.79	-1325. N	22
23	-1300. N	3.50	0.66	-5.60	3.90	-2.10	1.95	0.22	87.11	-13.95	-3.50	1.95	3.21	-6.60	-1300. N	23
24	-1275. N	3.50	0.64	-5.50	3.90	-2.10	1.95	0.21	85.18	-15.90	-3.40	1.95	3.11	-6.22	-1275. N	24
25	-1250. N	3.50	0.65	-5.40	4.00	-2.10	1.95	0.21	87.40	-13.39	-3.30	2.05	3.32	-6.13	-1250. N	25
26	-1225. N	3.50	0.64	-5.40	4.00	-2.10	1.95	0.21	87.07	-13.58	-3.30	2.05	3.27	-6.03	-1225. N	26
27	-1200. N	3.50	0.63	-5.50	4.00	-2.10	1.95	0.21	86.86	-13.61	-3.40	2.05	3.22	-6.12	-1200. N	27
28	-1175. N	3.50	0.62	-5.60	4.00	-2.10	1.95	0.20	86.76	-13.51	-3.50	2.05	3.17	-6.20	-1175. N	28
29	-1150. N	3.50	0.60	-5.60	4.00	-2.10	1.95	0.20	85.34	-14.72	-3.50	2.05	3.07	-6.00	-1150. N	29
30	-1125. N	3.50	0.60	-5.50	4.00	-2.10	1.95	0.20	86.85	-12.98	-3.40	2.05	3.07	-5.83	-1125. N	30
31	-1100. N	3.50	0.58	-5.40	3.90	-2.10	1.95	0.19	85.54	-14.00	-3.30	1.95	2.82	-5.47	-1100. N	31
32	-1075. N	3.50	0.57	-5.40	4.00	-2.10	1.95	0.19	85.75	-13.53	-3.30	2.05	2.91	-5.37	-1075. N	32
33	-1050. N	3.50	0.57	-5.50	4.10	-2.10	1.95	0.19	87.55	-11.58	-3.40	2.15	3.06	-5.54	-1050. N	33
34	-1025. N	3.50	0.53	-5.50	4.10	-2.10	1.95	0.18	83.20	-15.29	-3.40	2.15	2.84	-5.15	-1025. N	34
35	-1000. N	3.50	0.53	-5.50	4.20	-2.10	1.95	0.18	85.09	-13.27	-3.40	2.25	2.97	-5.15	-1000. N	35
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FORM No. 1115
0103207

XTOP= -1800.

XINC= 25.00

128088

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.		*	I	-10.41	1
2	-1775.		*	I	-8.15	2
3	-1750.		*	I	-11.58	3
4	-1725.		*	I	-12.10	4
5	-1700.		*	I	-12.58	5
6	-1675.		*	I	-10.12	6
7	-1650.		*	I	-9.01	7
8	-1625.	*		I	-16.37	8
9	-1600.	*		I	-13.61	9
10	-1575.		*	I	-10.72	10
11	-1550.		*	I	-10.53	11
12	-1525.		*	I	-8.76	12
13	-1500.		*	I	-11.09	13
14	-1475.	*		I	-14.67	14
15	-1450.		*	I	-12.33	15
16	-1425.		*	I	-11.21	16
17	-1400.	*		I	-14.18	17
18	-1375.	*		I	-15.50	18
19	-1350.	*		I	-16.61	19
20	-1325.	*		I	-14.67	20
21	-1300.	*		I	-13.95	21
22	-1275.	*		I	-15.90	22
23	-1250.		*	I	-13.39	23
24	-1225.	*		I	-13.58	24
25	-1200.	*		I	-13.61	25
26	-1175.	*		I	-13.51	26
27	-1150.	*		I	-14.72	27
28	-1125.	*		I	-12.98	28
29	-1100.	*		I	-14.00	29
30	-1075.	*		I	-13.53	30
31	-1050.		*	I	-11.58	31
32	-1025.	*		I	-15.29	32
33	-1000.		*	I	-13.27	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2500. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-13

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XTOP= -1800.

XINC= 25.00

128089

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	*	I	-5.95	1
2	-1775.	*	I	-5.45	2
3	-1750.	*	I	-5.55	3
4	-1725.	*	I	-5.25	4
5	-1700.	*	I	-5.15	5
6	-1675.	*	I	-4.55	6
7	-1650.	*	I	-4.45	7
8	-1625.	*	I	-4.65	8
9	-1600.	*	I	-4.35	9
10	-1575.	*	I	-4.15	10
11	-1550.	*	I	-4.05	11
12	-1525.	*	I	-3.95	12
13	-1500.	*	I	-3.95	13
14	-1475.	*	I	-3.85	14
15	-1450.	*	I	-3.75	15
16	-1425.	*	I	-3.65	16
17	-1400.	*	I	-3.65	17
18	-1375.	*	I	-3.70	18
19	-1350.	*	I	-3.60	19
20	-1325.	*	I	-3.60	20
21	-1300.	*	I	-3.50	21
22	-1275.	*	I	-3.40	22
23	-1250.	*	I	-3.30	23
24	-1225.	*	I	-3.30	24
25	-1200.	*	I	-3.40	25
26	-1175.	*	I	-3.50	26
27	-1150.	*	I	-3.50	27
28	-1125.	*	I	-3.40	28
29	-1100.	*	I	-3.30	29
30	-1075.	*	I	-3.30	30
31	-1050.	*	I	-3.40	31
32	-1025.	*	I	-3.40	32
33	-1000.	*	I	-3.40	33

XBOT= -1000.
YMIN= -5.950

YINC= 0.8450E-01
YMAX= 2.500

LINE 2500. F PERCENT FREQUENCY EFFECT PFE

FORM No. 11.15
0143209

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XTOP= -1800.

XINC= 25.00

128090

1	-1800.	I	*	2.85	1
2	-1775.	I	*	2.65	2
3	-1750.	I	*	2.85	3
4	-1725.	I	*	2.65	4
5	-1700.	I	*	2.65	5
6	-1675.	I	*	2.15	6
7	-1650.	I	*	2.25	7
8	-1625.	I	*	2.25	8
9	-1600.	I	*	2.15	9
10	-1575.	I	*	2.05	10
11	-1550.	I	*	2.15	11
12	-1525.	I	*	2.05	12
13	-1500.	I	*	2.15	13
14	-1475.	I	*	2.05	14
15	-1450.	I	*	2.05	15
16	-1425.	I	*	1.95	16
17	-1400.	I	*	1.85	17
18	-1375.	I	*	1.95	18
19	-1350.	I	*	2.05	19
20	-1325.	I	*	2.05	20
21	-1300.	I	*	1.95	21
22	-1275.	I	*	1.95	22
23	-1250.	I	*	2.05	23
24	-1225.	I	*	2.05	24
25	-1200.	I	*	2.05	25
26	-1175.	I	*	2.05	26
27	-1150.	I	*	2.05	27
28	-1125.	I	*	2.05	28
29	-1100.	I	*	1.95	29
30	-1075.	I	*	2.05	30
31	-1050.	I	*	2.15	31
32	-1025.	I	*	2.15	32
33	-1000.	I	*	2.25	33

XBOT= -1000.

YINC= 0.5350E-01

YMIN= -2.500

YMAX= 2.850

LINE 2500. F RELATIVE PHASE SHIFT RPS

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

FORM No 11 15

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

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STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RPS	HSQ/I	HSP/I	STATION
			PFF	RPS	PFF	RPS								
-1800. N	3.25	0.45	-8.50	5.20	-7.70	2.05	0.18	79.12	-18.27	-6.30	3.15	3.81	-8.72	-1800. N
-1775. N	3.25	0.53	-8.00	4.60	-2.70	2.05	0.18	91.41	-7.66	-5.80	2.55	3.63	-9.46	-1775. N
-1750. N	3.25	0.52	-8.00	4.60	-2.70	2.05	0.18	88.05	-10.86	-5.80	2.55	3.56	-9.28	-1750. N
-1725. N	3.25	0.52	-8.00	4.50	-2.70	2.05	0.18	86.52	-12.47	-5.80	2.45	3.42	-9.28	-1725. N
-1700. N	3.25	0.57	-7.50	4.40	-2.70	2.05	0.19	93.78	-6.32	-5.30	2.35	3.60	-9.30	-1700. N
-1675. N	3.25	0.56	-7.30	4.40	-2.70	2.05	0.19	90.23	-9.33	-5.10	2.35	3.53	-8.79	-1675. N
-1650. N	3.25	0.59	-6.80	4.20	-2.70	2.05	0.19	93.70	-6.10	-4.60	2.15	3.41	-8.35	-1650. N
-1625. N	3.25	0.57	-7.00	4.30	-2.70	2.05	0.20	89.33	-10.48	-4.80	2.25	3.44	-8.42	-1625. N
-1600. N	3.25	0.62	-6.50	4.20	-2.70	2.05	0.20	96.00	-3.98	-4.30	2.15	3.58	-8.20	-1600. N
-1575. N	3.25	0.58	-6.60	4.40	-2.70	2.05	0.20	88.84	-11.21	-4.40	2.35	3.66	-7.85	-1575. N
-1550. N	3.25	0.57	-7.00	4.50	-2.70	2.05	0.20	86.48	-13.71	-4.80	2.45	3.75	-8.42	-1550. N
-1525. N	3.25	0.57	-7.00	4.40	-2.20	2.10	0.20	85.78	-14.54	-4.80	2.30	3.52	-8.42	-1525. N
-1500. N	3.25	0.58	-6.80	4.40	-2.70	2.10	0.21	86.70	-13.69	-4.60	2.30	3.58	-8.21	-1500. N
-1475. N	3.25	0.60	-6.50	4.50	-2.70	2.10	0.21	89.77	-11.15	-4.30	2.40	3.87	-7.94	-1475. N
-1450. N	3.25	0.60	-6.50	4.30	-2.70	2.10	0.21	88.88	-11.54	-4.30	2.20	3.54	-7.94	-1450. N
-1425. N	3.25	0.59	-6.70	4.10	-2.70	2.10	0.21	87.20	-13.32	-4.00	2.00	3.17	-7.26	-1425. N
-1400. N	3.25	0.58	-6.70	4.10	-2.70	2.10	0.21	85.66	-14.94	-4.00	2.00	3.11	-7.14	-1400. N
-1375. N	3.25	0.59	-6.10	4.20	-2.20	2.10	0.21	87.20	-13.32	-3.90	2.10	3.33	-7.08	-1375. N
-1350. N	3.25	0.59	-6.00	4.20	-2.70	2.10	0.21	87.40	-13.08	-3.80	2.10	3.33	-6.90	-1350. N
-1325. N	3.25	0.57	-6.00	4.30	-2.70	2.10	0.21	84.76	-15.77	-3.80	2.20	3.37	-6.66	-1325. N
-1300. N	3.25	0.57	-6.00	4.20	-2.70	2.10	0.21	85.21	-15.23	-3.80	2.10	3.21	-6.66	-1300. N
-1275. N	3.25	0.57	-5.80	4.10	-2.70	2.10	0.20	85.78	-14.54	-3.60	2.00	3.06	-6.31	-1275. N
-1250. N	3.25	0.54	-6.00	4.20	-2.70	2.10	0.20	81.93	-18.33	-3.80	2.10	3.04	-6.31	-1250. N
-1225. N	3.25	0.52	-5.80	4.10	-2.70	2.10	0.20	79.65	-20.44	-3.60	2.00	2.79	-5.76	-1225. N
-1200. N	3.25	0.55	-5.80	4.10	-2.70	2.10	0.20	85.16	-14.75	-3.60	2.00	2.95	-6.09	-1200. N
-1175. N	3.25	0.55	-6.00	4.20	-2.70	2.10	0.20	86.19	-13.55	-3.80	2.10	3.10	-6.43	-1175. N
-1150. N	3.25	0.53	-6.00	4.40	-2.70	2.10	0.19	84.17	-15.33	-3.80	2.30	3.27	-6.20	-1150. N
-1125. N	3.25	0.53	-6.00	4.30	-2.70	2.10	0.19	85.40	-13.94	-3.80	2.20	3.13	-6.20	-1125. N
-1100. N	3.25	0.52	-6.00	4.20	-2.70	2.10	0.19	85.10	-14.01	-3.80	2.10	2.93	-6.08	-1100. N
-1075. N	3.25	0.54	-5.30	4.20	-2.70	2.10	0.18	89.85	-9.39	-3.10	2.10	3.04	-5.15	-1075. N
-1050. N	3.25	0.51	-5.70	4.40	-2.70	2.10	0.18	86.36	-12.40	-3.50	2.30	3.15	-5.49	-1050. N
-1025. N	3.25	0.49	-5.80	4.30	-2.70	2.10	0.18	84.51	-13.82	-3.60	2.20	2.89	-5.43	-1025. N
-1000. N	3.25	0.50	-5.50	4.20	-2.70	2.10	0.18	87.91	-10.58	-3.30	2.10	2.82	-5.08	-1000. N

XTOP= -1800.

XINC= 25.00

128093

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	-1800.	*		I		-18.27	1
2	-1775.		*	I		-7.66	2
3	-1750.		*	I		-10.86	3
4	-1725.		*	I		-12.47	4
5	-1700.		*	I		-6.32	5
6	-1675.		*	I		-9.33	6
7	-1650.		*	I		-6.10	7
8	-1625.		*	I		-10.48	8
9	-1600.		*	I		-3.98	9
10	-1575.		*	I		-11.21	10
11	-1550.	*		I		-13.71	11
12	-1525.	*		I		-14.54	12
13	-1500.	*		I		-13.69	13
14	-1475.		*	I		-11.15	14
15	-1450.		*	I		-11.54	15
16	-1425.		*	I		-13.32	16
17	-1400.	*		I		-14.94	17
18	-1375.	*		I		-13.32	18
19	-1350.	*		I		-13.08	19
20	-1325.	*		I		-15.77	20
21	-1300.	*		I		-15.23	21
22	-1275.	*		I		-14.54	22
23	-1250.	*		I		-18.33	23
24	-1225.	*		I		-20.44	24
25	-1200.	*		I		-14.75	25
26	-1175.	*		I		-13.55	26
27	-1150.	*		I		-15.33	27
28	-1125.	*		I		-13.94	28
29	-1100.	*		I		-14.01	29
30	-1075.		*	I		-9.39	30
31	-1050.		*	I		-12.40	31
32	-1025.	*		I		-13.82	32
33	-1000.		*	I		-10.58	33

XBOT= -1000.

YINC= 1.000

YMIN= -50.00

YMAX= 50.00

LINE 2600. F MAGNETOMETRIC RESISTIVITY MMR

FORM NO. 11-15
0143293

50 51 52 53 54 55 56 57 58 59 60

XTOP= -1800.

XINC= 25.00

128094

1	-1800.	*			I	-6.30
2	-1775.		*		I	-5.80
3	-1750.		*		I	-5.80
4	-1725.		*		I	-5.80
5	-1700.			*	I	-5.30
6	-1675.			*	I	-5.10
7	-1650.			*	I	-4.60
8	-1625.			*	I	-4.80
9	-1600.			*	I	-4.30
10	-1575.			*	I	-4.40
11	-1550.			*	I	-4.80
12	-1525.			*	I	-4.80
13	-1500.			*	I	-4.60
14	-1475.			*	I	-4.30
15	-1450.			*	I	-4.30
16	-1425.			*	I	-4.00
17	-1400.			*	I	-4.00
18	-1375.			*	I	-3.90
19	-1350.			*	I	-3.80
20	-1325.			*	I	-3.80
21	-1300.			*	I	-3.80
22	-1275.			*	I	-3.60
23	-1250.			*	I	-3.80
24	-1225.			*	I	-3.60
25	-1200.			*	I	-3.60
26	-1175.			*	I	-3.80
27	-1150.			*	I	-3.80
28	-1125.			*	I	-3.80
29	-1100.			*	I	-3.80
30	-1075.			*	I	-3.10
31	-1050.			*	I	-3.50
32	-1025.			*	I	-3.60
33	-1000.			*	I	-3.30

XBOT= -1000.

YINC= 0.8800E-01

YMIN= -6.300

YMAX= 2.500

LINE 2600. F PERCENT FREQUENCY EFFECT PFF

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

FORM No 11 13

XTOP=-1800.

XINC= 25.00

128095

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

094

1	-1800.	I	*	3.15	1
2	-1775.	I	*	2.55	2
3	-1750.	I	*	2.55	3
4	-1725.	I	*	2.45	4
5	-1700.	I	*	2.35	5
6	-1675.	I	*	2.35	6
7	-1650.	I	*	2.15	7
8	-1625.	I	*	2.25	8
9	-1600.	I	*	2.15	9
10	-1575.	I	*	2.35	10
11	-1550.	I	*	2.45	11
12	-1525.	I	*	2.30	12
13	-1500.	I	*	2.30	13
14	-1475.	I	*	2.40	14
15	-1450.	I	*	2.20	15
16	-1425.	I	*	2.00	16
17	-1400.	I	*	2.00	17
18	-1375.	I	*	2.10	18
19	-1350.	I	*	2.10	19
20	-1325.	I	*	2.20	20
21	-1300.	I	*	2.10	21
22	-1275.	I	*	2.00	22
23	-1250.	I	*	2.10	23
24	-1225.	I	*	2.00	24
25	-1200.	I	*	2.00	25
26	-1175.	I	*	2.10	26
27	-1150.	I	*	2.30	27
28	-1125.	I	*	2.20	28
29	-1100.	I	*	2.10	29
30	-1075.	I	*	2.10	30
31	-1050.	I	*	2.30	31
32	-1025.	I	*	2.20	32
33	-1000.	I	*	2.10	33

XBOT=-1000.
YMIN=-2.500

YINC= 0.5650E-01
YMAX= 3.150

LINE 2600. F RELATIVE PHASE SHIFT RPS

FORM No. 11-10
0103295

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58					58
59					59
60					60

XTOP=-1800.

XINC= 25.00

128096

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

1	-1800.	I	*	3.81	1
2	-1775.	I	*	3.63	2
3	-1750.	I	*	3.56	3
4	-1725.	I	*	3.42	4
5	-1700.	I	*	3.60	5
6	-1675.	I	*	3.53	6
7	-1650.	I	*	3.41	7
8	-1625.	I	*	3.44	8
9	-1600.	I	*	3.58	9
10	-1575.	I	*	3.66	10
11	-1550.	I	*	3.75	11
12	-1525.	I	*	3.52	12
13	-1500.	I	*	3.58	13
14	-1475.	I	*	3.87	14
15	-1450.	I	*	3.54	15
16	-1425.	I	*	3.17	16
17	-1400.	I	*	3.11	17
18	-1375.	I	*	3.33	18
19	-1350.	I	*	3.33	19
20	-1325.	I	*	3.37	20
21	-1300.	I	*	3.21	21
22	-1275.	I	*	3.06	22
23	-1250.	I	*	3.04	23
24	-1225.	I	*	2.79	24
25	-1200.	I	*	2.95	25
26	-1175.	I	*	3.10	26
27	-1150.	I	*	3.27	27
28	-1125.	I	*	3.13	28
29	-1100.	I	*	2.93	29
30	-1075.	I	*	3.04	30
31	-1050.	I	*	3.15	31
32	-1025.	I	*	2.89	32
33	-1000.	I	*	2.82	33

XBOT=-1000.
YMIN=-10.00

YINC= 0.2000
YMAX= 10.00

LINE 7600.E SECONDARY FIELD QUADRATURE HSO/I

FORM No 11-15

2700. F FREQUENCY=3H7 N001

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFIL

FORM No. 11-13 013207

STATION	CURRENT	HP	---FIELD---		---OFF SET---		HU	HN	MMR	PFE	RPS	HSQ/T	HSP/T	STATION
			PFE	RPS	PFF	RPS								
-1800. N	3.25	0.52	-8.00	4.80	-7.15	2.05	0.17	92.45	-6.54	-5.85	2.75	3.84	-9.36	-1800. N
-1775. N	3.25	0.54	-8.00	5.00	-7.15	2.05	0.18	94.34	-4.98	-5.85	2.95	4.28	-9.72	-1775. N
-1750. N	3.25	0.55	-7.50	4.80	-7.15	2.05	0.18	94.51	-4.92	-5.35	2.75	4.06	-9.05	-1750. N
-1725. N	3.25	0.55	-7.70	4.80	-7.15	2.05	0.18	93.03	-6.34	-5.55	2.75	4.06	-9.39	-1725. N
-1700. N	3.25	0.56	-7.50	4.70	-2.15	2.05	0.18	93.33	-6.15	-5.35	2.65	3.98	-9.22	-1700. N
-1675. N	3.25	0.57	-6.90	4.40	-2.15	2.05	0.19	93.70	-5.90	-4.75	2.35	3.60	-8.33	-1675. N
-1650. N	3.25	0.58	-6.80	4.50	-2.15	2.05	0.19	94.13	-5.57	-4.65	2.45	3.87	-8.30	-1650. N
-1625. N	3.25	0.59	-6.70	4.40	-2.15	2.05	0.19	94.63	-5.15	-4.55	2.35	3.72	-8.26	-1625. N
-1600. N	3.25	0.60	-6.60	4.30	-2.15	2.05	0.19	95.72	-4.63	-4.45	2.25	3.62	-8.22	-1600. N
-1575. N	3.25	0.60	-6.50	4.40	-2.15	2.05	0.20	94.32	-5.56	-4.35	2.35	3.79	-8.03	-1575. N
-1550. N	3.25	0.60	-6.50	4.30	-2.15	2.05	0.20	93.54	-6.37	-4.35	2.75	3.67	-8.03	-1550. N
-1525. N	3.25	0.60	-6.60	4.20	-2.15	2.00	0.20	92.88	-7.07	-4.45	2.20	3.54	-8.22	-1525. N
-1500. N	3.25	0.60	-6.50	4.20	-2.15	2.00	0.20	92.34	-7.65	-4.35	2.70	3.54	-8.03	-1500. N
-1475. N	3.25	0.60	-6.40	4.20	-2.15	2.00	0.20	91.92	-8.11	-4.25	2.20	3.54	-7.85	-1475. N
-1450. N	3.25	0.60	-6.30	4.30	-2.15	2.00	0.20	91.62	-8.44	-4.15	2.30	3.71	-7.66	-1450. N
-1425. N	3.25	0.59	-6.70	4.30	-2.15	2.00	0.20	89.97	-10.17	-4.05	2.30	3.64	-7.35	-1425. N
-1400. N	3.25	0.59	-6.10	4.20	-2.15	2.00	0.20	89.86	-10.24	-3.95	2.20	3.49	-7.17	-1400. N
-1375. N	3.25	0.58	-6.00	4.30	-2.15	2.00	0.20	88.40	-11.71	-3.85	2.30	3.58	-6.87	-1375. N
-1350. N	3.25	0.57	-6.10	4.20	-2.15	2.00	0.20	87.04	-13.05	-3.95	2.70	3.37	-6.93	-1350. N
-1325. N	3.25	0.57	-6.00	4.30	-2.15	2.00	0.20	87.33	-12.72	-3.85	2.30	3.52	-6.75	-1325. N
-1300. N	3.25	0.56	-6.00	4.20	-2.15	2.00	0.20	86.19	-13.81	-3.85	2.20	3.31	-6.63	-1300. N
-1275. N	3.25	0.55	-5.90	4.10	-2.15	2.00	0.20	85.14	-14.76	-3.75	2.10	3.10	-6.35	-1275. N
-1250. N	3.25	0.54	-6.00	4.20	-2.15	2.00	0.20	84.19	-15.60	-3.85	2.70	3.19	-6.40	-1250. N
-1225. N	3.25	0.54	-6.00	4.40	-2.15	2.00	0.20	84.89	-14.79	-3.85	2.40	3.48	-6.40	-1225. N
-1200. N	3.25	0.53	-6.10	4.40	-2.15	2.00	0.19	84.11	-15.40	-3.95	2.40	3.42	-6.44	-1200. N
-1175. N	3.25	0.53	-6.00	4.40	-2.15	2.00	0.19	85.01	-14.38	-3.85	2.40	3.42	-6.28	-1175. N
-1150. N	3.25	0.53	-6.00	4.20	-2.15	2.00	0.19	86.01	-13.26	-3.85	2.20	3.13	-6.28	-1150. N
-1125. N	3.25	0.51	-6.00	4.30	-2.15	2.00	0.19	83.83	-15.13	-3.85	2.30	3.15	-6.04	-1125. N
-1100. N	3.25	0.50	-6.00	4.00	-2.15	2.00	0.18	83.33	-15.38	-3.85	2.00	2.68	-5.92	-1100. N
-1075. N	3.25	0.50	-6.00	4.30	-2.15	2.00	0.18	84.58	-14.03	-3.85	2.30	3.09	-5.92	-1075. N
-1050. N	3.25	0.49	-6.00	4.40	-2.15	2.00	0.18	84.20	-14.15	-3.85	2.40	3.16	-5.80	-1050. N
-1025. N	3.25	0.48	-5.60	4.40	-2.15	2.00	0.18	83.86	-14.21	-3.45	2.40	3.09	-5.10	-1025. N
-1000. N	3.25	0.48	-5.70	4.40	-2.15	2.00	0.17	85.33	-12.69	-3.55	2.40	3.09	-5.24	-1000. N

XTOP= -1800.

XINC= 25.00

097

MOORE PARAGON (WA) WILD - FORMALINER PARAFLO

1	-1800.	*	I	-5.85	1
2	-1775.	*	I	-5.85	2
3	-1750.	*	I	-5.35	3
4	-1725.	*	I	-5.55	4
5	-1700.	*	I	-5.35	5
6	-1675.	*	I	-4.75	6
7	-1650.	*	I	-4.65	7
8	-1625.	*	I	-4.55	8
9	-1600.	*	I	-4.45	9
10	-1575.	*	I	-4.35	10
11	-1550.	*	I	-4.35	11
12	-1525.	*	I	-4.45	12
13	-1500.	*	I	-4.35	13
14	-1475.	*	I	-4.25	14
15	-1450.	*	I	-4.15	15
16	-1425.	*	I	-4.05	16
17	-1400.	*	I	-3.95	17
18	-1375.	*	I	-3.85	18
19	-1350.	*	I	-3.95	19
20	-1325.	*	I	-3.85	20
21	-1300.	*	I	-3.85	21
22	-1275.	*	I	-3.75	22
23	-1250.	*	I	-3.85	23
24	-1225.	*	I	-3.85	24
25	-1200.	*	I	-3.95	25
26	-1175.	*	I	-3.85	26
27	-1150.	*	I	-3.85	27
28	-1125.	*	I	-3.85	28
29	-1100.	*	I	-3.85	29
30	-1075.	*	I	-3.85	30
31	-1050.	*	I	-3.85	31
32	-1025.	*	I	-3.45	32
33	-1000.	*	I	-3.55	33

XBOT= -1000.
YMIN= -5.850

YINC= 0.8350E-01
YMAX= 7.500

LINE 2700. F PERCENT FREQUENCY EFFECT PFE

0103209

60

XTOP=-1800.

XINC= 25.00

099

MOORE PARSONS (WA) LIMITED - FORMALINER PARAFLO

1	-1800.	I		*	2.75	1
2	-1775.	I		*	2.95	2
3	-1750.	I		*	2.75	3
4	-1725.	I		*	2.75	4
5	-1700.	I		*	2.65	5
6	-1675.	I		*	2.35	6
7	-1650.	I		*	2.45	7
8	-1625.	I		*	2.35	8
9	-1600.	I		*	2.25	9
10	-1575.	I		*	2.35	10
11	-1550.	I		*	2.25	11
12	-1525.	I		*	2.20	12
13	-1500.	I		*	2.20	13
14	-1475.	I		*	2.20	14
15	-1450.	I		*	2.30	15
16	-1425.	I		*	2.30	16
17	-1400.	I		*	2.20	17
18	-1375.	I		*	2.30	18
19	-1350.	I		*	2.20	19
20	-1325.	I		*	2.30	20
21	-1300.	I		*	2.20	21
22	-1275.	I		*	2.10	22
23	-1250.	I		*	2.20	23
24	-1225.	I		*	2.40	24
25	-1200.	I		*	2.40	25
26	-1175.	I		*	2.40	26
27	-1150.	I		*	2.70	27
28	-1125.	I		*	2.30	28
29	-1100.	I	*	*	2.00	29
30	-1075.	I		*	2.30	30
31	-1050.	I		*	2.40	31
32	-1025.	I		*	2.40	32
33	-1000.	I		*	2.40	33

XBOT=-1000.
YMIN=-2.500

YINC= 0.5450E-01
YMAX= 2.950

LINE 2700. F RELATIVE PHASE SHIFT RPS

FORM No. 11 15

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35						35
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57						57
58						58
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XTOP= -1800.

XINC= 25.00

128101

100

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

1	1800.	I	*	3.84	1
2	-1775.	I	*	4.28	2
3	-1750.	I	*	4.06	3
4	-1725.	I	*	4.06	4
5	-1700.	I	*	3.98	5
6	-1675.	I	*	3.60	6
7	-1650.	I	*	3.82	7
8	-1625.	I	*	3.72	8
9	-1600.	I	*	3.62	9
10	-1575.	I	*	3.79	10
11	-1550.	I	*	3.62	11
12	-1525.	I	*	3.54	12
13	-1500.	I	*	3.54	13
14	-1475.	I	*	3.54	14
15	-1450.	I	*	3.71	15
16	-1425.	I	*	3.64	16
17	-1400.	I	*	3.49	17
18	-1375.	I	*	3.58	18
19	-1350.	I	*	3.37	19
20	-1325.	I	*	3.52	20
21	-1300.	I	*	3.31	21
22	-1275.	I	*	3.10	22
23	-1250.	I	*	3.19	23
24	-1225.	I	*	3.48	24
25	-1200.	I	*	3.42	25
26	-1175.	I	*	3.42	26
27	-1150.	I	*	3.13	27
28	-1125.	I	*	3.15	28
29	-1100.	I	*	2.68	29
30	-1075.	I	*	3.09	30
31	-1050.	I	*	3.16	31
32	-1025.	I	*	3.09	32
33	-1000.	I	*	3.09	33

XBDT= -1000.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 2700. F SECONDARY FIELD QUADRATURE HSQ/I

FORM No. 11.15
0103301

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XTOP= -1800.

XINC= 25.00

102

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	*	I	-4.67	1
2	-1775.	*	I	-3.06	2
3	-1750.	*	I	-2.93	3
4	-1725.	*	I	-2.75	4
5	-1700.	*	I	-5.59	5
6	-1675.	*	I	-3.74	6
7	-1650.	*	I	-3.35	7
8	-1625.	*	I	-5.95	8
9	-1600.	*	I	-5.38	9
10	-1575.	*	I	-7.80	10
11	-1550.	*	I	-8.57	11
12	-1525.	*	I	-4.62	12
13	-1500.	*	I	-6.70	13
14	-1475.	*	I	-10.21	14
15	-1450.	*	I	-5.90	15
16	-1425.	*	I	-10.71	16
17	-1400.	*	I	-9.23	17
18	-1375.	*	I	-9.17	18
19	-1350.	*	I	-10.52	19
20	-1325.	*	I	-10.21	20
21	-1300.	*	I	-11.32	21
22	-1275.	*	I	-10.77	22
23	-1250.	*	I	-17.80	23
24	-1225.	*	I	-10.87	24
25	-1200.	*	I	-11.54	25
26	-1175.	*	I	-10.57	26
27	-1150.	*	I	-11.04	27
28	-1125.	*	I	-11.43	28
29	-1100.	*	I	-10.20	29
30	-1075.	*	I	-10.45	30
31	-1050.	*	I	-10.63	31
32	-1025.	*	I	-10.75	32
33	-1000.	*	I	-10.82	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2800. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-15
013303

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60					60

XTOP= -1800.

XINC= 25.00

607

MOORE PARAGON (WVA) LIMITED - FORMALINER PARAFLO

1	-1800.	*	I	-6.75	1
2	-1775.	*	I	-5.95	2
3	-1750.		I	-5.55	3
4	-1725.	*	I	-5.45	4
5	-1700.	*	I	-5.35	5
6	-1675.	*	I	-5.15	6
7	-1650.	*	I	-5.05	7
8	-1625.	*	I	-5.15	8
9	-1600.	*	I	-5.15	9
10	-1575.	*	I	-5.05	10
11	-1550.	*	I	-4.75	11
12	-1525.	*	I	-4.85	12
13	-1500.	*	I	-4.75	13
14	-1475.	*	I	-4.85	14
15	-1450.	*	I	-4.65	15
16	-1425.	*	I	-4.75	16
17	-1400.	*	I	-4.85	17
18	-1375.	*	I	-4.75	18
19	-1350.	*	I	-4.55	19
20	-1325.	*	I	-4.75	20
21	-1300.	*	I	-4.15	21
22	-1275.	*	I	-3.95	22
23	-1250.	*	I	-3.75	23
24	-1225.	*	I	-3.85	24
25	-1200.	*	I	-3.75	25
26	-1175.	*	I	-3.95	26
27	-1150.	*	I	-3.85	27
28	-1125.	*	I	-3.85	28
29	-1100.	*	I	-3.95	29
30	-1075.	*	I	-3.95	30
31	-1050.	*	I	-4.05	31
32	-1025.	*	I	-3.85	32
33	-1000.	*	I	-3.85	33

XBOT= -1000.
YMIN= -6.750

YINC= 0.9750E-01
YMAX= 2.500

LINE 2800. F PERCENT FREQUENCY EFFECT PFE

FORM No 11-15

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XTOP= -1800.

XINC= 75.00

104

MOORE PARSON (WA) LIMITED - FORM 104

1	-1800.	I	*	2.70	1
2	-1775.	I	*	2.40	2
3	-1750.	I	*	2.70	3
4	-1725.	I	*	2.20	4
5	-1700.	I	*	2.10	5
6	-1675.	I	*	2.20	6
7	-1650.	I	*	2.20	7
8	-1625.	I	*	2.10	8
9	-1600.	I	*	2.30	9
10	-1575.	I	*	2.40	10
11	-1550.	I	*	2.10	11
12	-1525.	I	*	2.20	12
13	-1500.	I	*	2.50	13
14	-1475.	I	*	2.30	14
15	-1450.	I	*	2.20	15
16	-1425.	I	*	2.40	16
17	-1400.	I	*	2.30	17
18	-1375.	I	*	2.35	18
19	-1350.	I	*	2.25	19
20	-1325.	I	*	2.15	20
21	-1300.	I	*	2.05	21
22	-1275.	I	*	2.05	22
23	-1250.	I	*	2.15	23
24	-1225.	I	*	2.05	24
25	-1200.	I	*	1.95	25
26	-1175.	I	*	2.05	26
27	-1150.	I	*	2.15	27
28	-1125.	I	*	2.05	28
29	-1100.	I	*	2.15	29
30	-1075.	I	*	2.15	30
31	-1050.	I	*	2.25	31
32	-1025.	I	*	2.05	32
33	-1000.	I	*	2.45	33

XBOT= -1000.
YMIN= -7.500

YINC= 0.5200E-01
YMAX= 2.700

LINE 2800. F RELATIVE PHASE SHIFT RPS

FORM No. 104

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105

XTOP= -1800.

XINC= 25.00

128106

MOORE PARSON (VA) LIMITED - FORMALINER PARAFLO

1	-1800.	I	*	3.84	1
2	-1775.	I	*	3.54	2
3	-1750.	I	*	3.31	3
4	-1725.	I	*	3.37	4
5	-1700.	I	*	3.16	5
6	-1675.	I	*	3.43	6
7	-1650.	I	*	3.49	7
8	-1625.	I	*	3.27	8
9	-1600.	I	*	3.64	9
10	-1575.	I	*	3.74	10
11	-1550.	I	*	3.27	11
12	-1525.	I	*	3.60	12
13	-1500.	I	*	4.03	13
14	-1475.	I	*	3.58	14
15	-1450.	I	*	3.60	15
16	-1425.	I	*	3.74	16
17	-1400.	I	*	3.64	17
18	-1375.	I	*	3.72	18
19	-1350.	I	*	3.50	19
20	-1325.	I	*	3.35	20
21	-1300.	I	*	3.14	21
22	-1275.	I	*	3.14	22
23	-1250.	I	*	3.00	23
24	-1225.	I	*	3.08	24
25	-1200.	I	*	2.88	25
26	-1175.	I	*	3.03	26
27	-1150.	I	*	3.12	27
28	-1125.	I	*	2.92	28
29	-1100.	I	*	3.06	29
30	-1075.	I	*	3.00	30
31	-1050.	I	*	3.08	31
32	-1025.	I	*	2.75	32
33	-1000.	I	*	3.22	33

XBOT= -1000.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 2800. E SECONDARY FIELD QUADRATURE HSQ/I

FORM No. 11 13

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LINE= 2900.F FREQUENCY=3H7 N001

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

LINE	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RPS	HSQ/I	HSP/I	STATION
				PFE	RPS	PFF	RPS								
1															
2															
3	-1800.N	3.55	0.60	-5.40	6.40	0.75	3.65	0.17	97.65	-2.03	-6.15	2.75	4.06	-10.39	-1800.N
4	-1775.N	3.55	0.59	-5.10	5.90	0.75	3.65	0.18	94.37	-4.96	-5.85	2.25	3.26	-9.72	-1775.N
5	-1750.N	3.55	0.61	-4.90	5.90	0.80	3.65	0.18	95.96	-3.67	-5.70	2.75	3.37	-9.79	-1750.N
6	-1725.N	3.55	0.61	-4.90	5.70	0.80	3.65	0.18	94.46	-5.04	-5.70	2.05	3.07	-9.79	-1725.N
7	-1700.N	3.55	0.62	-4.80	6.00	0.80	3.65	0.18	94.60	-4.98	-5.60	2.35	3.58	-9.78	-1700.N
8	-1675.N	3.55	0.63	-4.30	6.00	0.80	3.70	0.19	94.81	-4.86	-5.10	2.30	3.56	-9.05	-1675.N
9	-1650.N	3.55	0.64	-4.20	6.00	0.80	3.70	0.19	95.09	-4.66	-5.00	2.30	3.62	-9.01	-1650.N
10	-1625.N	3.55	0.64	-4.20	6.00	0.85	3.70	0.19	93.98	-5.78	-5.05	2.30	3.62	-9.10	-1625.N
11	-1600.N	3.55	0.64	-3.90	6.00	0.85	3.70	0.19	92.99	-6.80	-4.75	2.30	3.67	-8.56	-1600.N
12	-1575.N	3.55	0.63	-4.00	6.20	0.85	3.70	0.20	90.67	-9.13	-4.85	2.50	3.87	-8.61	-1575.N
13	-1550.N	3.55	0.65	-3.60	6.10	0.85	3.70	0.20	92.78	-7.13	-4.45	2.40	3.83	-8.15	-1550.N
14	-1525.N	3.55	0.65	-3.50	5.90	0.85	3.70	0.20	92.12	-7.83	-4.35	2.20	3.52	-7.96	-1525.N
15	-1500.N	3.55	0.65	-3.50	6.00	0.90	3.75	0.20	91.59	-8.41	-4.40	2.25	3.59	-8.06	-1500.N
16	-1475.N	3.55	0.66	-3.20	6.00	0.90	3.75	0.20	92.57	-7.46	-4.10	2.25	3.65	-7.62	-1475.N
17	-1450.N	3.55	0.65	-3.10	5.90	0.90	3.75	0.20	90.87	-9.20	-4.00	2.15	3.44	-7.32	-1450.N
18	-1425.N	3.55	0.66	-3.20	6.00	0.90	3.75	0.20	92.09	-7.99	-4.10	2.25	3.65	-7.62	-1425.N
19	-1400.N	3.55	0.65	-3.00	6.00	0.90	3.75	0.20	90.63	-9.46	-3.90	2.25	3.59	-7.14	-1400.N
20	-1375.N	3.55	0.65	-3.10	6.00	0.95	3.75	0.20	90.69	-9.39	-4.05	2.25	3.59	-7.42	-1375.N
21	-1350.N	3.55	0.64	-3.00	5.90	0.95	3.75	0.20	89.47	-10.60	-3.95	2.15	3.38	-7.12	-1350.N
22	-1325.N	3.55	0.63	-3.00	6.00	0.95	3.80	0.20	88.36	-11.68	-3.95	2.20	3.41	-7.01	-1325.N
23	-1300.N	3.55	0.63	-2.90	5.90	0.95	3.80	0.20	88.77	-11.23	-3.85	2.10	3.75	-6.83	-1300.N
24	-1275.N	3.55	0.60	-3.10	6.00	0.95	3.80	0.20	85.03	-14.87	-4.05	2.20	3.24	-6.85	-1275.N
25	-1250.N	3.55	0.62	-3.00	6.00	1.00	3.80	0.20	88.49	-11.35	-4.00	2.20	3.35	-6.99	-1250.N
26	-1225.N	3.55	0.61	-2.90	6.00	1.00	3.80	0.20	87.79	-11.95	-3.90	2.20	3.30	-6.70	-1225.N
27	-1200.N	3.55	0.61	-2.70	5.90	1.00	3.80	0.19	88.63	-11.03	-3.70	2.10	3.15	-6.36	-1200.N
28	-1175.N	3.55	0.60	-2.70	6.00	1.00	3.80	0.19	88.10	-11.41	-3.70	2.20	3.24	-6.25	-1175.N
29	-1150.N	3.55	0.60	-2.80	5.90	1.00	3.85	0.19	89.14	-10.29	-3.80	2.05	3.02	-6.42	-1150.N
30	-1125.N	3.55	0.59	-2.70	5.90	1.05	3.85	0.19	88.79	-10.49	-3.75	2.05	2.97	-6.23	-1125.N
31	-1100.N	3.55	0.57	-3.00	6.00	1.05	3.85	0.18	86.97	-12.03	-4.05	2.15	3.01	-6.50	-1100.N
32	-1075.N	3.55	0.56	-2.70	6.00	1.05	3.85	0.18	86.72	-12.08	-3.75	2.15	2.96	-5.92	-1075.N
33	-1050.N	3.55	0.55	-2.70	6.00	1.05	3.85	0.18	86.52	-12.07	-3.75	2.15	2.91	-5.81	-1050.N
34	-1025.N	3.55	0.55	-2.60	6.20	1.05	3.85	0.18	87.97	-10.59	-3.65	2.35	3.18	-5.65	-1025.N
35	-1000.N	3.55	0.54	-2.70	6.20	1.05	3.85	0.17	87.89	-10.48	-3.75	2.35	3.12	-5.70	-1000.N
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FORM No. 11-13 0143307

XTOP= -1800.

XINC= 25.00

107

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.		* I	-2.03	1
2	-1775.		* I	-4.96	2
3	-1750.		* I	-3.62	3
4	-1725.		* I	-5.04	4
5	-1700.		* I	-4.98	5
6	-1675.		* I	-4.86	6
7	-1650.		* I	-4.66	7
8	-1625.		* I	-5.78	8
9	-1600.		* I	-6.80	9
10	-1575.		* I	-9.13	10
11	-1550.		* I	-7.13	11
12	-1525.		* I	-7.83	12
13	-1500.		* I	-8.41	13
14	-1475.		* I	-7.46	14
15	-1450.		* I	-9.20	15
16	-1425.		* I	-7.99	16
17	-1400.		* I	-9.46	17
18	-1375.		* I	-9.39	18
19	-1350.		* I	-10.60	19
20	-1325.		* I	-11.68	20
21	-1300.		* I	-11.23	21
22	-1275.	*	* I	-14.87	22
23	-1250.		* I	-11.35	23
24	-1225.		* I	-11.95	24
25	-1200.		* I	-11.03	25
26	-1175.		* I	-11.41	26
27	-1150.		* I	-10.29	27
28	-1125.		* I	-10.49	28
29	-1100.		* I	-12.03	29
30	-1075.		* I	-12.08	30
31	-1050.		* I	-12.07	31
32	-1025.		* I	-10.59	32
33	-1000.		* I	-10.48	33

XROT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2900. F MAGNETOMETRIC RESISTIVITY MMR

FORM No 11 11

34					34
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XTOP= -1800.

XINC= 75.00

128109

108

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	*	I	-6.15	1
2	-1775.	*	I	-5.85	2
3	-1750.	*	I	-5.70	3
4	-1725.	*	I	-5.70	4
5	-1700.	*	I	-5.60	5
6	-1675.	*	I	-5.10	6
7	-1650.	*	I	-5.00	7
8	-1625.	*	I	-5.05	8
9	-1600.	*	I	-4.75	9
10	-1575.	*	I	-4.85	10
11	-1550.	*	I	-4.45	11
12	-1525.	*	I	-4.35	12
13	-1500.	*	I	-4.40	13
14	-1475.	*	I	-4.10	14
15	-1450.	*	I	-4.00	15
16	-1425.	*	I	-4.10	16
17	-1400.	*	I	-3.90	17
18	-1375.	*	I	-4.05	18
19	-1350.	*	I	-3.95	19
20	-1325.	*	I	-3.95	20
21	-1300.	*	I	-3.85	21
22	-1275.	*	I	-4.05	22
23	-1250.	*	I	-4.00	23
24	-1225.	*	I	-3.90	24
25	-1200.	*	I	-3.70	25
26	-1175.	*	I	-3.70	26
27	-1150.	*	I	-3.80	27
28	-1125.	*	I	-3.75	28
29	-1100.	*	I	-4.05	29
30	-1075.	*	I	-3.75	30
31	-1050.	*	I	-3.75	31
32	-1025.	*	I	-3.65	32
33	-1000.	*	I	-3.75	33

XBOT= -1000.
YMIN= -6.150

YINC= 0.8650E-01
YMAX= 7.500

LINE 2900. F PERCENT FREQUENCY EFFECT PFF

FORM No. 11 15
013309

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XTOP= -1800.

XINC= 25.00

128110

MOORE PARSON (W.A.) LIMITED - FORMALINER-PARAFIELD

1	-1800.	I	*	2.75	1
2	-1775.	I	*	2.75	2
3	-1750.	I	*	2.25	3
4	-1725.	I	*	2.05	4
5	-1700.	I	*	2.35	5
6	-1675.	I	*	2.30	6
7	-1650.	I	*	2.30	7
8	-1625.	I	*	2.30	8
9	-1600.	I	*	2.30	9
10	-1575.	I	*	2.50	10
11	-1550.	I	*	2.40	11
12	-1525.	I	*	2.20	12
13	-1500.	I	*	2.25	13
14	-1475.	I	*	2.75	14
15	-1450.	I	*	2.15	15
16	-1425.	I	*	2.25	16
17	-1400.	I	*	2.25	17
18	-1375.	I	*	2.25	18
19	-1350.	I	*	2.15	19
20	-1325.	I	*	2.20	20
21	-1300.	I	*	2.10	21
22	-1275.	I	*	2.20	22
23	-1250.	I	*	2.20	23
24	-1225.	I	*	2.20	24
25	-1200.	I	*	2.10	25
26	-1175.	I	*	2.20	26
27	-1150.	I	*	2.05	27
28	-1125.	I	*	2.05	28
29	-1100.	I	*	2.15	29
30	-1075.	I	*	2.15	30
31	-1050.	I	*	2.15	31
32	-1025.	I	*	2.35	32
33	-1000.	I	*	2.35	33

XBOT= -1000.

YINC= 0.5250E-01

YMIN= -2.500

YMAX= 2.750

LINE 2900. F RELATIVE PHASE SHIFT RPS

FORM No. 11-15

XTOP= -1800.

XINC= 75.00

128111

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	1800.	I	*	4.06	1
2	1775.	I	*	3.26	2
3	-1750.	I	*	3.37	3
4	-1775.	I	*	3.07	4
5	-1700.	I	*	3.58	5
6	-1675.	I	*	3.56	6
7	-1650.	I	*	3.62	7
8	-1625.	I	*	3.62	8
9	-1600.	I	*	3.62	9
10	-1575.	I	*	3.87	10
11	-1550.	I	*	3.83	11
12	-1525.	I	*	3.52	12
13	-1500.	I	*	3.59	13
14	-1475.	I	*	3.65	14
15	-1450.	I	*	3.44	15
16	-1425.	I	*	3.65	16
17	-1400.	I	*	3.59	17
18	-1375.	I	*	3.59	18
19	-1350.	I	*	3.38	19
20	-1325.	I	*	3.41	20
21	-1300.	I	*	3.25	21
22	-1275.	I	*	3.24	22
23	-1250.	I	*	3.35	23
24	-1225.	I	*	3.30	24
25	-1200.	I	*	3.15	25
26	-1175.	I	*	3.24	26
27	-1150.	I	*	3.02	27
28	-1125.	I	*	2.97	28
29	-1100.	I	*	3.01	29
30	-1075.	I	*	2.96	30
31	-1050.	I	*	2.91	31
32	-1025.	I	*	3.18	32
33	-1000.	I	*	3.12	33

XBOT= -1000.
YMIN= -10.00

YINC= 0.7000
YMAX= 10.00

LINE 2900. F SECONDARY FIELD QUADRATURE HSD/1

FORM NO. 11-53
10331

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LINE# 3000. F FREQUENCY=3H7 N001

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARALFO

LINE#	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RPS	HSQ/T	HSP/T	STATION			
	STATION	CURRENT	HP	PFF									RPS		
1															
2															
3															
4	-1800. N	3.55	0.57	-6.10	6.40	0.75	3.65	0.18	91.75	-7.77	-6.85	2.75	3.85	-11.00	-1800. N
5	-1775. N	3.55	0.57	-5.40	6.30	0.75	3.65	0.18	90.00	-8.92	-6.15	2.65	3.71	-9.87	-1775. N
6	-1750. N	3.55	0.59	-5.40	6.30	0.75	3.60	0.18	91.46	-7.76	-6.15	2.70	3.92	-10.27	-1750. N
7	-1725. N	3.55	0.60	-5.30	6.30	0.70	3.60	0.18	91.39	-7.96	-6.00	2.70	3.98	-10.14	-1725. N
8	-1700. N	3.55	0.60	-4.50	6.20	0.70	3.60	0.19	89.89	-9.50	-5.70	2.60	3.83	-8.79	-1700. N
9	-1675. N	3.55	0.62	-4.30	6.00	0.70	3.60	0.19	91.46	-8.16	-5.00	2.40	3.66	-8.73	-1675. N
10	-1650. N	3.55	0.63	-4.30	6.20	0.70	3.60	0.19	91.60	-8.14	-5.00	2.60	4.03	-8.87	-1650. N
11	-1625. N	3.55	0.64	-4.00	6.00	0.70	3.60	0.20	91.82	-8.03	-4.70	2.40	3.78	-8.47	-1625. N
12	-1600. N	3.55	0.64	-4.00	6.00	0.65	3.60	0.20	90.77	-9.77	-4.65	2.40	3.78	-8.38	-1600. N
13	-1575. N	3.55	0.65	-4.00	6.00	0.65	3.55	0.20	91.14	-8.90	-4.65	2.45	3.91	-8.51	-1575. N
14	-1550. N	3.55	0.66	-3.90	5.90	0.65	3.55	0.20	91.67	-8.45	-4.55	2.35	3.81	-8.46	-1550. N
15	-1525. N	3.55	0.66	-3.70	6.00	0.65	3.55	0.20	90.93	-9.77	-4.35	2.45	3.97	-8.09	-1525. N
16	-1500. N	3.55	0.66	-3.70	5.90	0.65	3.55	0.21	90.32	-9.96	-4.35	2.35	3.81	-8.09	-1500. N
17	-1475. N	3.55	0.66	-3.60	5.70	0.60	3.55	0.21	89.85	-10.50	-4.70	2.15	3.49	-7.81	-1475. N
18	-1450. N	3.55	0.65	-3.70	5.80	0.60	3.55	0.21	88.15	-12.30	-3.80	2.25	3.59	-6.96	-1450. N
19	-1425. N	3.55	0.66	-3.70	5.80	0.60	3.55	0.21	89.31	-11.13	-3.80	2.25	3.65	-7.06	-1425. N
20	-1400. N	3.55	0.66	-3.00	5.70	0.60	3.55	0.21	89.74	-11.21	-3.60	2.15	3.49	-6.69	-1400. N
21	-1375. N	3.55	0.64	-3.00	5.60	0.60	3.50	0.21	86.60	-13.95	-3.60	2.10	3.30	-6.49	-1375. N
22	-1350. N	3.55	0.65	-3.70	5.70	0.55	3.50	0.21	88.15	-12.30	-3.75	2.20	3.57	-6.87	-1350. N
23	-1325. N	3.55	0.64	-3.40	5.80	0.55	3.50	0.21	87.13	-13.32	-3.95	2.30	3.62	-7.12	-1325. N
24	-1300. N	3.55	0.63	-2.90	5.60	0.55	3.50	0.21	86.72	-14.19	-3.45	2.10	3.25	-6.12	-1300. N
25	-1275. N	3.55	0.63	-3.00	5.70	0.55	3.50	0.20	86.80	-13.50	-3.55	2.20	3.41	-6.30	-1275. N
26	-1250. N	3.55	0.63	-3.20	5.90	0.55	3.50	0.20	87.50	-12.67	-3.75	2.40	3.72	-6.65	-1250. N
27	-1225. N	3.55	0.62	-3.70	6.00	0.50	3.50	0.20	86.94	-13.12	-3.70	2.50	3.81	-6.46	-1225. N
28	-1200. N	3.55	0.62	-3.00	5.70	0.50	3.50	0.20	87.88	-12.04	-3.50	2.20	3.35	-6.11	-1200. N
29	-1175. N	3.55	0.61	-3.00	5.70	0.50	3.45	0.20	87.52	-12.75	-3.50	2.25	3.37	-6.01	-1175. N
30	-1150. N	3.55	0.61	-3.10	5.80	0.50	3.45	0.19	88.69	-10.96	-3.60	2.35	3.52	-6.19	-1150. N
31	-1125. N	3.55	0.59	-3.30	5.90	0.50	3.45	0.19	87.03	-12.38	-3.80	2.45	3.55	-6.32	-1125. N
32	-1100. N	3.55	0.57	-3.70	6.00	0.45	3.45	0.19	85.40	-13.73	-3.65	2.55	3.57	-5.86	-1100. N
33	-1075. N	3.55	0.57	-2.80	5.70	0.45	3.45	0.18	86.82	-12.18	-3.25	2.75	3.15	-5.22	-1075. N
34	-1050. N	3.55	0.56	-3.10	5.70	0.45	3.45	0.18	86.81	-11.99	-3.55	2.75	3.10	-5.60	-1050. N
35	-1025. N	3.55	0.55	-3.30	5.80	0.45	3.45	0.18	86.84	-11.74	-3.75	2.35	3.18	-5.81	-1025. N
36	-1000. N	3.55	0.54	-2.60	5.10	0.45	3.45	0.18	86.92	-11.44	-3.05	1.65	2.19	-4.64	-1000. N
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FORM No. 11-15

XTOP= -1800.

XINC= 75.00

128113

112

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

1	1800.	*	I	-7.22	1
2	1775.	*	I	-8.92	2
3	1750.	*	I	-7.76	3
4	1725.	*	I	-7.96	4
5	1700.	*	I	-9.50	5
6	1675.	*	I	-8.16	6
7	1650.	*	I	-8.14	7
8	1625.	*	I	-8.03	8
9	1600.	*	I	-9.22	9
10	1575.	*	I	-8.90	10
11	1550.	*	I	-8.45	11
12	1525.	*	I	-9.27	12
13	1500.	*	I	-9.96	13
14	1475.	*	I	-10.50	14
15	1450.	*	I	-12.30	15
16	1425.	*	I	-11.13	16
17	1400.	*	I	-11.71	17
18	1375.	*	I	-13.95	18
19	1350.	*	I	-12.30	19
20	1325.	*	I	-13.32	20
21	1300.	*	I	-14.19	21
22	1275.	*	I	-13.50	22
23	1250.	*	I	-12.67	23
24	1225.	*	I	-13.12	24
25	1200.	*	I	-12.04	25
26	1175.	*	I	-12.25	26
27	1150.	*	I	-10.96	27
28	1125.	*	I	-12.38	28
29	1100.	*	I	-13.73	29
30	1075.	*	I	-12.18	30
31	1050.	*	I	-11.99	31
32	1025.	*	I	-11.74	32
33	1000.	*	I	-11.44	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 3000. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-15
0103313

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XTOP= -1800.

XINC= 25.00

113

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	*			I		-6.85	1
2	-1775.		*		I		-6.15	2
3	-1750.		*		I		-6.15	3
4	-1725.		*		I		-6.00	4
5	-1700.			*	I		-5.20	5
6	-1675.			*	I		-5.00	6
7	-1650.			*	I		-5.00	7
8	-1625.			*	I		-4.70	8
9	-1600.			*	I		-4.65	9
10	-1575.			*	I		-4.65	10
11	-1550.			*	I		-4.55	11
12	-1525.			*	I		-4.35	12
13	-1500.			*	I		-4.35	13
14	-1475.			*	I		-4.20	14
15	-1450.			*	I		-3.80	15
16	-1425.			*	I		-3.80	16
17	-1400.			*	I		-3.60	17
18	-1375.			*	I		-3.60	18
19	-1350.			*	I		-3.75	19
20	-1325.			*	I		-3.95	20
21	-1300.			*	I		-3.45	21
22	-1275.			*	I		-3.55	22
23	-1250.			*	I		-3.75	23
24	-1225.			*	I		-3.70	24
25	-1200.			*	I		-3.50	25
26	-1175.			*	I		-3.50	26
27	-1150.			*	I		-3.60	27
28	-1125.			*	I		-3.80	28
29	-1100.			*	I		-3.65	29
30	-1075.			*	I		-3.25	30
31	-1050.			*	I		-3.55	31
32	-1025.			*	I		-3.75	32
33	-1000.			*	I		-3.05	33

XROT= -1000.

YINC= 0.9350E-01

YMIN= -6.850

YMAX= 2.500

LINE 3000. F PERCENT FREQUENCY EFFECT PFE

FORM No. 11 15

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XTOP= -1800.

XINC= 25.00

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

1	1800.	I	*	2.75	1
2	-1775.	I	*	2.65	2
3	-1750.	I	*	2.70	3
4	-1725.	I	*	2.70	4
5	-1700.	I	*	2.60	5
6	-1675.	I	*	2.40	6
7	-1650.	I	*	2.60	7
8	-1625.	I	*	2.40	8
9	-1600.	I	*	2.40	9
10	-1575.	I	*	2.45	10
11	-1550.	I	*	2.35	11
12	-1525.	I	*	2.45	12
13	-1500.	I	*	2.35	13
14	-1475.	I	*	2.15	14
15	-1450.	I	*	2.25	15
16	-1425.	I	*	2.25	16
17	-1400.	I	*	2.15	17
18	-1375.	I	*	2.10	18
19	-1350.	I	*	2.20	19
20	-1325.	I	*	2.30	20
21	-1300.	I	*	2.10	21
22	-1275.	I	*	2.20	22
23	-1250.	I	*	2.40	23
24	-1225.	I	*	2.50	24
25	-1200.	I	*	2.20	25
26	-1175.	I	*	2.25	26
27	-1150.	I	*	2.35	27
28	-1125.	I	*	2.45	28
29	-1100.	I	*	2.55	29
30	-1075.	I	*	2.25	30
31	-1050.	I	*	2.25	31
32	-1025.	I	*	2.35	32
33	-1000.	I	*	1.65	33

XBOT= -1000.
YMIN= -7.500

YINC= 0.5250E-01
YMAX= 2.750

LINE 3000. F RELATIVE PHASE SHIFT RPS

FORM No. 11-15
0143315

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XTOP= -1800.

XINC= 75.00

128116

115

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	-1800.	I	*	3.85	1
2	-1775.	I	*	3.71	2
3	-1750.	I	*	3.92	3
4	-1725.	I	*	3.98	4
5	-1700.	I	*	3.83	5
6	-1675.	I	*	3.66	6
7	-1650.	I	*	4.03	7
8	-1625.	I	*	3.78	8
9	-1600.	I	*	3.78	9
10	-1575.	I	*	3.91	10
11	-1550.	I	*	3.81	11
12	-1525.	I	*	3.97	12
13	-1500.	I	*	3.81	13
14	-1475.	I	*	3.49	14
15	-1450.	I	*	3.59	15
16	-1425.	I	*	3.65	16
17	-1400.	I	*	3.49	17
18	-1375.	I	*	3.30	18
19	-1350.	I	*	3.52	19
20	-1325.	I	*	3.67	20
21	-1300.	I	*	3.25	21
22	-1275.	I	*	3.41	22
23	-1250.	I	*	3.72	23
24	-1225.	I	*	3.81	24
25	-1200.	I	*	3.35	25
26	-1175.	I	*	3.37	26
27	-1150.	I	*	3.52	27
28	-1125.	I	*	3.55	28
29	-1100.	I	*	3.57	29
30	-1075.	I	*	3.15	30
31	-1050.	I	*	3.10	31
32	-1025.	I	*	3.18	32
33	-1000.	I	*	2.19	33

XBOT= -1000.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3000. F SECONDARY FIELD QUADRATURE HSG/I

FORM No 11-15

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STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RPS	HSQ/I	HSP/I	STATION
			PFF	RPS	PFF	RPS								
-1800. N	3.56	0.56	-8.00	4.80	-1.90	2.00	0.18	88.39	-10.33	-6.10	2.80	3.84	-9.60	-1800. N
-1775. N	3.56	0.58	-7.60	4.60	-1.90	2.00	0.18	89.51	-9.55	-5.70	2.60	3.70	-9.29	-1775. N
-1750. N	3.56	0.60	-7.20	4.40	-1.90	2.00	0.19	90.61	-8.74	-5.30	2.40	3.53	-8.93	-1750. N
-1725. N	3.56	0.62	-7.20	4.30	-1.90	2.00	0.19	91.70	-7.88	-5.30	2.30	3.50	-9.23	-1725. N
-1700. N	3.56	0.62	-6.90	4.40	-1.90	2.00	0.19	89.90	-9.78	-5.00	2.40	3.65	-8.71	-1700. N
-1675. N	3.56	0.63	-6.70	4.30	-1.90	2.00	0.20	89.66	-10.21	-4.80	2.30	3.55	-8.49	-1675. N
-1650. N	3.56	0.65	-6.60	4.20	-1.90	2.00	0.20	90.89	-9.15	-4.70	2.20	3.51	-8.58	-1650. N
-1625. N	3.56	0.65	-6.50	4.10	-1.90	2.00	0.20	89.43	-10.79	-4.60	2.10	3.35	-8.40	-1625. N
-1600. N	3.56	0.65	-6.40	4.10	-1.90	2.00	0.21	88.11	-12.32	-4.50	2.10	3.35	-8.22	-1600. N
-1575. N	3.56	0.67	-6.30	4.20	-1.90	2.00	0.21	89.62	-10.90	-4.40	2.20	3.61	-8.28	-1575. N
-1550. N	3.56	0.67	-6.40	4.20	-1.90	2.00	0.21	88.57	-12.15	-4.50	2.20	3.61	-8.47	-1550. N
-1525. N	3.56	0.67	-6.30	4.10	-1.90	2.00	0.21	87.67	-13.23	-4.40	2.10	3.45	-8.28	-1525. N
-1500. N	3.56	0.68	-6.20	4.20	-1.90	2.00	0.22	88.24	-12.73	-4.30	2.20	3.67	-8.21	-1500. N
-1475. N	3.56	0.68	-6.00	4.20	-1.90	2.00	0.22	87.66	-13.45	-4.10	2.20	3.67	-7.83	-1475. N
-1450. N	3.56	0.67	-6.20	4.20	-1.90	2.00	0.22	85.96	-15.37	-4.30	2.20	3.61	-8.09	-1450. N
-1425. N	3.56	0.67	-6.00	4.00	-1.90	2.00	0.22	85.71	-15.68	-4.10	2.00	3.28	-7.72	-1425. N
-1400. N	3.56	0.67	-6.00	4.10	-1.90	2.00	0.22	85.63	-15.79	-4.10	2.10	3.45	-7.72	-1400. N
-1375. N	3.56	0.65	-6.00	4.10	-1.90	2.00	0.22	83.16	-18.49	-4.10	2.10	3.35	-7.49	-1375. N
-1350. N	3.56	0.65	-6.00	4.20	-1.90	2.00	0.22	83.39	-18.18	-4.10	2.20	3.51	-7.49	-1350. N
-1325. N	3.56	0.64	-5.90	4.20	-1.90	2.00	0.22	82.50	-19.06	-4.00	2.20	3.45	-7.19	-1325. N
-1300. N	3.56	0.63	-6.00	4.20	-1.90	2.00	0.22	81.75	-19.75	-4.10	2.20	3.40	-7.26	-1300. N
-1275. N	3.56	0.62	-6.00	4.20	-1.90	2.00	0.21	81.13	-20.25	-4.10	2.20	3.34	-7.14	-1275. N
-1250. N	3.56	0.60	-6.10	4.50	-1.90	2.00	0.21	79.31	-21.98	-4.20	2.50	3.68	-7.08	-1250. N
-1225. N	3.56	0.60	-5.80	4.10	-1.90	2.00	0.21	80.25	-20.73	-3.90	2.10	3.09	-6.57	-1225. N
-1200. N	3.56	0.59	-6.00	4.40	-1.90	2.00	0.21	79.98	-20.74	-4.10	2.40	3.47	-6.79	-1200. N
-1175. N	3.56	0.57	-6.00	4.40	-1.90	2.00	0.20	78.42	-22.03	-4.10	2.40	3.35	-6.56	-1175. N
-1150. N	3.56	0.56	-6.00	4.30	-1.90	2.00	0.20	78.31	-21.79	-4.10	2.30	3.16	-6.45	-1150. N
-1125. N	3.56	0.56	-5.90	4.40	-1.90	2.00	0.20	79.69	-20.04	-4.00	2.40	3.29	-6.29	-1125. N
-1100. N	3.56	0.54	-5.90	4.50	-1.90	2.00	0.19	78.30	-21.02	-4.00	2.50	3.31	-6.07	-1100. N
-1075. N	3.56	0.52	-6.00	4.50	-1.90	2.00	0.19	76.91	-21.93	-4.10	2.50	3.19	-5.99	-1075. N
-1050. N	3.56	0.52	-6.00	4.50	-1.90	2.00	0.19	78.53	-19.97	-4.10	2.50	3.19	-5.99	-1050. N
-1025. N	3.56	0.51	-5.90	4.50	-1.90	2.00	0.18	78.71	-19.38	-4.00	2.50	3.13	-5.73	-1025. N
-1000. N	3.56	0.50	-6.00	4.40	-1.90	2.00	0.18	78.92	-18.76	-4.10	2.40	2.94	-5.76	-1000. N

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No. 11-15
013337

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XTOP= -1800.

XINC= 25.00

128118

117

MOORE PARSON (W.A.) LIMITED - FORMALINER PARATLO

1	-1800.	*	I	-10.33	1
2	-1775.	*	I	-9.55	2
3	-1750.	*	I	-8.74	3
4	-1725.	*	I	-7.88	4
5	-1700.	*	I	-9.78	5
6	-1675.	*	I	-10.71	6
7	-1650.	*	I	-9.15	7
8	-1625.	*	I	-10.79	8
9	-1600.	*	I	-12.32	9
10	-1575.	*	I	-10.90	10
11	-1550.	*	I	-12.15	11
12	-1525.	*	I	-13.23	12
13	-1500.	*	I	-12.73	13
14	-1475.	*	I	-13.45	14
15	-1450.	*	I	-15.37	15
16	-1425.	*	I	-15.68	16
17	-1400.	*	I	-15.79	17
18	-1375.	*	I	-18.49	18
19	-1350.	*	I	-18.18	19
20	-1325.	*	I	-19.06	20
21	-1300.	*	I	-19.75	21
22	-1275.	*	I	-20.75	22
23	-1250.	*	I	-21.98	23
24	-1225.	*	I	-20.73	24
25	-1200.	*	I	-20.74	25
26	-1175.	*	I	-22.03	26
27	-1150.	*	I	-21.79	27
28	-1125.	*	I	-20.04	28
29	-1100.	*	I	-21.02	29
30	-1075.	*	I	-21.93	30
31	-1050.	*	I	-19.97	31
32	-1025.	*	I	-19.38	32
33	-1000.	*	I	-18.76	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 3100. F MAGNETOMETRIC RESISTIVITY MMR

FORM No 11 13

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XTOP= -1800.

XINC= 75.00

118

FORMALINER PARAFLO

FORM NO. 1145 013349

1	-1800.	*	I	-6.10	1
2	-1775.	*	I	-5.70	2
3	-1750.	*	I	-5.30	3
4	-1725.	*	I	-5.30	4
5	-1700.	*	I	-5.00	5
6	-1675.	*	I	-4.80	6
7	-1650.	*	I	-4.70	7
8	-1625.	*	I	-4.60	8
9	-1600.	*	I	-4.50	9
10	-1575.	*	I	-4.40	10
11	-1550.	*	I	-4.50	11
12	-1525.	*	I	-4.40	12
13	-1500.	*	I	-4.30	13
14	-1475.	*	I	-4.10	14
15	-1450.	*	I	-4.30	15
16	-1425.	*	I	-4.10	16
17	-1400.	*	I	-4.10	17
18	-1375.	*	I	-4.10	18
19	-1350.	*	I	-4.10	19
20	-1325.	*	I	-4.00	20
21	-1300.	*	I	-4.10	21
22	-1275.	*	I	-4.10	22
23	-1250.	*	I	-4.20	23
24	-1225.	*	I	-3.90	24
25	-1200.	*	I	-4.10	25
26	-1175.	*	I	-4.10	26
27	-1150.	*	I	-4.10	27
28	-1125.	*	I	-4.00	28
29	-1100.	*	I	-4.00	29
30	-1075.	*	I	-4.10	30
31	-1050.	*	I	-4.10	31
32	-1025.	*	I	-4.00	32
33	-1000.	*	I	-4.10	33

XBOT= -1000.

YINC= 0.8600E-01

YMIN= -6.100

YMAX= 7.500

LINE 3100.F PERCENT FREQUENCY EFFECT PFE

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XTOP= -1800.

XINC= 25.00

128120

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	I	*	2.80	1
2	-1775.	I	*	2.60	2
3	-1750.	I	*	2.40	3
4	-1725.	I	*	2.30	4
5	-1700.	I	*	2.40	5
6	-1675.	I	*	2.30	6
7	-1650.	I	*	2.20	7
8	-1625.	I	*	2.10	8
9	-1600.	I	*	2.10	9
10	-1575.	I	*	2.20	10
11	-1550.	I	*	2.20	11
12	-1525.	I	*	2.10	12
13	-1500.	I	*	2.20	13
14	-1475.	I	*	2.20	14
15	-1450.	I	*	2.20	15
16	-1425.	I	*	2.00	16
17	-1400.	I	*	2.10	17
18	-1375.	I	*	2.10	18
19	-1350.	I	*	2.20	19
20	-1325.	I	*	2.20	20
21	-1300.	I	*	2.20	21
22	-1275.	I	*	2.20	22
23	-1250.	I	*	2.50	23
24	-1225.	I	*	2.10	24
25	-1200.	I	*	2.40	25
26	-1175.	I	*	2.40	26
27	-1150.	I	*	2.30	27
28	-1125.	I	*	2.40	28
29	-1100.	I	*	2.50	29
30	-1075.	I	*	2.50	30
31	-1050.	I	*	2.50	31
32	-1025.	I	*	2.50	32
33	-1000.	I	*	2.40	33

XBOT= -1000.
YMIN= -2.500

YINC= 0.5300F-01
YMAX= 2.800

LINE 3100. F RELATIVE PHASE SHIFT RPS

M No. 11-15

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XTOP= -1800.

XINC= 25.00

128121

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	1800.	I	*	3.84	1
2	1775.	I	*	3.70	2
3	-1750.	I	*	3.53	3
4	-1725.	I	*	3.50	4
5	-1700.	I	*	3.65	5
6	-1675.	I	*	3.55	6
7	-1650.	I	*	3.51	7
8	-1625.	I	*	3.35	8
9	-1600.	I	*	3.35	9
10	-1575.	I	*	3.61	10
11	-1550.	I	*	3.61	11
12	-1525.	I	*	3.45	12
13	-1500.	I	*	3.67	13
14	-1475.	I	*	3.67	14
15	-1450.	I	*	3.61	15
16	-1425.	I	*	3.28	16
17	-1400.	I	*	3.45	17
18	-1375.	I	*	3.35	18
19	-1350.	I	*	3.51	19
20	-1325.	I	*	3.45	20
21	-1300.	I	*	3.40	21
22	-1275.	I	*	3.34	22
23	-1250.	I	*	3.68	23
24	-1225.	I	*	3.09	24
25	-1200.	I	*	3.47	25
26	-1175.	I	*	3.35	26
27	-1150.	I	*	3.16	27
28	-1125.	I	*	3.29	28
29	-1100.	I	*	3.31	29
30	-1075.	I	*	3.19	30
31	-1050.	I	*	3.19	31
32	-1025.	I	*	3.13	32
33	-1000.	I	*	2.94	33

XBOT= -1000.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3100. E SECONDARY FIELD QUADRATURE HSG/I

FORM No. 11-15
0143301

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LINE= 3400. F FREQUENCY=3H7 N001

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

LINE	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RPS	HSQ/I	HSP/I	STATION	
				PFF	RPS	PFF	RPS									
1																
2																
3	-1800. N	3.55	0.55	-8.20	4.80	-1.95	2.05	0.18	84.28	-14.45	-6.25	2.75	3.72	-9.68	-1800. N	
4	-1775. N	3.55	0.59	-8.00	4.60	-1.95	2.05	0.19	86.43	-13.05	-6.05	2.55	3.70	-10.05	-1775. N	
5	-1750. N	3.55	0.64	-7.80	4.60	-1.95	2.05	0.20	89.59	-10.48	-5.85	2.55	4.01	-10.55	-1750. N	
6	-1725. N	3.55	0.63	-7.60	4.50	-1.95	2.05	0.21	84.26	-16.57	-5.65	2.45	3.79	-10.03	-1725. N	
7	-1700. N	3.55	0.65	-7.40	4.50	-1.95	2.05	0.22	83.08	-18.64	-5.45	2.45	3.91	-9.98	-1700. N	
8	-1675. N	3.55	0.67	-7.10	4.30	-1.95	2.05	0.23	81.89	-20.87	-5.15	2.25	3.71	-9.72	-1675. N	
9	-1650. N	3.55	0.67	-6.30	4.00	-1.95	2.05	0.24	78.38	-26.03	-4.35	1.95	3.21	-8.21	-1650. N	
10	-1625. N	3.55	0.80	-5.90	3.80	-1.95	2.05	0.25	89.71	-12.92	-3.95	1.75	3.44	-8.90	-1625. N	
11	-1600. N	3.55	0.80	-5.80	3.60	-1.95	2.05	0.26	86.16	-18.09	-3.85	1.55	3.05	-8.68	-1600. N	
12	-1575. N	3.55	0.77	-5.80	3.60	-1.95	2.05	0.27	79.86	-27.35	-3.85	1.55	2.93	-8.35	-1575. N	
13	-1550. N	3.55	0.82	-5.60	3.60	-1.95	2.05	0.28	82.16	-25.07	-3.65	1.55	3.17	-8.43	-1550. N	
14	-1525. N	3.55	0.90	-5.40	3.50	-1.95	2.05	0.29	87.46	-18.18	-3.45	1.45	3.21	-8.75	-1525. N	
15	-1500. N	3.55	0.91	-5.40	3.60	-1.95	2.05	0.30	86.15	-20.61	-3.45	1.55	3.47	-8.84	-1500. N	
16	-1475. N	3.55	0.91	-5.50	3.50	-1.95	2.05	0.30	84.36	-23.77	-3.55	1.45	3.24	-9.10	-1475. N	
17	-1450. N	3.55	0.96	-5.30	3.50	-1.95	2.05	0.31	87.63	-19.09	-3.35	1.45	3.42	-9.06	-1450. N	
18	-1425. N	3.55	0.97	-5.40	3.50	-1.95	2.05	0.31	87.71	-19.14	-3.45	1.45	3.46	-9.43	-1425. N	
19	-1400. N	3.55	0.96	-5.30	3.40	-1.95	2.05	0.31	86.54	-21.04	-3.35	1.35	3.19	-9.06	-1400. N	
20	-1375. N	3.55	0.95	-5.30	3.50	-1.95	2.05	0.31	85.91	-21.95	-3.35	1.45	3.39	-8.96	-1375. N	
21	-1350. N	3.55	0.96	-5.00	3.40	-1.95	2.05	0.31	87.63	-19.09	-3.05	1.35	3.19	-8.25	-1350. N	
22	-1325. N	3.55	0.92	-5.40	3.50	-1.95	2.05	0.30	85.28	-22.36	-3.45	1.45	3.28	-8.94	-1325. N	
23	-1300. N	3.55	0.91	-5.30	3.40	-1.95	2.05	0.30	86.15	-20.61	-3.35	1.35	3.02	-8.59	-1300. N	
24	-1275. N	3.55	0.87	-5.40	3.60	-1.95	2.05	0.29	84.54	-22.40	-3.45	1.55	3.31	-8.45	-1275. N	
25	-1250. N	3.55	0.89	-5.00	3.50	-1.95	2.05	0.28	89.18	-15.71	-3.05	1.45	3.17	-7.65	-1250. N	
26	-1225. N	3.55	0.86	-5.00	3.50	-1.95	2.05	0.27	89.20	-14.67	-3.05	1.45	3.07	-7.39	-1225. N	
27	-1200. N	3.55	0.81	-5.40	3.50	-1.95	2.05	0.26	87.24	-16.68	-3.45	1.45	2.89	-7.87	-1200. N	
28	-1175. N	3.55	0.78	-5.30	3.70	-1.95	2.05	0.25	87.47	-15.74	-3.35	1.65	3.16	-7.36	-1175. N	
29	-1150. N	3.55	0.75	-5.50	3.80	-1.95	2.05	0.24	87.74	-14.76	-3.55	1.75	3.23	-7.50	-1150. N	
30	-1125. N	3.55	0.75	-5.30	3.70	-1.95	2.05	0.23	91.67	-9.60	-3.35	1.65	3.04	-7.08	-1125. N	
31	-1100. N	3.55	0.67	-5.70	3.90	-1.95	2.05	0.22	85.64	-15.82	-3.75	1.85	3.05	-7.08	-1100. N	
32	-1075. N	3.55	0.65	-5.90	4.10	-1.95	2.05	0.21	86.94	-13.76	-3.95	2.05	3.28	-7.23	-1075. N	
33	-1050. N	3.55	0.61	-6.00	4.10	-1.95	2.05	0.20	85.39	-14.70	-4.05	2.05	3.07	-6.96	-1050. N	
34	-1025. N	3.55	0.64	-5.50	4.10	-1.95	2.05	0.19	93.75	-6.01	-3.55	2.05	3.22	-6.40	-1025. N	
35	-1000. N	3.55	0.60	-5.70	3.90	-1.95	2.05	0.18	91.94	-7.40	-3.75	1.85	2.73	-6.34	-1000. N	
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FORM No 11 13

XTOP= -1800.

XINC= 25.00

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

122

1	-1800.		*	I	-14.45	1
2	-1775.		*	I	-13.05	2
3	-1750.		*	I	-10.48	3
4	-1725.		*	I	-16.57	4
5	-1700.		*	I	-18.64	5
6	-1675.		*	I	-20.87	6
7	-1650.	*		I	-26.03	7
8	-1625.		*	I	-12.92	8
9	-1600.		*	I	-18.09	9
10	-1575.	*		I	-27.35	10
11	-1550.	*		I	-25.07	11
12	-1525.		*	I	-18.18	12
13	-1500.		*	I	-20.61	13
14	-1475.	*		I	-23.77	14
15	-1450.		*	I	-19.09	15
16	-1425.		*	I	-19.14	16
17	-1400.		*	I	-21.04	17
18	-1375.	*		I	-21.95	18
19	-1350.		*	I	-19.09	19
20	-1325.	*		I	-22.36	20
21	-1300.	*		I	-20.61	21
22	-1275.	*		I	-22.40	22
23	-1250.		*	I	-15.21	23
24	-1225.		*	I	-14.67	24
25	-1200.		*	I	-16.68	25
26	-1175.		*	I	-15.74	26
27	-1150.		*	I	-14.76	27
28	-1125.		*	I	-9.60	28
29	-1100.		*	I	-15.82	29
30	-1075.		*	I	-13.76	30
31	-1050.		*	I	-14.70	31
32	-1025.		*	I	-6.01	32
33	-1000.		*	I	-7.40	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 3400. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-15
0143333

XTOP= -1800.

XINC= 25.00

123

MOORE PARAGON (N.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	*				I		-6.25	1
2	-1775.	*				I		-6.05	2
3	-1750.		*			I		-5.85	3
4	-1725.			*		I		-5.65	4
5	-1700.				*	I		-5.45	5
6	-1675.				*	I		-5.15	6
7	-1650.			*		I		-4.35	7
8	-1625.				*	I		-3.95	8
9	-1600.				*	I		-3.85	9
10	-1575.				*	I		-3.85	10
11	-1550.				*	I		-3.65	11
12	-1525.				*	I		-3.45	12
13	-1500.				*	I		-3.45	13
14	-1475.				*	I		-3.55	14
15	-1450.				*	I		-3.35	15
16	-1425.				*	I		-3.45	16
17	-1400.				*	I		-3.35	17
18	-1375.				*	I		-3.35	18
19	-1350.				*	I		-3.05	19
20	-1325.				*	I		-3.45	20
21	-1300.				*	I		-3.35	21
22	-1275.				*	I		-3.45	22
23	-1250.				*	I		-3.05	23
24	-1225.				*	I		-3.05	24
25	-1200.				*	I		-3.45	25
26	-1175.				*	I		-3.35	26
27	-1150.				*	I		-3.55	27
28	-1125.				*	I		-3.35	28
29	-1100.			*		I		-3.75	29
30	-1075.		*			I		-3.95	30
31	-1050.		*			I		-4.05	31
32	-1025.		*		*	I		-3.55	32
33	-1000.		*			I		-3.75	33

XBOT= -1000.

YINC= 0.8750E-01

YMIN= -6.250

YMAX= 2.500

LINE 3400. F PERCENT FREQUENCY EFFECT PFE

FORM No 11 13

XTOP= -1800.

XINC= 25.00

1	-1800.	I		*	2.75	1
2	-1775.	I		*	2.55	2
3	-1750.	I		*	2.55	3
4	-1725.	I		*	2.45	4
5	-1700.	I		*	2.45	5
6	-1675.	I		*	2.25	6
7	-1650.	I		*	1.95	7
8	-1625.	I		*	1.75	8
9	-1600.	I	*		1.55	9
10	-1575.	I	*		1.55	10
11	-1550.	I	*		1.55	11
12	-1525.	I	*		1.45	12
13	-1500.	I	*		1.55	13
14	-1475.	I	*		1.45	14
15	-1450.	I	*		1.45	15
16	-1425.	I	*		1.45	16
17	-1400.	I	*		1.35	17
18	-1375.	I	*		1.45	18
19	-1350.	I	*		1.35	19
20	-1325.	I	*		1.45	20
21	-1300.	I	*		1.35	21
22	-1275.	I	*		1.55	22
23	-1250.	I	*		1.45	23
24	-1225.	I	*		1.45	24
25	-1200.	I	*		1.45	25
26	-1175.	I	*		1.65	26
27	-1150.	I	*		1.75	27
28	-1125.	I	*		1.65	28
29	-1100.	I	*		1.85	29
30	-1075.	I	*		2.05	30
31	-1050.	I	*		2.05	31
32	-1025.	I	*		2.05	32
33	-1000.	I	*		1.85	33

XBOT= -1000.
YMIN= -2.500

YINC= 0.5250E-01
YMAX= 2.750

LINE 3400. F RELATIVE PHASE SHIFT RPS

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

FORM No. 11-19
013305

XTOP= -1800.

XINC= 75.00

128126

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	I	*	3.72	1
2	-1775.	I	*	3.70	2
3	-1750.	I	*	4.01	3
4	-1725.	I	*	3.79	4
5	-1700.	I	*	3.91	5
6	-1675.	I	*	3.71	6
7	-1650.	I	*	3.21	7
8	-1625.	I	*	3.44	8
9	-1600.	I	*	3.05	9
10	-1575.	I	*	2.93	10
11	-1550.	I	*	3.12	11
12	-1525.	I	*	3.21	12
13	-1500.	I	*	3.47	13
14	-1475.	I	*	3.24	14
15	-1450.	I	*	3.42	15
16	-1425.	I	*	3.46	16
17	-1400.	I	*	3.19	17
18	-1375.	I	*	3.39	18
19	-1350.	I	*	3.19	19
20	-1325.	I	*	3.78	20
21	-1300.	I	*	3.02	21
22	-1275.	I	*	3.31	22
23	-1250.	I	*	3.17	23
24	-1225.	I	*	3.07	24
25	-1200.	I	*	2.89	25
26	-1175.	I	*	3.16	26
27	-1150.	I	*	3.23	27
28	-1125.	I	*	3.04	28
29	-1100.	I	*	3.05	29
30	-1075.	I	*	3.78	30
31	-1050.	I	*	3.07	31
32	-1025.	I	*	3.27	32
33	-1000.	I	*	2.73	33

XBOT= -1000.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3400. F SECONDARY FIELD QUADRATURE HSQ/I

FORM No. 11-13

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128

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

PROGRAM MIP2 . CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

1HZ, 3HZ RRMIP SURVEY M1 PEARSE AREA 1AS 070R ARRAYNO 2

79-1593 2/2

FORM No. 11-15
0103339

128

INTERP TAPE FLAG= 0 GRIDDATA TAPE FLAG= 0

LINE POSITIONING MULTIPLYING FACTOR= 1.0

MODRE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No. 11 15

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UNITS FLAG= 0 CURRENT ELECTRODE CO-ORDS= 2700. E -1400. N 3400. E -1400. N

128129

1 PLOT SCALE= 2500. HN SCALE 10. PFF & RPS SCALE= 1. HSD & HSP SCALE= 1.

2 ORIGIN CO-ORDS= 2690. E -1810. N ARRAY IDENTIFIER= MPOZ ANNOTATION SUPPRESSION FLAG= 0

3 SPLINE INTERVAL = 0.

4 PLOT BASE LEVELS FOR PFF, RPS, HSD, HSP ARE 0.00 0.00 0.00 0.00

5 PLOTTING OPTION FLAG FOLLOW - 1-STRAIGHT PLOT, 2-SPLINE PLOT WHERE APPLICABLE

6	HN	=	0
7	MMR	=	1
8	PFF	=	1
9	RPS	=	1
10	HSD	=	1
11	HSP	=	0

12 FOR HN , MMR 100.00 0.00

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM No. 11-35
0143341

130

XTOP= -1800.

XINC= 25.00

128131

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	-1800.		*	I	-3.56	1
2	-1775.		*	I	-4.37	2
3	-1750.		*	I	-6.55	3
4	-1725.		*	I	-6.10	4
5	-1700.		*	I	-4.32	5
6	-1675.		*	I	-5.86	6
7	-1650.		*	I	-6.01	7
8	-1625.		*	I	-5.41	8
9	-1600.		*	I	-9.35	9
10	-1575.		*	I	-7.12	10
11	-1550.		*	I	-6.69	11
12	-1525.		*	I	-7.34	12
13	-1500.		*	I	-9.03	13
14	-1475.		*	I	-9.05	14
15	-1450.		*	I	-11.38	15
16	-1425.		*	I	-13.32	16
17	-1400.		*	I	-14.19	17
18	-1375.		*	I	-14.65	18
19	-1350.		*	I	-14.71	19
20	-1325.		*	I	-15.72	20
21	-1300.	*	*	I	-17.69	21
22	-1275.	*	*	I	-16.67	22
23	-1250.	*	*	I	-17.35	23
24	-1225.	*	*	I	-15.79	24
25	-1200.	*	*	I	-15.35	25
26	-1175.	*	*	I	-14.07	26
27	-1150.	*	*	I	-14.68	27
28	-1125.	*	*	I	-14.53	28
29	-1100.	*	*	I	-13.66	29
30	-1075.	*	*	I	-12.77	30
31	-1050.	*	*	I	-11.89	31
32	-1025.	*	*	I	-11.03	32
33	-1000.	*	*	I	-10.23	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2700. E MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11 15
0143343

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XTOP= -1800.

XINC= 25.00

128132

181

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	*		I	-2.20	1
2	-1775.	*		I	-2.10	2
3	-1750.	*		I	-1.90	3
4	-1725.	*		I	-1.70	4
5	-1700.	*	*	I	-1.50	5
6	-1675.	*	*	I	-1.50	6
7	-1650.	*	*	I	-1.40	7
8	-1625.	*	*	I	-1.40	8
9	-1600.	*	*	I	-1.40	9
10	-1575.	*	*	I	-1.20	10
11	-1550.	*	*	I	-1.10	11
12	-1525.	*	*	I	-1.10	12
13	-1500.	*	*	I	-1.00	13
14	-1475.	*	*	I	-1.00	14
15	-1450.	*	*	I	-0.90	15
16	-1425.	*	*	I	-1.00	16
17	-1400.	*	*	I	-1.00	17
18	-1375.	*	*	I	-0.90	18
19	-1350.	*	*	I	-1.00	19
20	-1325.	*	*	I	-1.00	20
21	-1300.	*	*	I	-0.90	21
22	-1275.	*	*	I	-0.90	22
23	-1250.	*	*	I	-0.90	23
24	-1225.	*	*	I	-0.90	24
25	-1200.	*	*	I	-0.90	25
26	-1175.	*	*	I	-1.00	26
27	-1150.	*	*	I	-1.00	27
28	-1125.	*	*	I	-0.90	28
29	-1100.	*	*	I	-0.90	29
30	-1075.	*	*	I	-1.00	30
31	-1050.	*	*	I	-1.00	31
32	-1025.	*	*	I	-1.00	32
33	-1000.	*	*	I	-1.00	33

XBOT= -1000.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 2700. F PERCENT FREQUENCY EFFECT PFF

FORM No 11 13

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35						35
36						36
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59						59
60						60

XTOP= -1800.

XINC= 25.00

128133

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

132

1	1800.	I	*	1.10	1
2	1775.	I	*	1.10	2
3	-1750.	I	*	1.00	3
4	-1725.	I	*	0.90	4
5	-1700.	I	*	0.80	5
6	-1675.	I	*	0.80	6
7	-1650.	I	*	0.90	7
8	-1625.	I	*	0.80	8
9	-1600.	I	*	0.80	9
10	-1575.	I	*	0.70	10
11	-1550.	I	*	0.60	11
12	-1525.	I	*	0.75	12
13	-1500.	I	*	0.75	13
14	-1475.	I	*	0.75	14
15	-1450.	I	*	0.65	15
16	-1425.	I	*	0.75	16
17	-1400.	I	*	0.75	17
18	-1375.	I	*	0.75	18
19	-1350.	I	*	0.75	19
20	-1325.	I	*	0.75	20
21	-1300.	I	*	0.85	21
22	-1275.	I	*	0.75	22
23	-1250.	I	*	0.85	23
24	-1225.	I	*	0.85	24
25	-1200.	I	*	0.85	25
26	-1175.	I	*	0.85	26
27	-1150.	I	*	0.75	27
28	-1125.	I	*	0.85	28
29	-1100.	I	*	0.85	29
30	-1075.	I	*	0.95	30
31	-1050.	I	*	0.95	31
32	-1025.	I	*	1.05	32
33	-1000.	I	*	0.95	33

XBOT= -1000.
YMIN= -7.500

YINC= 0.5000E-01
YMAX= 7.500

LINE 2700. F RELATIVE PHASE SHIFT RPS

FORM No. 11 13
0103345

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XTOP= -1800.

XINC= 25.00

128134

133

MOORE PARASON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	I	*	2.09	1
2	-1775.	I	*	2.15	2
3	-1750.	I	*	1.98	3
4	-1725.	I	*	1.87	4
5	-1700.	I	*	1.77	5
6	-1675.	I	*	1.80	6
7	-1650.	I	*	2.09	7
8	-1625.	I	*	1.94	8
9	-1600.	I	*	1.91	9
10	-1575.	I	*	1.76	10
11	-1550.	I	*	1.56	11
12	-1525.	I	*	1.98	12
13	-1500.	I	*	1.98	13
14	-1475.	I	*	2.01	14
15	-1450.	I	*	1.71	15
16	-1425.	I	*	1.95	16
17	-1400.	I	*	1.93	17
18	-1375.	I	*	1.92	18
19	-1350.	I	*	1.91	19
20	-1325.	I	*	1.86	20
21	-1300.	I	*	2.03	21
22	-1275.	I	*	1.77	22
23	-1250.	I	*	1.95	23
24	-1225.	I	*	1.93	24
25	-1200.	I	*	1.88	25
26	-1175.	I	*	1.85	26
27	-1150.	I	*	1.56	27
28	-1125.	I	*	1.70	28
29	-1100.	I	*	1.65	29
30	-1075.	I	*	1.79	30
31	-1050.	I	*	1.73	31
32	-1025.	I	*	1.85	32
33	-1000.	I	*	1.62	33

XBOT= -1000.

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 2700. F SECONDARY FIELD QUADRATURE HSO/I

FORM No 11 15

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LINE	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RFS	HSG/I	HSP/I	STATION
				PFF	RFS	PFF	RFS								
1															
2															
3	-1800. N	4.50	0.98	-0.50	3.60	2.15	2.55	0.23	94.37	-3.90	-2.65	1.05	2.00	-5.77	-1800. N
4	-1775. N	4.50	1.03	-0.40	3.50	2.15	2.55	0.24	95.49	-3.24	-2.55	0.95	1.90	-5.84	-1775. N
5	-1750. N	4.50	1.06	0.00	3.30	2.15	2.55	0.25	94.71	-3.94	-2.15	0.75	1.54	-5.06	-1750. N
6	-1725. N	4.50	1.09	0.10	3.30	2.15	2.55	0.26	93.99	-4.65	-2.05	0.75	1.59	-4.97	-1725. N
7	-1700. N	4.50	1.11	0.20	3.20	2.15	2.55	0.27	92.50	-6.00	-1.95	0.65	1.40	-4.81	-1700. N
8	-1675. N	4.50	1.15	0.50	3.30	2.15	2.55	0.28	92.77	-5.97	-1.65	0.75	1.67	-4.27	-1675. N
9	-1650. N	4.50	1.19	0.50	3.30	2.15	2.55	0.28	93.11	-5.87	-1.65	0.75	1.73	-4.36	-1650. N
10	-1625. N	4.50	1.23	0.50	3.30	2.15	2.55	0.29	93.53	-5.67	-1.65	0.75	1.79	-4.51	-1625. N
11	-1600. N	4.50	1.27	0.50	3.30	2.15	2.55	0.30	94.07	-5.33	-1.65	0.75	1.85	-4.66	-1600. N
12	-1575. N	4.50	1.28	0.60	3.20	2.15	2.55	0.31	92.59	-6.83	-1.55	0.65	1.61	-4.41	-1575. N
13	-1550. N	4.50	1.31	0.70	3.20	2.15	2.55	0.31	92.79	-6.78	-1.45	0.65	1.65	-4.22	-1550. N
14	-1537. N	4.50	1.32	0.60	3.20	2.15	2.55	0.32	92.59	-7.04	-1.55	0.65	1.66	-4.55	-1537. N
15	-1525. N	4.50	1.33	0.60	3.20	2.15	2.55	0.32	92.52	-7.17	-1.55	0.65	1.68	-4.58	-1525. N
16	-1512. N	4.50	1.33	0.60	3.20	2.20	2.55	0.32	91.76	-7.97	-1.60	0.65	1.68	-4.73	-1512. N
17	-1500. N	4.50	1.34	0.80	3.20	2.20	2.55	0.32	91.81	-7.96	-1.40	0.65	1.69	-4.17	-1500. N
18	-1487. N	4.50	1.35	0.80	3.20	2.20	2.55	0.33	91.89	-7.94	-1.40	0.65	1.70	-4.20	-1487. N
19	-1475. N	4.50	1.33	0.60	3.20	2.20	2.55	0.33	90.05	-9.79	-1.60	0.65	1.68	-4.73	-1475. N
20	-1462. N	4.50	1.34	0.70	3.20	2.20	2.55	0.33	90.29	-9.61	-1.50	0.65	1.69	-4.47	-1462. N
21	-1450. N	4.50	1.34	0.80	3.20	2.20	2.55	0.33	89.95	-9.98	-1.40	0.65	1.69	-4.17	-1450. N
22	-1437. N	4.50	1.36	0.80	3.20	2.20	2.55	0.33	91.01	-8.95	-1.40	0.65	1.71	-4.23	-1437. N
23	-1425. N	4.50	1.30	0.80	3.10	2.20	2.55	0.33	86.82	-13.16	-1.40	0.55	1.39	-4.04	-1425. N
24	-1412. N	4.50	1.34	0.90	3.20	2.20	2.55	0.33	89.37	-10.63	-1.30	0.65	1.69	-3.87	-1412. N
25	-1400. N	4.50	1.31	0.90	3.30	2.20	2.55	0.33	87.33	-12.67	-1.30	0.75	1.91	-3.78	-1400. N
26	-1387. N	4.50	1.33	0.80	3.20	2.20	2.55	0.33	88.71	-11.29	-1.40	0.65	1.68	-4.14	-1387. N
27	-1375. N	4.50	1.31	0.80	3.20	2.20	2.55	0.33	87.48	-12.49	-1.40	0.65	1.65	-4.08	-1375. N
28	-1362. N	4.50	1.31	0.90	3.30	2.20	2.55	0.33	87.68	-12.27	-1.30	0.75	1.91	-3.78	-1362. N
29	-1350. N	4.50	1.28	0.90	3.20	2.20	2.55	0.33	85.93	-13.98	-1.30	0.65	1.61	-3.70	-1350. N
30	-1325. N	4.50	1.27	1.00	3.20	2.25	2.55	0.33	85.99	-13.79	-1.25	0.65	1.60	-3.53	-1325. N
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MOORE PARAGON (W.A.) LIMITED - FORMALINER BARAFLO

FORM No. 11-15
0103367

XTOP= -1800.

XINC= 75.00

128137

136

MOORE PARSONS (WA) LIMITED - FORMALINER PARAFLO

1	-1800.	*	I	-3.56	1
2	-1775.	*	I	-4.37	2
3	-1750.	*	I	-6.55	3
4	-1725.	*	I	-6.10	4
5	-1700.	*	I	-4.32	5
6	-1675.	*	I	-5.86	6
7	-1650.	*	I	-6.01	7
8	-1625.	*	I	-5.41	8
9	-1600.	*	I	-9.35	9
10	-1575.	*	I	-7.12	10
11	-1550.	*	I	-6.69	11
12	-1525.	*	I	-7.34	12
13	-1500.	*	I	-9.03	13
14	-1475.	*	I	-9.05	14
15	-1450.	*	I	-11.38	15
16	-1425.	*	I	-13.32	16
17	-1400.	*	I	-14.19	17
18	-1375.	*	I	-14.65	18
19	-1350.	*	I	-14.71	19
20	-1325.	*	I	-15.72	20
21	-1300.	*	I	-17.69	21
22	-1275.	*	I	-16.67	22
23	-1250.	*	I	-17.35	23
24	-1225.	*	I	-15.79	24
25	-1200.	*	I	-15.35	25
26	-1175.	*	I	-14.07	26
27	-1150.	*	I	-14.68	27
28	-1125.	*	I	-14.53	28
29	-1100.	*	I	-13.66	29
30	-1075.	*	I	-12.77	30
31	-1050.	*	I	-11.89	31
32	-1025.	*	I	-11.03	32
33	-1000.	*	I	-10.23	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2700. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-15
013349

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137

XTOP= -1800.

XINC= 75.00

128138

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.	*	I	-2.20	1
2	-1775.	*	I	-2.10	2
3	-1750.	*	I	-1.90	3
4	-1725.	*	I	-1.70	4
5	-1700.	*	I	-1.50	5
6	-1675.	*	I	-1.50	6
7	-1650.	*	I	-1.40	7
8	-1625.	*	I	-1.40	8
9	-1600.	*	I	-1.40	9
10	-1575.	*	I	-1.20	10
11	-1550.	*	I	-1.10	11
12	-1525.	*	I	-1.10	12
13	-1500.	*	I	-1.00	13
14	-1475.	*	I	-1.00	14
15	-1450.	*	I	-0.90	15
16	-1425.	*	I	-1.00	16
17	-1400.	*	I	-1.00	17
18	-1375.	*	I	-0.90	18
19	-1350.	*	I	-1.00	19
20	-1325.	*	I	-1.00	20
21	-1300.	*	I	-0.90	21
22	-1275.	*	I	-0.90	22
23	-1250.	*	I	-0.90	23
24	-1225.	*	I	-0.90	24
25	-1200.	*	I	-0.90	25
26	-1175.	*	I	-1.00	26
27	-1150.	*	I	-1.00	27
28	-1125.	*	I	-0.90	28
29	-1100.	*	I	-0.90	29
30	-1075.	*	I	-1.00	30
31	-1050.	*	I	-1.00	31
32	-1025.	*	I	-1.00	32
33	-1000.	*	I	-1.00	33

XBOT= -1000.

YMIN= -2.500

YINC= 0.5000E-01

YMAX= 2.500

LINE 7700. F PERCENT FREQUENCY EFFECT PFF

FORM No. 11-15

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138

XTOP= -1800.

XINC= 75.00

128139

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	1800.	I	*	1.10	1
2	1775.	I	*	1.10	2
3	1750.	I	*	1.00	3
4	1725.	I	*	0.90	4
5	1700.	I	*	0.80	5
6	1675.	I	*	0.80	6
7	1650.	I	*	0.90	7
8	1625.	I	*	0.80	8
9	1600.	I	*	0.80	9
10	1575.	I	*	0.70	10
11	1550.	I	*	0.60	11
12	1525.	I	*	0.75	12
13	1500.	I	*	0.75	13
14	1475.	I	*	0.75	14
15	1450.	I	*	0.65	15
16	1425.	I	*	0.75	16
17	1400.	I	*	0.75	17
18	1375.	I	*	0.75	18
19	1350.	I	*	0.75	19
20	1325.	I	*	0.75	20
21	1300.	I	*	0.85	21
22	1275.	I	*	0.75	22
23	1250.	I	*	0.85	23
24	1225.	I	*	0.85	24
25	1200.	I	*	0.85	25
26	1175.	I	*	0.85	26
27	1150.	I	*	0.75	27
28	1125.	I	*	0.85	28
29	1100.	I	*	0.85	29
30	1075.	I	*	0.95	30
31	1050.	I	*	0.95	31
32	1025.	I	*	1.05	32
33	1000.	I	*	0.95	33

XBOT= -1000.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 2700. E RELATIVE PHASE SHIFT RPS

FORM No. 11 13
0103301

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XTOP= -1800.

XINC= 25.00

128140

689

MOORE PAKSON (WAI) LIMITED - FORMALINER PARAS

1	1800.	I	*	2.09	1
2	-1775.	I	*	2.15	2
3	-1750.	I	*	1.98	3
4	-1725.	I	*	1.87	4
5	-1700.	I	*	1.77	5
6	-1675.	I	*	1.80	6
7	-1650.	I	*	2.09	7
8	-1625.	I	*	1.94	8
9	-1600.	I	*	1.91	9
10	-1575.	I	*	1.76	10
11	-1550.	I	*	1.56	11
12	-1525.	I	*	1.98	12
13	-1500.	I	*	1.98	13
14	-1475.	I	*	2.01	14
15	-1450.	I	*	1.71	15
16	-1425.	I	*	1.95	16
17	-1400.	I	*	1.93	17
18	-1375.	I	*	1.92	18
19	-1350.	I	*	1.91	19
20	-1325.	I	*	1.86	20
21	-1300.	I	*	2.03	21
22	-1275.	I	*	1.77	22
23	-1250.	I	*	1.95	23
24	-1225.	I	*	1.93	24
25	-1200.	I	*	1.88	25
26	-1175.	I	*	1.85	26
27	-1150.	I	*	1.56	27
28	-1125.	I	*	1.70	28
29	-1100.	I	*	1.65	29
30	-1075.	I	*	1.79	30
31	-1050.	I	*	1.73	31
32	-1025.	I	*	1.85	32
33	-1000.	I	*	1.62	33

XBOT= -1000.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 2700. F SECONDARY FIELD QUADRATURE HSG/I

FORM No 11 15

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LINE	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSP/I	HSP/I	STATION	
				PFE	RPS	PFE	RPS									
1																
2																
3	-1800. N	4.50	0.98	0.50	3.60	2.15	2.55	0.23	94.37	-3.90	-2.65	1.05	2.00	-5.77	-1800. N	
4	-1775. N	4.50	1.03	-0.40	3.50	2.15	2.55	0.24	95.49	-3.24	-2.55	0.95	1.90	-5.84	-1775. N	
5	-1750. N	4.50	1.06	0.00	3.30	2.15	2.55	0.25	94.71	-3.94	-2.15	0.75	1.54	-5.06	-1750. N	
6	-1725. N	4.50	1.09	0.10	3.30	2.15	2.55	0.26	93.99	-4.65	-2.05	0.75	1.59	-4.97	-1725. N	
7	-1700. N	4.50	1.11	0.20	3.20	2.15	2.55	0.27	92.50	-6.00	-1.95	0.65	1.40	-4.81	-1700. N	
8	-1675. N	4.50	1.15	0.50	3.30	2.15	2.55	0.28	92.77	-5.97	-1.65	0.75	1.67	-4.27	-1675. N	
9	-1650. N	4.50	1.19	0.50	3.30	2.15	2.55	0.28	93.11	-5.87	-1.65	0.75	1.73	-4.36	-1650. N	
10	-1625. N	4.50	1.23	0.50	3.30	2.15	2.55	0.29	93.53	-5.67	-1.65	0.75	1.79	-4.51	-1625. N	
11	-1600. N	4.50	1.27	0.50	3.30	2.15	2.55	0.30	94.07	-5.33	-1.65	0.75	1.85	-4.66	-1600. N	
12	-1575. N	4.50	1.28	0.60	3.20	2.15	2.55	0.31	92.59	-6.83	-1.55	0.65	1.61	-4.41	-1575. N	
13	-1550. N	4.50	1.31	0.70	3.20	2.15	2.55	0.31	92.79	-6.78	-1.45	0.65	1.65	-4.27	-1550. N	
14	-1537. N	4.50	1.32	0.60	3.20	2.15	2.55	0.32	92.59	-7.04	-1.55	0.65	1.66	-4.55	-1537. N	
15	-1525. N	4.50	1.33	0.60	3.20	2.15	2.55	0.32	92.52	-7.17	-1.55	0.65	1.68	-4.58	-1525. N	
16	-1512. N	4.50	1.33	0.60	3.20	2.20	2.55	0.32	91.76	-7.97	-1.60	0.65	1.68	-4.73	-1512. N	
17	-1500. N	4.50	1.34	0.80	3.20	2.20	2.55	0.32	91.81	-7.96	-1.40	0.65	1.69	-4.17	-1500. N	
18	-1487. N	4.50	1.35	0.80	3.20	2.20	2.55	0.33	91.89	-7.94	-1.40	0.65	1.70	-4.20	-1487. N	
19	-1475. N	4.50	1.33	0.60	3.20	2.20	2.55	0.33	90.05	-9.79	-1.60	0.65	1.68	-4.73	-1475. N	
20	-1462. N	4.50	1.34	0.70	3.20	2.20	2.55	0.33	90.29	-9.61	-1.50	0.65	1.69	-4.47	-1462. N	
21	-1450. N	4.50	1.34	0.80	3.20	2.20	2.55	0.33	89.95	-9.98	-1.40	0.65	1.69	-4.17	-1450. N	
22	-1437. N	4.50	1.36	0.80	3.20	2.20	2.55	0.33	91.01	-8.95	-1.40	0.65	1.71	-4.23	-1437. N	
23	-1425. N	4.50	1.30	0.80	3.10	2.20	2.55	0.33	86.82	-13.16	-1.40	0.55	1.39	-4.04	-1425. N	
24	-1412. N	4.50	1.34	0.90	3.20	2.20	2.55	0.33	89.37	-10.63	-1.30	0.65	1.69	-3.87	-1412. N	
25	-1400. N	4.50	1.31	0.90	3.30	2.20	2.55	0.33	87.33	-12.67	-1.30	0.75	1.91	-3.78	-1400. N	
26	-1387. N	4.50	1.33	0.80	3.20	2.20	2.55	0.33	88.71	-11.29	-1.40	0.65	1.68	-4.14	-1387. N	
27	-1375. N	4.50	1.31	0.80	3.20	2.20	2.55	0.33	87.48	-12.49	-1.40	0.65	1.65	-4.08	-1375. N	
28	-1362. N	4.50	1.31	0.90	3.30	2.20	2.55	0.33	87.68	-12.27	-1.30	0.75	1.91	-3.78	-1362. N	
29	-1350. N	4.50	1.28	0.90	3.20	2.20	2.55	0.33	85.93	-13.98	-1.30	0.65	1.61	-3.70	-1350. N	
30	-1325. N	4.50	1.27	1.00	3.20	2.25	2.55	0.33	85.99	-13.79	-1.25	0.65	1.60	-3.53	-1325. N	
31	-1300. N	4.50	1.24	1.00	3.20	2.25	2.55	0.32	84.96	-14.63	-1.25	0.65	1.56	-3.44	-1300. N	
32	-1275. N	4.50	1.23	0.90	3.20	2.25	2.55	0.32	85.56	-13.84	-1.35	0.65	1.55	-3.69	-1275. N	
33	-1250. N	4.50	1.21	1.00	3.30	2.25	2.55	0.31	85.71	-13.45	-1.25	0.75	1.76	-3.36	-1250. N	
34	-1225. N	4.50	1.17	1.10	3.30	2.25	2.55	0.31	84.64	-14.16	-1.15	0.75	1.70	-2.99	-1225. N	
35	-1200. N	4.50	1.13	1.10	3.30	2.25	2.55	0.30	83.70	-14.67	-1.15	0.75	1.64	-2.89	-1200. N	
36	-1175. N	4.50	1.11	1.10	3.30	2.25	2.55	0.29	84.41	-13.67	-1.15	0.75	1.61	-2.84	-1175. N	
37	-1150. N	4.50	1.08	1.00	3.40	2.25	2.55	0.28	84.50	-13.21	-1.25	0.85	1.78	-3.00	-1150. N	
38	-1125. N	4.50	1.05	0.90	3.30	2.25	2.55	0.28	84.70	-12.64	-1.35	0.75	1.53	-3.15	-1125. N	
39	-1100. N	4.50	1.02	1.00	3.40	2.25	2.55	0.27	85.00	-12.00	-1.25	0.85	1.68	-2.83	-1100. N	
40	-1075. N	4.50	0.99	0.80	3.20	2.25	2.55	0.26	85.36	-11.32	-1.45	0.65	1.25	-3.19	-1075. N	
41	-1050. N	4.50	0.95	0.70	3.30	2.25	2.55	0.25	84.88	-11.28	-1.55	0.75	1.38	-3.27	-1050. N	
42	-1025. N	4.50	0.91	0.70	3.40	2.25	2.55	0.24	84.36	-11.24	-1.55	0.85	1.50	-3.13	-1025. N	
43	-1000. N	4.50	0.88	0.80	3.40	2.25	2.55	0.23	84.74	-10.56	-1.45	0.85	1.45	-2.84	-1000. N	
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MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM No. 11-15
0143353

XTOP= -1800.

XINC= 25.00

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

141

1	-1800.	*	I	-3.90	1
2	-1775.	*	I	-3.24	2
3	-1750.	*	I	-3.94	3
4	-1725.	*	I	-4.65	4
5	-1700.	*	I	-6.00	5
6	-1675.	*	I	-5.97	6
7	-1650.	*	I	-5.87	7
8	-1625.	*	I	-5.67	8
9	-1600.	*	I	-5.33	9
10	-1575.	*	I	-6.83	10
11	-1550.	*	I	-6.78	11
12	-1537.	*	I	-7.04	12
13	-1525.	*	I	-7.17	13
14	-1512.	*	I	-7.97	14
15	-1500.	*	I	-7.96	15
16	-1487.	*	I	-7.94	16
17	-1475.	*	I	-9.79	17
18	-1462.	*	I	-9.61	18
19	-1450.	*	I	-9.98	19
20	-1437.	*	I	-8.95	20
21	-1425.	*	I	-13.16	21
22	-1417.	*	I	-10.63	22
23	-1400.	*	I	-12.67	23
24	-1387.	*	I	-11.29	24
25	-1375.	*	I	-12.49	25
26	-1362.	*	I	-12.27	26
27	-1350.	*	I	-13.98	27
28	-1325.	*	I	-13.79	28
29	-1300.	*	I	-14.63	29
30	-1275.	*	I	-13.84	30
31	-1250.	*	I	-13.45	31
32	-1225.	*	I	-14.16	32
33	-1200.	*	I	-14.67	33
34	-1175.	*	I	-13.67	34
35	-1150.	*	I	-13.21	35
36	-1125.	*	I	-12.64	36
37	-1100.	*	I	-12.00	37
38	-1075.	*	I	-11.32	38
39	-1050.	*	I	-11.28	39
40	-1025.	*	I	-11.24	40
41	-1000.	*	I	-10.56	41

XBOT= -1000.

YINC= 1.000

YMIN= -50.00

YMAX= 50.00

LINE 2800. E MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-13

42					42
43					43
44					44
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58					58
59					59
60					60

142

XTOP= -1800.

XINC= 25.00

128143

MOORE PARSON (WA) LIMITED - FORMALINER PARABLO

1	-1800.	*	I	-2.65	1
2	-1775.	*	I	-2.55	2
3	-1750.	*	I	-2.15	3
4	-1725.	*	I	-2.05	4
5	-1700.	*	I	-1.95	5
6	-1675.	*	I	-1.65	6
7	-1650.	*	I	-1.65	7
8	-1625.	*	I	-1.65	8
9	-1600.	*	I	-1.65	9
10	-1575.	*	I	-1.55	10
11	-1550.	*	I	-1.45	11
12	-1525.	*	I	-1.55	12
13	-1500.	*	I	-1.55	13
14	-1475.	*	I	-1.60	14
15	-1450.	*	I	-1.40	15
16	-1425.	*	I	-1.40	16
17	-1400.	*	I	-1.60	17
18	-1375.	*	I	-1.50	18
19	-1350.	*	I	-1.40	19
20	-1325.	*	I	-1.40	20
21	-1300.	*	I	-1.40	21
22	-1275.	*	I	-1.30	22
23	-1250.	*	I	-1.30	23
24	-1225.	*	I	-1.40	24
25	-1200.	*	I	-1.40	25
26	-1175.	*	I	-1.30	26
27	-1150.	*	I	-1.30	27
28	-1125.	*	I	-1.25	28
29	-1100.	*	I	-1.25	29
30	-1075.	*	I	-1.35	30
31	-1050.	*	I	-1.25	31
32	-1025.	*	I	-1.15	32
33	-1000.	*	I	-1.15	33
34	-1175.	*	I	-1.15	34
35	-1150.	*	I	-1.25	35
36	-1125.	*	I	-1.35	36
37	-1100.	*	I	-1.25	37
38	-1075.	*	I	-1.45	38
39	-1050.	*	I	-1.55	39
40	-1025.	*	I	-1.55	40
41	-1000.	*	I	-1.45	41

XBOT= -1000.

YINC= 0.5150E-01

YMIN= -2.650

YMAX= 2.500

LINE 2800. F PERCENT FREQUENCY EFFECT PFF

FORM NO. 11-15 0143355

53 54 55 56 57 58 59 60

XTOP= -1800.

XINC= 25.00

128144

1	-1800.	I	*	1.05
2	-1775.	I	*	0.75
3	-1750.	I	*	0.75
4	-1725.	I	*	0.75
5	-1700.	I	*	0.65
6	-1675.	I	*	0.75
7	-1650.	I	*	0.75
8	-1625.	I	*	0.75
9	-1600.	I	*	0.75
10	-1575.	I	*	0.65
11	-1550.	I	*	0.65
12	-1537.	I	*	0.65
13	-1525.	I	*	0.65
14	-1512.	I	*	0.65
15	-1500.	I	*	0.65
16	-1487.	I	*	0.65
17	-1475.	I	*	0.65
18	-1462.	I	*	0.65
19	-1450.	I	*	0.65
20	-1437.	I	*	0.65
21	-1425.	I	*	0.55
22	-1412.	I	*	0.65
23	-1400.	I	*	0.75
24	-1387.	I	*	0.65
25	-1375.	I	*	0.65
26	-1362.	I	*	0.75
27	-1350.	I	*	0.65
28	-1337.	I	*	0.65
29	-1325.	I	*	0.65
30	-1312.	I	*	0.65
31	-1300.	I	*	0.75
32	-1287.	I	*	0.75
33	-1275.	I	*	0.75
34	-1262.	I	*	0.75
35	-1250.	I	*	0.85
36	-1237.	I	*	0.75
37	-1225.	I	*	0.85
38	-1212.	I	*	0.65
39	-1200.	I	*	0.75
40	-1187.	I	*	0.85
41	-1175.	I	*	0.85

XBOT= -1000.

YINC= 0.5000E-01

YMIN= -2.500

YMAX= 2.500

LINE 2800. E RELATIVE PHASE SHIFT RPS

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No 11-15

XTOP= -1800.

XINC= 25.00

128145

MOORE PARSONS (WA) LIMITED - FORMALINERPARAFLO

1	1800.	I	*	2.00	1
2	1775.	I	*	1.90	2
3	-1750.	I	*	1.54	3
4	-1725.	I	*	1.59	4
5	-1700.	I	*	1.40	5
6	-1675.	I	*	1.67	6
7	-1650.	I	*	1.73	7
8	-1625.	I	*	1.79	8
9	-1600.	I	*	1.85	9
10	-1575.	I	*	1.61	10
11	-1550.	I	*	1.65	11
12	-1537.	I	*	1.66	12
13	-1525.	I	*	1.68	13
14	-1512.	I	*	1.68	14
15	-1500.	I	*	1.69	15
16	-1487.	I	*	1.70	16
17	-1475.	I	*	1.68	17
18	-1462.	I	*	1.69	18
19	-1450.	I	*	1.69	19
20	-1437.	I	*	1.71	20
21	-1425.	I	*	1.39	21
22	-1412.	I	*	1.69	22
23	-1400.	I	*	1.91	23
24	-1387.	I	*	1.68	24
25	-1375.	I	*	1.65	25
26	-1362.	I	*	1.91	26
27	-1350.	I	*	1.61	27
28	-1325.	I	*	1.60	28
29	-1300.	I	*	1.56	29
30	-1275.	I	*	1.55	30
31	-1250.	I	*	1.76	31
32	-1225.	I	*	1.70	32
33	-1200.	I	*	1.64	33
34	-1175.	I	*	1.61	34
35	-1150.	I	*	1.78	35
36	-1125.	I	*	1.53	36
37	-1100.	I	*	1.68	37
38	-1075.	I	*	1.25	38
39	-1050.	I	*	1.38	39
40	-1025.	I	*	1.50	40
41	-1000.	I	*	1.45	41

XBOT= -1000.

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 2800. F SECONDARY FIELD QUADRATURE HSG/I

FORM No. 11-15
0103357

42					42
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145

MOORE PARSON (W.A.) LIMITED - FORMALINER PARAFLO

LINE	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RFS	HSQ/I	HSP/I	STATION	
				PFE	RFS	PFF	RFS									
1																1
2																2
3	-1700. N	4.50	1.09	-1.00	0.60	-0.75	0.30	0.27	90.83	-7.33	-0.75	0.30	0.63	-0.61	-1700. N	3
4	-1675. N	4.50	1.12	-1.00	0.60	-0.75	0.30	0.28	90.35	-7.97	-0.75	0.30	0.65	-0.62	-1675. N	4
5	-1650. N	4.50	1.16	-1.10	0.60	-0.75	0.30	0.28	90.76	-7.87	-0.35	0.30	0.67	-0.90	-1650. N	5
6	-1625. N	4.50	1.19	-1.10	0.50	-0.75	0.30	0.29	90.49	-8.34	-0.35	0.70	0.46	-0.93	-1625. N	6
7	-1600. N	4.50	1.27	-1.10	0.50	-0.75	0.30	0.30	90.37	-8.67	-0.35	0.70	0.47	-0.95	-1600. N	7
8	-1575. N	4.50	1.20	-1.00	0.50	-0.75	0.30	0.31	86.81	-12.16	-0.75	0.70	0.47	-0.67	-1575. N	8
9	-1550. N	4.50	1.26	-1.00	0.60	-0.75	0.35	0.31	89.25	-10.12	-0.75	0.25	0.61	-0.70	-1550. N	9
10	-1525. N	4.50	1.28	-1.00	0.60	-0.75	0.35	0.32	89.04	-10.51	-0.75	0.25	0.62	-0.71	-1525. N	10
11	-1500. N	4.50	1.30	-1.10	0.60	-0.75	0.35	0.32	89.07	-10.63	-0.35	0.75	0.63	-1.01	-1500. N	11
12	-1475. N	4.50	1.26	-1.00	0.70	-0.75	0.35	0.33	85.31	-14.46	-0.75	0.35	0.86	-0.70	-1475. N	12
13	-1450. N	4.50	1.30	-0.90	0.60	-0.75	0.35	0.33	87.27	-12.64	-0.15	0.75	0.63	-0.43	-1450. N	13
14	-1425. N	4.50	1.25	-1.00	0.60	-0.75	0.35	0.33	83.48	-16.49	-0.75	0.25	0.61	-0.69	-1425. N	14
15	-1400. N	4.50	1.25	-1.10	0.50	-0.75	0.35	0.33	83.33	-16.67	-0.35	0.15	0.36	-0.97	-1400. N	15
16	-1375. N	4.50	1.27	-1.10	0.60	-0.75	0.35	0.33	84.81	-15.16	-0.35	0.25	0.62	-0.99	-1375. N	16
17	-1350. N	4.50	1.24	-1.00	0.60	-0.75	0.35	0.33	83.24	-16.64	-0.75	0.75	0.60	-0.69	-1350. N	17
18	-1325. N	4.50	1.23	-1.00	0.60	-0.75	0.35	0.33	83.28	-16.46	-0.75	0.25	0.60	-0.68	-1325. N	18
19	-1300. N	4.50	1.21	-1.00	0.60	-0.75	0.35	0.32	82.91	-16.63	-0.75	0.25	0.59	-0.67	-1300. N	19
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FORM No. 11-15

XTOP= -1700.

XINC= 75.00

128147

1	-1700.		*	I	-7.33	1
2	-1675.		*	I	-7.97	2
3	-1650.		*	I	-7.87	3
4	-1625.		*	I	-8.34	4
5	-1600.		*	I	-8.67	5
6	-1575.		*	I	-12.16	6
7	-1550.		*	I	-10.12	7
8	-1525.		*	I	-10.51	8
9	-1500.		*	I	-10.63	9
10	-1475.		*	I	-14.46	10
11	-1450.		*	I	-12.64	11
12	-1425.	*		I	-16.49	12
13	-1400.	*		I	-16.67	13
14	-1375.	*		I	-15.16	14
15	-1350.	*		I	-16.64	15
16	-1325.	*		I	-16.46	16
17	-1300.	*		I	-16.63	17

XBOT= -1300.

YINC= 1.000

YMIN= -50.00

YMAX= 50.00

LINE 2800. F MAGNETOMETRIC RESESTIVITY MMR

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM No. 11 01
0103359

XTOP= -1700.

XINC= 25.00

128148

147

1	-1700.	*	I	-0.25	1
2	-1675.	*	I	-0.25	2
3	-1650.	*	I	-0.35	3
4	-1625.	*	I	-0.35	4
5	-1600.	*	I	-0.35	5
6	-1575.	*	I	-0.25	6
7	-1550.	*	I	-0.25	7
8	-1525.	*	I	-0.25	8
9	-1500.	*	I	-0.35	9
10	-1475.	*	I	-0.25	10
11	-1450.	*	I	-0.15	11
12	-1425.	*	I	-0.25	12
13	-1400.	*	I	-0.35	13
14	-1375.	*	I	-0.35	14
15	-1350.	*	I	-0.25	15
16	-1325.	*	I	-0.25	16
17	-1300.	*	I	-0.25	17

XBOT= -1300.

YINC= 0.5000E-01

YMIN= -7.500

YMAX= 2.500

LINE 2800. E PERCENT FREQUENCY EFFECT PFE

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No. 11-15

XTOP= -1700.

XINC= 25.00

128149

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	-1700.	I	*	0.30	1
2	-1675.	I	*	0.30	2
3	-1650.	I	*	0.30	3
4	-1625.	I	*	0.20	4
5	-1600.	I	*	0.20	5
6	-1575.	I	*	0.20	6
7	-1550.	I	*	0.25	7
8	-1525.	I	*	0.25	8
9	-1500.	I	*	0.25	9
10	-1475.	I	*	0.35	10
11	-1450.	I	*	0.25	11
12	-1425.	I	*	0.25	12
13	-1400.	I	*	0.15	13
14	-1375.	I	*	0.25	14
15	-1350.	I	*	0.25	15
16	-1325.	I	*	0.25	16
17	-1300.	I	*	0.25	17

XBOT= -1300.

YINC= 0.5000E-01

YMIN= -7.500

YMAX= 7.500

LINE 2800. F RELATIVE PHASE SHIFT RPS

FORM No. 11-15 013301

18					18
19					19
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60					60

XTOP= -1700.

XINC= 25.00

128150

149
-1700.

I *

0.63

-1675.

I *

0.65

-1650.

I *

0.67

-1625.

I *

0.46

-1600.

I *

0.47

-1575.

I *

0.47

-1550.

I *

0.61

-1525.

I *

0.62

-1500.

I *

0.63

-1475.

I *

0.86

-1450.

I *

0.63

-1425.

I *

0.61

-1400.

I *

0.36

-1375.

I *

0.62

-1350.

I *

0.60

-1325.

I *

0.60

-1300.

I *

0.59

XBOT= -1300.

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 2800. E SECONDARY FIELD QUADRATURE H50/1

MOORE PARSONS (W.A.) LIMITED - FORMALINER PARAFLO

FORM No. 11-15

LINE 150

2900. E FREQUENCY=3HZ N002

128151

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

STATION	CURR/FNT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RPS	HSQ/I	HSP/I	STATION
			PFF	RPS	PFF	RPS								
-1800. N	4.50	0.97	-3.20	1.70	-0.85	0.60	0.23	93.87	-4.23	-2.35	1.10	2.07	-5.07	-1800. N
-1775. N	4.50	1.00	-3.00	1.70	-0.85	0.60	0.24	92.98	-5.03	-2.15	1.10	2.13	-4.78	-1775. N
-1750. N	4.50	1.04	-2.80	1.60	-0.85	0.60	0.25	93.00	-5.22	-1.95	1.00	2.02	-4.51	-1750. N
-1725. N	4.50	1.07	-2.70	1.60	-0.85	0.60	0.26	92.12	-6.10	-1.85	1.00	2.07	-4.40	-1725. N
-1700. N	4.50	1.13	-2.70	1.70	-0.85	0.60	0.27	93.79	-4.99	-1.85	1.10	2.41	-4.65	-1700. N
-1675. N	4.50	1.17	-2.60	1.50	-0.85	0.60	0.28	93.76	-5.19	-1.75	0.90	2.04	-4.55	-1675. N
-1650. N	4.50	1.19	-2.40	1.40	-0.85	0.60	0.29	92.24	-6.68	-1.55	0.80	1.85	-4.10	-1650. N
-1625. N	4.50	1.27	-2.50	1.50	-0.85	0.60	0.30	91.65	-7.41	-1.65	0.90	2.13	-4.47	-1625. N
-1600. N	4.50	1.23	-2.40	1.40	-0.85	0.60	0.30	89.77	-9.35	-1.55	0.80	1.91	-4.24	-1600. N
-1575. N	4.50	1.28	-2.20	1.40	-0.85	0.60	0.31	90.99	-8.45	-1.35	0.80	1.99	-3.84	-1575. N
-1550. N	4.50	1.30	-2.20	1.40	-0.85	0.60	0.32	90.26	-9.35	-1.35	0.80	2.02	-3.90	-1550. N
-1525. N	4.50	1.29	-2.00	1.40	-0.85	0.65	0.33	87.75	-12.00	-1.15	0.75	1.88	-3.30	-1525. N
-1500. N	4.50	1.32	-2.00	1.40	-0.85	0.65	0.33	88.27	-11.69	-1.15	0.75	1.92	-3.37	-1500. N
-1475. N	4.50	1.33	-2.00	1.40	-0.85	0.65	0.34	87.74	-12.38	-1.15	0.75	1.93	-3.40	-1475. N
-1450. N	4.50	1.35	-2.00	1.40	-0.85	0.65	0.34	88.20	-12.05	-1.15	0.75	1.96	-3.45	-1450. N
-1425. N	4.50	1.35	-2.00	1.40	-0.85	0.65	0.34	87.67	-12.65	-1.15	0.75	1.96	-3.45	-1425. N
-1400. N	4.50	1.33	-2.00	1.40	-0.85	0.65	0.34	86.20	-14.19	-1.15	0.75	1.93	-3.40	-1400. N
-1375. N	4.50	1.32	-2.00	1.40	-0.85	0.65	0.34	85.73	-14.65	-1.15	0.75	1.92	-3.37	-1375. N
-1350. N	4.50	1.30	-1.90	1.40	-0.85	0.65	0.34	84.93	-15.38	-1.05	0.75	1.89	-3.03	-1350. N
-1325. N	4.50	1.29	-1.90	1.40	-0.85	0.65	0.34	85.11	-15.05	-1.05	0.75	1.88	-3.01	-1325. N
-1300. N	4.50	1.26	-1.90	1.40	-0.85	0.65	0.33	84.26	-15.69	-1.05	0.75	1.83	-2.94	-1300. N
-1275. N	4.50	1.23	-1.90	1.40	-0.85	0.65	0.33	83.67	-16.00	-1.05	0.75	1.79	-2.87	-1275. N
-1250. N	4.50	1.21	-1.90	1.40	-0.85	0.65	0.32	84.01	-15.35	-1.05	0.75	1.76	-2.82	-1250. N
-1225. N	4.50	1.18	-1.90	1.40	-0.85	0.65	0.31	83.88	-15.12	-1.05	0.75	1.72	-2.75	-1225. N
-1200. N	4.50	1.15	-1.90	1.40	-0.85	0.65	0.30	83.93	-14.68	-1.05	0.75	1.67	-2.68	-1200. N
-1175. N	4.50	1.11	-1.90	1.40	-0.85	0.65	0.30	83.39	-14.74	-1.05	0.75	1.61	-2.59	-1175. N
-1150. N	4.50	1.08	-1.90	1.40	-0.85	0.65	0.29	83.71	-14.01	-1.05	0.75	1.57	-2.52	-1150. N
-1125. N	4.50	1.04	-1.80	1.40	-0.85	0.65	0.28	83.34	-13.86	-0.95	0.75	1.51	-2.20	-1125. N
-1100. N	4.50	1.00	-1.90	1.50	-0.85	0.65	0.27	83.00	-13.66	-1.05	0.85	1.65	-2.33	-1100. N
-1075. N	4.50	0.97	-2.00	1.50	-0.85	0.65	0.26	83.51	-12.77	-1.15	0.85	1.60	-2.48	-1075. N
-1050. N	4.50	0.93	-2.00	1.60	-0.85	0.65	0.25	83.16	-12.55	-1.15	0.95	1.71	-2.38	-1050. N
-1025. N	4.50	0.90	-1.90	1.70	-0.85	0.65	0.24	83.68	-11.70	-1.05	1.05	1.83	-2.10	-1025. N
-1000. N	4.50	0.87	-1.90	1.70	-0.85	0.65	0.23	84.19	-10.89	-1.05	1.05	1.77	-2.03	-1000. N

FORM No. 11.15 013303

XTOP= -1800.

XINC= 25.00

151

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-1800.		*	I	-4.73	1
2	-1775.		*	I	-5.03	2
3	-1750.		*	I	-5.22	3
4	-1725.		*	I	-6.10	4
5	-1700.		*	I	-4.99	5
6	-1675.		*	I	-5.19	6
7	-1650.		*	I	-6.68	7
8	-1625.		*	I	-7.41	8
9	-1600.		*	I	-9.35	9
10	-1575.		*	I	-8.45	10
11	-1550.		*	I	-9.35	11
12	-1525.		*	I	-12.00	12
13	-1500.		*	I	-11.69	13
14	-1475.		*	I	-12.38	14
15	-1450.		*	I	-12.05	15
16	-1425.		*	I	-12.65	16
17	-1400.		*	I	-14.19	17
18	-1375.		*	I	-14.65	18
19	-1350.		*	I	-15.38	19
20	-1325.		*	I	-15.05	20
21	-1300.		*	I	-15.69	21
22	-1275.		*	I	-16.00	22
23	-1250.		*	I	-15.35	23
24	-1225.		*	I	-15.12	24
25	-1200.		*	I	-14.68	25
26	-1175.		*	I	-14.74	26
27	-1150.		*	I	-14.01	27
28	-1125.		*	I	-13.86	28
29	-1100.		*	I	-13.66	29
30	-1075.		*	I	-12.77	30
31	-1050.		*	I	-12.55	31
32	-1025.		*	I	-11.70	32
33	-1000.		*	I	-10.89	33

XBOT= -1000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2900. E MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-19

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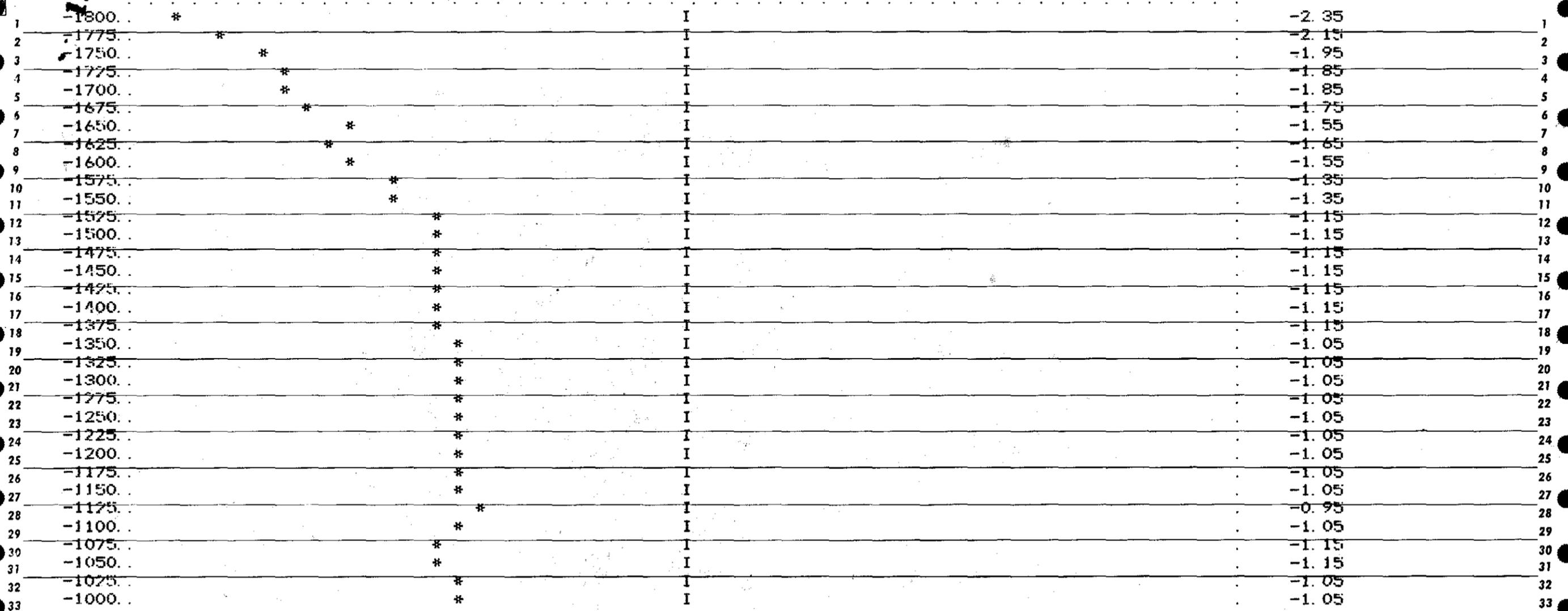
MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

152

XTOP= -1800.

XINC= 25.00

128153



XBOT= -1000.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 2900. F PERCENT FREQUENCY EFFECT PFF

FORM No. 11.15
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XTOP= -1800.

XINC= 25.00

128154

MOORE PARSON (WA) LIMITED - FORMALINER PARAFLO

1	-1800.	I	*	1.10	1
2	-1775.	I	*	1.10	2
3	-1750.	I	*	1.00	3
4	-1725.	I	*	1.00	4
5	-1700.	I	*	1.10	5
6	-1675.	I	*	0.90	6
7	-1650.	I	*	0.80	7
8	-1625.	I	*	0.90	8
9	-1600.	I	*	0.80	9
10	-1575.	I	*	0.80	10
11	-1550.	I	*	0.80	11
12	-1525.	I	*	0.75	12
13	-1500.	I	*	0.75	13
14	-1475.	I	*	0.75	14
15	-1450.	I	*	0.75	15
16	-1425.	I	*	0.75	16
17	-1400.	I	*	0.75	17
18	-1375.	I	*	0.75	18
19	-1350.	I	*	0.75	19
20	-1325.	I	*	0.75	20
21	-1300.	I	*	0.75	21
22	-1275.	I	*	0.75	22
23	-1250.	I	*	0.75	23
24	-1225.	I	*	0.75	24
25	-1200.	I	*	0.75	25
26	-1175.	I	*	0.75	26
27	-1150.	I	*	0.75	27
28	-1125.	I	*	0.75	28
29	-1100.	I	*	0.85	29
30	-1075.	I	*	0.85	30
31	-1050.	I	*	0.95	31
32	-1025.	I	*	1.05	32
33	-1000.	I	*	1.05	33

XBOT= -1000.
YMIN= -2.500

YINC= 0.5000E-01
YMAX= 2.500

LINE 2900. F RELATIVE PHASE SHIFT RPS

FORM No. 11-15

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XTOP=-1800.

XINC= 25.00

154

MOORE PARAGON (WA) L IN 81- FOJ V INER PARAFLO

1	-1800.	I	*	2.07	1
2	-1775.	I	*	2.13	2
3	-1750.	I	*	2.07	3
4	-1725.	I	*	2.07	4
5	-1700.	I	*	2.41	5
6	-1675.	I	*	2.04	6
7	-1650.	I	*	1.85	7
8	-1625.	I	*	2.13	8
9	-1600.	I	*	1.91	9
10	-1575.	I	*	1.99	10
11	-1550.	I	*	2.02	11
12	-1525.	I	*	1.88	12
13	-1500.	I	*	1.92	13
14	-1475.	I	*	1.93	14
15	-1450.	I	*	1.96	15
16	-1425.	I	*	1.96	16
17	-1400.	I	*	1.93	17
18	-1375.	I	*	1.92	18
19	-1350.	I	*	1.89	19
20	-1325.	I	*	1.88	20
21	-1300.	I	*	1.83	21
22	-1275.	I	*	1.79	22
23	-1250.	I	*	1.76	23
24	-1225.	I	*	1.72	24
25	-1200.	I	*	1.67	25
26	-1175.	I	*	1.61	26
27	-1150.	I	*	1.57	27
28	-1125.	I	*	1.51	28
29	-1100.	I	*	1.65	29
30	-1075.	I	*	1.60	30
31	-1050.	I	*	1.71	31
32	-1025.	I	*	1.83	32
33	-1000.	I	*	1.77	33

XBOT=-1000.
YMIN=-10.00

YINC= 0.2000
YMAX= 10.00

LINE 2900. E SECONDARY FIELD QUADRATURE HSG/I

UM No 11.15
0143367

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PROGRAM MIP2 . CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

3HZ RRMIP SURVEY MT PEARSE AREA TASMANIA 063R ARRAY N003

79-1393 Vol 2/2

155

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INTERP TAPE FLAG= 0 GRIDDATA TAPE FLAG= 0

128157

LINE POSITIONING MULTIPLYING FACTOR= 1.0

MOORE PARAGON PARAFIC

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UNITS FLAG= 0 CURRENT ELECTRODE CO-ORDS= 2500. E -1800. N 4350. E -1800. N 128158

PLOT SCALE= 2500. HN SCALE 10. PFE & RPS SCALE= 1. HSQ & HSP SCALE= 1.

ORIGIN CO-ORDS= 3100. E -1300. N ARRAY IDENTIFIER= MP03 ANNOTATION SUPPRESSION FLAG= 0

SPLINE INTERVAL= 0.

PLOT BASE LEVELS FOR PFE, RPS, HSQ, HSP ARE 0.00 0.00 0.00 0.00

PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

HN = 0
MMR = 1
PFE = 0
RPS = 1
HSQ = 1
HSP = 0

FOR HN , MMR 100.00 0.00

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSG/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
-2300 N	3.05	0.38	-9.50	7.00	-1.40	3.35	0.17	74.46	-19.77	-8.10	3.65	3.97	-10.09	-2300 N
-2275 N	3.05	0.40	-9.00	7.00	-1.40	3.35	0.17	76.09	-19.06	-7.60	3.65	4.18	-9.97	-2275 N
-2250 N	3.05	0.45	-7.50	6.00	-1.40	3.40	0.18	83.13	-13.85	-6.10	2.60	3.35	-9.00	-2250 N
-2225 N	3.05	0.39	-7.00	6.50	-1.40	3.40	0.18	69.99	-25.36	-5.60	3.10	3.46	-7.16	-2225 N
-2200 N	3.05	0.45	-7.50	6.00	-1.40	3.40	0.19	78.50	-18.69	-6.10	2.60	3.35	-9.00	-2200 N
-2175 N	3.05	0.47	-7.00	6.00	-1.40	3.45	0.19	79.74	-18.11	-5.60	2.55	3.43	-8.63	-2175 N
-2150 N	3.05	0.47	-7.00	6.00	-1.40	3.45	0.20	77.62	-20.55	-5.60	2.55	3.43	-8.63	-2150 N
-2125 N	3.05	0.48	-7.00	5.80	-1.40	3.45	0.20	77.22	-21.47	-5.60	2.35	3.23	-8.81	-2125 N
-2100 N	3.05	0.50	-6.50	5.50	-1.40	3.50	0.21	78.45	-20.83	-5.10	2.00	2.86	-8.36	-2100 N
-2075 N	3.05	0.51	-6.00	5.50	-1.35	3.50	0.21	78.12	-21.66	-4.65	2.00	2.92	-7.78	-2075 N
-2050 N	3.05	0.54	-6.00	5.50	-1.35	3.50	0.22	80.87	-19.37	-4.65	2.00	3.09	-8.23	-2050 N
-2025 N	3.05	0.55	-5.80	5.50	-1.35	3.55	0.22	80.64	-20.02	-4.45	1.95	3.07	-8.02	-2025 N
-2000 N	3.05	0.54	-5.80	5.50	-1.35	3.55	0.23	77.65	-23.57	-4.45	1.95	3.01	-7.88	-2000 N
-1975 N	3.05	0.56	-5.50	5.00	-1.35	3.55	0.23	79.12	-22.41	-4.15	1.45	2.32	-7.62	-1975 N
-1950 N	3.05	0.57	-5.00	5.00	-1.35	3.60	0.24	79.28	-22.59	-3.65	1.40	2.28	-6.82	-1950 N
-1925 N	3.05	0.58	-5.00	5.00	-1.35	3.60	0.24	79.59	-22.56	-3.65	1.40	2.32	-6.94	-1925 N
-1900 N	3.05	0.59	-5.00	5.00	-1.35	3.60	0.24	80.05	-22.30	-3.65	1.40	2.36	-7.06	-1900 N
-1875 N	3.05	0.60	-5.00	5.00	-1.30	3.65	0.24	80.68	-21.78	-3.70	1.35	2.32	-7.28	-1875 N
-1850 N	3.05	0.62	-4.80	5.00	-1.30	3.65	0.25	82.84	-19.48	-3.50	1.35	2.39	-7.11	-1850 N
-1825 N	3.05	0.62	-5.00	5.00	-1.30	3.65	0.25	82.52	-19.92	-3.70	1.35	2.39	-7.52	-1825 N
-1800 N	3.05	0.62	-4.60	5.00	-1.30	3.70	0.25	82.41	-20.07	-3.50	1.30	2.31	-6.71	-1800 N
-1775 N	3.05	0.62	-4.60	5.50	-1.30	3.70	0.25	82.52	-19.92	-3.30	1.80	3.19	-6.71	-1775 N
-1750 N	3.05	0.63	-4.60	5.00	-1.30	3.70	0.25	84.18	-17.96	-3.50	1.30	2.54	-6.82	-1750 N
-1725 N	3.05	0.61	-4.60	5.00	-1.30	3.75	0.24	82.03	-20.26	-3.30	1.25	2.18	-6.60	-1725 N
-1700 N	3.05	0.63	-4.40	5.00	-1.30	3.75	0.24	85.48	-16.23	-3.10	1.25	2.25	-6.40	-1700 N
-1675 N	3.05	0.62	-4.40	5.00	-1.25	3.75	0.24	85.07	-16.49	-3.15	1.25	2.22	-6.40	-1675 N
-1650 N	3.05	0.61	-4.40	5.50	-1.25	3.80	0.24	84.84	-16.52	-3.15	1.70	2.97	-6.30	-1650 N
-1625 N	3.05	0.60	-4.40	5.50	-1.25	3.80	0.23	84.77	-16.35	-3.15	1.70	2.92	-6.20	-1625 N
-1600 N	3.05	0.60	-4.40	5.50	-1.25	3.80	0.23	86.28	-14.47	-3.15	1.70	2.92	-6.20	-1600 N
-1575 N	3.05	0.59	-4.20	5.50	-1.25	3.85	0.22	86.51	-13.95	-2.95	1.65	2.79	-5.71	-1575 N
-1550 N	3.05	0.58	-4.00	5.50	-1.25	3.85	0.22	86.86	-13.31	-2.75	1.65	2.74	-5.23	-1550 N
-1525 N	3.05	0.55	-4.40	6.00	-1.25	3.85	0.21	84.25	-15.59	-3.15	2.15	3.38	-5.68	-1525 N
-1500 N	3.05	0.55	-4.20	5.50	-1.25	3.90	0.21	86.29	-13.25	-2.95	1.60	2.52	-5.32	-1500 N
-1475 N	3.05	0.53	-4.20	6.00	-1.20	3.90	0.20	85.27	-13.89	-3.00	2.10	3.18	-5.21	-1475 N
-1450 N	3.05	0.52	-4.40	6.00	-1.20	3.90	0.20	85.87	-12.97	-3.20	2.10	3.12	-5.46	-1450 N
-1425 N	3.05	0.50	-4.60	6.00	-1.20	3.95	0.19	84.83	-13.56	-3.40	2.05	2.93	-5.57	-1425 N
-1400 N	3.05	0.48	-4.60	5.50	-1.20	3.95	0.19	83.73	-14.14	-3.40	1.55	2.13	-5.35	-1400 N
-1375 N	3.05	0.47	-4.50	6.00	-1.20	3.95	0.18	84.35	-13.22	-3.30	2.05	2.76	-5.09	-1375 N
-1350 N	3.05	0.44	-4.80	6.00	-1.20	4.00	0.18	81.28	-15.37	-3.60	2.00	2.52	-5.19	-1350 N
-1325 N	3.05	0.42	-5.00	6.00	-1.20	4.00	0.17	79.89	-16.03	-3.80	2.00	2.40	-5.23	-1325 N
-1300 N	3.05	0.40	-5.00	6.50	-1.20	4.00	0.17	78.38	-16.73	-3.80	2.50	2.86	-4.98	-1300 N

A. MOORE PARAGON PARAFIC

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STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
-2300. N	3.05	0.43	-9.20	4.40	-2.80	1.80	0.17	84.25	-12.19	-6.40	2.60	3.20	-9.02	-2300. N
-2275. N	3.05	0.43	-9.20	4.30	-2.80	1.80	0.17	82.39	-13.94	-6.40	2.50	3.08	-9.02	-2275. N
-2250. N	3.05	0.44	-9.10	4.20	-2.80	1.80	0.17	82.50	-14.15	-6.30	2.40	3.02	-9.09	-2250. N
-2225. N	3.05	0.45	-8.70	4.10	-2.80	1.80	0.18	82.63	-14.35	-5.90	2.30	2.96	-8.70	-2225. N
-2200. N	3.05	0.44	-8.70	4.10	-2.80	1.80	0.18	79.18	-17.54	-5.90	2.30	2.90	-8.51	-2200. N
-2175. N	3.05	0.46	-8.50	4.20	-2.80	1.80	0.19	81.20	-16.15	-5.70	2.40	3.16	-8.60	-2175. N
-2150. N	3.05	0.49	-8.30	4.10	-2.80	1.80	0.19	84.91	-13.20	-5.50	2.30	3.22	-8.84	-2150. N
-2125. N	3.05	0.50	-8.20	4.10	-2.80	1.80	0.19	85.15	-13.22	-5.40	2.30	3.29	-8.85	-2125. N
-2100. N	3.05	0.48	-8.30	4.00	-2.80	1.80	0.20	80.41	-17.73	-5.50	2.20	3.02	-8.66	-2100. N
-2075. N	3.05	0.50	-8.60	4.00	-2.80	1.80	0.20	82.48	-16.10	-5.80	2.20	3.15	-9.51	-2075. N
-2050. N	3.05	0.47	-8.10	3.90	-2.80	1.80	0.20	76.44	-21.97	-5.30	2.10	2.82	-8.17	-2050. N
-2025. N	3.05	0.51	-7.90	3.90	-2.80	1.80	0.20	81.87	-17.13	-5.10	2.10	3.06	-8.53	-2025. N
-2000. N	3.05	0.51	-7.50	4.00	-2.80	1.80	0.21	80.91	-18.25	-4.70	2.20	3.21	-7.86	-2000. N
-1975. N	3.05	0.53	-7.40	3.80	-2.80	1.80	0.21	83.19	-16.23	-4.60	2.00	3.03	-7.99	-1975. N
-1950. N	3.05	0.52	-7.30	3.80	-2.80	1.80	0.21	80.87	-18.65	-4.50	2.00	2.98	-7.67	-1950. N
-1925. N	3.05	0.54	-7.20	3.70	-2.80	1.80	0.21	83.33	-16.39	-4.40	1.90	2.94	-7.79	-1925. N
-1900. N	3.05	0.55	-6.90	3.70	-2.80	1.80	0.21	84.32	-15.51	-4.10	1.90	2.99	-7.39	-1900. N
-1875. N	3.05	0.54	-6.90	3.70	-2.80	1.80	0.21	82.37	-17.53	-4.10	1.90	2.94	-7.26	-1875. N
-1850. N	3.05	0.52	-7.00	3.90	-2.80	1.80	0.22	79.03	-20.93	-4.20	2.10	3.12	-7.16	-1850. N
-1825. N	3.05	0.55	-7.20	3.90	-2.80	1.80	0.22	83.40	-16.60	-4.40	2.10	3.30	-7.93	-1825. N
-1800. N	3.05	0.54	-7.10	3.80	-2.80	1.80	0.22	81.83	-18.19	-4.30	2.00	3.09	-7.61	-1800. N
-1775. N	3.05	0.54	-7.00	3.90	-2.75	1.85	0.22	81.89	-18.11	-4.25	2.05	3.17	-7.52	-1775. N
-1750. N	3.05	0.53	-6.90	4.00	-2.75	1.85	0.22	80.55	-19.41	-4.15	2.15	3.26	-7.21	-1750. N
-1725. N	3.05	0.52	-6.70	4.00	-2.75	1.85	0.21	79.31	-20.56	-3.95	2.15	3.20	-6.73	-1725. N
-1700. N	3.05	0.54	-6.60	3.90	-2.75	1.85	0.21	82.79	-17.03	-3.85	2.05	3.17	-6.82	-1700. N
-1675. N	3.05	0.53	-6.70	3.90	-2.75	1.85	0.21	81.78	-17.90	-3.95	2.05	3.11	-6.86	-1675. N
-1650. N	3.05	0.53	-6.70	4.00	-2.75	1.85	0.21	82.43	-17.13	-3.95	2.15	3.26	-6.86	-1650. N
-1625. N	3.05	0.51	-6.70	3.90	-2.75	1.85	0.21	80.06	-19.27	-3.95	2.05	2.99	-6.60	-1625. N
-1600. N	3.05	0.53	-6.60	3.80	-2.75	1.85	0.21	84.08	-15.22	-3.85	1.95	2.96	-6.69	-1600. N
-1575. N	3.05	0.53	-6.50	3.90	-2.75	1.85	0.20	85.08	-14.10	-3.75	2.05	3.11	-6.52	-1575. N
-1550. N	3.05	0.49	-6.50	4.00	-2.75	1.85	0.20	79.69	-18.94	-3.75	2.15	3.01	-6.02	-1550. N
-1525. N	3.05	0.50	-6.50	3.70	-2.75	1.85	0.20	82.48	-16.10	-3.75	1.85	2.65	-6.15	-1525. N
-1500. N	3.05	0.52	-6.70	3.80	-2.75	1.85	0.20	87.11	-11.67	-3.95	1.95	2.90	-6.73	-1500. N
-1475. N	3.05	0.50	-6.60	3.90	-2.75	1.85	0.19	85.15	-13.22	-3.85	2.05	2.93	-6.31	-1475. N
-1450. N	3.05	0.52	-6.40	4.00	-2.75	1.85	0.19	90.11	-8.65	-3.65	2.15	3.20	-6.22	-1450. N
-1425. N	3.05	0.52	-6.30	3.90	-2.75	1.85	0.19	91.79	-7.06	-3.55	2.05	3.05	-6.05	-1425. N
-1400. N	3.05	0.47	-6.40	4.00	-2.75	1.85	0.18	84.58	-12.99	-3.65	2.15	2.89	-5.62	-1400. N
-1375. N	3.05	0.49	-6.60	4.10	-2.75	1.85	0.18	89.97	-8.28	-3.85	2.25	3.15	-6.19	-1375. N
-1350. N	3.05	0.46	-6.70	3.90	-2.75	1.85	0.17	86.25	-11.12	-3.95	2.05	2.70	-5.96	-1350. N
-1325. N	3.05	0.49	-6.50	4.00	-2.75	1.85	0.17	93.89	-4.84	-3.75	2.15	3.01	-6.02	-1325. N
-1300. N	3.05	0.44	-6.80	4.00	-2.75	1.85	0.17	86.21	-10.67	-4.05	2.15	2.71	-5.84	-1300. N

L. MOORE PARAGON PARALIC

XTOP= -2300.

XINC= 25.00

128164

1	-2300.			I	-12.19
2	-2275.		*	I	-13.94
3	-2250.		*	I	-14.15
4	-2225.		*	I	-14.35
5	-2200.	*		I	-17.54
6	-2175.	*	*	I	-16.15
7	-2150.		*	I	-13.20
8	-2125.		*	I	-13.22
9	-2100.	*		I	-17.73
10	-2075.	*	*	I	-16.10
11	-2050.	*		I	-21.97
12	-2025.	*	*	I	-17.13
13	-2000.	*		I	-18.25
14	-1975.	*	*	I	-16.23
15	-1950.	*		I	-18.65
16	-1925.	*	*	I	-16.39
17	-1900.	*	*	I	-15.51
18	-1875.	*	*	I	-17.53
19	-1850.	*		I	-20.93
20	-1825.	*	*	I	-16.60
21	-1800.	*	*	I	-18.19
22	-1775.	*	*	I	-18.11
23	-1750.	*	*	I	-19.41
24	-1725.	*	*	I	-20.56
25	-1700.	*	*	I	-17.03
26	-1675.	*	*	I	-17.90
27	-1650.	*	*	I	-17.13
28	-1625.	*	*	I	-19.27
29	-1600.	*	*	I	-15.22
30	-1575.	*	*	I	-14.10
31	-1550.	*	*	I	-18.94
32	-1525.	*	*	I	-16.10
33	-1500.	*	*	I	-11.67
34	-1475.	*	*	I	-13.22
35	-1450.	*	*	I	-8.65
36	-1425.	*	*	I	-7.06
37	-1400.	*	*	I	-12.99
38	-1375.	*	*	I	-8.28
39	-1350.	*	*	I	-11.12
40	-1325.	*	*	I	-4.84
41	-1300.	*	*	I	-10.67

XBOT= -1300.

YINC= 1.000

YMIN= -50.00

YMAX= 50.00

LINE 3400 E MAGNETOMETRIC RESESTIVITY MMR

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XTOP= -2300.

XINC= 25.00

128166

2	-2300.	I	*	3.20	1
3	-2275.	I	*	3.08	2
4	-2250.	I	*	3.02	3
5	-2225.	I	*	2.96	4
6	-2200.	I	*	2.90	5
7	-2175.	I	*	3.16	6
8	-2150.	I	*	3.22	7
9	-2125.	I	*	3.29	8
10	-2100.	I	*	3.02	9
11	-2075.	I	*	3.15	10
12	-2050.	I	*	2.82	11
13	-2025.	I	*	3.06	12
14	-2000.	I	*	3.21	13
15	-1975.	I	*	3.03	14
16	-1950.	I	*	2.98	15
17	-1925.	I	*	2.94	16
18	-1900.	I	*	2.99	17
19	-1875.	I	*	2.94	18
20	-1850.	I	*	3.12	19
21	-1825.	I	*	3.30	20
22	-1800.	I	*	3.09	21
23	-1775.	I	*	3.17	22
24	-1750.	I	*	3.26	23
25	-1725.	I	*	3.20	24
26	-1700.	I	*	3.17	25
27	-1675.	I	*	3.11	26
28	-1650.	I	*	3.26	27
29	-1625.	I	*	2.99	28
30	-1600.	I	*	2.96	29
31	-1575.	I	*	3.11	30
32	-1550.	I	*	3.01	31
33	-1525.	I	*	2.65	32
34	-1500.	I	*	2.90	33
35	-1475.	I	*	2.93	34
36	-1450.	I	*	3.20	35
37	-1425.	I	*	3.05	36
38	-1400.	I	*	2.89	37
39	-1375.	I	*	3.15	38
40	-1350.	I	*	2.70	39
41	-1325.	I	*	3.01	40
42	-1300.	I	*	2.71	41

XBOT= -1300.
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3400 E SECONDARY FIELD QUADRATURE HSO/I

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LINE#	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	MN	MMR	PFE	RPS	HSG/I	HSP/I	STATION
				PFE	RPS	PFE	RPS								
5	-2300. N	3.06	0.43	-9.10	4.30	-2.60	2.00	0.17	83.81	-12.55	-6.50	2.50	2.82	-9.13	-2300. N
6	-2275. N	3.06	0.37	-9.10	4.30	-2.60	2.00	0.17	70.16	-23.78	-6.50	2.30	2.43	-7.86	-2275. N
7	-2250. N	3.06	0.45	-8.40	4.20	-2.60	2.00	0.18	83.06	-13.88	-5.80	2.20	2.82	-8.53	-2250. N
8	-2225. N	3.06	0.45	-8.30	4.00	-2.60	2.00	0.18	80.88	-16.08	-5.70	2.00	2.57	-8.38	-2225. N
9	-2200. N	3.06	0.46	-8.40	4.10	-2.60	2.00	0.19	80.57	-16.77	-5.80	2.10	2.75	-8.72	-2200. N
10	-2175. N	3.06	0.45	-8.40	4.10	-2.60	2.00	0.19	76.85	-20.48	-5.80	2.10	2.69	-8.53	-2175. N
11	-2150. N	3.06	0.44	-8.10	4.00	-2.60	2.00	0.20	73.34	-24.18	-5.50	2.00	2.51	-7.91	-2150. N
12	-2125. N	3.06	0.48	-7.90	3.90	-2.60	2.00	0.20	78.15	-20.28	-5.30	1.90	2.60	-8.31	-2125. N
13	-2100. N	3.06	0.48	-7.50	3.70	-2.60	2.00	0.21	76.42	-22.38	-4.90	1.70	2.33	-7.69	-2100. N
14	-2075. N	3.06	0.50	-7.50	3.70	-2.60	2.00	0.21	77.93	-21.40	-4.90	1.70	2.42	-8.01	-2075. N
15	-2050. N	3.06	0.51	-7.40	3.80	-2.60	2.00	0.21	77.92	-21.84	-4.80	1.80	2.62	-8.00	-2050. N
16	-2025. N	3.06	0.53	-7.40	3.80	-2.60	2.00	0.22	79.49	-20.67	-4.80	1.80	2.72	-8.31	-2025. N
17	-2000. N	3.06	0.55	-7.30	3.80	-2.60	2.00	0.22	81.10	-19.37	-4.70	1.80	2.82	-8.45	-2000. N
18	-1975. N	3.06	0.54	-7.10	3.70	-2.60	2.00	0.23	78.42	-22.47	-4.50	1.70	2.62	-7.94	-1975. N
19	-1950. N	3.06	0.55	-6.80	3.70	-2.65	1.95	0.23	78.79	-22.38	-4.15	1.75	2.74	-7.46	-1950. N
20	-1925. N	3.06	0.55	-6.70	3.60	-2.65	1.95	0.23	77.88	-23.62	-4.05	1.65	2.59	-7.28	-1925. N
21	-1900. N	3.06	0.55	-6.70	3.70	-2.65	1.95	0.23	77.13	-24.66	-4.05	1.75	2.74	-7.28	-1900. N
22	-1875. N	3.06	0.56	-6.80	3.70	-2.65	1.95	0.23	77.93	-23.97	-4.15	1.75	2.79	-7.59	-1875. N
23	-1850. N	3.06	0.55	-6.70	3.80	-2.65	1.95	0.24	76.12	-26.08	-4.05	1.85	2.90	-7.28	-1850. N
24	-1825. N	3.06	0.56	-6.80	3.70	-2.65	1.95	0.24	77.25	-24.93	-4.15	1.75	2.79	-7.59	-1825. N
25	-1800. N	3.06	0.56	-6.80	3.80	-2.65	1.95	0.24	77.16	-25.05	-4.15	1.85	2.95	-7.59	-1800. N
26	-1775. N	3.06	0.57	-6.60	3.90	-2.65	1.95	0.24	78.62	-23.42	-3.95	1.95	3.17	-7.36	-1775. N
27	-1750. N	3.06	0.52	-7.00	4.00	-2.65	1.95	0.24	71.97	-30.62	-4.35	2.05	3.04	-7.39	-1750. N
28	-1725. N	3.06	0.56	-6.80	4.00	-2.65	1.95	0.23	77.93	-23.97	-4.15	2.05	3.27	-7.59	-1725. N
29	-1700. N	3.06	0.52	-7.00	4.00	-2.65	1.95	0.23	72.92	-29.19	-4.35	2.05	3.04	-7.39	-1700. N
30	-1675. N	3.06	0.54	-6.90	3.90	-2.65	1.95	0.23	76.46	-25.13	-4.25	1.95	3.00	-7.50	-1675. N
31	-1650. N	3.06	0.55	-6.80	4.00	-2.65	1.95	0.23	78.79	-22.38	-4.15	2.05	3.22	-7.46	-1650. N
32	-1625. N	3.06	0.55	-6.50	3.90	-2.70	1.90	0.23	79.87	-20.95	-3.80	2.00	3.14	-6.83	-1625. N
33	-1600. N	3.06	0.57	-6.50	3.90	-2.70	1.90	0.22	84.05	-16.35	-3.80	2.00	3.25	-7.08	-1600. N
34	-1575. N	3.06	0.56	-6.60	4.00	-2.70	1.90	0.22	83.99	-16.13	-3.90	2.10	3.35	-7.14	-1575. N
35	-1550. N	3.06	0.55	-6.70	3.90	-2.70	1.90	0.21	84.03	-15.79	-4.00	2.00	3.14	-7.19	-1550. N
36	-1525. N	3.06	0.55	-6.60	4.00	-2.70	1.90	0.21	85.73	-13.84	-3.90	2.10	3.29	-7.01	-1525. N
37	-1500. N	3.06	0.54	-6.70	4.10	-2.70	1.90	0.21	85.97	-13.32	-4.00	2.20	3.39	-7.06	-1500. N
38	-1475. N	3.06	0.52	-6.70	4.20	-2.70	1.90	0.20	84.66	-14.24	-4.00	2.30	3.41	-6.80	-1475. N
39	-1450. N	3.06	0.51	-6.80	4.20	-2.70	1.90	0.20	85.01	-13.60	-4.10	2.30	3.34	-6.83	-1450. N
40	-1425. N	3.06	0.49	-7.10	4.10	-2.70	1.90	0.19	83.69	-14.44	-4.40	2.20	3.07	-7.05	-1425. N
41	-1400. N	3.06	0.51	-6.70	4.10	-2.70	1.90	0.19	89.32	-9.21	-4.00	2.20	3.20	-6.67	-1400. N
42	-1375. N	3.06	0.48	-6.90	4.30	-2.70	1.90	0.18	86.27	-11.54	-4.20	2.40	3.29	-6.59	-1375. N
43	-1350. N	3.06	0.46	-6.80	4.40	-2.70	1.90	0.18	84.90	-12.36	-4.10	2.50	3.28	-6.16	-1350. N
44	-1325. N	3.06	0.34	-7.80	5.30	-2.70	1.90	0.17	64.47	-28.32	-5.10	3.40	3.30	-5.67	-1325. N
45	-1300. N	3.06	0.46	-6.70	4.20	-2.70	1.90	0.17	89.66	-8.02	-4.00	2.30	3.02	-6.01	-1300. N

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STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
-2300 N	3.10	0.44	-8.70	3.89	-2.55	1.85	0.15	92.19	-5.56	-6.15	1.95	2.42	-8.78	-2300 N
-2275 N	3.10	0.45	-8.50	3.70	-2.55	1.85	0.16	90.09	-7.39	-5.95	1.85	2.34	-8.64	-2275 N
-2250 N	3.10	0.46	-7.90	3.50	-2.55	1.85	0.17	87.88	-9.47	-5.35	1.65	2.14	-7.94	-2250 N
-2225 N	3.10	0.49	-7.70	3.40	-2.55	1.85	0.18	89.21	-8.84	-5.15	1.55	2.14	-8.14	-2225 N
-2200 N	3.10	0.52	-7.40	3.50	-2.55	1.85	0.19	90.12	-8.51	-4.85	1.65	2.42	-8.14	-2200 N
-2175 N	3.10	0.55	-7.40	3.40	-2.55	1.85	0.20	90.63	-8.48	-4.85	1.55	2.40	-8.60	-2175 N
-2150 N	3.10	0.57	-7.10	3.20	-2.55	1.85	0.21	89.22	-10.27	-4.55	1.55	2.17	-8.57	-2150 N
-2125 N	3.10	0.57	-6.80	3.20	-2.55	1.85	0.22	84.69	-15.37	-4.25	1.35	2.17	-7.81	-2125 N
-2100 N	3.10	0.62	-6.60	3.10	-2.55	1.85	0.23	87.41	-13.32	-4.05	1.25	2.18	-8.10	-2100 N
-2075 N	3.10	0.63	-6.60	3.00	-2.55	1.85	0.24	84.27	-17.54	-4.05	1.15	2.04	-8.23	-2075 N
-2050 N	3.10	0.65	-6.40	3.00	-2.55	1.85	0.25	82.53	-20.52	-3.85	1.15	2.10	-8.07	-2050 N
-2025 N	3.10	0.69	-6.50	3.10	-2.55	1.85	0.27	83.25	-20.71	-3.95	1.25	2.43	-8.79	-2025 N
-2000 N	3.10	0.70	-6.30	3.00	-2.55	1.85	0.28	80.39	-25.47	-3.75	1.15	2.27	-8.47	-2000 N
-1975 N	3.10	0.72	-6.20	2.90	-2.55	1.85	0.29	78.91	-28.71	-3.65	1.05	2.13	-8.48	-1975 N
-1950 N	3.10	0.73	-6.10	3.00	-2.55	1.85	0.31	76.61	-33.25	-3.55	1.15	2.36	-8.36	-1950 N
-1925 N	3.10	0.75	-5.90	2.90	-2.55	1.85	0.32	75.70	-35.92	-3.35	1.05	2.22	-8.10	-1925 N
-1900 N	3.10	0.75	-5.80	2.90	-2.55	1.85	0.33	73.20	-40.97	-3.25	1.05	2.22	-7.86	-1900 N
-1875 N	3.10	0.76	-5.80	2.80	-2.55	1.85	0.34	72.18	-43.71	-3.25	0.95	2.03	-7.97	-1875 N
-1850 N	3.10	0.77	-5.80	2.90	-2.55	1.85	0.35	71.67	-45.42	-3.25	1.05	2.28	-8.07	-1850 N
-1825 N	3.10	0.79	-5.70	3.00	-2.55	1.85	0.35	72.62	-44.43	-3.15	1.15	2.56	-8.03	-1825 N
-1800 N	3.10	0.78	-5.80	3.10	-2.55	1.85	0.35	71.40	-46.61	-3.25	1.25	2.74	-8.18	-1800 N
-1775 N	3.11	0.79	-5.70	3.20	-2.60	1.90	0.35	72.39	-44.81	-3.10	1.30	2.88	-7.87	-1775 N
-1750 N	3.11	0.78	-5.80	3.10	-2.60	1.90	0.35	72.36	-44.30	-3.20	1.20	2.63	-8.03	-1750 N
-1725 N	3.11	0.78	-5.80	3.10	-2.60	1.90	0.34	73.84	-41.10	-3.20	1.20	2.63	-8.03	-1725 N
-1700 N	3.11	0.76	-5.70	3.20	-2.60	1.90	0.33	73.94	-39.84	-3.10	1.30	2.77	-7.58	-1700 N
-1675 N	3.11	0.75	-5.80	3.30	-2.60	1.90	0.32	75.46	-36.28	-3.20	1.40	2.95	-7.72	-1675 N
-1650 N	3.11	0.76	-5.80	3.20	-2.60	1.90	0.31	79.50	-29.14	-3.20	1.30	2.77	-7.82	-1650 N
-1625 N	3.11	0.74	-5.80	3.30	-2.60	1.90	0.29	80.84	-26.09	-3.20	1.40	2.91	-7.61	-1625 N
-1600 N	3.11	0.73	-5.60	3.40	-2.60	1.90	0.28	83.57	-21.35	-3.00	1.50	3.07	-7.04	-1600 N
-1575 N	3.11	0.72	-5.70	3.40	-2.60	1.90	0.27	86.59	-16.58	-3.10	1.50	3.03	-7.18	-1575 N
-1550 N	3.11	0.70	-5.80	3.40	-2.60	1.90	0.25	88.60	-13.40	-3.20	1.50	2.95	-7.20	-1550 N
-1525 N	3.11	0.67	-6.10	3.60	-2.60	1.90	0.24	89.33	-11.90	-3.50	1.70	3.20	-7.54	-1525 N
-1500 N	3.11	0.65	-6.20	3.60	-2.60	1.90	0.23	91.34	-9.16	-3.60	1.70	3.10	-7.52	-1500 N
-1475 N	3.11	0.62	-6.20	3.80	-2.60	1.90	0.22	91.83	-8.21	-3.60	1.90	3.31	-7.18	-1475 N
-1450 N	3.11	0.61	-6.40	3.80	-2.60	1.90	0.21	95.18	-4.60	-3.80	1.90	3.25	-7.45	-1450 N
-1425 N	3.11	0.58	-6.50	3.90	-2.60	1.90	0.20	95.27	-4.29	-3.90	2.00	3.25	-7.27	-1425 N
-1400 N	3.11	0.57	-6.50	4.00	-2.60	1.90	0.19	98.47	-1.32	-3.90	2.10	3.36	-7.15	-1400 N
-1375 N	3.11	0.54	-6.70	4.00	-2.60	1.90	0.18	98.00	-1.64	-4.10	2.10	3.18	-7.12	-1375 N
-1350 N	3.11	0.50	-6.80	4.10	-2.60	1.90	0.17	95.21	-3.74	-4.20	2.20	3.09	-6.75	-1350 N
-1325 N	3.11	0.50	-6.90	4.30	-2.60	1.90	0.16	99.78	-0.17	-4.30	2.40	3.37	-6.91	-1325 N
-1300 N	3.11	0.47	-7.20	4.60	-2.60	1.90	0.15	98.16	-1.31	-4.60	2.70	3.56	-6.95	-1300 N

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PROGRAM MIP2 . CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

3HZ RRMIP SURVEY MT PEARSE TASMANIA 063R ARRAY N004

79-1393 Vol 2

W 0001 11 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63

INTER TAPE FLAG= 0 GRIDDATA TAPE FLAG= 0

LINE POSITIONING MULTIPLYING FACTOR= 1.0

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4 PLOT SCALE= 2500 HN SCALE 10. PFE & RPS SCALE= 1 HSG & HSP SCALE= 1
5
6 ORIGIN CO-ORDS= 3400. E -2700. N ARRAY IDENTIFIER= MP04 ANNOTATION SUPPRESSION FLAG= 0
7
8 SPLINE INTERVAL= 0
9
10 PLOT BASE LEVELS FOR PFE, RPS, HSG, HSP ARE 0.00 0.00 0.00 0.00
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13 PLOTTING OPTION FLAGS FOLLOW - 1-STRAIGHT PLOT, 2-SPLINE PLOT WHERE APPLICABLE

14 HN = 0
15 MMR = 1
16 PFE = 0
17 RPS = 1
18 HSG = 1
19 HSP = 0
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LINE# 3400. E FREQUENCY=3HZ N004

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
-3725. N	2.94	0.47	-5.50	7.50	-1.80	5.20	0.15	103.46	2.67	-3.70	2.30	3.21	-5.91	-3725. N
-3700. N	2.94	0.46	-5.70	7.60	-1.80	5.20	0.16	97.79	-1.77	-3.90	2.40	3.28	-6.10	-3700. N
-3675. N	2.94	0.46	-5.80	7.50	-1.80	5.20	0.17	94.42	-4.63	-4.00	2.30	3.14	-6.26	-3675. N
-3650. N	2.94	0.57	-5.50	7.60	-1.80	5.20	0.17	112.94	11.11	-3.70	2.40	4.06	-7.17	-3650. N
-3625. N	2.94	0.57	-5.30	7.20	-1.80	5.20	0.18	109.03	8.03	-3.50	2.00	3.38	-6.79	-3625. N
-3600. N	2.94	0.55	-5.00	7.30	-1.80	5.20	0.18	101.57	1.44	-3.20	2.10	3.43	-5.99	-3600. N
-3575. N	2.94	0.57	-5.00	7.20	-1.80	5.20	0.19	101.64	1.57	-3.20	2.00	3.38	-6.20	-3575. N
-3550. N	2.94	0.60	-4.80	7.10	-1.80	5.15	0.20	103.36	3.31	-3.00	1.95	3.47	-6.12	-3550. N
-3525. N	2.94	0.61	-4.40	7.00	-1.80	5.15	0.20	101.57	1.60	-2.60	1.85	3.35	-5.39	-3525. N
-3500. N	2.94	0.62	-4.50	6.90	-1.80	5.15	0.21	99.87	-0.14	-2.70	1.75	3.22	-5.69	-3500. N
-3475. N	2.94	0.67	-4.20	6.80	-1.80	5.15	0.22	104.51	4.92	-2.40	1.65	3.28	-5.47	-3475. N
-3450. N	2.94	0.67	-4.20	6.70	-1.80	5.15	0.22	101.35	1.51	-2.40	1.55	3.08	-5.47	-3450. N
-3425. N	2.94	0.70	-4.10	6.60	-1.80	5.15	0.23	102.84	3.29	-2.30	1.45	3.01	-5.48	-3425. N
-3400. N	2.94	0.71	-4.00	6.60	-1.85	5.15	0.24	101.50	1.79	-2.15	1.45	3.06	-5.19	-3400. N
-3375. N	2.94	0.75	-3.80	6.50	-1.85	5.10	0.24	104.57	5.58	-1.95	1.40	3.12	-4.97	-3375. N
-3350. N	2.94	0.72	-3.60	6.30	-1.85	5.10	0.25	98.16	-2.30	-1.75	1.20	2.56	-4.29	-3350. N
-3325. N	2.94	0.79	-3.60	6.40	-1.85	5.10	0.25	105.61	7.13	-1.75	1.30	3.05	-4.70	-3325. N
-3300. N	2.94	0.81	-3.60	6.50	-1.85	5.10	0.26	106.51	8.42	-1.75	1.40	3.37	-4.82	-3300. N
-3275. N	2.94	0.00	0.00	0.00	-1.85	5.10	0.26	0.00	-131.05	1.85	-5.10	0.00	0.00	-3275. N
-3250. N	2.94	0.00	0.00	0.00	-1.85	5.10	0.26	0.00	-132.31	1.85	-5.10	0.00	0.00	-3250. N
-3225. N	2.94	0.00	0.00	0.00	-1.85	5.10	0.27	0.00	-133.07	1.85	-5.10	0.00	0.00	-3225. N
-3200. N	2.95	0.84	-3.00	6.30	-1.85	5.05	0.27	106.78	9.04	-1.15	1.25	3.11	-3.27	-3200. N
-3175. N	2.95	0.84	-3.20	6.20	-1.85	5.05	0.27	106.99	9.30	-1.35	1.15	2.86	-3.84	-3175. N
-3150. N	2.95	0.84	-3.00	6.30	-1.85	5.05	0.26	107.61	10.07	-1.15	1.25	3.11	-3.27	-3150. N
-3125. N	2.95	0.83	-3.00	6.20	-1.85	5.05	0.26	107.35	9.63	-1.15	1.15	2.82	-3.24	-3125. N
-3100. N	2.95	0.81	-3.20	6.20	-1.85	5.05	0.26	106.15	7.95	-1.35	1.15	2.76	-3.71	-3100. N
-3075. N	2.95	0.80	-3.10	6.20	-1.85	5.05	0.25	106.58	8.37	-1.25	1.15	2.72	-3.39	-3075. N
-3050. N	2.95	0.00	0.00	0.00	-1.90	5.05	0.25	0.00	-124.75	1.90	-5.05	0.00	0.00	-3050. N
-3025. N	2.95	0.00	0.00	0.00	-1.90	5.00	0.24	0.00	-121.97	1.90	-5.00	0.00	0.00	-3025. N
-3000. N	2.95	0.72	-2.80	6.00	-1.90	5.00	0.24	102.59	3.08	-0.90	1.00	2.13	-2.20	-3000. N
-2975. N	2.95	0.68	-3.00	6.30	-1.90	5.00	0.23	99.56	-0.51	-1.10	1.30	2.61	-2.54	-2975. N
-2950. N	2.95	0.63	-3.20	6.50	-1.90	5.00	0.22	94.97	-5.65	-1.30	1.50	2.80	-2.78	-2950. N
-2925. N	2.95	0.58	-3.50	6.50	-1.90	5.00	0.22	90.17	-10.72	-1.60	1.50	2.57	-3.15	-2925. N
-2900. N	2.95	0.52	-3.80	6.50	-1.90	5.00	0.21	83.48	-17.45	-1.90	1.50	2.31	-3.35	-2900. N
-2875. N	2.95	0.48	-4.00	6.60	-1.90	5.00	0.20	79.65	-20.78	-2.10	1.60	2.27	-3.42	-2875. N
-2850. N	2.95	0.49	-3.80	6.50	-1.90	4.95	0.20	84.12	-15.68	-1.90	1.55	2.25	-3.16	-2850. N
-2825. N	2.95	0.46	-3.60	6.50	-1.90	4.95	0.19	81.75	-17.41	-1.70	1.55	2.11	-2.65	-2825. N
-2800. N	2.95	0.43	-3.60	6.50	-1.90	4.95	0.18	79.14	-19.21	-1.70	1.55	1.97	-2.48	-2800. N
-2775. N	2.95	0.44	-3.40	6.60	-1.90	4.95	0.18	83.88	-14.34	-1.50	1.65	2.15	-2.24	-2775. N
-2750. N	2.95	0.38	-3.60	7.00	-1.90	4.95	0.17	75.04	-21.42	-1.70	2.05	2.30	-2.19	-2750. N
-2725. N	2.95	0.38	-3.80	6.80	-1.90	4.95	0.17	77.73	-18.45	-1.90	1.85	2.08	-2.45	-2725. N
-2700. N	2.95	0.35	-3.80	6.80	-1.90	4.95	0.16	74.15	-20.68	-1.90	1.85	1.92	-2.25	-2700. N

MOORE PARAGON PARAFIC

XTOP= -3725

XINC= 25.00

4	-3725			I*	2.67
5	-3700			*I	-1.77
6	-3675			* I	-4.63
7	-3650			I *	11.11
8	-3625			I *	8.03
9	-3600			*	1.44
10	-3575			I*	1.57
11	-3550			I*	3.31
12	-3525			I*	1.60
13	-3500			*	-0.14
14	-3475			I *	4.92
15	-3450			I*	1.51
16	-3425			I*	3.29
17	-3400			I*	1.79
18	-3375			I *	5.58
19	-3350			* I	-2.30
20	-3325			I *	7.13
21	-3300			I *	8.42
22	-3275	*	POWER LINES	I	-131.05
23	-3250	*		I	-132.31
24	-3225	*		I	-133.07
25	-3200			I *	9.04
26	-3175			I *	9.30
27	-3150			I *	10.67
28	-3125			I *	9.63
29	-3100			I *	7.95
30	-3075			I *	8.37
31	-3050	*	WIRE FENCE	I	-124.75
32	-3025	*		I	-121.97
33	-3000			I*	3.08
34	-2975			*I	-0.51
35	-2950			* I	-5.65
36	-2925			* I	-10.72
37	-2900			I *	-17.45
38	-2875	*		I	-20.78
39	-2850	*		I	-15.68
40	-2825	*		I	-17.41
41	-2800	*		I	-19.21
42	-2775			I *	-14.34
43	-2750	*		I	-21.42
44	-2725	*		I	-18.45
45	-2700	*		I	-20.68

XBOT= -2700

YINC= 1.831

YMIN= -133.1

YMAX= 50.00

LINE 3400. E MAGNETOMETRIC RESESTIVITY MMR

XTOP= -3725

XINC= 25.00

4	-3725	I	*	2.30
5	-3700	I	*	2.40
6	-3675	I	*	2.30
7	-3650	I	*	2.40
8	-3625	I	*	2.00
9	-3600	I	*	2.10
10	-3575	I	*	2.00
11	-3550	I	*	1.95
12	-3525	I	*	1.85
13	-3500	I	*	1.75
14	-3475	I	*	1.65
15	-3450	I	*	1.55
16	-3425	I	*	1.45
17	-3400	I	*	1.45
18	-3375	I	*	1.40
19	-3350	I	*	1.20
20	-3325	I	*	1.30
21	-3300	I	*	1.40
22	-3275 *	I		-5.10
23	-3250 *	I		-5.10
24	-3225 *	I		-5.10
25	-3200	I	*	1.25
26	-3175	I	*	1.15
27	-3150	I	*	1.25
28	-3125	I	*	1.15
29	-3100	I	*	1.15
30	-3075	I	*	1.15
31	-3050 *	I		-5.05
32	-3025 *	I		-5.00
33	-3000	I	*	1.00
34	-2975	I	*	1.30
35	-2950	I	*	1.50
36	-2925	I	*	1.50
37	-2900	I	*	1.50
38	-2875	I	*	1.60
39	-2850	I	*	1.55
40	-2825	I	*	1.55
41	-2800	I	*	1.55
42	-2775	I	*	1.65
43	-2750	I	*	2.05
44	-2725	I	*	1.85
45	-2700	I	*	1.85

XBOT= -2700

YINC= 0.7600E-01

YMIN= -5.100

YMAX= 2.500

LINE 3400. E RELATIVE PHASE SHIFT RPS

MOORE PARAGON PARAFLO

XTOP= -3725

XINC= 25.00

4	-3725	I	*	3.21
5	-3700	I	*	3.28
6	-3675	I	*	3.14
7	-3650	I	*	4.06
8	-3625	I	*	3.38
9	-3600	I	*	3.43
10	-3575	I	*	3.38
11	-3550	I	*	3.47
12	-3525	I	*	3.35
13	-3500	I	*	3.22
14	-3475	I	*	3.28
15	-3450	I	*	3.08
16	-3425	I	*	3.01
17	-3400	I	*	3.06
18	-3375	I	*	3.12
19	-3350	I	*	2.56
20	-3325	I	*	3.05
21	-3300	I	*	3.37
22	-3275	*		0.00
23	-3250	*		0.00
24	-3225	*		0.00
25	-3200	I	*	3.11
26	-3175	I	*	2.86
27	-3150	I	*	3.11
28	-3125	I	*	2.82
29	-3100	I	*	2.76
30	-3075	I	*	2.72
31	-3050	*		0.00
32	-3025	*		0.00
33	-3000	I	*	2.13
34	-2975	I	*	2.61
35	-2950	I	*	2.80
36	-2925	I	*	2.57
37	-2900	I	*	2.31
38	-2875	I	*	2.27
39	-2850	I	*	2.25
40	-2825	I	*	2.11
41	-2800	I	*	1.97
42	-2775	I	*	2.15
43	-2750	I	*	2.30
44	-2725	I	*	2.08
45	-2700	I	*	1.92

XBOT= -2700

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 3400. E SECONDARY FIELD QUADRATURE HSQ/I

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LINE= 3700. E FREQUENCY=3HZ N004

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSP/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
-3725. N	2.94	0.47	-6.00	7.80	-1.75	5.25	0.16	101.62	1.27	-4.25	2.55	3.56	-6.79	-3725. N
-3700. N	2.94	0.47	-6.00	7.80	-1.75	5.25	0.16	99.36	-0.51	-4.25	2.55	3.56	-6.79	-3700. N
-3675. N	2.94	0.51	-5.80	7.70	-1.75	5.25	0.16	105.48	4.50	-4.05	2.45	3.71	-7.03	-3675. N
-3650. N	2.94	0.50	-5.40	7.60	-1.75	5.25	0.17	101.22	1.03	-3.65	2.35	3.49	-6.21	-3650. N
-3625. N	2.94	0.50	-5.10	7.70	-1.75	5.25	0.17	99.15	-0.73	-3.55	2.45	3.64	-5.70	-3625. N
-3600. N	2.94	0.51	-5.00	7.50	-1.75	5.25	0.18	99.13	-0.77	-3.25	2.25	3.41	-5.64	-3600. N
-3575. N	2.94	0.52	-5.10	7.40	-1.75	5.25	0.18	99.14	-0.77	-3.35	2.15	3.32	-5.93	-3575. N
-3550. N	2.94	0.50	-5.00	7.50	-1.75	5.30	0.18	93.59	-5.83	-3.25	2.20	3.26	-5.53	-3550. N
-3525. N	2.94	0.43	-4.40	7.50	-1.75	5.30	0.18	79.09	-19.34	-2.65	2.20	2.81	-3.88	-3525. N
-3500. N	2.94	0.50	-4.40	7.50	-1.75	5.30	0.19	90.45	-8.98	-2.65	2.20	3.26	-4.51	-3500. N
-3475. N	2.94	0.00	0.00	0.00	-1.75	5.30	0.19	0.00	-95.48	1.75	-5.30	0.00	0.00	-3475. N
-3450. N	2.94	0.00	0.00	0.00	-1.75	5.30	0.19	0.00	-96.87	1.75	-5.30	0.00	0.00	-3450. N
-3425. N	2.94	0.00	0.00	0.00	-1.75	5.30	0.20	0.00	-98.17	1.75	-5.30	0.00	0.00	-3425. N
-3400. N	2.94	0.55	-4.20	7.00	-1.75	5.30	0.20	94.14	-5.83	-2.45	1.70	2.78	-4.58	-3400. N
-3375. N	2.94	0.54	-4.00	7.00	-1.75	5.35	0.20	91.43	-8.61	-2.25	1.65	2.64	-4.13	-3375. N
-3350. N	2.94	0.56	-4.10	7.10	-1.70	5.35	0.20	93.92	-6.16	-2.40	1.75	2.91	-4.57	-3350. N
-3325. N	2.94	0.56	-4.20	7.10	-1.70	5.35	0.20	93.16	-6.99	-2.50	1.75	2.91	-4.76	-3325. N
-3300. N	2.94	0.57	-4.00	7.00	-1.70	5.35	0.21	94.19	-5.98	-2.30	1.65	2.79	-4.46	-3300. N
-3275. N	2.94	0.58	-3.90	7.00	-1.70	5.35	0.21	95.34	-4.82	-2.20	1.65	2.84	-4.34	-3275. N
-3250. N	2.94	0.59	-3.80	7.10	-1.70	5.35	0.21	96.62	-3.51	-2.10	1.75	3.06	-4.21	-3250. N
-3225. N	2.94	0.59	-3.90	7.00	-1.70	5.35	0.21	96.40	-3.75	-2.20	1.65	2.89	-4.41	-3225. N
-3200. N	2.94	0.60	-3.80	7.10	-1.70	5.40	0.21	97.96	-2.13	-2.10	1.70	3.03	-4.29	-3200. N
-3175. N	2.94	0.59	-3.90	7.10	-1.70	5.40	0.21	96.40	-3.75	-2.20	1.70	2.98	-4.41	-3175. N
-3150. N	2.94	0.60	-3.80	7.20	-1.70	5.40	0.21	98.26	-1.81	-2.10	1.80	3.21	-4.29	-3150. N
-3125. N	2.94	0.60	-3.80	7.20	-1.70	5.40	0.21	98.63	-1.42	-2.10	1.80	3.21	-4.29	-3125. N
-3100. N	2.94	0.61	-3.80	7.10	-1.70	5.40	0.21	100.80	0.82	-2.10	1.70	3.08	-4.36	-3100. N
-3075. N	2.94	0.62	-3.70	7.10	-1.70	5.40	0.20	103.14	3.21	-2.00	1.70	3.13	-4.22	-3075. N
-3050. N	2.94	0.62	-3.80	7.20	-1.70	5.40	0.20	103.98	4.04	-2.10	1.80	3.31	-4.43	-3050. N
-3025. N	2.94	0.60	-3.70	7.10	-1.70	5.45	0.20	101.59	1.60	-2.00	1.65	2.94	-4.08	-3025. N
-3000. N	2.94	0.59	-3.60	7.10	-1.65	5.45	0.20	100.98	0.98	-1.95	1.65	2.89	-3.91	-3000. N
-2975. N	2.94	0.58	-3.60	7.10	-1.65	5.45	0.20	100.48	0.47	-1.95	1.65	2.84	-3.85	-2975. N
-2950. N	2.94	0.56	-3.50	7.00	-1.65	5.45	0.19	98.31	-1.63	-1.85	1.55	2.58	-3.52	-2950. N
-2925. N	2.94	0.55	-2.40	7.00	-1.65	5.45	0.19	97.96	-1.95	-0.75	1.55	2.53	-1.40	-2925. N
-2900. N	2.94	0.53	-2.40	7.10	-1.65	5.45	0.19	95.88	-3.87	-0.75	1.65	2.60	-1.35	-2900. N
-2875. N	2.94	0.51	-2.40	7.00	-1.65	5.45	0.18	93.80	-5.73	-0.75	1.55	2.35	-1.30	-2875. N
-2850. N	2.94	0.51	-3.30	7.10	-1.65	5.50	0.18	95.46	-4.12	-1.65	1.60	2.42	-2.86	-2850. N
-2825. N	2.94	0.48	-3.20	7.00	-1.65	5.50	0.18	91.52	-7.57	-1.55	1.50	2.14	-2.53	-2825. N
-2800. N	2.94	0.46	-3.20	6.90	-1.65	5.50	0.18	89.41	-9.27	-1.55	1.40	1.91	-2.43	-2800. N
-2775. N	2.94	0.45	-3.20	6.80	-1.65	5.50	0.17	89.23	-9.24	-1.55	1.30	1.74	-2.37	-2775. N
-2750. N	2.94	0.43	-3.00	6.90	-1.65	5.50	0.17	87.05	-10.88	-1.35	1.40	1.79	-1.97	-2750. N
-2725. N	2.94	0.42	-2.90	6.80	-1.65	5.50	0.16	86.86	-10.80	-1.25	1.30	1.62	-1.79	-2725. N
-2700. N	2.94	0.41	-2.80	6.70	-1.65	5.50	0.16	86.68	-10.72	-1.15	1.20	1.46	-1.60	-2700. N

AVL MOORE PARAGON P-1741 C

XTOP= -3725

XINC= 25.00

4	-3725		I*	1.27
5	-3700		*	-0.91
6	-3675		I*	4.50
7	-3650		I*	1.03
8	-3625		*	-0.73
9	-3600		*	-0.77
10	-3575		*	-0.77
11	-3550		*	-5.83
12	-3525	*	I	-19.34
13	-3500		I	-8.98
14	-3475		I	-95.48
15	-3450	*	I	-98.87
16	-3425	*	I	-98.17
17	-3400		*	-5.83
18	-3375		*	-8.61
19	-3350		*	-6.16
20	-3325		*	-6.99
21	-3300		*	-5.98
22	-3275		*	-4.82
23	-3250		*	-3.51
24	-3225		*	-3.75
25	-3200		*	-2.13
26	-3175		*	-3.75
27	-3150		*	-1.81
28	-3125		*	-1.42
29	-3100		I*	0.82
30	-3075		I*	3.21
31	-3050		I*	4.04
32	-3025		I*	1.60
33	-3000		I*	0.98
34	-2975		I*	0.47
35	-2950		*	-1.63
36	-2925		*	-1.95
37	-2900		*	-3.87
38	-2875		*	-5.73
39	-2850		*	-4.12
40	-2825		*	-7.57
41	-2800		*	-9.27
42	-2775		*	-9.24
43	-2750		*	-10.88
44	-2725		*	-10.80
45	-2700		*	-10.72

POWER LINES

XBOT= -2700
YMIN= -98.17

YINC= 1.482
YMAX= 50.00

LINE 3700.E MAGNETOMETRIC RESESTIVITY MMR

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XTOP= -3725

XINC= 25.00

4	-3725	I	*	2.55
5	-3700	I	*	2.55
6	-3675	I	*	2.45
7	-3650	I	*	2.35
8	-3625	I	*	2.45
9	-3600	I	*	2.25
10	-3575	I	*	2.15
11	-3550	I	*	2.20
12	-3525	I	*	2.20
13	-3500	I	*	2.20
14	-3475 *	I		-5.30
15	-3450 *	I		-5.30
16	-3425 *	I		-5.30
17	-3400	I	*	1.70
18	-3375	I	*	1.65
19	-3350	I	*	1.75
20	-3325	I	*	1.75
21	-3300	I	*	1.65
22	-3275	I	*	1.65
23	-3250	I	*	1.75
24	-3225	I	*	1.65
25	-3200	I	*	1.70
26	-3175	I	*	1.70
27	-3150	I	*	1.80
28	-3125	I	*	1.80
29	-3100	I	*	1.70
30	-3075	I	*	1.70
31	-3050	I	*	1.80
32	-3025	I	*	1.65
33	-3000	I	*	1.65
34	-2975	I	*	1.65
35	-2950	I	*	1.55
36	-2925	I	*	1.55
37	-2900	I	*	1.65
38	-2875	I	*	1.55
39	-2850	I	*	1.60
40	-2825	I	*	1.50
41	-2800	I	*	1.40
42	-2775	I	*	1.30
43	-2750	I	*	1.40
44	-2725	I	*	1.30
45	-2700	I	*	1.20

XBOT= -2700

YINC= 0.7856E-01

YMIN= -5.300

YMAX= 2.550

LINE 3700. E RELATIVE PHASE SHIFT RPS

MOORE PARAGON PARAFLO

XTOP= -3725

XINC= 25.00

3725	I	*	3.56
-3700	I	*	3.56
-3675	I	*	3.71
-3650	I	*	3.49
-3625	I	*	3.64
-3600	I	*	3.41
-3575	I	*	3.32
-3550	I	*	3.26
-3525	I	*	2.81
-3500	I	*	3.26
-3475	*		0.00
-3450	*		0.00
-3425	*		0.00
-3400	I	*	2.78
-3375	I	*	2.64
-3350	I	*	2.91
-3325	I	*	2.91
-3300	I	*	2.79
-3275	I	*	2.84
-3250	I	*	3.06
-3225	I	*	2.89
-3200	I	*	3.03
-3175	I	*	2.98
-3150	I	*	3.21
-3125	I	*	3.21
-3100	I	*	3.08
-3075	I	*	3.13
-3050	I	*	3.31
-3025	I	*	2.94
-3000	I	*	2.89
-2975	I	*	2.84
-2950	I	*	2.58
-2925	I	*	2.53
-2900	I	*	2.60
-2875	I	*	2.35
-2850	I	*	2.42
-2825	I	*	2.14
-2800	I	*	1.91
-2775	I	*	1.74
-2750	I	*	1.79
-2725	I	*	1.62
-2700	I	*	1.46

XBOT= -2700
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 3700 E SECONDARY FIELD QUADRATURE HSQ/I

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LINE= 4000. E FREQUENCY=3HZ N004

173

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	HMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
-3700. N	2.94	0.00	0.00	0.00	-4.10	2.60	0.16	0.00	-80.12	4.10	-2.60	0.00	0.00	-3700. N
-3675. N	2.94	0.00	0.00	0.00	-4.10	2.60	0.16	0.00	-81.76	4.10	-2.60	0.00	0.00	-3675. N
-3650. N	2.94	0.48	-8.30	4.40	-4.10	2.60	0.17	97.90	-1.75	-4.20	1.80	2.56	-6.86	-3650. N
-3625. N	2.94	0.48	-8.00	4.30	-4.10	2.60	0.17	96.07	-3.34	-3.90	1.70	2.42	-6.37	-3625. N
-3600. N	2.94	0.48	-8.10	4.30	-4.10	2.60	0.17	94.33	-4.91	-4.00	1.70	2.42	-6.53	-3600. N
-3575. N	2.94	0.49	-7.70	4.10	-4.10	2.60	0.18	94.63	-4.73	-3.60	1.50	2.18	-6.00	-3575. N
-3550. N	2.94	0.49	-7.60	4.20	-4.10	2.60	0.18	93.08	-6.20	-3.50	1.60	2.33	-5.83	-3550. N
-3525. N	2.94	0.48	-7.50	4.10	-4.10	2.60	0.18	89.75	-9.32	-3.40	1.50	2.14	-5.55	-3525. N
-3500. N	2.94	0.50	-7.50	4.10	-4.10	2.60	0.18	92.12	-7.27	-3.40	1.50	2.23	-5.78	-3500. N
-3475. N	2.94	0.50	-7.60	4.00	-4.10	2.60	0.19	90.86	-8.56	-3.50	1.40	2.08	-5.95	-3475. N
-3450. N	2.94	0.50	-7.40	4.00	-4.10	2.60	0.19	89.70	-9.76	-3.30	1.40	2.08	-5.61	-3450. N
-3425. N	2.94	0.51	-7.30	4.10	-4.10	2.60	0.19	90.43	-9.18	-3.20	1.50	2.27	-5.55	-3425. N
-3400. N	2.94	0.52	-7.30	4.20	-4.10	2.60	0.19	91.23	-8.51	-3.20	1.60	2.47	-5.66	-3400. N
-3375. N	2.94	0.53	-7.20	4.00	-4.10	2.60	0.20	92.10	-7.73	-3.10	1.40	2.20	-5.59	-3375. N
-3350. N	2.94	0.54	-7.20	4.10	-4.10	2.60	0.20	93.07	-6.84	-3.10	1.50	2.40	-5.69	-3350. N
-3325. N	2.94	0.54	-7.30	4.10	-4.10	2.60	0.20	92.41	-7.54	-3.20	1.50	2.40	-5.88	-3325. N
-3300. N	2.94	0.55	-7.20	4.10	-4.10	2.60	0.20	93.57	-6.42	-3.10	1.50	2.45	-5.80	-3300. N
-3275. N	2.94	0.54	-7.00	4.00	-4.10	2.60	0.20	91.46	-8.58	-2.90	1.40	2.24	-5.33	-3275. N
-3250. N	2.94	0.55	-6.90	4.10	-4.10	2.60	0.20	92.85	-7.21	-2.80	1.50	2.45	-5.24	-3250. N
-3225. N	2.94	0.55	-6.80	4.00	-4.10	2.60	0.20	92.66	-7.41	-2.70	1.40	2.29	-5.05	-3225. N
-3200. N	2.94	0.54	-6.80	4.20	-4.10	2.60	0.20	90.92	-9.17	-2.70	1.60	2.56	-4.96	-3200. N
-3175. N	2.94	0.55	-6.60	3.90	-4.05	2.60	0.20	92.66	-7.41	-2.55	1.30	2.12	-4.77	-3175. N
-3150. N	2.94	0.54	-6.70	3.90	-4.05	2.60	0.20	91.16	-8.91	-2.65	1.30	2.08	-4.87	-3150. N
-3125. N	2.94	0.55	-6.80	3.90	-4.05	2.60	0.20	93.15	-6.88	-2.75	1.30	2.12	-5.14	-3125. N
-3100. N	2.94	0.50	-6.70	3.80	-4.05	2.60	0.20	85.07	-14.93	-2.65	1.20	1.78	-4.51	-3100. N
-3075. N	2.94	0.54	-6.80	3.90	-4.05	2.60	0.20	92.41	-7.54	-2.75	1.30	2.08	-5.05	-3075. N
-3050. N	2.94	0.52	-6.60	3.80	-4.05	2.60	0.20	89.62	-10.24	-2.55	1.20	1.85	-4.51	-3050. N
-3025. N	2.94	0.52	-6.60	3.90	-4.05	2.60	0.20	90.37	-9.43	-2.55	1.30	2.01	-4.51	-3025. N
-3000. N	2.94	0.51	-6.50	3.90	-4.05	2.60	0.19	89.47	-10.21	-2.45	1.30	1.97	-4.25	-3000. N
-2975. N	2.94	0.50	-6.70	3.90	-4.05	2.60	0.19	88.65	-10.88	-2.65	1.30	1.93	-4.51	-2975. N
-2950. N	2.94	0.48	-6.40	4.00	-4.05	2.60	0.19	86.11	-13.17	-2.35	1.40	1.99	-3.84	-2950. N
-2925. N	2.94	0.48	-5.90	3.90	-4.05	2.60	0.19	87.22	-11.96	-1.85	1.30	1.85	-3.02	-2925. N
-2900. N	2.94	0.46	-6.50	3.80	-4.05	2.60	0.18	84.75	-14.08	-2.45	1.20	1.64	-3.83	-2900. N
-2875. N	2.94	0.45	-6.00	3.70	-4.05	2.60	0.18	84.14	-14.42	-1.95	1.10	1.47	-2.98	-2875. N
-2850. N	2.94	0.44	-5.90	3.90	-4.05	2.60	0.18	83.58	-14.70	-1.85	1.30	1.70	-2.77	-2850. N
-2825. N	2.94	0.42	-6.00	3.80	-4.05	2.60	0.18	81.11	-16.63	-1.95	1.20	1.50	-2.79	-2825. N
-2800. N	2.94	0.42	-5.90	3.70	-4.05	2.60	0.17	82.54	-15.11	-1.85	1.10	1.37	-2.64	-2800. N
-2775. N	2.94	0.41	-6.00	3.70	-4.05	2.60	0.17	82.06	-15.25	-1.95	1.10	1.34	-2.72	-2775. N
-2750. N	2.94	0.40	-6.10	3.60	-4.05	2.60	0.17	81.58	-15.36	-2.05	1.00	1.19	-2.79	-2750. N
-2725. N	2.94	0.00	0.00	0.00	-4.05	2.60	0.16	0.00	-81.76	4.05	-2.60	0.00	0.00	-2725. N
-2700. N	2.94	0.00	0.00	0.00	-4.05	2.60	0.16	0.00	-80.12	4.05	-2.60	0.00	0.00	-2700. N

MOORE PARAGON PARALELO

XTOP= -3700.

XINC= 25.00

POWER LINES

4	-3700.	*		I	-80.12
5	-3675.	*		I	-81.76
6	-3650.			*I	-1.75
7	-3625.			*I	-3.34
8	-3600.		*	I	-4.91
9	-3575.		*	I	-4.73
10	-3550.		*	I	-6.20
11	-3525.		*	I	-9.32
12	-3500.		*	I	-7.27
13	-3475.		*	I	-8.56
14	-3450.		*	I	-9.76
15	-3425.		*	I	-9.18
16	-3400.		*	I	-8.51
17	-3375.		*	I	-7.73
18	-3350.		*	I	-6.84
19	-3325.		*	I	-7.54
20	-3300.		*	I	-6.42
21	-3275.		*	I	-8.58
22	-3250.		*	I	-7.21
23	-3225.		*	I	-7.41
24	-3200.		*	I	-9.17
25	-3175.		*	I	-7.41
26	-3150.		*	I	-8.91
27	-3125.		*	I	-6.88
28	-3100.	*		I	-14.93
29	-3075.		*	I	-7.54
30	-3050.		*	I	-10.24
31	-3025.		*	I	-9.43
32	-3000.		*	I	-10.21
33	-2975.		*	I	-10.88
34	-2950.		*	I	-13.17
35	-2925.		*	I	-11.96
36	-2900.	*		I	-14.08
37	-2875.	*		I	-14.42
38	-2850.	*		I	-14.70
39	-2825.	*		I	-16.63
40	-2800.	*		I	-15.11
41	-2775.	*		I	-15.25
42	-2750.	*		I	-15.36
43	-2725.	*		I	-81.76
44	-2700.	*		I	-80.12

XBOT= -2700.
YMIN= -81.76

YINC= 1.318
YMAX= 50.00

LINE 4000. E MAGNETOMETRIC RESESTIVITY MMR

MOURE PARAGON PAMAF O

XTOP= -3700

XINC= 25.00

4	-3700	*	I		-2.60
5	-3675	*	I		-2.60
6	-3650		I	*	1.60
7	-3625		I	*	1.70
8	-3600		I	*	1.70
9	-3575		I	*	1.50
10	-3550		I	*	1.60
11	-3525		I	*	1.50
12	-3500		I	*	1.50
13	-3475		I	*	1.40
14	-3450		I	*	1.40
15	-3425		I	*	1.50
16	-3400		I	*	1.60
17	-3375		I	*	1.40
18	-3350		I	*	1.50
19	-3325		I	*	1.50
20	-3300		I	*	1.50
21	-3275		I	*	1.40
22	-3250		I	*	1.50
23	-3225		I	*	1.40
24	-3200		I	*	1.60
25	-3175		I	*	1.30
26	-3150		I	*	1.30
27	-3125		I	*	1.30
28	-3100		I	*	1.20
29	-3075		I	*	1.30
30	-3050		I	*	1.20
31	-3025		I	*	1.30
32	-3000		I	*	1.30
33	-2975		I	*	1.30
34	-2950		I	*	1.40
35	-2925		I	*	1.30
36	-2900		I	*	1.20
37	-2875		I	*	1.10
38	-2850		I	*	1.30
39	-2825		I	*	1.20
40	-2800		I	*	1.10
41	-2775		I	*	1.10
42	-2750		I	*	1.00
43	-2725	*	I		-2.60
44	-2700	*	I		-2.60

XBOT= -2700

YINC= 0.5100E-01

YMIN= -2.600

YMAX= 2.500

LINE 4000. E RELATIVE PHASE SHIFT RPS

MOORE PARAGON PARAFIC

XTOP= -3700

XINC= 25.00

1									
2									
3									
4								0.00	
5								0.00	
6								2.56	
7								2.42	
8								2.42	
9								2.18	
10								2.33	
11								2.14	
12								2.23	
13								2.08	
14								2.08	
15								2.27	
16								2.47	
17								2.20	
18								2.40	
19								2.40	
20								2.45	
21								2.24	
22								2.45	
23								2.29	
24								2.56	
25								2.12	
26								2.08	
27								2.12	
28								1.78	
29								2.08	
30								1.85	
31								2.01	
32								1.97	
33								1.93	
34								1.99	
35								1.85	
36								1.64	
37								1.47	
38								1.70	
39								1.50	
40								1.37	
41								1.34	
42								1.19	
43								0.00	
44								0.00	

XBOT= -2700
YMIN= -10.00

YINC= 0.2000
YMAX= 10.00

LINE 4000 E SECONDARY FIELD QUADRATURE HSD/I

UJ MCH EBARAC N 274 C

LINE= 4300 E FREQUENCY=3HZ N004

STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
			PFE	RPS	PFE	RPS								
-3700 N	2.94	0.49	-8.50	4.70	-4.15	2.60	0.16	103.07	2.48	-4.35	2.10	3.05	-7.25	-3700 N
-3675 N	2.94	0.51	-8.30	4.60	-4.15	2.60	0.17	104.18	3.48	-4.15	2.00	3.03	-7.20	-3675 N
-3650 N	2.94	0.51	-8.20	4.40	-4.15	2.60	0.17	101.20	1.03	-4.05	1.80	2.72	-7.03	-3650 N
-3625 N	2.94	0.51	-8.00	4.30	-4.15	2.60	0.18	98.35	-1.46	-3.85	1.70	2.57	-6.68	-3625 N
-3600 N	2.94	0.51	-7.90	4.30	-4.15	2.60	0.18	95.62	-3.98	-3.75	1.70	2.57	-6.51	-3600 N
-3575 N	2.94	0.52	-7.80	4.40	-4.15	2.60	0.19	94.84	-4.81	-3.65	1.80	2.78	-6.46	-3575 N
-3550 N	2.94	0.55	-7.30	4.20	-4.15	2.60	0.19	97.65	-2.25	-3.15	1.60	2.61	-5.89	-3550 N
-3525 N	2.94	0.52	-7.40	4.10	-4.15	2.60	0.20	89.95	-9.88	-3.25	1.50	2.32	-5.75	-3525 N
-3500 N	2.94	0.51	-7.40	4.00	-4.15	2.60	0.20	86.04	-14.08	-3.25	1.40	2.12	-5.64	-3500 N
-3475 N	2.94	0.54	-7.30	3.80	-4.15	2.60	0.21	88.94	-11.42	-3.15	1.20	1.92	-5.79	-3475 N
-3450 N	2.94	0.56	-7.20	3.60	-4.15	2.60	0.21	90.17	-10.38	-3.05	1.00	1.66	-5.81	-3450 N
-3425 N	2.94	0.57	-7.00	3.80	-4.15	2.60	0.22	89.86	-10.94	-2.85	1.20	2.03	-5.53	-3425 N
-3400 N	2.94	0.57	-6.70	3.90	-4.15	2.60	0.22	88.13	-13.06	-2.55	1.30	2.20	-4.94	-3400 N
-3375 N	2.94	0.58	-6.80	3.80	-4.15	2.60	0.22	88.10	-13.33	-2.65	1.20	2.07	-5.23	-3375 N
-3350 N	2.94	0.58	-6.80	3.70	-4.15	2.60	0.23	86.72	-15.10	-2.65	1.10	1.89	-5.23	-3350 N
-3325 N	2.94	0.58	-6.90	3.80	-4.15	2.60	0.23	85.55	-16.66	-2.75	1.20	2.07	-5.43	-3325 N
-3300 N	2.94	0.56	-6.90	3.80	-4.15	2.60	0.23	81.67	-21.38	-2.75	1.20	1.99	-5.24	-3300 N
-3275 N	2.94	0.58	-6.80	3.80	-4.15	2.60	0.24	83.83	-19.02	-2.65	1.20	2.07	-5.23	-3275 N
-3250 N	2.94	0.59	-6.70	3.90	-4.15	2.60	0.24	84.73	-18.09	-2.55	1.30	2.28	-5.12	-3250 N
-3225 N	2.94	0.58	-6.80	3.80	-4.15	2.60	0.24	82.97	-20.25	-2.65	1.20	2.07	-5.23	-3225 N
-3200 N	2.94	0.57	-6.60	3.80	-4.15	2.60	0.24	81.43	-22.11	-2.45	1.20	2.03	-4.75	-3200 N
-3175 N	2.94	0.56	-6.50	3.90	-4.20	2.60	0.24	80.10	-23.65	-2.30	1.30	2.16	-4.38	-3175 N
-3150 N	2.94	0.55	-6.40	3.90	-4.20	2.60	0.24	78.98	-24.89	-2.20	1.30	2.12	-4.12	-3150 N
-3125 N	2.94	0.54	-6.30	4.00	-4.20	2.60	0.24	78.05	-25.83	-2.10	1.40	2.24	-3.86	-3125 N
-3100 N	2.94	0.54	-6.40	4.10	-4.20	2.60	0.23	78.75	-24.78	-2.20	1.50	2.40	-4.64	-3100 N
-3075 N	2.94	0.53	-6.50	4.20	-4.20	2.60	0.23	78.18	-25.16	-2.30	1.60	2.52	-4.15	-3075 N
-3050 N	2.94	0.45	-6.60	4.10	-4.20	2.60	0.23	67.29	-37.21	-2.40	1.50	2.00	-3.67	-3050 N
-3025 N	2.94	0.51	-6.30	3.60	-4.20	2.60	0.22	77.47	-25.23	-2.10	1.00	1.51	-3.64	-3025 N
-3000 N	2.94	0.50	-6.30	3.70	-4.20	2.60	0.22	77.30	-24.97	-2.10	1.10	1.63	-3.57	-3000 N
-2975 N	2.94	0.50	-6.30	3.70	-4.20	2.60	0.22	78.83	-22.84	-2.10	1.10	1.63	-3.57	-2975 N
-2950 N	2.94	0.51	-6.20	3.80	-4.20	2.60	0.21	82.12	-18.88	-2.00	1.20	1.82	-3.47	-2950 N
-2925 N	2.94	0.49	-6.20	3.80	-4.20	2.60	0.21	80.71	-19.92	-2.00	1.20	1.75	-3.33	-2925 N
-2900 N	2.94	0.47	-6.10	3.90	-4.20	2.60	0.20	79.29	-20.88	-1.90	1.30	1.81	-3.04	-2900 N
-2875 N	2.94	0.42	-6.30	3.80	-4.20	2.60	0.20	72.65	-26.89	-2.10	1.20	1.50	-3.00	-2875 N
-2850 N	2.94	0.44	-6.20	3.80	-4.20	2.60	0.19	78.12	-20.96	-2.00	1.20	1.57	-2.99	-2850 N
-2825 N	2.94	0.45	-6.30	3.70	-4.20	2.60	0.19	82.07	-16.72	-2.10	1.10	1.47	-3.21	-2825 N
-2800 N	2.94	0.42	-6.60	3.90	-4.20	2.60	0.18	78.74	-19.26	-2.40	1.30	1.62	-3.43	-2800 N
-2775 N	2.94	0.40	-6.50	3.90	-4.20	2.60	0.18	77.14	-20.16	-2.30	1.30	1.54	-3.13	-2775 N
-2750 N	2.94	0.39	-6.60	4.00	-4.20	2.60	0.17	77.39	-19.38	-2.40	1.40	1.62	-3.18	-2750 N
-2725 N	2.94	0.37	-5.70	4.10	-4.20	2.60	0.17	75.58	-20.33	-1.50	1.50	1.65	-1.89	-2725 N
-2700 N	2.94	0.38	-5.90	4.20	-4.20	2.60	0.16	79.93	-16.23	-1.70	1.60	1.80	-2.20	-2700 N

MOORE PARACON PARALIC

XTOP= -3700.

XINC= 25.00

4	-3700			I *	2.48
5	-3675			I *	3.48
6	-3650			I *	1.03
7	-3625			* I	-1.46
8	-3600			I	-3.98
9	-3575			* I	-4.81
10	-3550			* I	-2.25
11	-3525			I	-9.88
12	-3500		*	I	-14.08
13	-3475		*	I	-11.42
14	-3450		*	I	-10.38
15	-3425		*	I	-10.94
16	-3400		*	I	-13.06
17	-3375		*	I	-13.33
18	-3350		*	I	-15.10
19	-3325		*	I	-16.66
20	-3300		*	I	-21.38
21	-3275		*	I	-19.02
22	-3250		*	I	-18.09
23	-3225		*	I	-20.25
24	-3200		*	I	-22.11
25	-3175		*	I	-23.65
26	-3150		*	I	-24.89
27	-3125		*	I	-25.83
28	-3100		*	I	-24.78
29	-3075		*	I	-25.16
30	-3050	*		I	-37.21
31	-3025		*	I	-25.23
32	-3000		*	I	-24.97
33	-2975		*	I	-22.84
34	-2950		*	I	-18.88
35	-2925		*	I	-19.92
36	-2900		*	I	-20.88
37	-2875	*		I	-26.89
38	-2850		*	I	-20.96
39	-2825		*	I	-16.72
40	-2800		*	I	-19.28
41	-2775		*	I	-20.16
42	-2750		*	I	-19.38
43	-2725		*	I	-20.33
44	-2700		*	I	-16.23

XBOT= -2700.

YMIN= -50.00

YINC= 1.000

YMAX= 50.00

LINE 4300. E MAGNETOMETRIC RESESTIVITY MMR

CUI ARACUN FAPARI

XTOP= -3700

XINC= 25.00

4	-3700	I		*	2.10
5	-3675	I		*	2.00
6	-3650	I		*	1.80
7	-3625	I		*	1.70
8	-3600	I		*	1.70
9	-3575	I		*	1.80
10	-3550	I		*	1.60
11	-3525	I		*	1.50
12	-3500	I		*	1.40
13	-3475	I		*	1.20
14	-3450	I	*		1.00
15	-3425	I	*		1.20
16	-3400	I	*		1.30
17	-3375	I	*		1.20
18	-3350	I	*		1.10
19	-3325	I	*		1.20
20	-3300	I	*		1.20
21	-3275	I	*		1.20
22	-3250	I	*		1.30
23	-3225	I	*		1.20
24	-3200	I	*		1.20
25	-3175	I	*		1.30
26	-3150	I	*		1.30
27	-3125	I	*		1.40
28	-3100	I	*		1.50
29	-3075	I	*		1.60
30	-3050	I	*		1.50
31	-3025	I	*		1.00
32	-3000	I	*		1.10
33	-2975	I	*		1.10
34	-2950	I	*		1.20
35	-2925	I	*		1.20
36	-2900	I	*		1.30
37	-2875	I	*		1.20
38	-2850	I	*		1.20
39	-2825	I	*		1.10
40	-2800	I	*		1.30
41	-2775	I	*		1.30
42	-2750	I	*		1.40
43	-2725	I	*		1.50
44	-2700	I	*		1.60

XBOT= -2700

YINC= 0.5000E-01

YMIN= -2.500

YMAX= 2.500

LINE 4300. E RELATIVE PHASE SHIFT RPS

MOORE PAPER P. 247 C

XTOP= -3700

XINC= 25.00

1	-3700	I	*	3.05
2	-3675	I	*	3.03
3	-3650	I	*	2.72
4	-3625	I	*	2.57
5	-3600	I	*	2.57
6	-3575	I	*	2.78
7	-3550	I	*	2.61
8	-3525	I	*	2.32
9	-3500	I	*	2.12
10	-3475	I	*	1.92
11	-3450	I	*	1.66
12	-3425	I	*	2.03
13	-3400	I	*	2.20
14	-3375	I	*	2.07
15	-3350	I	*	1.89
16	-3325	I	*	2.07
17	-3300	I	*	1.99
18	-3275	I	*	2.07
19	-3250	I	*	2.28
20	-3225	I	*	2.07
21	-3200	I	*	2.03
22	-3175	I	*	2.16
23	-3150	I	*	2.12
24	-3125	I	*	2.24
25	-3100	I	*	2.40
26	-3075	I	*	2.52
27	-3050	I	*	2.00
28	-3025	I	*	1.51
29	-3000	I	*	1.63
30	-2975	I	*	1.63
31	-2950	I	*	1.82
32	-2925	I	*	1.75
33	-2900	I	*	1.81
34	-2875	I	*	1.50
35	-2850	I	*	1.57
36	-2825	I	*	1.47
37	-2800	I	*	1.62
38	-2775	I	*	1.54
39	-2750	I	*	1.62
40	-2725	I	*	1.65
41	-2700	I	*	1.80

XBOT= -2700

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 4300. E SECONDARY FIELD QUADRATURE HSQ/I

XYNETICS, INC. NO. RECORDS 52
NO. OF DRAWINGS 2

MOORE PARAGON PARALIO

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PROGRAM MIP2 . CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

3HZ. RRMIP SURVEY MT PEARSE TASMANIA 063R ARRAY N005

19-1393 2/2

MOORE PARSONS PAPATIO

INTERP TAPE FLAG= 0 GRIDDATA TAPE FLAG= 0

128196

LINE POSITIONING MULTIPLYING FACTOR= 1.0

MOORE PARAGON PARAFIC

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UNITS FLAG= CURRENT ELECTRODE CO-ORDS= 2900. E -4500. N 4900. E -4500. N

128197

1 PLOT SCALE= 500. HN SCALE 10. PFE & RPS SCALE= 1. HSQ & HSP SCALE= 1.

4 ORIGIN CO-ORDS= 3400. E -4000. N ARRAY IDENTIFIER= MTP5 ANNOTATION SUPPRESSION FLAG= 0

6 SPLINE INTERVAL= 0.

8 PLOT BASE LEVELS FOR PFE, RPS, HSQ, HSP ARE 0.00 0.00 0.00 0.00

11 PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

12 HN = 0
13 MMR = 1
14 PFE = 0
15 RPS = 1
16 HSQ = 1
17 HSP = 0

21 FOR HN, MMR 100.00 0.00

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LINE	STATION	CURRENT	HP	FIELD		OFFSET		HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
				PFE	RPS	PFE	RPS								
6	-5000.N	3.01	0.43	-6.80	4.10	-4.05	2.60	0.16	89.29	-8.57	-2.75	1.50	1.87	-3.93	-5000.N
7	-4975.N	3.01	0.41	-7.20	4.50	-4.05	2.60	0.17	82.20	-14.75	-3.15	1.90	2.26	-4.29	-4975.N
8	-4950.N	3.01	0.42	-7.20	4.40	-4.05	2.60	0.17	81.29	-16.06	-3.15	1.80	2.19	-4.40	-4950.N
9	-4925.N	3.01	0.40	-7.40	4.40	-4.05	2.60	0.18	74.73	-22.47	-3.35	1.80	2.09	-4.45	-4925.N
10	-4900.N	3.01	0.45	-7.50	4.20	-4.05	2.60	0.18	81.17	-17.35	-3.45	1.60	2.09	-5.16	-4900.N
11	-4875.N	3.01	0.44	-7.30	4.10	-4.05	2.60	0.19	76.64	-22.28	-3.25	1.50	1.91	-4.75	-4875.N
12	-4850.N	3.01	0.48	-7.00	4.10	-4.05	2.60	0.20	80.76	-18.99	-2.95	1.50	2.09	-4.70	-4850.N
13	-4825.N	3.01	0.51	-7.10	4.00	-4.05	2.60	0.20	82.94	-17.42	-3.05	1.40	2.07	-5.17	-4825.N
14	-4800.N	3.01	0.54	-7.20	4.10	-4.10	2.55	0.21	84.96	-15.88	-3.10	1.55	2.43	-5.56	-4800.N
15	-4775.N	3.01	0.53	-7.30	4.00	-4.10	2.55	0.22	80.75	-20.98	-3.20	1.45	2.23	-5.63	-4775.N
16	-4750.N	3.01	0.59	-7.20	4.10	-4.10	2.55	0.22	87.17	-14.43	-3.10	1.55	2.65	-6.08	-4750.N
17	-4725.N	3.01	0.58	-7.50	4.10	-4.10	2.55	0.23	83.23	-19.41	-3.40	1.55	2.61	-6.55	-4725.N
18	-4700.N	3.01	0.62	-6.80	3.90	-4.10	2.55	0.24	86.58	-15.97	-2.70	1.35	2.43	-5.56	-4700.N
19	-4675.N	3.01	0.66	-6.70	3.80	-4.10	2.55	0.24	89.88	-12.34	-2.60	1.25	2.39	-5.70	-4675.N
20	-4650.N	3.01	0.65	-7.10	3.70	-4.10	2.55	0.25	86.55	-16.77	-3.00	1.15	2.17	-6.48	-4650.N
21	-4625.N	3.01	0.68	-6.80	3.60	-4.10	2.55	0.25	88.79	-14.26	-2.70	1.05	2.07	-6.10	-4625.N
22	-4600.N	3.01	0.70	-6.80	3.70	-4.10	2.55	0.26	89.90	-13.06	-2.70	1.15	2.33	-6.28	-4600.N
23	-4575.N	3.01	0.72	-6.90	3.60	-4.10	2.55	0.26	91.26	-11.45	-2.80	1.05	2.19	-6.70	-4575.N
24	-4550.N	3.01	0.72	-6.90	3.50	-4.10	2.55	0.26	90.40	-12.70	-2.80	0.95	1.98	-6.70	-4550.N
25	-4525.N	3.01	0.73	-7.00	3.60	-4.10	2.55	0.27	91.12	-11.81	-2.90	1.05	2.22	-7.03	-4525.N
26	-4500.N	3.01	0.70	-7.50	3.60	-4.10	2.55	0.27	87.21	-17.05	-3.40	1.05	2.13	-7.91	-4500.N
27	-4475.N	3.01	0.70	-6.90	3.60	-4.05	2.60	0.27	87.38	-16.80	-2.85	1.00	2.03	-6.63	-4475.N
28	-4450.N	3.01	0.73	-6.90	3.80	-4.05	2.60	0.26	91.65	-11.04	-2.85	1.20	2.54	-6.91	-4450.N
29	-4425.N	3.01	0.70	-7.30	3.90	-4.05	2.60	0.26	88.73	-14.77	-3.25	1.30	2.64	-7.56	-4425.N
30	-4400.N	3.01	0.69	-7.50	3.90	-4.05	2.60	0.26	88.62	-14.72	-3.45	1.30	2.60	-7.91	-4400.N
31	-4375.N	3.01	0.66	-7.40	4.00	-4.05	2.60	0.25	86.18	-17.59	-3.35	1.40	2.68	-7.35	-4375.N
32	-4350.N	3.01	0.68	-7.50	4.00	-4.05	2.60	0.25	90.55	-11.79	-3.45	1.40	2.76	-7.79	-4350.N
33	-4325.N	3.01	0.69	-7.70	4.10	-4.05	2.65	0.24	93.97	-7.35	-3.70	1.45	2.90	-8.48	-4325.N
34	-4300.N	3.01	0.65	-7.80	4.30	-4.00	2.65	0.24	90.77	-10.98	-3.80	1.65	3.11	-8.21	-4300.N
35	-4275.N	3.01	0.67	-7.90	4.30	-4.00	2.65	0.23	96.14	-4.46	-3.90	1.65	3.20	-8.68	-4275.N
36	-4250.N	3.01	0.62	-8.20	4.30	-4.00	2.65	0.22	91.60	-9.44	-4.20	1.65	2.97	-8.65	-4250.N
37	-4225.N	3.01	0.60	-8.50	4.40	-4.00	2.65	0.22	91.42	-9.36	-4.50	1.75	3.04	-8.97	-4225.N
38	-4200.N	3.01	0.50	-8.80	4.50	-4.00	2.65	0.21	78.67	-22.52	-4.80	1.85	2.68	-7.97	-4200.N
39	-4175.N	3.01	0.54	-8.80	4.30	-4.00	2.65	0.20	87.82	-12.44	-4.80	1.65	2.58	-8.61	-4175.N
40	-4150.N	3.01	0.55	-8.90	4.40	-4.00	2.65	0.20	92.54	-7.36	-4.90	1.75	2.79	-8.95	-4150.N
41	-4125.N	3.01	0.42	-9.10	4.60	-4.00	2.65	0.19	73.15	-25.61	-5.10	1.95	2.37	-7.12	-4125.N
42	-4100.N	3.01	0.52	-9.20	4.70	-4.00	2.65	0.18	93.79	-5.72	-5.20	2.05	3.09	-8.98	-4100.N
43	-4075.N	3.01	0.48	-9.80	5.10	-4.00	2.65	0.18	89.68	-9.18	-5.80	2.45	3.41	-9.25	-4075.N
44	-4050.N	3.01	0.47	-1.05	5.10	-4.00	2.65	0.17	90.96	-7.76	2.95	2.45	3.34	4.61	-4050.N
45	-4025.N	3.01	0.42	-1.07	5.30	-4.00	2.65	0.17	84.20	-13.09	2.93	2.65	3.23	4.09	-4025.N
46	-4000.N	3.01	0.44	-10.90	5.50	-4.00	2.65	0.16	91.36	-6.91	-6.90	2.85	3.64	-10.09	-4000.N

DAY MOORE PARAGON PARAFIC

1	-5000.				I		-8.57	1
2	-4975.				I		-14.75	2
3	-4950.				I		-16.06	3
4	-4925.	*			I		-22.47	4
5	-4900.		*		I		-17.35	5
6	-4875.	*			I		-22.28	6
7	-4850.		*		I		-18.99	7
8	-4825.		*		I		-17.42	8
9	-4800.		*		I		-15.88	9
10	-4775.	*			I		-20.98	10
11	-4750.		*		I		-14.43	11
12	-4725.	*			I		-19.41	12
13	-4700.		*		I		-15.97	13
14	-4675.		*	*	I		-12.34	14
15	-4650.		*		I		-16.77	15
16	-4625.		*	*	I		-14.26	16
17	-4600.		*	*	I		-13.06	17
18	-4575.		*	*	I		-11.45	18
19	-4550.		*	*	I		-12.70	19
20	-4525.		*	*	I		-11.81	20
21	-4500.		*		I		-17.05	21
22	-4475.	*			I		-16.80	22
23	-4450.		*	*	I		-11.04	23
24	-4425.		*	*	I		-14.77	24
25	-4400.		*	*	I		-14.72	25
26	-4375.	*			I		-17.59	26
27	-4350.		*	*	I		-11.79	27
28	-4325.		*	*	I		-7.35	28
29	-4300.		*	*	I		-10.98	29
30	-4275.		*	*	I		-4.46	30
31	-4250.		*	*	I		-9.44	31
32	-4225.		*	*	I		-9.36	32
33	-4200.	*			I		-22.52	33
34	-4175.		*	*	I		-12.44	34
35	-4150.		*	*	I		-7.36	35
36	-4125.	*			I		-25.61	36
37	-4100.		*	*	I		-5.72	37
38	-4075.		*	*	I		-9.18	38
39	-4050.		*	*	I		-7.76	39
40	-4025.		*	*	I		-13.09	40
41	-4000.		*	*	I		-6.91	41

XBOT= -4000.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 3400. E MAGNETOMETRIC RESESTIVITY MMR

MAGNETOMETRIC RESESTIVITY MMR

LINE#	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSG/I	HSP/I	STATION
				PFE	RPS	PFE	RPS								
5	-5000 N	3.01	0.45	-4.60	7.10	-1.80	5.40	0.16	92.92	-5.70	-2.80	1.70	2.22	-4.19	-5000 N
6	-4975 N	3.01	0.45	-4.80	7.30	-1.80	5.40	0.16	90.90	-7.48	-3.00	1.90	2.48	-4.49	-4975 N
7	-4950 N	3.01	0.46	-4.80	7.30	-1.80	5.35	0.17	90.96	-7.60	-3.00	1.95	2.60	-4.58	-4950 N
8	-4925 N	3.01	0.48	-4.70	7.10	-1.80	5.35	0.17	92.97	-6.03	-2.90	1.75	2.44	-4.62	-4925 N
9	-4900 N	3.01	0.49	-4.80	7.20	-1.80	5.30	0.18	93.02	-6.10	-3.00	1.90	2.70	-4.88	-4900 N
10	-4875 N	3.01	0.50	-4.90	7.20	-1.80	5.30	0.18	93.11	-6.14	-3.10	1.90	2.75	-5.15	-4875 N
11	-4850 N	3.01	0.50	-5.00	7.10	-1.80	5.25	0.18	91.41	-7.80	-3.20	1.85	2.68	-5.32	-4850 N
12	-4825 N	3.01	0.53	-4.90	7.00	-1.80	5.25	0.18	95.21	-4.43	-3.10	1.75	2.69	-5.46	-4825 N
13	-4800 N	3.01	0.53	-4.90	7.00	-1.85	5.20	0.19	93.65	-5.97	-3.05	1.80	2.77	-5.37	-4800 N
14	-4775 N	3.01	0.53	-5.00	7.10	-1.85	5.20	0.19	92.20	-7.44	-3.15	1.90	2.92	-5.55	-4775 N
15	-4750 N	3.01	0.54	-5.00	7.10	-1.85	5.15	0.19	92.60	-7.17	-3.15	1.95	3.05	-5.65	-4750 N
16	-4725 N	3.01	0.54	-4.90	7.10	-1.85	5.15	0.20	91.37	-8.47	-3.05	1.95	3.05	-5.47	-4725 N
17	-4700 N	3.01	0.55	-5.10	7.20	-1.85	5.10	0.20	91.95	-8.00	-3.25	2.10	3.35	-5.94	-4700 N
18	-4675 N	3.01	0.56	-5.00	7.10	-1.85	5.10	0.20	92.61	-7.42	-3.15	2.00	3.25	-5.86	-4675 N
19	-4650 N	3.01	0.56	-5.10	7.00	-1.85	5.05	0.20	91.74	-8.38	-3.25	1.95	3.17	-6.05	-4650 N
20	-4625 N	3.01	0.58	-5.20	7.00	-1.85	5.05	0.20	94.24	-5.88	-3.35	1.95	3.28	-6.46	-4625 N
21	-4600 N	3.01	0.58	-5.40	6.90	-1.90	5.00	0.21	93.61	-6.57	-3.50	1.90	3.19	-6.74	-4600 N
22	-4575 N	3.01	0.57	-5.50	6.70	-1.90	5.00	0.21	91.52	-8.78	-3.60	1.70	2.81	-6.82	-4575 N
23	-4550 N	3.01	0.58	-5.50	6.80	-1.90	4.95	0.21	92.77	-7.51	-3.60	1.85	3.11	-6.94	-4550 N
24	-4525 N	3.01	0.59	-5.50	6.80	-1.90	4.95	0.21	94.16	-6.08	-3.60	1.85	3.16	-7.06	-4525 N
25	-4500 N	3.01	0.59	-5.60	6.90	-1.90	4.90	0.21	94.09	-6.16	-3.70	2.00	3.42	-7.25	-4500 N
26	-4475 N	3.01	0.59	-5.60	6.80	-1.90	4.90	0.21	94.16	-6.08	-3.70	1.90	3.25	-7.25	-4475 N
27	-4450 N	3.01	0.58	-5.70	6.90	-1.90	4.85	0.21	92.77	-7.51	-3.80	2.05	3.45	-7.32	-4450 N
28	-4425 N	3.01	0.58	-5.70	6.80	-1.90	4.85	0.21	93.12	-7.11	-3.80	1.95	3.28	-7.32	-4425 N
29	-4400 N	3.01	0.57	-5.70	6.90	-1.95	4.80	0.21	92.00	-8.23	-3.75	2.10	3.47	-7.10	-4400 N
30	-4375 N	3.01	0.57	-5.80	6.90	-1.95	4.80	0.20	92.62	-7.55	-3.85	2.10	3.47	-7.29	-4375 N
31	-4350 N	3.01	0.57	-6.00	7.00	-1.95	4.75	0.20	93.37	-6.72	-4.05	2.25	3.72	-7.67	-4350 N
32	-4325 N	3.01	0.57	-6.00	7.00	-1.95	4.75	0.20	94.27	-5.76	-4.05	2.25	3.72	-7.67	-4325 N
33	-4300 N	3.01	0.56	-6.00	7.00	-1.95	4.70	0.20	93.62	-6.34	-4.05	2.30	3.73	-7.53	-4300 N
34	-4275 N	3.01	0.57	-6.30	7.10	-1.95	4.70	0.20	96.45	-3.49	-4.35	2.40	3.97	-8.24	-4275 N
35	-4250 N	3.01	0.57	-6.60	7.20	-1.95	4.65	0.19	97.74	-2.19	-4.65	2.55	4.21	-8.81	-4250 N
36	-4225 N	3.01	0.56	-6.80	7.30	-1.95	4.60	0.19	97.42	-2.46	-4.85	2.70	4.38	-9.02	-4225 N
37	-4200 N	3.01	0.54	-7.00	7.40	-2.00	4.55	0.19	95.42	-4.31	-5.00	2.85	4.46	-8.97	-4200 N
38	-4175 N	3.01	0.54	-7.50	7.30	-2.00	4.50	0.18	97.01	-2.76	-5.50	2.80	4.38	-9.87	-4175 N
39	-4150 N	3.01	0.53	-7.60	7.30	-2.00	4.45	0.18	96.90	-2.82	-5.60	2.85	4.38	-9.86	-4150 N
40	-4125 N	3.01	0.52	-7.60	7.40	-2.00	4.45	0.18	96.84	-2.82	-5.60	2.95	4.45	-9.67	-4125 N
41	-4100 N	3.01	0.52	-7.80	7.60	-2.00	4.40	0.18	98.72	-1.12	-5.80	3.20	4.82	-10.02	-4100 N
42	-4075 N	3.01	0.51	-8.00	7.50	-2.00	4.40	0.17	98.78	-1.05	-6.00	3.10	4.58	-10.17	-4075 N
43	-4050 N	3.01	0.50	-8.50	7.60	-2.00	4.35	0.17	98.87	-0.95	-6.50	3.25	4.71	-10.80	-4050 N
44	-4025 N	3.01	0.48	-8.70	7.80	-2.00	4.35	0.16	96.96	-2.50	-6.70	3.45	4.80	-10.68	-4025 N
45	-4000 N	3.01	0.46	-9.00	8.20	-2.00	4.35	0.16	94.98	-4.03	-7.00	3.85	5.13	-10.70	-4000 N

MOORE PARAGON PARAF C

LINE#	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSD/I	HSP/I	STATION
				PFE	RPS	PFE	RPS								
5	-5000. N	3.02	0.46	-5.50	6.80	-1.85	4.75	0.16	95.05	-3.97	-3.65	2.05	2.72	-5.56	-5000. N
6	-4975. N	3.02	0.48	-5.00	6.50	-1.85	4.75	0.16	97.20	-2.29	-3.15	1.75	2.43	-5.01	-4975. N
7	-4950. N	3.02	0.49	-4.80	6.30	-1.85	4.75	0.17	97.29	-2.26	-2.95	1.55	2.19	-4.79	-4950. N
8	-4925. N	3.02	0.49	-5.00	6.60	-1.85	4.75	0.17	95.47	-3.85	-3.15	1.85	2.62	-5.11	-4925. N
9	-4900. N	3.02	0.48	-5.10	6.70	-1.85	4.75	0.17	91.83	-7.07	-3.25	1.95	2.70	-5.17	-4900. N
10	-4875. N	3.02	0.51	-4.80	6.60	-1.85	4.75	0.18	95.89	-3.62	-2.95	1.85	2.73	-4.98	-4875. N
11	-4850. N	3.02	0.52	-5.00	6.70	-1.85	4.75	0.18	96.16	-3.44	-3.15	1.95	2.93	-5.42	-4850. N
12	-4825. N	3.02	0.50	-5.20	6.40	-1.85	4.75	0.18	91.02	-8.17	-3.35	1.65	2.38	-5.55	-4825. N
13	-4800. N	3.02	0.51	-5.20	6.30	-1.85	4.75	0.18	91.47	-7.87	-3.35	1.55	2.28	-5.66	-4800. N
14	-4775. N	3.02	0.48	-5.10	6.50	-1.85	4.75	0.19	84.91	-14.12	-3.25	1.75	2.43	-5.17	-4775. N
15	-4750. N	3.02	0.55	-5.20	6.30	-1.85	4.70	0.19	96.06	-3.74	-3.35	1.60	2.54	-6.10	-4750. N
16	-4725. N	3.02	0.53	-5.30	6.50	-1.85	4.70	0.19	91.48	-8.17	-3.45	1.80	2.76	-6.05	-4725. N
17	-4700. N	3.02	0.53	-5.10	6.50	-1.85	4.70	0.19	90.52	-9.19	-3.25	1.80	2.76	-5.70	-4700. N
18	-4675. N	3.02	0.53	-5.30	6.40	-1.85	4.70	0.20	89.66	-10.12	-3.45	1.70	2.60	-6.05	-4675. N
19	-4650. N	3.02	0.56	-5.50	6.50	-1.85	4.70	0.20	93.96	-5.96	-3.65	1.80	2.91	-6.77	-4650. N
20	-4625. N	3.02	0.54	-5.50	6.50	-1.85	4.70	0.20	89.96	-9.98	-3.65	1.80	2.81	-6.53	-4625. N
21	-4600. N	3.02	0.54	-5.50	6.60	-1.85	4.70	0.20	89.44	-10.56	-3.65	1.90	2.96	-6.53	-4600. N
22	-4575. N	3.02	0.56	-5.60	6.50	-1.85	4.70	0.20	92.33	-7.70	-3.75	1.80	2.91	-6.95	-4575. N
23	-4550. N	3.02	0.54	-5.70	6.60	-1.85	4.70	0.20	88.74	-11.34	-3.85	1.90	2.96	-6.88	-4550. N
24	-4525. N	3.02	0.56	-5.80	6.70	-1.85	4.70	0.20	91.85	-8.23	-3.95	2.00	3.24	-7.32	-4525. N
25	-4500. N	3.02	0.54	-5.80	6.60	-1.90	4.65	0.20	88.51	-11.61	-3.90	1.95	3.04	-6.97	-4500. N
26	-4475. N	3.02	0.55	-6.10	6.50	-1.90	4.65	0.20	90.21	-9.88	-4.20	1.85	2.94	-7.65	-4475. N
27	-4450. N	3.02	0.54	-5.90	6.60	-1.90	4.65	0.20	88.74	-11.34	-4.00	1.95	3.04	-7.15	-4450. N
28	-4425. N	3.02	0.58	-5.70	6.50	-1.90	4.65	0.20	95.63	-4.39	-3.80	1.85	3.10	-7.30	-4425. N
29	-4400. N	3.02	0.51	-6.50	6.80	-1.90	4.65	0.20	84.47	-15.52	-4.60	2.15	3.17	-7.77	-4400. N
30	-4375. N	3.02	0.52	-6.80	6.90	-1.90	4.65	0.20	86.63	-13.29	-4.90	2.25	3.38	-8.44	-4375. N
31	-4350. N	3.02	0.54	-6.60	6.90	-1.90	4.65	0.20	90.60	-9.27	-4.70	2.25	3.51	-8.40	-4350. N
32	-4325. N	3.02	0.54	-6.60	7.00	-1.90	4.65	0.20	91.36	-8.46	-4.70	2.35	3.67	-8.40	-4325. N
33	-4300. N	3.02	0.54	-6.60	7.00	-1.90	4.65	0.19	92.22	-7.54	-4.70	2.35	3.67	-8.40	-4300. N
34	-4275. N	3.02	0.53	-7.00	7.00	-1.90	4.65	0.19	91.48	-8.17	-5.10	2.35	3.60	-8.95	-4275. N
35	-4250. N	3.02	0.52	-6.80	6.90	-1.90	4.60	0.19	90.82	-8.71	-4.90	2.30	3.46	-8.44	-4250. N
36	-4225. N	3.02	0.51	-7.50	7.30	-1.90	4.60	0.19	90.22	-9.16	-5.60	2.70	3.98	-9.46	-4225. N
37	-4200. N	3.02	0.57	-7.20	7.00	-1.90	4.60	0.18	102.24	2.06	-5.30	2.40	3.95	-10.00	-4200. N
38	-4175. N	3.02	0.51	-8.50	7.50	-1.90	4.60	0.18	92.84	-6.51	-6.60	2.90	4.27	-11.15	-4175. N
39	-4150. N	3.02	0.48	-8.50	7.50	-1.90	4.60	0.18	88.76	-10.06	-6.60	2.90	4.02	-10.49	-4150. N
40	-4125. N	3.02	0.51	-8.60	7.60	-1.90	4.60	0.18	95.89	-3.62	-6.70	3.00	4.42	-11.31	-4125. N
41	-4100. N	3.02	0.47	-9.00	8.00	-1.90	4.60	0.17	89.92	-8.72	-7.10	3.40	4.62	-11.05	-4100. N
42	-4075. N	3.02	0.49	-8.80	7.70	-1.90	4.60	0.17	95.47	-3.85	-6.90	3.10	4.39	-11.20	-4075. N
43	-4050. N	3.02	0.49	-9.30	7.60	-1.90	4.60	0.17	97.29	-2.26	-7.40	3.00	4.25	-12.01	-4050. N
44	-4025. N	3.02	0.49	-9.00	7.90	-1.90	4.60	0.16	99.22	-0.64	-7.10	3.30	4.67	-11.52	-4025. N
45	-4000. N	3.02	0.42	-11.00	8.50	-1.90	4.60	0.16	86.79	-10.59	-9.10	3.90	4.73	-12.66	-4000. N

MOORE PARAGON PARAFIC

LINE#	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFE	RPS	HSG/I	HSP/I	STATION
				PFE	RPS	PFE	RPS								
5	-5000. N	3.01	0.47	-4.90	6.80	-1.80	4.80	0.16	96.56	-2.78	-3.10	2.00	2.73	-4.84	-5000. N
6	-4975. N	3.01	0.50	-4.70	6.70	-1.80	4.80	0.17	99.76	-0.20	-2.90	1.90	2.75	-4.82	-4975. N
7	-4950. N	3.01	0.52	-4.60	6.60	-1.80	4.80	0.17	100.79	0.68	-2.80	1.80	2.71	-4.84	-4950. N
8	-4925. N	3.01	0.53	-4.60	6.60	-1.80	4.80	0.18	99.83	-0.15	-2.80	1.80	2.77	-4.93	-4925. N
9	-4900. N	3.01	0.55	-4.40	6.50	-1.80	4.80	0.18	100.72	0.65	-2.60	1.70	2.71	-4.75	-4900. N
10	-4875. N	3.01	0.55	-4.90	6.60	-1.80	4.80	0.19	97.98	-1.89	-3.10	1.80	2.87	-5.66	-4875. N
11	-4850. N	3.01	0.56	-5.00	6.60	-1.80	4.80	0.19	97.11	-2.77	-3.20	1.80	2.92	-5.95	-4850. N
12	-4825. N	3.01	0.52	-5.30	6.40	-1.80	4.80	0.20	87.86	-11.94	-3.50	1.60	2.41	-6.05	-4825. N
13	-4800. N	3.01	0.52	-5.10	6.40	-1.80	4.80	0.20	97.22	-2.91	-3.30	1.60	2.74	-6.47	-4800. N
14	-4775. N	3.01	0.58	-5.20	6.40	-1.80	4.80	0.21	93.31	-6.91	-3.40	1.60	2.69	-6.55	-4775. N
15	-4750. N	3.01	0.57	-5.20	6.40	-1.80	4.85	0.21	89.65	-10.93	-3.40	1.55	2.56	-6.44	-4750. N
16	-4725. N	3.01	0.61	-5.00	6.50	-1.80	4.85	0.22	93.93	-6.55	-3.20	1.65	2.92	-6.49	-4725. N
17	-4700. N	3.01	0.56	-5.40	6.50	-1.80	4.85	0.22	84.57	-16.98	-3.60	1.65	2.68	-6.70	-4700. N
18	-4675. N	3.01	0.60	-4.70	6.40	-1.80	4.85	0.22	89.02	-12.30	-2.90	1.55	2.70	-5.78	-4675. N
19	-4650. N	3.01	0.63	-4.90	6.40	-1.80	4.85	0.23	92.01	-9.09	-3.10	1.55	2.83	-6.49	-4650. N
20	-4625. N	3.01	0.62	-5.40	6.70	-1.80	4.85	0.23	89.32	-12.31	-3.60	1.85	3.33	-7.42	-4625. N
21	-4600. N	3.01	0.63	-5.40	6.60	-1.80	4.85	0.23	89.74	-11.96	-3.60	1.75	3.20	-7.53	-4600. N
22	-4575. N	3.01	0.64	-5.20	6.50	-1.80	4.90	0.24	90.35	-11.35	-3.40	1.60	2.97	-7.23	-4575. N
23	-4550. N	3.01	0.64	-5.10	6.40	-1.80	4.90	0.24	89.77	-12.12	-3.30	1.50	2.78	-7.02	-4550. N
24	-4525. N	3.01	0.63	-5.30	6.50	-1.80	4.90	0.24	88.02	-14.24	-3.50	1.60	2.92	-7.33	-4525. N
25	-4500. N	3.01	0.64	-5.50	7.00	-1.75	5.00	0.24	89.30	-12.74	-3.75	2.00	3.71	-7.97	-4500. N
26	-4475. N	3.01	0.64	-5.40	6.80	-1.75	5.00	0.24	89.42	-12.58	-3.65	1.80	3.34	-7.76	-4475. N
27	-4450. N	3.01	0.64	-5.50	6.80	-1.75	5.00	0.24	89.77	-12.12	-3.75	1.80	3.34	-7.97	-4450. N
28	-4425. N	3.01	0.64	-5.70	6.90	-1.75	5.00	0.24	90.35	-11.35	-3.95	1.90	3.53	-8.40	-4425. N
29	-4400. N	3.01	0.63	-5.70	6.90	-1.75	5.00	0.23	89.74	-11.96	-3.95	1.90	3.47	-8.27	-4400. N
30	-4375. N	3.01	0.63	-5.90	7.00	-1.75	5.00	0.23	90.77	-10.65	-4.15	2.00	3.65	-8.69	-4375. N
31	-4350. N	3.01	0.61	-6.00	7.00	-1.75	5.00	0.23	89.09	-12.41	-4.25	2.00	3.54	-8.61	-4350. N
32	-4325. N	3.01	0.62	-6.50	7.10	-1.75	5.00	0.22	91.98	-8.97	-4.75	2.10	3.77	-9.78	-4325. N
33	-4300. N	3.01	0.59	-6.40	7.10	-1.75	4.95	0.22	89.10	-11.99	-4.65	2.15	3.68	-9.11	-4300. N
34	-4275. N	3.01	0.60	-6.50	7.20	-1.75	4.95	0.22	92.39	-8.21	-4.75	2.25	3.91	-9.47	-4275. N
35	-4250. N	3.01	0.58	-6.80	7.20	-1.75	4.95	0.21	91.22	-9.27	-5.05	2.25	3.78	-9.73	-4250. N
36	-4225. N	3.01	0.60	-7.00	7.30	-1.75	4.95	0.21	96.53	-3.59	-5.25	2.35	4.09	-10.47	-4225. N
37	-4200. N	3.01	0.58	-7.60	7.40	-1.75	4.95	0.20	95.57	-4.47	-5.85	2.45	4.12	-11.27	-4200. N
38	-4175. N	3.01	0.57	-7.80	7.50	-1.75	4.95	0.20	96.30	-3.63	-6.05	2.55	4.21	-11.46	-4175. N
39	-4150. N	3.01	0.58	-8.10	7.60	-1.75	4.95	0.19	100.58	0.56	-6.35	2.65	4.46	-12.24	-4150. N
40	-4125. N	3.01	0.57	-8.20	7.60	-1.75	4.95	0.19	101.54	1.44	-6.45	2.65	4.38	-12.21	-4125. N
41	-4100. N	3.01	0.52	-8.80	7.70	-1.75	4.90	0.18	95.22	-4.33	-7.05	2.80	4.22	-12.18	-4100. N
42	-4075. N	3.01	0.57	-8.80	7.70	-1.75	4.90	0.18	107.36	6.49	-7.05	2.80	4.63	-13.35	-4075. N
43	-4050. N	3.01	0.56	-9.50	7.80	-1.75	4.90	0.17	108.54	7.92	-7.75	2.90	4.71	-14.42	-4050. N
44	-4025. N	3.01	0.51	-9.60	7.90	-1.75	4.90	0.17	101.76	1.46	-7.85	3.00	4.44	-13.30	-4025. N
45	-4000. N	3.01	0.49	-9.80	8.20	-1.80	4.90	0.16	100.67	0.54	-8.00	3.30	4.69	-13.02	-4000. N

MOORE PARAGON PAPER CO

XVNETICS, INC. NO. RECORDS 52
NO. OF DRAWINGS 2

128214

201

MOORE PARAY ON PARAFLO

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202

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

PROGRAM MIPZ . CALCULATES MAGNETIC INDUCED POLARIZATION RESULTS

3HZ RRMIP SURVEY MT PEARSE AREA TASMANIA 063R ARRAY N006

79-1393 2/2

FORM No. 11 15
010341

203

128216

INTERP TAPE FLAG= 0 GRIDDATA TAPE FLAG= 0

LINE POSITIONING MULTIPLYING FACTOR= 1.0

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM No. 11 13

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204

128217

UNITS FLAG= 0 CURRENT ELECTRODE CO-ORDS= 1250. E -5800. N 3100. E -5800. N

1 PLOT SCALE= 2500. HN SCALE 10. PFF & RPS SCALE= 1. HSD & HSP SCALE= 1.

3 ORIGIN CO-ORDS= 1700. E -5300. N ARRAY IDENTIFIER= MP06 ANNOTATION SUPPRESSION FLAG= 0

5 SPLINE INTERVAL= 0.

7 PLOT BASE LEVELS FOR PFF, RPS, HSD, HSP ARE 0.00 0.00 0.00 0.00

10 PLOTTING OPTION FLAGS FOLLOW - 1=STRAIGHT PLOT, 2=SPLINE PLOT WHERE APPLICABLE

12	HN	=	0
13	MMR	=	1
14	PFF	=	0
15	RPS	=	1
16	HSD	=	1
17	HSP	=	0

20 FOR HN , MMR 100.00 0.00

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

FORM No. 11 IS 0103413

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No. 11 13

		---FIELD---				---OFFSET---								
STATION	CURRENT	HP	PFF	RPS	PFF	RPS	HU	HN	MMR	PFE	RPS	HSQ/I	HSP/I	STATION
-6300. N	3.50	0.60	-6.20	7.70	-1.55	5.50	0.16	105.30	3.99	-4.65	1.70	2.54	-7.97	-6300. N
-6275. N	3.50	0.57	-6.40	7.30	-1.55	5.50	0.17	96.27	-2.92	-4.85	1.80	2.56	-7.90	-6275. N
-6250. N	3.50	0.62	-6.50	7.50	-1.55	5.50	0.18	100.73	0.60	-4.95	2.00	3.09	-8.77	-6250. N
-6225. N	3.50	0.65	-6.00	7.00	-1.55	5.50	0.18	101.56	1.32	-4.45	1.50	2.43	-8.26	-6225. N
-6200. N	3.50	0.72	-5.50	6.80	-1.55	5.45	0.19	108.17	7.19	-3.95	1.35	2.42	-8.13	-6200. N
-6175. N	3.50	0.72	-5.50	6.90	-1.55	5.45	0.20	104.00	3.66	-3.95	1.45	2.60	-8.13	-6175. N
-6150. N	3.50	0.70	-5.30	7.00	-1.55	5.45	0.21	97.23	-2.63	-3.75	1.55	2.71	-7.50	-6150. N
-6125. N	3.50	0.80	0.00	0.00	-1.55	5.45	0.21	106.90	6.82	1.55	-5.45	-10.87	-3.54	-6125. N
-6100. N	3.50	0.82	-4.50	6.70	-1.60	5.40	0.22	105.47	5.67	-2.90	1.30	2.66	-6.79	-6100. N
-6075. N	3.50	0.86	-4.70	6.50	-1.60	5.40	0.23	106.57	7.00	-3.10	1.10	2.36	-7.62	-6075. N
-6050. N	3.50	0.84	-4.50	6.50	-1.60	5.40	0.24	100.40	0.45	-2.90	1.10	2.30	-6.96	-6050. N
-6025. N	3.50	0.88	-4.20	6.40	-1.60	5.40	0.25	101.63	1.86	-2.60	1.00	2.19	-6.54	-6025. N
-6000. N	3.50	0.89	-4.00	6.30	-1.60	5.35	0.26	99.50	-0.59	-2.40	0.95	2.11	-6.10	-6000. N
-5975. N	3.50	0.95	-3.90	6.20	-1.60	5.35	0.26	103.06	3.73	-2.30	0.85	2.01	-6.24	-5975. N
-5950. N	3.50	1.00	-4.20	6.30	-1.60	5.35	0.27	105.58	6.98	-2.60	0.95	2.37	-7.43	-5950. N
-5925. N	3.50	0.99	-3.90	6.20	-1.60	5.35	0.28	102.05	2.63	-2.30	0.85	2.10	-6.51	-5925. N
-5900. N	3.50	1.02	-4.00	6.20	-1.65	5.30	0.28	103.04	3.98	-2.35	0.90	2.29	-6.85	-5900. N
-5875. N	3.50	1.03	-3.90	6.20	-1.65	5.30	0.29	102.38	3.17	-2.25	0.90	2.31	-6.62	-5875. N
-5850. N	3.50	1.03	-3.70	6.10	-1.65	5.30	0.29	101.18	1.59	-2.05	0.80	2.05	-6.03	-5850. N
-5825. N	3.50	1.03	-3.70	6.00	-1.65	5.30	0.29	100.46	0.62	-2.05	0.70	1.80	-6.03	-5825. N
-5800. N	3.50	1.03	-3.60	6.10	-1.65	5.25	0.29	100.27	0.29	-1.95	0.85	2.18	-5.74	-5800. N
-5775. N	3.51	1.03	-3.40	6.00	-1.65	5.25	0.29	100.17	0.23	-1.75	0.75	1.92	-5.14	-5775. N
-5750. N	3.51	1.02	-3.50	5.90	-1.65	5.25	0.29	99.91	-0.12	-1.85	0.65	1.65	-5.38	-5750. N
-5725. N	3.51	1.02	-3.30	6.00	-1.65	5.25	0.29	101.10	1.46	-1.65	0.75	1.90	-4.79	-5725. N
-5700. N	3.51	0.98	-3.60	6.10	-1.70	5.20	0.28	98.72	-1.68	-1.90	0.90	2.19	-5.30	-5700. N
-5675. N	3.51	0.98	-3.50	6.00	-1.70	5.20	0.28	100.73	0.94	-1.80	0.80	1.95	-5.03	-5675. N
-5650. N	3.51	0.95	-3.40	6.00	-1.70	5.20	0.27	100.01	0.02	-1.70	0.80	1.89	-4.60	-5650. N
-5625. N	3.51	0.90	-3.60	6.00	-1.70	5.20	0.26	97.36	-3.21	-1.90	0.80	1.79	-4.87	-5625. N
-5600. N	3.51	0.89	-3.60	6.10	-1.70	5.15	0.26	99.27	-0.93	-1.90	0.95	2.10	-4.82	-5600. N
-5575. N	3.51	0.88	-3.60	6.00	-1.70	5.15	0.25	101.34	1.53	-1.90	0.85	1.86	-4.76	-5575. N
-5550. N	3.51	0.83	-3.60	6.00	-1.70	5.15	0.24	98.93	-1.19	-1.90	0.85	1.75	-4.49	-5550. N
-5525. N	3.51	0.81	-3.60	6.00	-1.70	5.10	0.23	100.09	0.09	-1.90	0.90	1.81	-4.38	-5525. N
-5500. N	3.51	0.75	-3.80	6.20	-1.75	5.10	0.22	96.19	-3.91	-2.05	1.10	2.05	-4.38	-5500. N
-5475. N	3.51	0.74	-3.80	6.30	-1.75	5.10	0.21	98.60	-1.38	-2.05	1.20	2.21	-4.32	-5475. N
-5450. N	3.51	0.71	-3.80	6.30	-1.75	5.05	0.21	98.34	-1.58	-2.05	1.25	2.21	-4.15	-5450. N
-5425. N	3.51	0.69	-3.80	6.30	-1.75	5.05	0.20	99.39	-0.56	-2.05	1.25	2.14	-4.03	-5425. N
-5400. N	3.51	0.66	-3.80	6.40	-1.75	5.05	0.19	98.87	-0.99	-2.05	1.35	2.22	-3.85	-5400. N
-5375. N	3.51	0.62	-3.80	6.40	-1.75	5.00	0.18	96.60	-2.88	-2.05	1.40	2.16	-3.62	-5375. N
-5350. N	3.51	0.57	-4.00	6.50	-1.75	5.00	0.18	92.35	-6.27	-2.25	1.50	2.13	-3.65	-5350. N
-5325. N	3.51	0.56	-4.20	6.60	-1.75	5.00	0.17	94.31	-4.45	-2.45	1.60	2.23	-3.91	-5325. N
-5300. N	3.51	0.53	-4.20	6.70	-1.75	5.00	0.16	92.75	-5.46	-2.45	1.70	2.24	-3.70	-5300. N

206

XTOP= -6300.

XINC= 75.00

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	6300.		I	*		3.99
2	-6275.		* I			-2.92
3	-6250.		I*			0.60
4	-6225.		I*			1.32
5	-6200.		I	*		7.19
6	-6175.		I	*		3.66
7	-6150.		* I			-2.63
8	-6125.		I	*		6.87
9	-6100.		I	*		5.62
10	-6075.		I	*		7.00
11	-6050.		*			0.45
12	-6025.		I *			1.86
13	-6000.		* I			0.59
14	-5975.		I	*		3.73
15	-5950.		I	*		6.98
16	-5925.		I	*		2.63
17	-5900.		I	*		3.98
18	-5875.		I	*		3.17
19	-5850.		I *			1.59
20	-5825.		I*			0.62
21	-5800.		*			0.29
22	-5775.		*			0.23
23	-5750.		*			0.12
24	-5725.		I*			1.46
25	-5700.		* I			1.68
26	-5675.		I*			0.94
27	-5650.		*			0.02
28	-5625.		* I			-3.71
29	-5600.		* I			-0.93
30	-5575.		I *			1.53
31	-5550.		* I			-1.19
32	-5525.		*			0.09
33	-5500.		* I			-3.91
34	-5475.		* I			-1.38
35	-5450.		* I			1.58
36	-5425.		* I			-0.56
37	-5400.		* I			-0.99
38	-5375.		* I			-2.88
39	-5350.		* I			-6.27
40	-5325.		* I			-4.45
41	-5300.		* I			-5.46

XBOT= 5300.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 1700. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11-15
0103415

207

XTOP= -6300.

XINC= 25.00

128220

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	-6300.	I		*	1.70	1
2	-6275.	I		*	1.80	2
3	-6250.	I		*	2.00	3
4	-6225.	I		*	1.50	4
5	-6200.	I		*	1.35	5
6	-6175.	I		*	1.45	6
7	-6150.	I		*	1.55	7
8	-6125. *	I			-5.45	8
9	-6100.	I		*	1.30	9
10	-6075.	I		*	1.10	10
11	-6050.	I		*	1.10	11
12	-6025.	I		*	1.00	12
13	-6000.	I		*	0.95	13
14	-5975.	I		*	0.85	14
15	-5950.	I		*	0.95	15
16	-5925.	I		*	0.85	16
17	-5900.	I		*	0.90	17
18	-5875.	I		*	0.90	18
19	-5850.	I		*	0.80	19
20	-5825.	I	*		0.70	20
21	-5800.	I	*		0.85	21
22	-5775.	I	*		0.75	22
23	-5750.	I	*		0.65	23
24	-5725.	I	*		0.75	24
25	-5700.	I	*		0.90	25
26	-5675.	I	*		0.80	26
27	-5650.	I	*		0.80	27
28	-5625.	I	*		0.80	28
29	-5600.	I	*		0.95	29
30	-5575.	I	*		0.85	30
31	-5550.	I	*		0.85	31
32	-5525.	I	*		0.90	32
33	-5500.	I	*		1.10	33
34	-5475.	I	*		1.20	34
35	-5450.	I	*		1.25	35
36	-5425.	I	*		1.25	36
37	-5400.	I	*		1.35	37
38	-5375.	I	*		1.40	38
39	-5350.	I	*		1.50	39
40	-5325.	I	*		1.60	40
41	-5300.	I	*		1.70	41

XBOT= -5300.

YINC= 0.7950E-01

YMIN= -5.450

YMAX= 2.500

LINE 1700. F RELATIVE PHASE SHIFT RPS

FORM No 11 15

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60						60

208

XTOP= -6300.

XINC= 75.00

128221

MOORE PARAGON (WA) LIMITED - FORMALINER PARATLO

1	-6300.	I	*	2.54	1
2	-6275.	I	*	2.56	2
3	-6250.	I	*	3.09	3
4	-6225.	I	*	2.43	4
5	-6200.	I	*	2.42	5
6	-6175.	I	*	2.60	6
7	-6150.	I	*	2.71	7
8	-6125. *	I		-10.87	8
9	-6100.	I	*	2.66	9
10	-6075.	I	*	2.36	10
11	-6050.	I	*	2.30	11
12	-6025.	I	*	2.19	12
13	-6000.	I	*	2.11	13
14	-5975.	I	*	2.01	14
15	-5950.	I	*	2.37	15
16	-5925.	I	*	2.10	16
17	-5900.	I	*	2.79	17
18	-5875.	I	*	2.31	18
19	-5850.	I	*	2.05	19
20	-5825.	I	*	1.80	20
21	-5800.	I	*	2.18	21
22	-5775.	I	*	1.92	22
23	-5750.	I	*	1.65	23
24	-5725.	I	*	1.90	24
25	-5700.	I	*	2.19	25
26	-5675.	I	*	1.95	26
27	-5650.	I	*	1.89	27
28	-5625.	I	*	1.79	28
29	-5600.	I	*	2.10	29
30	-5575.	I	*	1.86	30
31	-5550.	I	*	1.75	31
32	-5525.	I	*	1.81	32
33	-5500.	I	*	2.05	33
34	-5475.	I	*	2.21	34
35	-5450.	I	*	2.21	35
36	-5425.	I	*	2.14	36
37	-5400.	I	*	2.77	37
38	-5375.	I	*	2.16	38
39	-5350.	I	*	2.13	39
40	-5325.	I	*	2.73	40
41	-5300.	I	*	2.74	41

XBOT= 5300.
YMIN= -10.87

YINC= 0.2087
YMAX= 10.00

LINE 1700. E SECONDARY FIELD QUADRATURE HSO/I

FORM No. 11 15
010347

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MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

		FIELD						OFFSET							
STATION	CURRENT	HP	PFF	RFS	PFF	RFS	HU	HN	MMR	PFF	RFS	HSQ/I	HSP/I	STATION	
-6300. N	3.76	0.71	-6.40	7.60	-1.40	5.50	0.17	112.63	9.80	-5.00	2.10	3.46	-9.44	-6300. N	
-6275. N	3.76	0.70	-6.40	7.60	-1.40	5.50	0.17	108.37	6.65	-5.00	2.10	3.41	-9.31	-6275. N	
-6250. N	3.76	0.71	-6.00	7.60	-1.40	5.50	0.18	107.34	5.97	-4.60	2.10	3.46	-8.69	-6250. N	
-6225. N	3.76	0.71	-6.00	7.60	-1.40	5.50	0.18	104.89	4.07	-4.60	2.10	3.46	-8.69	-6225. N	
-6200. N	3.76	0.71	-5.80	7.60	-1.40	5.50	0.18	102.57	2.19	-4.40	2.10	3.46	-8.31	-6200. N	
-6175. N	3.76	0.73	-5.60	7.60	-1.45	5.50	0.19	103.71	2.79	-4.15	2.10	3.56	-8.06	-6175. N	
-6150. N	3.76	0.74	-5.40	7.40	-1.45	5.50	0.19	102.48	2.71	-3.95	1.90	3.76	-7.77	-6150. N	
-6125. N	3.76	0.77	-5.40	7.70	-1.45	5.50	0.20	97.77	-2.02	-3.95	1.70	2.84	-7.56	-6125. N	
-6100. N	3.76	0.75	-5.20	7.00	-1.45	5.50	0.20	99.95	-0.04	-3.75	1.50	2.61	-7.48	-6100. N	
-6075. N	3.76	0.74	-5.20	7.00	-1.45	5.50	0.20	96.91	-2.91	-3.75	1.50	2.58	-7.38	-6075. N	
-6050. N	3.76	0.74	-5.20	7.00	-1.45	5.50	0.21	95.33	-4.46	-3.75	1.50	2.58	-7.38	-6050. N	
-6025. N	3.76	0.77	-5.00	7.00	-1.50	5.50	0.21	97.71	-2.27	-3.50	1.50	2.68	-7.17	-6025. N	
-6000. N	3.76	0.77	-5.00	7.00	-1.50	5.50	0.21	96.38	-3.56	-3.50	1.50	2.68	-7.17	-6000. N	
-5975. N	3.76	0.79	-5.00	6.80	-1.50	5.50	0.22	97.67	-2.32	-3.50	1.30	2.38	-7.35	-5975. N	
-5950. N	3.76	0.77	-4.60	6.70	-1.50	5.50	0.22	94.17	-5.86	-3.10	1.70	2.14	-6.35	-5950. N	
-5925. N	3.76	0.76	-4.40	6.70	-1.50	5.50	0.22	92.09	-8.03	-2.90	1.70	2.12	-5.86	-5925. N	
-5900. N	3.76	0.80	-4.40	6.70	-1.50	5.50	0.22	96.70	-3.89	-7.90	1.20	2.73	-6.17	-5900. N	
-5875. N	3.76	0.79	-4.40	6.70	-1.55	5.50	0.22	94.43	-5.73	-7.85	1.70	2.70	-5.99	-5875. N	
-5850. N	3.76	0.80	-4.20	6.70	-1.55	5.50	0.22	95.21	-4.95	-7.65	1.70	2.73	-5.64	-5850. N	
-5825. N	3.76	0.81	-4.20	6.80	-1.55	5.50	0.22	96.15	-3.99	-7.65	1.30	2.44	-5.71	-5825. N	
-5800. N	3.76	0.81	-4.00	6.80	-1.55	5.50	0.22	96.07	-4.08	-7.45	1.30	2.44	-5.28	-5800. N	
-5775. N	3.75	0.79	-4.20	7.00	-1.55	5.50	0.22	94.03	-6.19	-7.65	1.50	2.76	-5.58	-5775. N	
-5750. N	3.75	0.79	-4.20	6.90	-1.55	5.50	0.22	94.77	-5.92	-7.65	1.40	2.57	-5.58	-5750. N	
-5725. N	3.75	0.79	-4.00	6.80	-1.60	5.50	0.22	94.60	-5.47	-7.40	1.30	2.39	-5.06	-5725. N	
-5700. N	3.75	0.80	-4.00	6.70	-1.60	5.50	0.22	96.46	-3.62	-7.40	1.20	2.23	-5.12	-5700. N	
-5675. N	3.75	0.78	-4.20	6.80	-1.60	5.50	0.22	94.77	-5.31	-7.60	1.30	2.36	-5.41	-5675. N	
-5650. N	3.75	0.77	-4.00	6.70	-1.60	5.50	0.22	94.43	-5.61	-7.40	1.20	2.15	-4.93	-5650. N	
-5625. N	3.75	0.76	-4.00	6.70	-1.60	5.50	0.22	94.71	-5.76	-7.40	1.20	2.17	-4.86	-5625. N	
-5600. N	3.75	0.75	-3.80	6.80	-1.60	5.50	0.21	94.13	-5.77	-7.20	1.30	2.27	-4.40	-5600. N	
-5575. N	3.75	0.74	-3.80	6.50	-1.65	5.50	0.21	94.16	-5.67	-7.15	1.00	1.72	-4.74	-5575. N	
-5550. N	3.75	0.73	-3.80	6.60	-1.65	5.50	0.21	94.30	-5.45	-7.15	1.10	1.87	-4.19	-5550. N	
-5525. N	3.75	0.72	-3.80	6.80	-1.65	5.50	0.20	94.54	-5.13	-7.15	1.30	2.16	-4.13	-5525. N	
-5500. N	3.75	0.72	-3.80	7.00	-1.65	5.50	0.20	96.21	-3.50	-7.15	1.50	2.51	-4.13	-5500. N	
-5475. N	3.75	0.71	-4.00	6.90	-1.65	5.50	0.20	96.67	-3.02	-7.35	1.40	2.31	-4.45	-5475. N	
-5450. N	3.75	0.68	-3.80	6.70	-1.65	5.50	0.19	94.42	-4.95	-7.15	1.20	1.90	-3.90	-5450. N	
-5425. N	3.75	0.67	-3.60	6.80	-1.70	5.50	0.19	94.98	-4.37	-6.90	1.30	2.03	-3.39	-5425. N	
-5400. N	3.75	0.73	-4.20	7.00	-1.70	5.50	0.18	105.74	4.89	-6.50	1.50	2.55	-4.87	-5400. N	
-5375. N	3.75	0.64	-3.60	7.00	-1.70	5.50	0.18	94.80	-4.33	-6.90	1.50	2.73	-3.74	-5375. N	
-5350. N	3.75	0.63	-3.80	7.00	-1.70	5.50	0.18	95.50	-3.66	-6.10	1.50	2.20	-3.53	-5350. N	
-5325. N	3.75	0.63	-3.60	6.90	-1.70	5.50	0.17	97.80	-1.75	-6.90	1.40	2.05	-3.19	-5325. N	
-5300. N	3.75	0.59	-3.80	7.00	-1.70	5.50	0.17	93.85	-4.77	-6.10	1.50	2.06	-3.30	-5300. N	

210

128223

XTOP= -6300.

XINC= 75.00

MOORE PARAGON (WA) LIMITED - FORMALINER PARAFLO

1	-6300.		I	*	9.80	1
2	-6275.		I	*	6.65	2
3	-6250.		I	*	5.97	3
4	-6225.		I	*	4.07	4
5	-6200.		I	*	2.19	5
6	-6175.		I	*	2.79	6
7	-6150.		I	*	2.21	7
8	-6125.		* I		-2.02	8
9	-6100.		*		-0.04	9
10	-6075.		* I		-2.91	10
11	-6050.		* I		-4.46	11
12	-6025.		* I		-2.27	12
13	-6000.		* I		-3.56	13
14	-5975.		* I		-2.32	14
15	-5950.		*		-5.86	15
16	-5925.	*	I		-8.03	16
17	-5900.	*	I		-3.89	17
18	-5875.	*	I		-5.73	18
19	-5850.	*	I		4.95	19
20	-5825.	*	I		-3.99	20
21	-5800.	*	I		-4.08	21
22	-5775.	*	I		-6.19	22
23	-5750.	*	I		-5.92	23
24	-5725.	*	I		-5.47	24
25	-5700.	*	I		-3.62	25
26	-5675.	*	I		-5.31	26
27	-5650.	*	I		-5.61	27
28	-5625.	*	I		-5.76	28
29	-5600.	*	I		-5.77	29
30	-5575.	*	I		-5.67	30
31	-5550.	*	I		-5.45	31
32	-5525.	*	I		-5.13	32
33	-5500.	*	I		-3.50	33
34	-5475.	*	I		-3.02	34
35	-5450.	*	I		-4.95	35
36	-5425.	*	I		-4.37	36
37	-5400.		I	*	4.89	37
38	-5375.	*	I		-4.33	38
39	-5350.	*	I		-3.66	39
40	-5325.	*	I		-1.75	40
41	-5300.	*	I		-4.77	41

XBOT= -5300.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINF 2000. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11 15
010349

211

XTOP= -6300.

XINC= 25.00

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-6300.	I		*	2.10	1
2	-6275.	I		*	2.10	2
3	-6250.	I		*	2.10	3
4	-6225.	I		*	2.10	4
5	-6200.	I		*	2.10	5
6	-6175.	I		*	2.10	6
7	-6150.	I		*	1.90	7
8	-6125.	I		*	1.70	8
9	-6100.	I		*	1.50	9
10	-6075.	I		*	1.50	10
11	-6050.	I		*	1.50	11
12	-6025.	I		*	1.50	12
13	-6000.	I		*	1.50	13
14	-5975.	I		*	1.30	14
15	-5950.	I		*	1.20	15
16	-5925.	I		*	1.20	16
17	-5900.	I		*	1.20	17
18	-5875.	I		*	1.20	18
19	-5850.	I		*	1.20	19
20	-5825.	I		*	1.30	20
21	-5800.	I		*	1.30	21
22	-5775.	I		*	1.50	22
23	-5750.	I		*	1.40	23
24	-5725.	I		*	1.30	24
25	-5700.	I		*	1.20	25
26	-5675.	I		*	1.30	26
27	-5650.	I		*	1.20	27
28	-5625.	I		*	1.20	28
29	-5600.	I		*	1.30	29
30	-5575.	I		*	1.00	30
31	-5550.	I		*	1.10	31
32	-5525.	I		*	1.30	32
33	-5500.	I		*	1.50	33
34	-5475.	I		*	1.40	34
35	-5450.	I		*	1.20	35
36	-5425.	I		*	1.30	36
37	-5400.	I		*	1.50	37
38	-5375.	I		*	1.50	38
39	-5350.	I		*	1.50	39
40	-5325.	I		*	1.40	40
41	-5300.	I		*	1.50	41

XBOT= -5300.

YINC= 0.5000E-01

YMIN= -2.500

YMAX= 2.500

L INF 2000. F RELATIVE PHASE SHIFT RPS

FORM No 11 15

42						42
43						43
44						44
45						45
46						46
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51						51
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53						53
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56						56
57						57
58						58
59						59
60						60

212

XTOP= -6300.

XINC= 25.00

128225

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-6300.	I	*	3.46	1
2	-6275.	I	*	3.41	2
3	-6250.	I	*	3.46	3
4	-6225.	I	*	3.46	4
5	-6200.	I	*	3.46	5
6	-6175.	I	*	3.56	6
7	-6150.	I	*	3.76	7
8	-6125.	I	*	2.84	8
9	-6100.	I	*	2.61	9
10	-6075.	I	*	2.58	10
11	-6050.	I	*	2.58	11
12	-6025.	I	*	2.68	12
13	-6000.	I	*	2.68	13
14	-5975.	I	*	2.38	14
15	-5950.	I	*	2.14	15
16	-5925.	I	*	2.12	16
17	-5900.	I	*	2.23	17
18	-5875.	I	*	2.20	18
19	-5850.	I	*	2.23	19
20	-5825.	I	*	2.44	20
21	-5800.	I	*	2.44	21
22	-5775.	I	*	2.76	22
23	-5750.	I	*	2.57	23
24	-5725.	I	*	2.39	24
25	-5700.	I	*	2.23	25
26	-5675.	I	*	2.36	26
27	-5650.	I	*	2.15	27
28	-5625.	I	*	2.17	28
29	-5600.	I	*	2.27	29
30	-5575.	I	*	1.72	30
31	-5550.	I	*	1.87	31
32	-5525.	I	*	2.18	32
33	-5500.	I	*	2.51	33
34	-5475.	I	*	2.31	34
35	-5450.	I	*	1.90	35
36	-5425.	I	*	2.03	36
37	-5400.	I	*	2.55	37
38	-5375.	I	*	2.23	38
39	-5350.	I	*	2.70	39
40	-5325.	I	*	2.05	40
41	-5300.	I	*	2.06	41

XBOT= -5300.

YINC= 0.2000

YMIN= -10.00

YMAX= 10.00

LINE 2000. F SECONDARY FIELD QUADRATURE HSQ/I

FORM No. 11-15 013421

XTDP= -6300.

XINC= 25.00

128227

214

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-6300.			I	*	4.31	1
2	-6275.			I	*	4.61	2
3	-6250.		*	I		-9.62	3
4	-6225.			I*		1.15	4
5	-6200.			*I		-1.28	5
6	-6175.			*I		-2.41	6
7	-6150.		*	I		-6.17	7
8	-6125.		*	I		-5.97	8
9	-6100.		*	I		-5.73	9
10	-6075.		*	I		-6.76	10
11	-6050.		*	I		-7.70	11
12	-6025.		*	I		-9.86	12
13	-6000.		*	I		-10.58	13
14	-5975.		*	I		-13.77	14
15	-5950.		*	I		-12.83	15
16	-5925.		*	I		-13.00	16
17	-5900.	*		I		-23.48	17
18	-5875.		*	I		-15.26	18
19	-5850.		*	I		-15.99	19
20	-5825.	*		I		-17.75	20
21	-5800.	*		I		-20.53	21
22	-5775.		*	I		-17.47	22
23	-5750.	*		I		-19.67	23
24	-5725.	*		I		-20.26	24
25	-5700.	*		I		-19.26	25
26	-5675.	*		I		-20.65	26
27	-5650.	*		I		-20.49	27
28	-5625.	*		I		-18.79	28
29	-5600.	*		I		-19.56	29
30	-5575.	*		I		-18.85	30
31	-5550.	*		I		-16.69	31
32	-5525.		*	I		-14.42	32
33	-5500.		*	I		-13.40	33
34	-5475.		*	I		-12.33	34
35	-5450.		*	I		-12.54	35
36	-5425.		*	I		-10.09	36
37	-5400.		*	I		-10.29	37
38	-5375.		*	I		-10.50	38
39	-5350.		*	I		-9.41	39
40	-5325.		*	I		-7.04	40
41	-5300.		*	I		-6.03	41

XBOT= -5300.
YMIN= -50.00

YINC= 1.000
YMAX= 50.00

LINE 2500. F MAGNETOMETRIC RESISTIVITY MMR

FORM NO. 1
0143433

216

XTOP= -6300.

XINC= 75.00

128229

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

1	-6300.	I	*	2.62	1
2	-6275.	I	*	2.70	2
3	-6250.	I	*	2.73	3
4	-6225.	I	*	2.42	4
5	-6200.	I	*	2.26	5
6	-6175.	I	*	2.30	6
7	-6150.	I	*	2.10	7
8	-6125.	I	*	2.17	8
9	-6100.	I	*	2.06	9
10	-6075.	I	*	2.76	10
11	-6050.	I	*	2.12	11
12	-6025.	I	*	2.12	12
13	-6000.	I	*	1.97	13
14	-5975.	I	*	1.94	14
15	-5950.	I	*	2.18	15
16	-5925.	I	*	2.21	16
17	-5900.	I	*	2.33	17
18	-5875.	I	*	2.02	18
19	-5850.	I	*	2.21	19
20	-5825.	I	*	2.00	20
21	-5800.	I	*	1.94	21
22	-5775.	I	*	1.91	22
23	-5750.	I	*	1.86	23
24	-5725.	I	*	2.01	24
25	-5700.	I	*	1.83	25
26	-5675.	I	*	1.78	26
27	-5650.	I	*	1.92	27
28	-5625.	I	*	1.75	28
29	-5600.	I	*	1.54	29
30	-5575.	I	*	1.68	30
31	-5550.	I	*	1.52	31
32	-5525.	I	*	1.52	32
33	-5500.	I	*	1.49	33
34	-5475.	I	*	1.62	34
35	-5450.	I	*	1.87	35
36	-5425.	I	*	2.02	36
37	-5400.	I	*	1.95	37
38	-5375.	I	*	1.75	38
39	-5350.	I	*	1.85	39
40	-5325.	I	*	1.85	40
41	-5300.	I	*	1.68	41

XBOT= -5300.

YINC= 0.7000

YMIN= -10.00

YMAX= 10.00

LINE 2500. F SECONDARY FIELD QUADRATURE HSD/I

FORM No. 11 15
0143405

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59					59
60					60

LINE 217 2600. E FREQUENCY=3HZ N006

MOORE PARAGON (WA) LIMITED

LINE	STATION	CURRENT	HP	---FIELD---		---OFFSET---		HU	HN	MMR	PFF	RPS	HSD/I	HSP/I	STATION
				PFE	RPS	PFE	RPS								
5	-6300. N	3.74	0.65	-11.80	4.70	-4.50	2.55	0.17	105.74	4.00	-7.30	2.15	3.26	-12.69	-6300. N
6	-6275. N	3.74	0.58	-11.60	4.60	-4.50	2.55	0.17	90.67	-7.38	-7.10	2.05	2.77	-11.01	-6275. N
7	-6250. N	3.74	0.62	-11.20	4.60	-4.50	2.55	0.18	93.57	-5.27	-6.70	2.05	2.97	-11.11	-6250. N
8	-6225. N	3.74	0.64	-10.50	4.70	-4.50	2.55	0.18	93.25	-5.73	-6.00	2.15	3.21	-10.27	-6225. N
9	-6200. N	3.74	0.71	-10.00	4.70	-4.50	2.55	0.19	92.89	-0.10	-5.50	1.65	2.73	-10.44	-6200. N
10	-6175. N	3.74	0.80	-9.30	3.80	-4.50	2.55	0.20	108.71	7.93	-4.80	1.75	2.33	-10.27	-6175. N
11	-6150. N	3.74	0.81	-8.70	3.80	-4.50	2.55	0.20	106.35	5.99	-4.20	1.25	2.36	-9.10	-6150. N
12	-6125. N	3.74	0.81	-8.40	3.70	-4.50	2.55	0.21	102.83	2.76	-3.90	1.15	2.17	-8.45	-6125. N
13	-6100. N	3.74	0.75	-8.30	3.80	-4.50	2.55	0.22	92.14	-7.91	-3.80	1.25	2.19	-7.67	-6100. N
14	-6075. N	3.74	0.80	-7.80	3.80	-4.50	2.55	0.22	95.21	-4.98	-3.30	1.25	2.33	-7.06	-6075. N
15	-6050. N	3.74	0.85	-7.50	3.70	-4.50	2.55	0.23	98.12	-2.01	-3.00	1.15	2.28	-6.82	-6050. N
16	-6025. N	3.74	0.99	-7.70	3.70	-4.50	2.55	0.24	111.04	12.17	-3.70	1.15	2.66	-8.47	-6025. N
17	-6000. N	3.74	0.93	-7.60	3.40	-4.50	2.55	0.24	101.54	1.74	-3.10	0.85	1.84	-7.71	-6000. N
18	-5975. N	3.74	0.93	-7.50	3.40	-4.50	2.55	0.25	99.06	-1.09	-3.00	0.85	1.84	-7.46	-5975. N
19	-5950. N	3.74	0.94	-7.50	3.50	-4.50	2.55	0.26	97.93	-2.46	-3.00	0.95	2.08	-7.54	-5950. N
20	-5925. N	3.75	0.95	-7.30	3.30	-4.50	2.55	0.26	96.81	-3.86	-2.80	0.75	1.66	-7.09	-5925. N
21	-5900. N	3.75	0.92	-7.00	3.30	-4.50	2.55	0.27	92.74	-9.55	-2.50	0.75	1.61	-6.13	-5900. N
22	-5875. N	3.75	0.98	-7.00	3.30	-4.50	2.55	0.27	96.99	-3.75	-2.50	0.75	1.71	-6.53	-5875. N
23	-5850. N	3.75	1.00	-6.90	3.20	-4.50	2.55	0.27	98.04	-2.46	-2.40	0.65	1.51	-6.40	-5850. N
24	-5825. N	3.75	0.00	0.00	0.00	-4.50	2.55	0.27	0.00	-126.52	4.50	-2.55	0.00	0.00	-5825. N
25	-5800. N	3.75	0.00	0.00	0.00	-4.50	2.60	0.27	0.00	-126.76	4.50	-2.60	0.00	0.00	-5800. N
26	-5775. N	3.75	0.95	-7.00	3.20	-4.50	2.60	0.27	92.61	-9.35	-2.50	0.60	1.33	-6.33	-5775. N
27	-5750. N	3.75	0.94	-6.90	3.70	-4.50	2.60	0.27	92.16	-9.86	-2.40	0.60	1.31	-6.02	-5750. N
28	-5725. N	3.75	0.92	-6.80	3.70	-4.50	2.60	0.27	91.05	-11.15	-2.30	0.60	1.28	-5.64	-5725. N
29	-5700. N	3.75	0.92	-6.70	3.30	-4.50	2.60	0.27	92.74	-9.55	-2.20	0.70	1.50	-5.40	-5700. N
30	-5675. N	3.75	0.90	-6.90	3.30	-4.50	2.60	0.26	91.72	-10.03	-2.40	0.70	1.47	-5.76	-5675. N
31	-5650. N	3.75	0.87	-6.90	3.20	-4.50	2.60	0.26	90.39	11.40	-2.40	0.60	1.21	-5.57	-5650. N
32	-5625. N	3.75	0.87	-6.90	3.30	-4.50	2.60	0.25	92.42	-8.80	-2.40	0.70	1.42	-5.57	-5625. N
33	-5600. N	3.75	0.85	-7.00	3.30	-4.50	2.60	0.24	92.56	-8.43	-2.50	0.70	1.38	-5.67	-5600. N
34	-5575. N	3.75	0.84	-6.90	3.20	-4.50	2.60	0.24	93.96	-6.66	-2.40	0.60	1.17	-5.38	-5575. N
35	-5550. N	3.76	0.77	-7.70	3.30	-4.50	2.60	0.23	88.42	-12.41	-2.70	0.70	1.25	-5.53	-5550. N
36	-5525. N	3.76	0.82	-6.90	3.30	-4.50	2.60	0.22	97.07	-3.05	-2.40	0.70	1.33	-5.23	-5525. N
37	-5500. N	3.76	0.75	-6.80	3.20	-4.50	2.60	0.22	91.65	-8.41	-2.30	0.60	1.04	-4.59	-5500. N
38	-5475. N	3.76	0.76	-6.90	3.50	-4.50	2.60	0.21	95.97	-3.92	-2.40	0.90	1.59	-4.85	-5475. N
39	-5450. N	3.76	0.76	-6.80	3.40	-4.50	2.60	0.20	99.76	-0.70	-2.30	0.80	1.41	-4.65	-5450. N
40	-5425. N	3.76	0.75	-6.80	3.30	-4.50	2.60	0.20	101.37	1.25	-2.30	0.70	1.27	-4.59	-5425. N
41	-5400. N	3.76	0.69	-7.00	3.40	-4.50	2.60	0.19	96.56	-3.02	-2.50	0.80	1.28	-4.59	-5400. N
42	-5375. N	3.76	0.70	-6.90	3.40	-4.50	2.60	0.18	101.45	1.23	-2.40	0.80	1.30	-4.47	-5375. N
43	-5350. N	3.76	0.68	-6.80	3.50	-4.50	2.60	0.18	102.08	1.71	-2.30	0.90	1.42	-4.16	-5350. N
44	-5325. N	3.76	0.65	-6.80	3.40	-4.50	2.60	0.17	101.07	0.85	-2.30	0.80	1.21	-3.98	-5325. N
45	-5300. N	3.76	0.65	-6.80	3.50	-4.50	2.60	0.17	104.68	3.58	-2.30	0.90	1.36	-3.98	-5300. N

FORM No 11 15

218

XTOP# -6300.

XINC# 25.00

128231

MOORE PARAGON (WA) LIMITED - FORMALINER PARALO

1	-6300		I *	4.00
2	-6275	*	I	-7.38
3	-6250	*	I	-5.27
4	-6225	*	I	-5.73
5	-6200		*	-0.10
6	-6175		I *	7.93
7	-6150		I *	5.99
8	-6125		I *	2.76
9	-6100	*	I	-7.91
10	-6075	*	I	-4.98
11	-6050		*I	-2.01
12	-6025		I *	12.17
13	-6000		I *	1.74
14	-5975		*I	-1.09
15	-5950		*I	-2.46
16	-5925		*I	-3.86
17	-5900	*	I	-9.55
18	-5875	*	I	-3.75
19	-5850	*	I	-2.46
20	-5825	*	I	-126.52
21	-5800	*	I	126.76
22	-5775	*	I	-9.35
23	-5750	*	I	-9.86
24	-5725	*	I	-11.15
25	-5700	*	I	-9.55
26	-5675	*	I	-10.03
27	-5650	*	I	-11.40
28	-5625	*	I	-8.80
29	-5600	*	I	-8.43
30	-5575	*	I	-6.66
31	-5550	*	I	12.41
32	-5525	*	I	-3.05
33	-5500	*	I	-8.41
34	-5475	*	I	-3.92
35	-5450	*	I	0.70
36	-5425	*	*	1.25
37	-5400	*	I	-3.02
38	-5375	*	*	1.23
39	-5350	*	I *	1.71
40	-5325	*	*	0.85
41	-5300	*	I *	3.58

XBOT# -5300.
YMIN# -126.8

YINC# 1.768
YMAX# 50.00

LINE 2600. F MAGNETOMETRIC RESISTIVITY MMR

FORM No. 11 15
0103407

219

XTOP= -6300.

XINC= 75. 00

128232

MOORE PARAGON (W.A.) LIMITED - FORMALINER PARAFLO

FORM No. 11 15

1	-6300	I		*	2.15	1
2	-6275	I		*	2.05	2
3	-6250	I		*	2.05	3
4	-6225	I		*	2.15	4
5	-6200	I		*	1.65	5
6	-6175	I		*	1.25	6
7	-6150	I		*	1.25	7
8	-6125	I		*	1.15	8
9	-6100	I		*	1.25	9
10	-6075	I		*	1.25	10
11	-6050	I		*	1.15	11
12	-6025	I		*	1.15	12
13	-6000	I		*	0.85	13
14	-5975	I		*	0.85	14
15	-5950	I		*	0.95	15
16	-5925	I		*	0.75	16
17	-5900	I		*	0.75	17
18	-5875	I		*	0.75	18
19	-5850	I		*	0.65	19
20	-5825	I	*		-2.55	20
21	-5800	I	*		-2.60	21
22	-5775	I	*		0.60	22
23	-5750	I	*		0.60	23
24	-5725	I	*		0.60	24
25	-5700	I	*		0.70	25
26	-5675	I	*		0.70	26
27	-5650	I	*		0.60	27
28	-5625	I	*		0.70	28
29	-5600	I	*		0.70	29
30	-5575	I	*		0.60	30
31	-5550	I	*		0.70	31
32	-5525	I	*		0.70	32
33	-5500	I	*		0.60	33
34	-5475	I	*		0.90	34
35	-5450	I	*		0.80	35
36	-5425	I	*		0.70	36
37	-5400	I	*		0.80	37
38	-5375	I	*		0.80	38
39	-5350	I	*		0.90	39
40	-5325	I	*		0.80	40
41	-5300	I	*		0.90	41

XBOT= 5300.

YINC= 0.5100E-01

YMIN= -2.600

YMAX= 2.500

LINE 2600. F RELATIVE PHASE SHIFT RPS

42						42
43						43
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