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169 MILLER STREET, NORTH SYDNEY, AUSTRALIA 2060

TECHNICAL REPORT

REPORT ON WALLIS DRILLING COMPANY,
TEST DRILLING PROGRAMME

NORTH-EAST TASMANIA
JANUARY TO FEBRUARY, 1980

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Kibuka Mines Pty. Limited

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PROJECT: D 136/140/141 Pioneer/Endurance/Monarch, Tasmania

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SUMMARY

A test drilling programme was carried out using the Wallis Drilling Company reverse circulation system on cassiterite bearing alluvials in North-East Tasmania. Check holes were completed adjacent to cable tool percussion holes to evaluate recovery and grade. Sixty-six holes for a total of 1,370 metres of drilling were completed at Pioneer, Endurance and Monarch thereby testing the system in different types of alluvial sequence and for different thicknesses of alluvial section. The Wallis system performed satisfactorily. It is faster, cheaper and of the same order of accuracy as cable tool percussion drilling. It is recommended that this drilling method be used for future drilling of stanniferous placer deposits in North-East Tasmania.

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INTRODUCTION

Wallis Drilling Company Pty. Ltd. of Perth, W.A. was contracted to carry out a drilling programme in the Pioneer area using a reverse circulation drilling system.

The programme was aimed at testing the Wallis system on the cassiterite bearing Tertiary alluvial sequences in North-East Tasmania. The objective of the programme was to determine if the Wallis drilling system could provide a faster, cheaper but equally accurate drilling alternative to the cable tool percussion rigs which have been used in the area for decades.

The Wallis rig and personnel were mobilised from W.A. and arrived on site at Pioneer on 15th January, 1980.

The testing programme of twenty holes at Pioneer, two holes at Endurance and forty-four holes at Monarch was completed on 5th February, 1980. A total of 1,370 metres of drilling was completed in seventeen days at an agreed contract rate of \$1,250/day or \$15.50/metre. Total cost for the drilling programme was \$30,300 which includes \$10,000 for mobilisation.

The daily drilling production is shown in Table I.

TABLE I

Wallis DrillingDaily Drilling Production

Date	Location	Metres Drilled	Holes Drilled	Hours Drilled	Hours Delay	Total Hours
16.1.80	Pioneer	56	1	6	5	11½
17.1.80	"	99	2	7½	2¾	10½
18.1.80	"	40	1	7	2	9
19.1.80	"	48	1	5½	1	6½
21.1.80	"	88	2	5¾	2	7¾
22.1.80	"	78	2	6	2½	8½
23.1.80	"	110	2	6½	1	7½
24.1.80	"	81	2	7½	4	11½
25.1.80	"	105	2	7	2½	9½
26.1.80	"	98	2	7	1½	8½
29.1.80	Endurance	57	1	6	3	9
30.1.80	"	54	1	7¼	2½	9½
31.1.80	Monarch	99	18		Drilling	10
1.2.80	"	65	10		and	10
2.2.80	"	79	16		Setting Up	10
4.2.80	Pioneer	108	2	7	1	8
5.2.80	"	105	2	7¾	1	8¾
<u>TOTAL</u>	-	1,370	-	-	-	-

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DRILLING METHOD

The Wallis system is based on an H 13 model Gemco drill rig which is mounted on a six-wheel drive truck (Plate 1). The drill is fitted with a Wallis patented reverse circulation air core drilling and sampling system which is hydraulically operated. Details are provided in Table II.

The Wallis system uses twin tube rods 3 metres in length and tungsten carbide bits (Plate 2).

Air and/or water are forced down the outer tube by either a compressor or a piston pump and the sample is forced up the inner tube. The sample is collected continuously as the rods advance through each 2 metre interval by cycloning into bins.

When 'tight' ground is encountered, reaming of the hole becomes necessary to prevent jamming of the rods. Reaming involves the raising and lowering of the rods with continuous rotation. This action enlarges the hole sufficiently to prevent jamming of the rods. The hole is then flushed out, usually with water, and sampling of the hole is recommenced. Material recovered during reaming is not collected for assay.

TABLE IISpecifications of Gemco Drill Used at Pioneer, Tasmania

The drill is a modified Gemco Model H 12 top drive hydraulic drill rig of the following specifications.

Stroke	4 metres
Pull out	18,000 lbs.
Pull down	14,000 lbs.
Rotation	1,100 ft. lbs.
Slow feed	20 ft./min.
Injection pump	20 gpm Worthington
Compressor	250 cfm F.A.D. Delivery pressure 100 psi
Rig carrier	Reo Model M 6 x 6
Sampling system	Wallis Air Core (patents held by Wallis Drilling)
Nominal hole size	3-3/32" (80 mm)
System type	Reverse circulation dual tube

SAMPLE TREATMENT

Samples collected in plastic bins were transported to the sample washing shed where they were left standing to allow settling of finer grained material.

Recovered volume of sample was measured in litres by inserting a calibrated rod into the bin of material.

Clay-rich samples were tumbled to reduce clay fragments to a slurry.

The initial concentrating mechanism in the sample washing process is cradling (Plate 5). This is followed by panning (Plate 6) to a heavy mineral-rich concentrate weighing about 100 grams.

This concentrate is dried, weighed, pulverised and then assayed with the Company's XRF unit (Plate 7).

COMPARISON OF PERCUSSION AND WALLIS METHODS

Four reverse circulation holes were drilled by Wallis adjacent to three cable tool percussion holes drilled by Amdex at Pioneer.

<u>Amdex Holes</u>	<u>Wallis Holes</u>
K 111	K 150 A
	K 150 B
K 110	K 151
K 81	K 153

These check holes were drilled so that Wallis results could be compared with results for cable tool percussion drilling, a method of drilling that Amdex considers to be reliable and satisfactory.

The Wallis drilling produced much greater variation in recovered volumes than the percussion drilling (Appendix I). Variation in recovered volume seems to be a universal problem with alluvial drilling and appears to be accentuated by the Wallis method.

The Wallis recoveries are generally less than the theoretical volume for about the first 20 metres and greater than the theoretical volume for the remainder of the hole until basement where there is a marked decrease in the volumes recovered (see drill holes K 150 B and K 169 in Appendix I). The recovered volumes for various Wallis and percussion holes are shown on histograms in Appendix I). The histograms clearly show the recovery

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characteristics of the two drilling methods.

The percussion drilling method produces more consistent recovered volumes which average approximately 65% of the theoretical volume. Recovered volumes (see drill holes K 110 and K 111 in Appendix I) greater than the theoretical volume are not commonly obtained with the cable tool percussion method. It is generally considered that the more consistent the sample size the more reliable are the relative grades single drill hole.

A comparison of grades for the check holes completed at Pioneer is shown in Table III. Obviously this comparison must be regarded with caution because of the inherent variability in tin content of the alluvial sequence.

At K 81 the Wallis grade is slightly higher than the cable tool grade.

At K 110 the grades for the two Wallis holes are at variance with the cable tool percussion grades but this is thought to be due to variations in the cassiterite content in the ground.

At K 111 the grades for two Wallis holes show excellent correlation with grades from the percussion drilling. The Wallis grades are slightly less than the percussion hole grades.

PIONEER, NORTH-EAST TASMANIA

TABLE III

WALLIS DRILLING COMPANY - TEST HOLES

HOLE NUMBER	REC. VOL. (1) Surface to int. basement	TH. VOL. (1) Surf. to int. basement	TOTAL REC. SnO ₂ (g)	GRADE OF HOLE SURFACE TO BASEMENT (g SnO ₂ /m ³) SnO ₂ in granite added to last interval of alluvials		
				Tot. tin/ Rec. vol. (A)	Average of intervals	
					Rec. tin/ Rec. vol. (B)	Rec. tin/ Rad. Fac. Th. vol. (C)
* 111	638	1040	277	434	468	365
K 150	343	280	98	286	317	313
K 150 redrill	261	280	105	401	325	319
* 110	582	1050	173	297	384	206
K 151	206	227	204	990	1735	936
K 154	183	212	25	139	130	131
* 81	639	920	318	498	545	432
K 153	223	248	126	565	538	465

* = Cable tool percussion drilling

K = Reverse circulation drilling

A. Fleming 22nd January 1980

It can be concluded that there is quite a good correlation between the grades obtained by the two drilling methods.

The comparative grade calculation exercise which has been completed is shown in Table III. Three methods of grade calculation were completed.

Method A - Grade determined by relating total recovered tin to recovered volume for the alluvial section.

Method B - Grade determined by relating recovered tin to recovered volume for each sample interval. Drag tin in the basement added to last sample of alluvial material. Overall hole grade determined by summing all intervals and calculating mean.

Method C - Same as Method B but recovered tin related to Radford Factored theoretical volume. Where recovered volume exceeds theoretical volume, recovered volume used.

For Method A, if the recoveries are significantly over or under theoretical volume, grades are disproportionately over or undervalued respectively, e.g. K 150 vs. K 150 redrill.

For Method B, if recoveries are small in tin-bearing ground dramatic overvaluing of the grade of the hole occurs, e.g. K 151.

Method C produces the most realistic grade results under all circumstances.

It appears Method C grades, calculated by relating recovered tin to Radford Factored theoretical volume, although slightly conservative compensates best for variations in recovered volume.

Inspection of drill logs for the reverse circulation and percussion holes at Pioneer indicates the Wallis system gives a more accurate picture of the vertical distribution of tin mineralisation in the sequence than the percussion method. Drag tin in the percussion drilling produces a wider vertical distribution of higher grade values whereas in the Wallis drilling higher grade intersections are narrower; The Wallis drilling gives a more realistic representation of distribution of tin which usually occurs in narrow seams.

The continuous sampling method used by the Wallis drill should show a rapid drop in the tin value when basement is intersected, however the rate of decrease in grade for the Wallis method does not appear to be much better than for the percussion method. Some drag tin is apparently being carried into the basement.

COMMENTS

1. The greatest asset of the Wallis system is its mobility and speed of drilling. Wallis takes approximately 15 minutes to set up and commence drilling whereas for percussion the set up time is longer.

A percussion rig takes nearly seven working days to complete an average 50 metre hole whereas two such holes can be drilled by Wallis each day.

2. The size of the rods used by Wallis - 10 litre theoretical volume per 2 metre section compared to 40 litres for the same interval of 150 mm casing on a percussion drill rig - is certainly a major drawback.

The smaller the sample, the less representative it is and the greater the sampling error.

3. The greater variation in recovered volume for Wallis drilling as compared to percussion drilling is another factor of concern.

It appears that the Wallis system does not sample the alluvial sequence as consistently as percussion drilling. The over volumes obtained by both methods are most certainly the result of run-in due to waterlogged ground.

Calculation of grade for holes with excessive recovered volume is a problem. However, if it is assumed that no selective sampling has occurred and the grades are calculated using total recovered volume, then the results should be fairly reliable.

4. The quality of the Wallis results appears to be closely related to the ability and experience of the driller. Holes drilled by A. Cameron, while exhibiting the variation in recovered volumes described previously do not show as great a variation in recovered volume as holes drilled by Jamie Wallis. Jamie Wallis' holes (K 162, K 163 and K 164) show quite marked overvolumes in the lower section of the holes.

The competence of the driller appears to be less critical to the results obtained from percussion drilling.

5. Once a Wallis hole is commenced it must be completed because of the continuous sampling system. Withdrawal of rods to clear blockages or replace bits necessitates the drilling of a new hole. However this is a minor problem because of the speed at which Wallis can drill.

This problem is easily overcome if the contract on a meterage basis instead of a daily rate.

6. The range of materials which can be sampled by the Wallis system is more limited than that for percussion drilling methods.

Wallis encounters problems when drilling alluvial material with a mean size of 20 mm as this material blocks the rods. Problems are also encountered with the sampling of coarse gravels which are too large to be pumped up the inner tube.

7. Considerable difficulty was experienced during the drilling at Endurance because of the tightness of the ground and small gravel blocking the rods.

The drill frequently stalled when operating at the recommended hydraulic pressure of 1,500 p.s.i. The pressure had to be raised to 2,000 p.s.i. and even at this level difficulties were still being experienced.

Similar problems were encountered at Pioneer when drilling the coarse gravels at K 153.

The driller (A. Cameron) mentioned that with a little more experience, these problems would be overcome.

8. The Monarch drilling provided an indication of the production which could be expected in shallow ground. The average depth of the holes drilled was 5.5 metres.

The majority of the working day was spent moving between drill sites and setting up. However, an average of 81 metres/day was achieved.

At Monarch variability in recovered volumes similar to that at Pioneer was experienced.

Considering the quite variable nature of the Monarch ground and differences in drilling methods the grades of Wallis holes compare reasonably well with those of the large diameter Conrad drill holes completed by B.H.P. Wallis used 80 mm diameter rods whereas B.H.P. used a 400 mm diameter casing. The evaluation of this data is the subject of another report.

9. One problem in using the Wallis system on a contract basis is the exorbitant mobilisation cost of transporting the rig from Perth. In future programmes attempts should be made to share mobilisation costs with other clients or to undertake a sufficiently large programme to reduce mobilisation charges to a reasonable proportion of the total contract cost.

10. Some thought should be given to purchasing or constructing a rig using the patented Wallis reverse circulation air core drilling and sampling system. To set up such a system properly would cost around \$75,000. This could only be justified if the total meterage of drilling on the company's own properties plus contract drilling for other clients in Tasmania was significant - say 3,000 metres per year to amortise the machine over 3 years.

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11. The cost of this drilling contract was \$22.04/metre if total cost of \$30,200 is divided by the 1,370 metres drilled. When it is remembered that of the total contract cost \$10,000 was for mobilisation the meterage rate is very cheap. By way of comparison the present cost of percussion drilling on Amdex properties using machines either owned by the Company or leased from the Mines Department is of the order of \$27/metre. The cost of Wallis drilling is very competitive.

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CONCLUSIONS

Wallis drilling is approximately fourteen times faster and considerably cheaper than the percussion method.

The small size of the Wallis rods and greater variability of recovered volumes must be weighed up against speed and cost.

An experienced and competent driller is critical to the quality of the results and any contract should specify a very experienced driller.

The Wallis system experienced difficulty recovering coarse grained alluvial material and pebbles of 20 mm mean diameter. However it satisfactorily recovers most of the lithologies of the Tertiary alluvial sequence.

The Wallis system provides results which compare well with those obtained by percussion drilling methods.

If consideration is being given to the construction of a Wallis type rig then the possibilities of using larger diameter rods should be investigated.

RECOMMENDATIONS

The Wallis Drilling Company reverse circulation drilling system is faster and cheaper than cable tool percussion drilling. It appears to provide similarly reliable results to percussion drilling when used to evaluate cassiterite-bearing alluvials in North-East Tasmania.

It is recommended that the Wallis system be used for future drilling programmes in North-East Tasmania.

Some arrangement should be made to circumvent the exorbitant mobilisation costs of bringing the rig from Perth.

Andrew Fleming

T.I. Neale and A.W. Fleming

Kibuka Mines Pty. Limited
24th March 1980

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Plate 1 Wallis drilling system, truck mounted drilling rig, water truck with rods



Plate 2 Wallis drilling bits and twin tube rods



Plate 3 Drive head showing swivel for air/water injection and gooseneck through which sample carried to cyclone

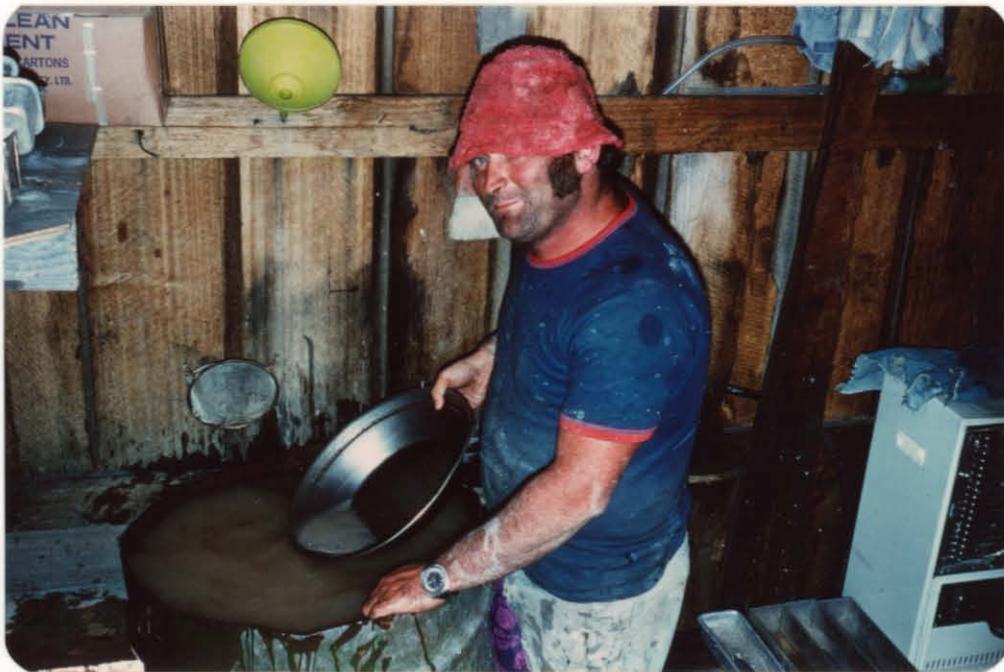


Plate 4 Recovered material passes through a cyclone into plastic bins



Bisley Sean ?

Plate 5 Cradling sample. Note one riffle has been removed as sample about to be transferred to panning dish



Tos. King ?

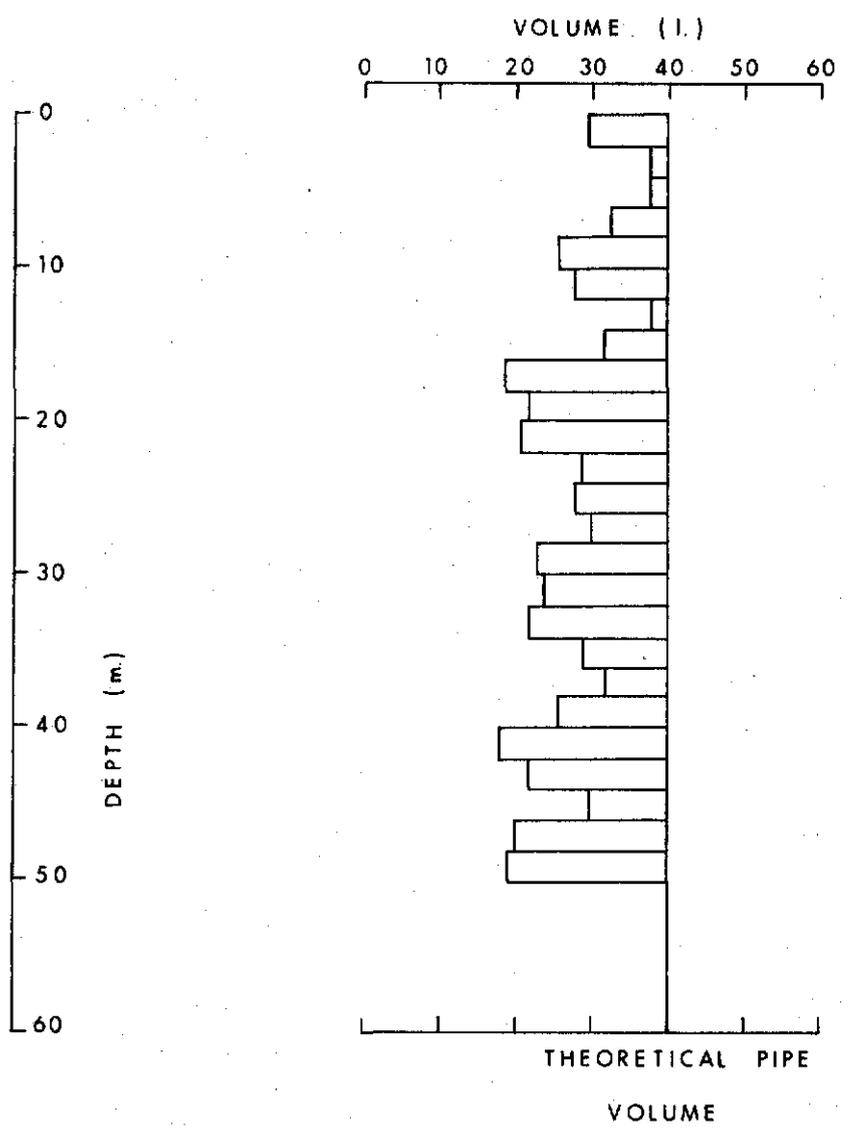
Plate 6 Panning drill sample down to concentrate



Plate 7 Amdel XRF analyser

APPENDIX I

Comparative Recovered
Volume Histograms



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PIONEER, TASMANIA

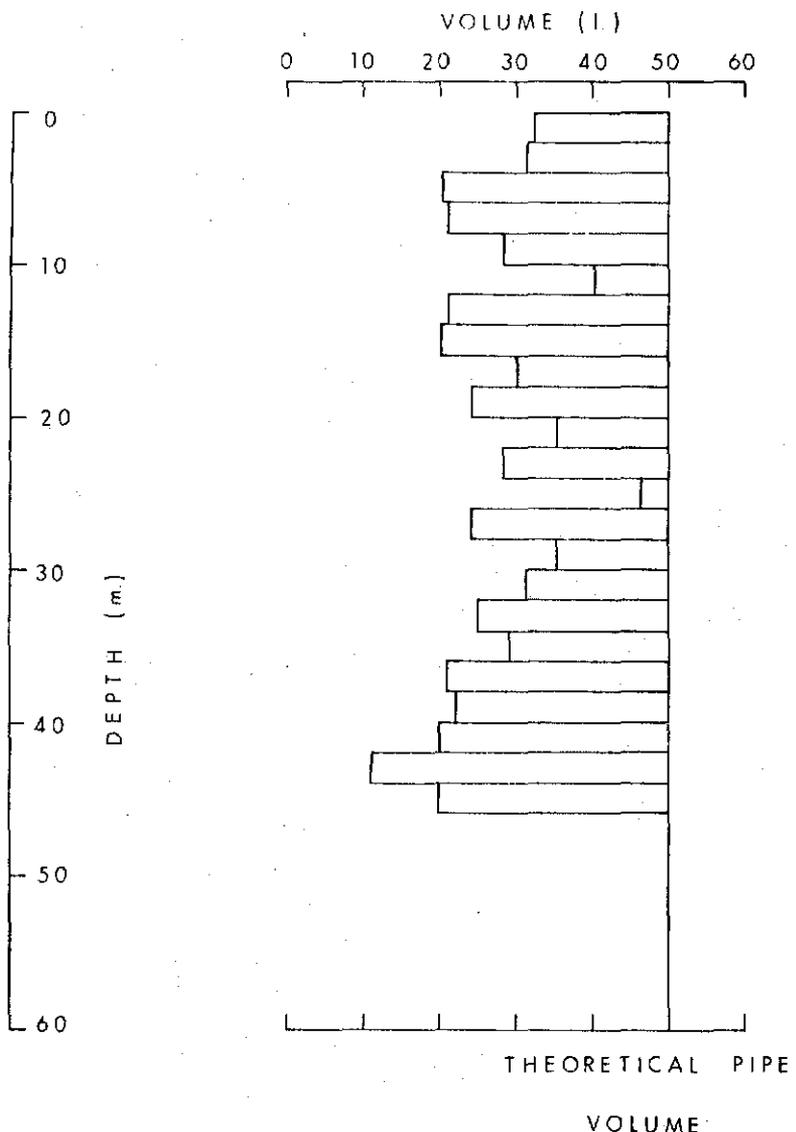
K 81

RECOVERED VOLUME

HISTOGRAM

Drilling Method: PERCUSSION

Author: T. I. NEALE	Date: February, 1980	Dwg. No.:	
Drafting: B. G.	Report No.:	Base Plan:	



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PIONEER, TASMANIA

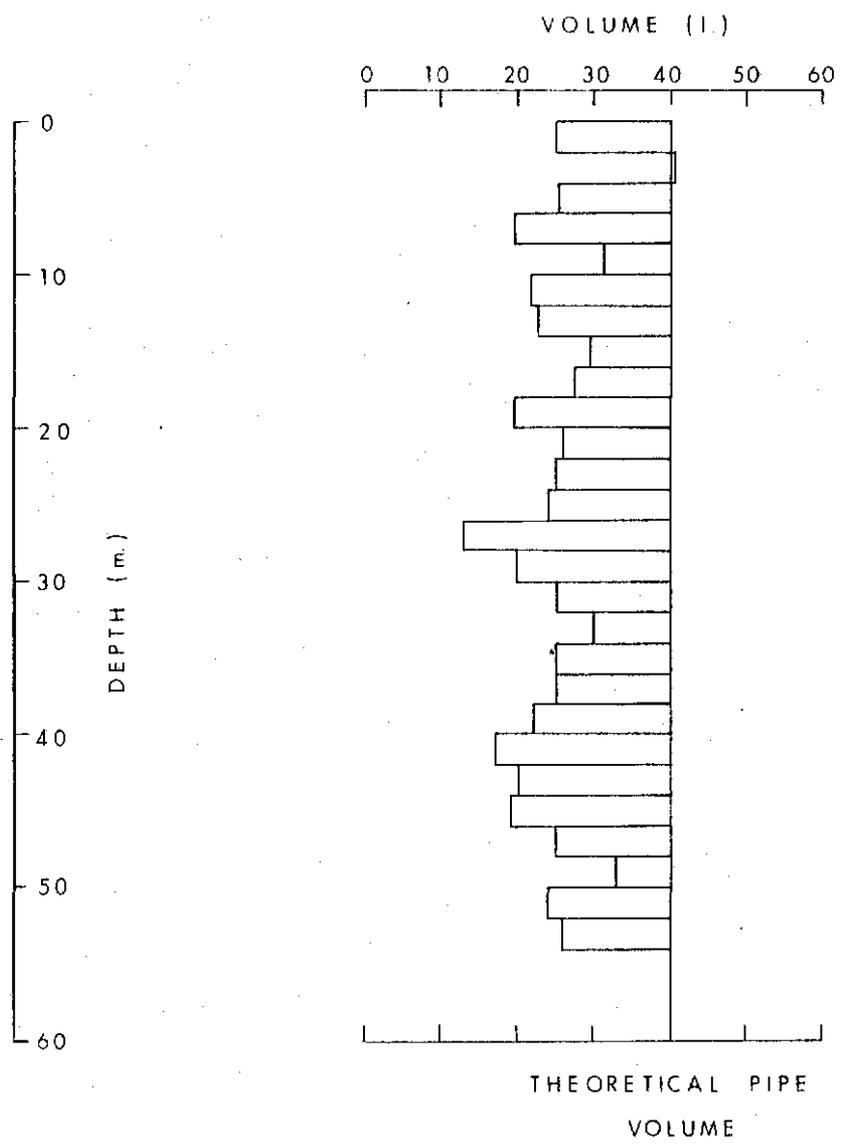
K 110

RECOVERED VOLUME

HISTOGRAM

Drilling Method: PERCUSSION

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Drafting: B. G.	Report No.:	Base Plan:



Amdex Mining Limited

PIONEER, TASMANIA

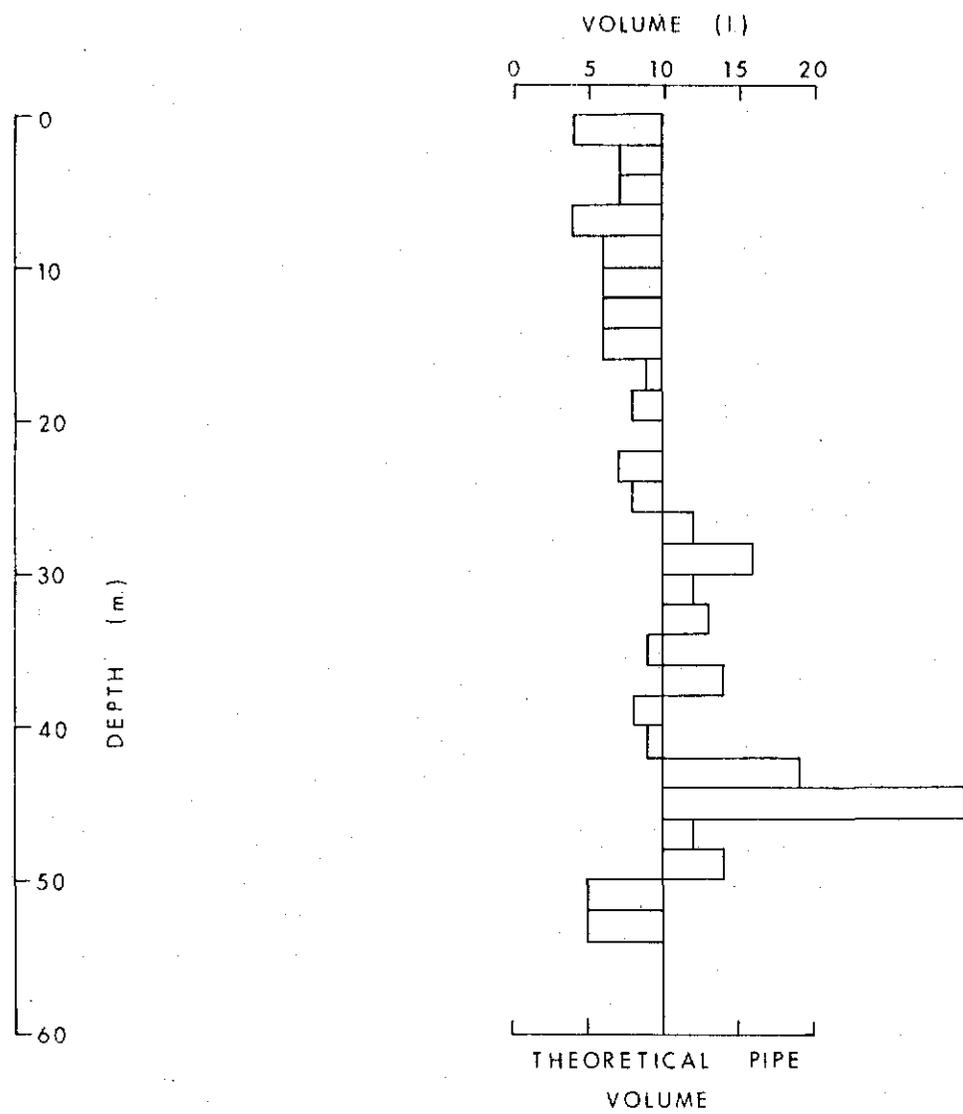
K 111

RECOVERED VOLUME

HISTOGRAM

Drilling Method: PERCUSSION

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Drafting: B. G.	Report No.:	Base Plan:	



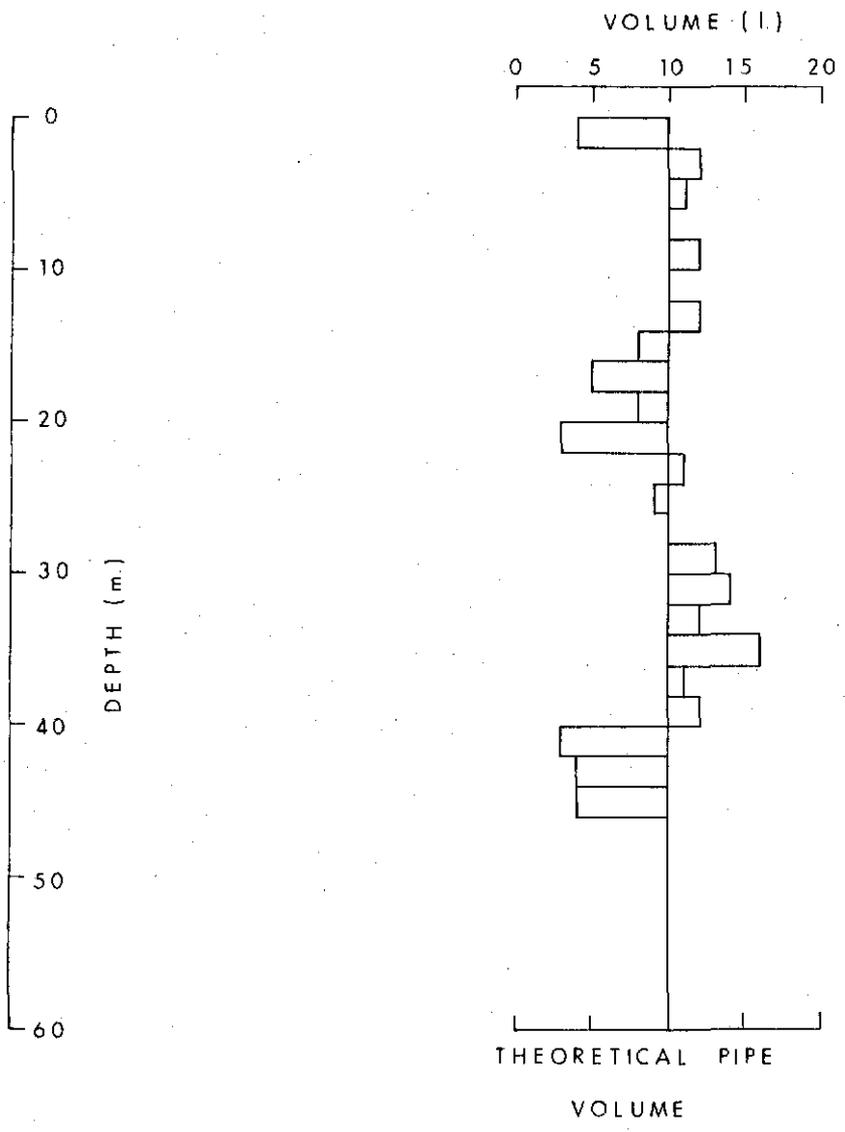
Amdex Mining Limited
 PIONEER, TASMANIA

K 150

RECOVERED VOLUME
 HISTOGRAM

Drilling Method: WALLIS

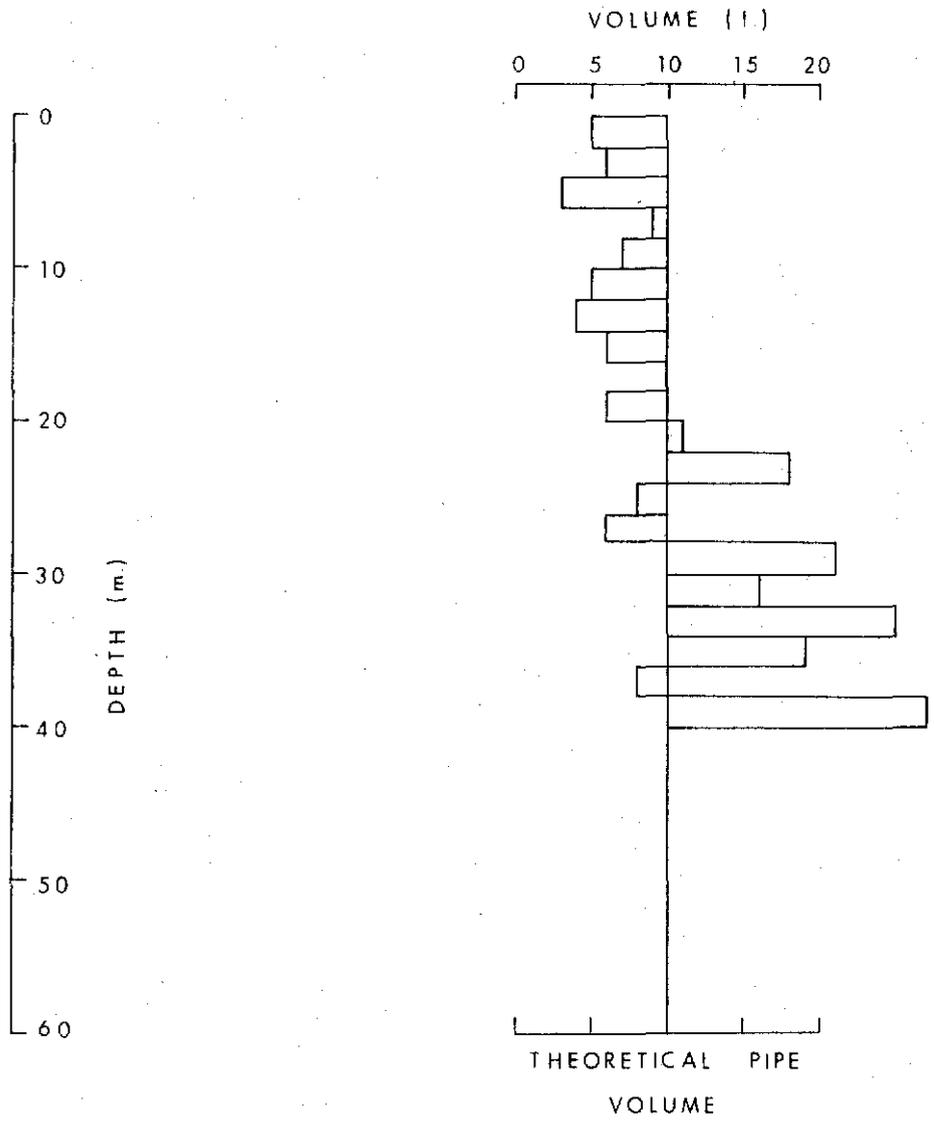
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Drafting: B. G.	Report No.:	Base Plan:	



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 PIONEER, TASMANIA
 K 151
 RECOVERED VOLUME
 HISTOGRAM

Drilling Method: WALLIS

Author: T. I. NEALE	Date: March, 1980	Dwg. No.:	
Drafting: B. G.	Report No.:	Base Plan:	



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PIONEER, TASMANIA

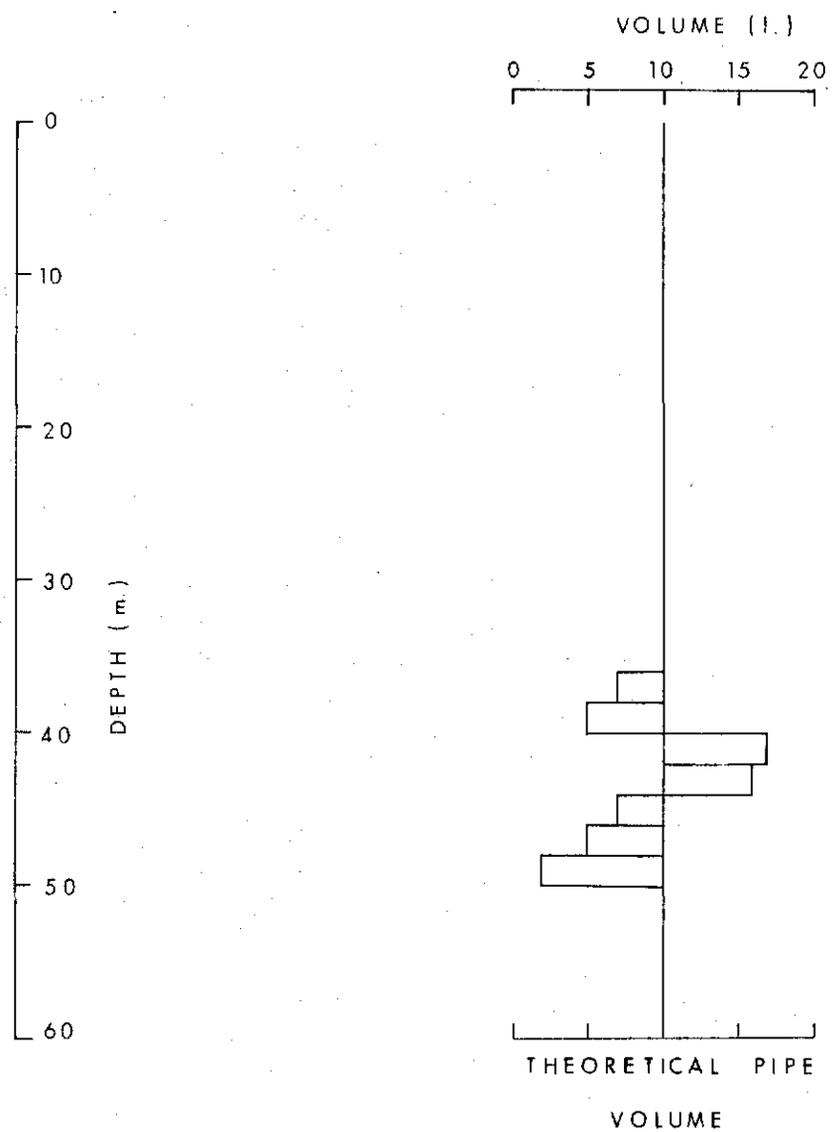
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RECOVERED VOLUME

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Drafting: B.G	Report No.:	Base Plan:	



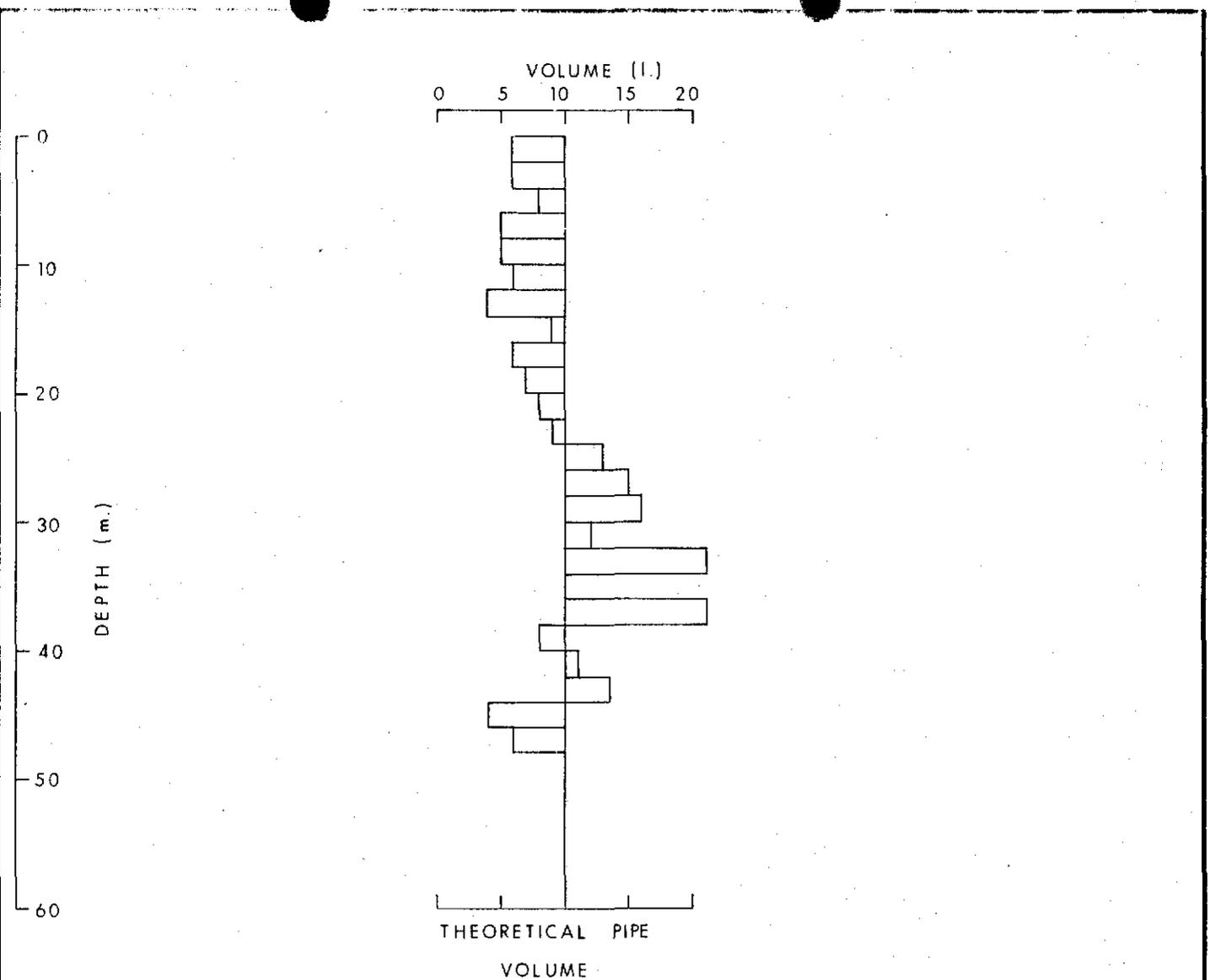
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 PIONEER, TASMANIA

K 152 R

**RECOVERED VOLUME
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Drilling Method: WALLIS

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Drafting: B. G.	Report No.:	Base Plan:	



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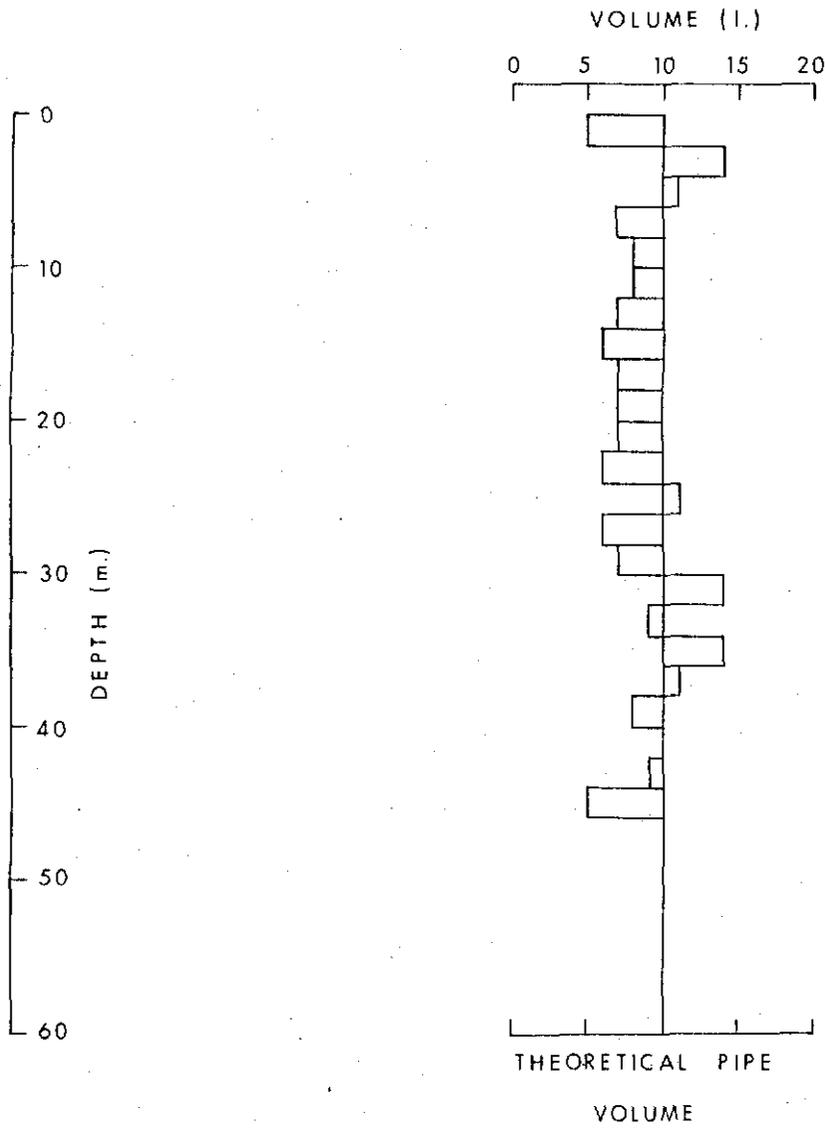
PIONEER, TASMANIA

K 153

RECOVERED VOLUME
HISTOGRAM

Drilling Method: WALLIS

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Drafting: B. G.	Report No.:	Base Plan:	



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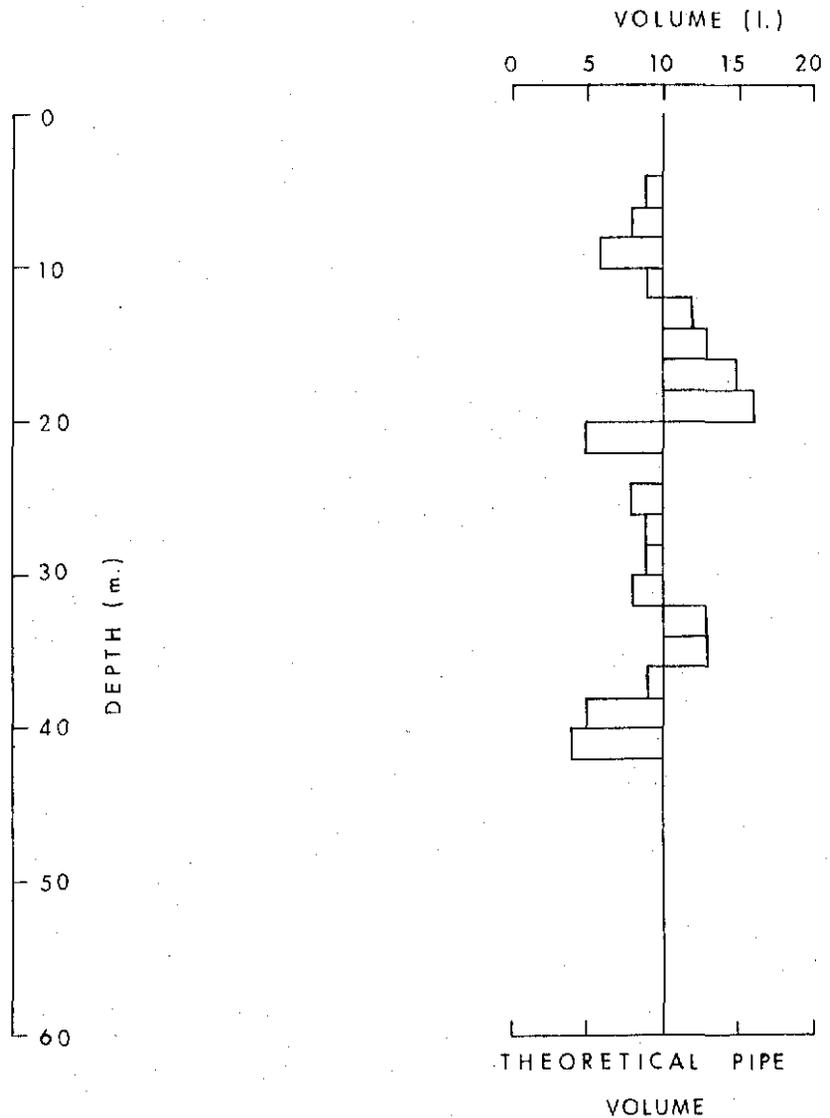
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RECOVERED VOLUME

HISTOGRAM

Drilling Method: WALLIS

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Drafting: B. G.	Report No.:	Base Plan:	



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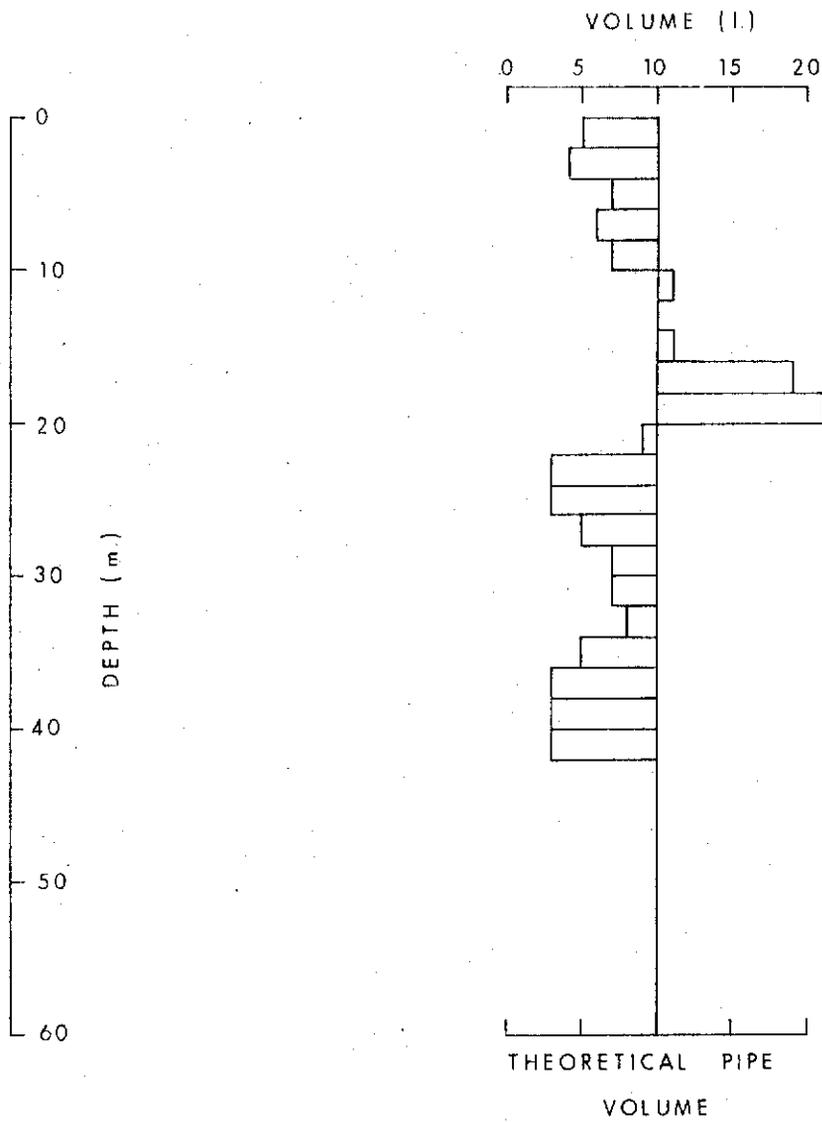
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HISTOGRAM

Drilling Method: WALLIS

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Drafting: B. G.	Report No.:	Base Plan:	



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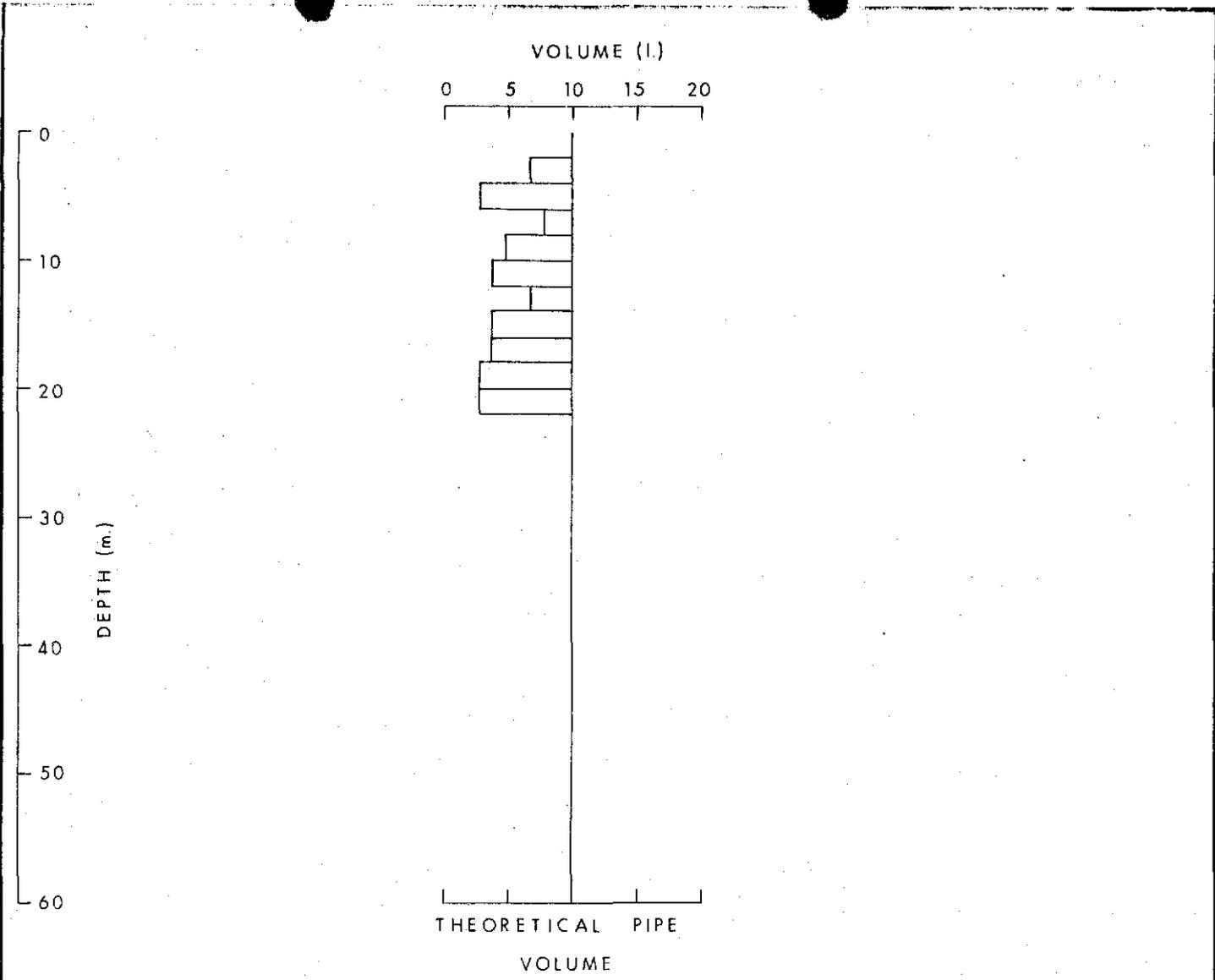
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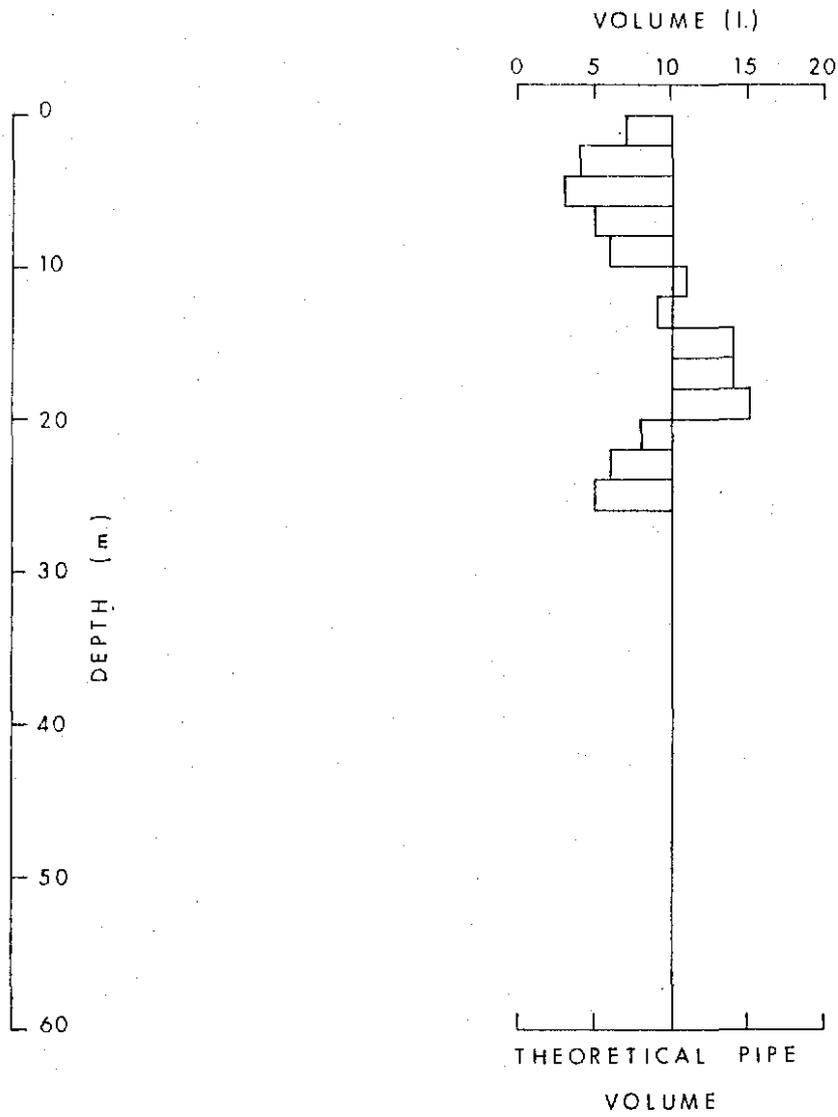
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K 157

RECOVERED VOLUME
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Drilling Method: WALLIS

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Drafting: B. G.	Report No.:	Base Plan:	



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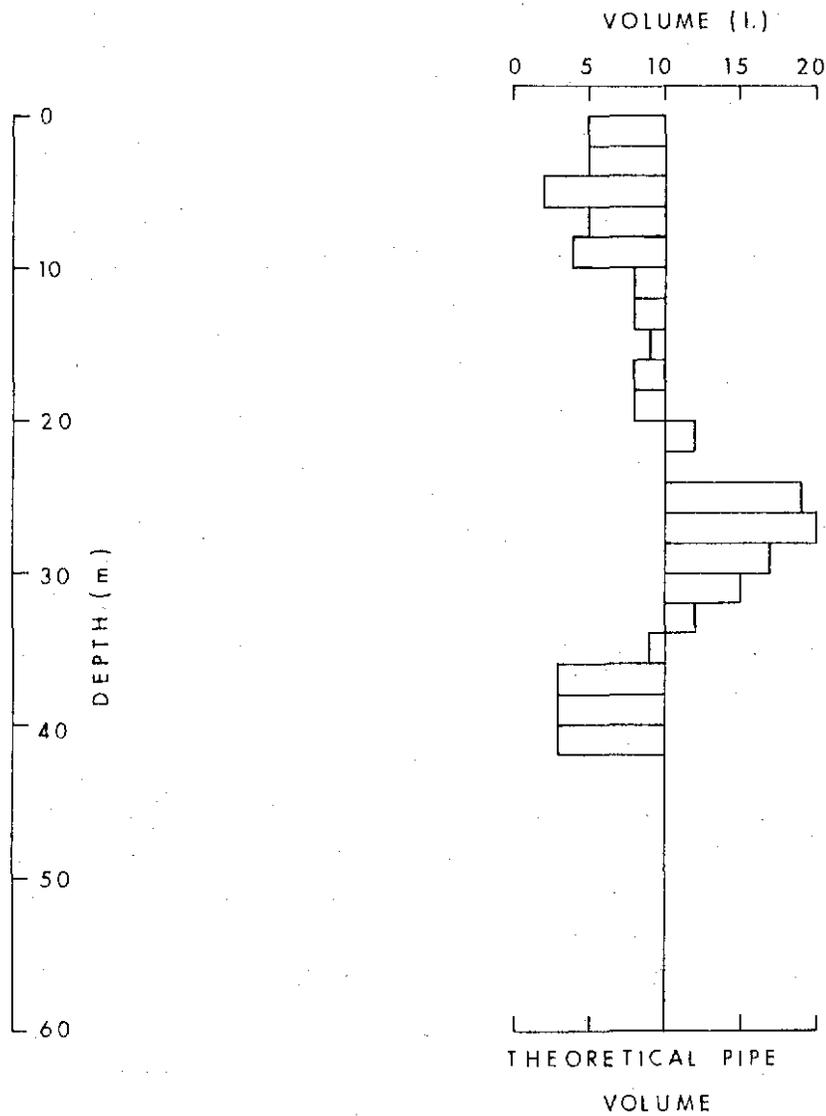
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HISTOGRAM

Drilling Method: WALLIS

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PIONEER, TASMANIA

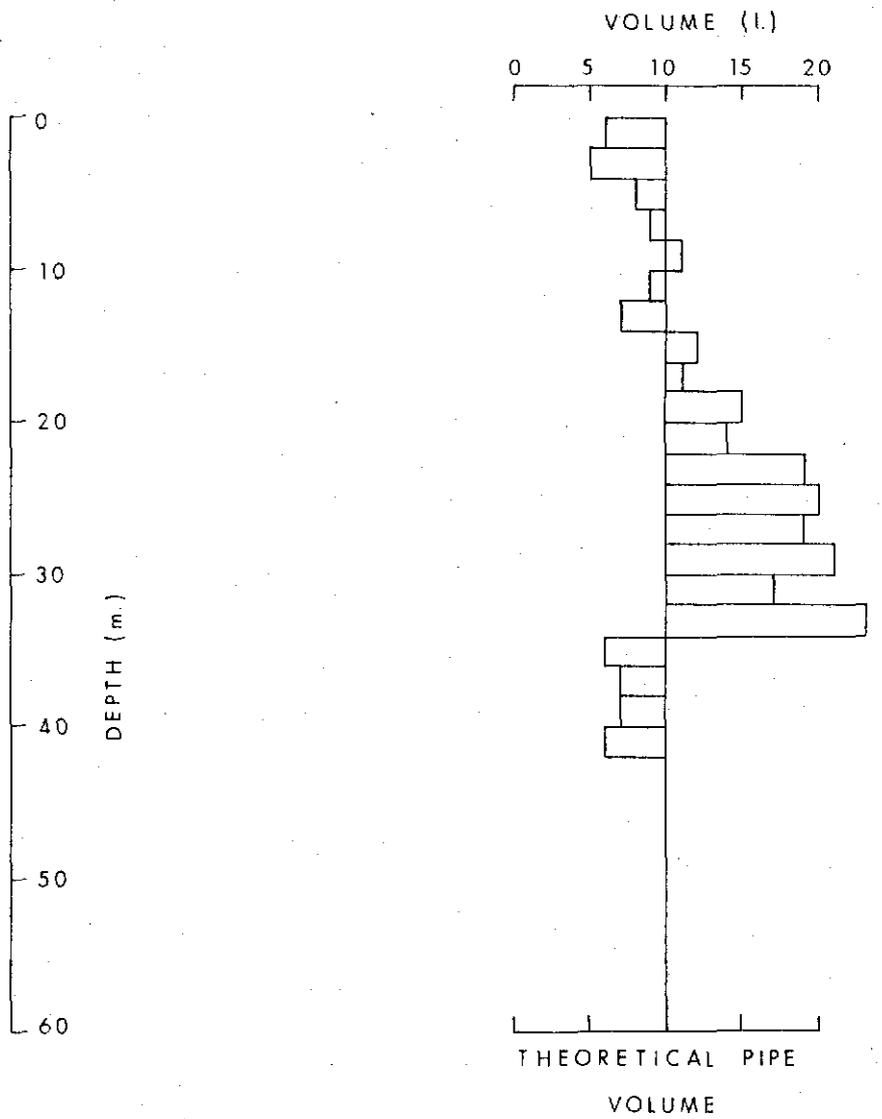
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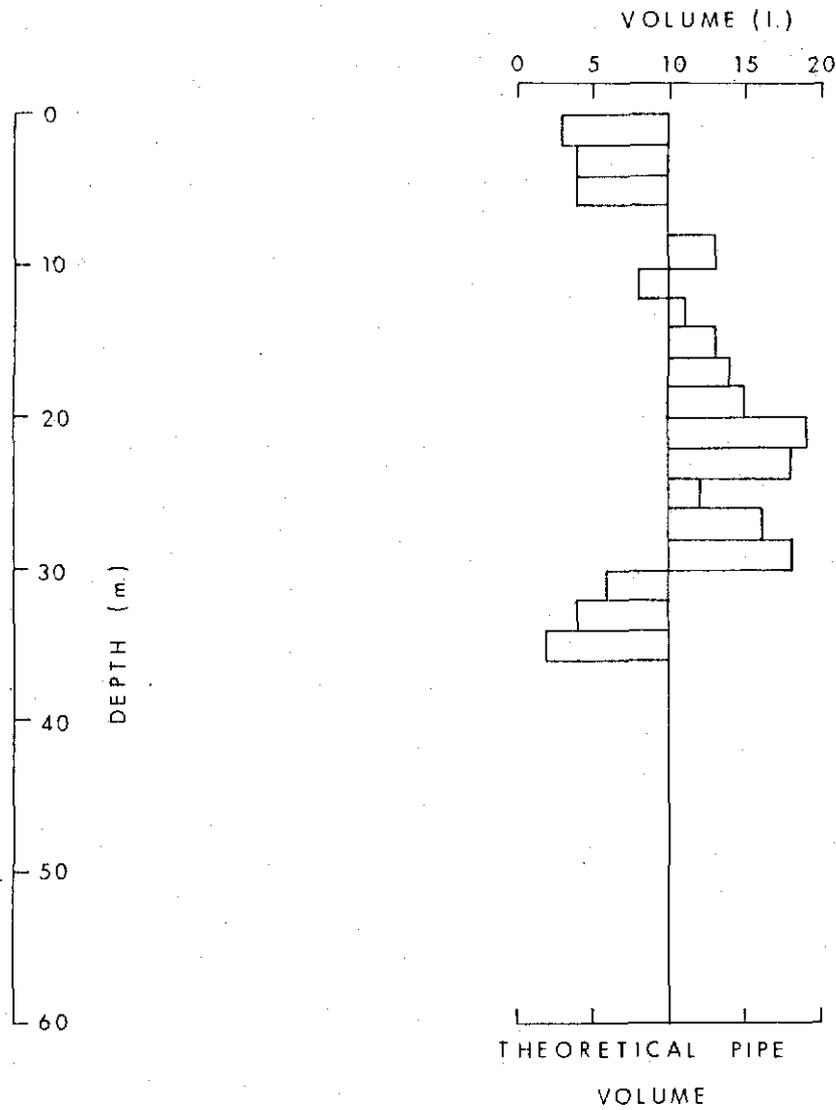
Author: T. J. NEALE	Date: March, 1980	Dwg. No.:	
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PIONEER, TASMANIA
K 160
RECOVERED VOLUME
HISTOGRAM

Drilling Method: WALLIS

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PIONEER, TASMANIA

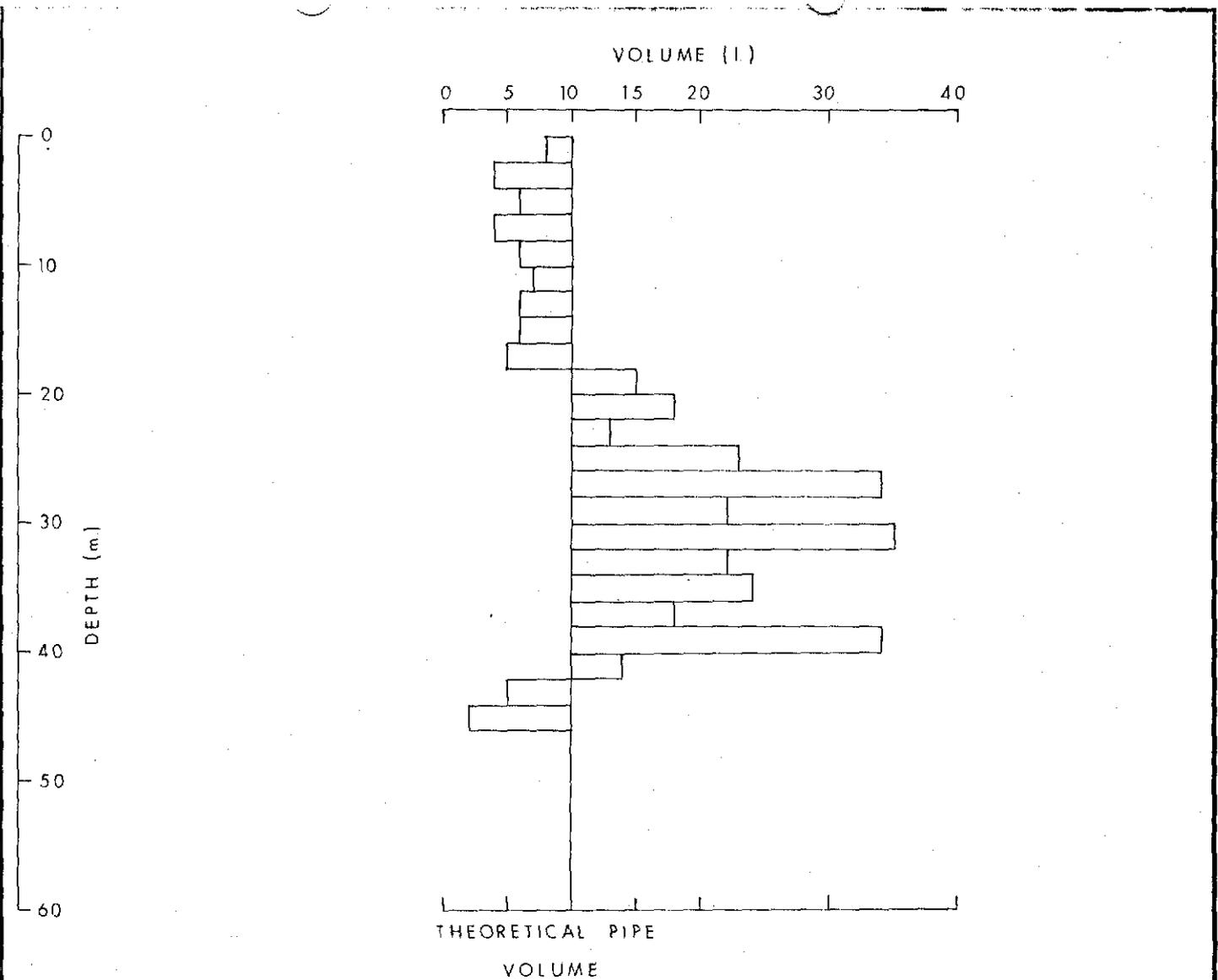
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HISTOGRAM

Drilling Method: WALLIS

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PIONEER, TASMANIA

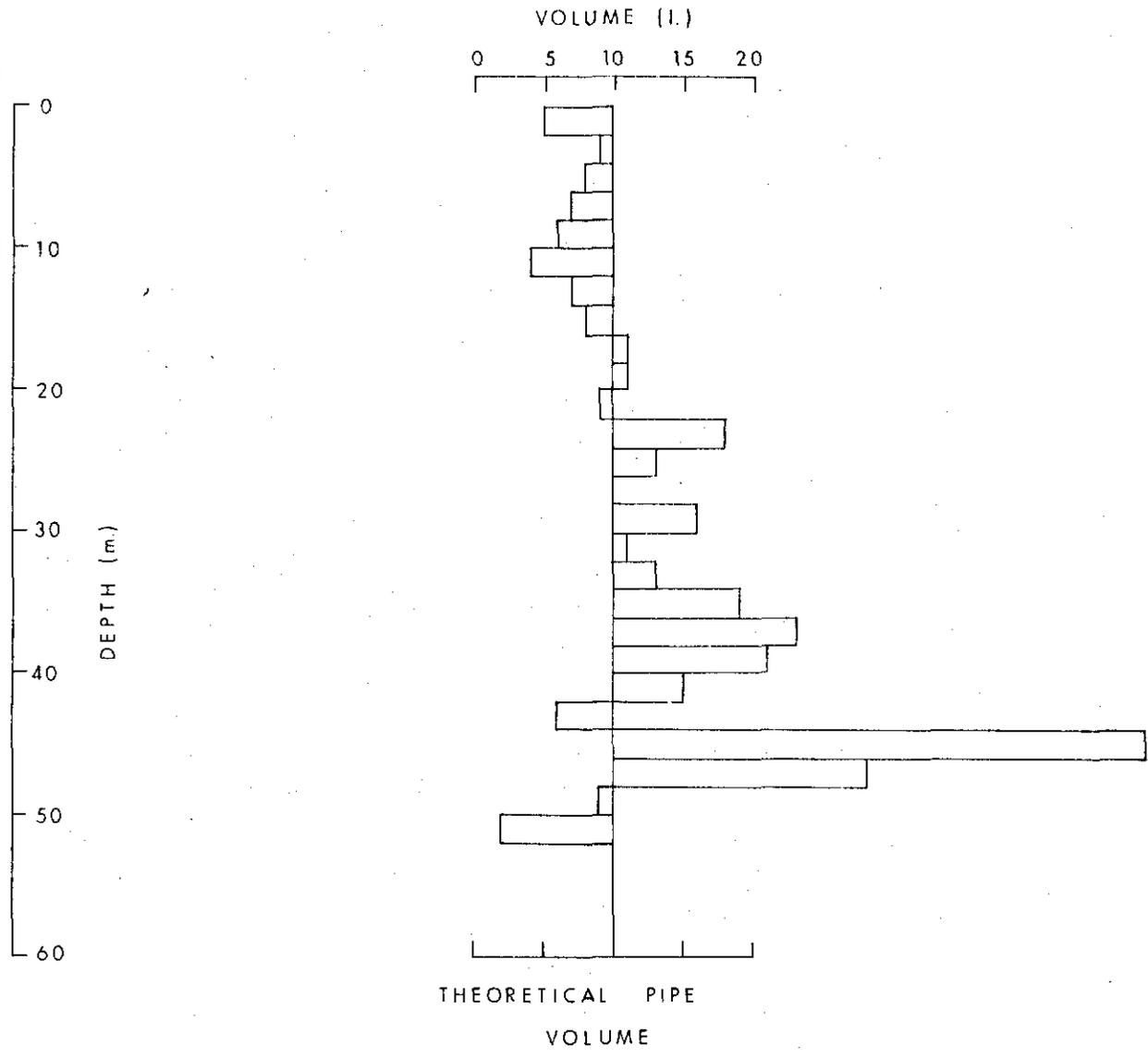
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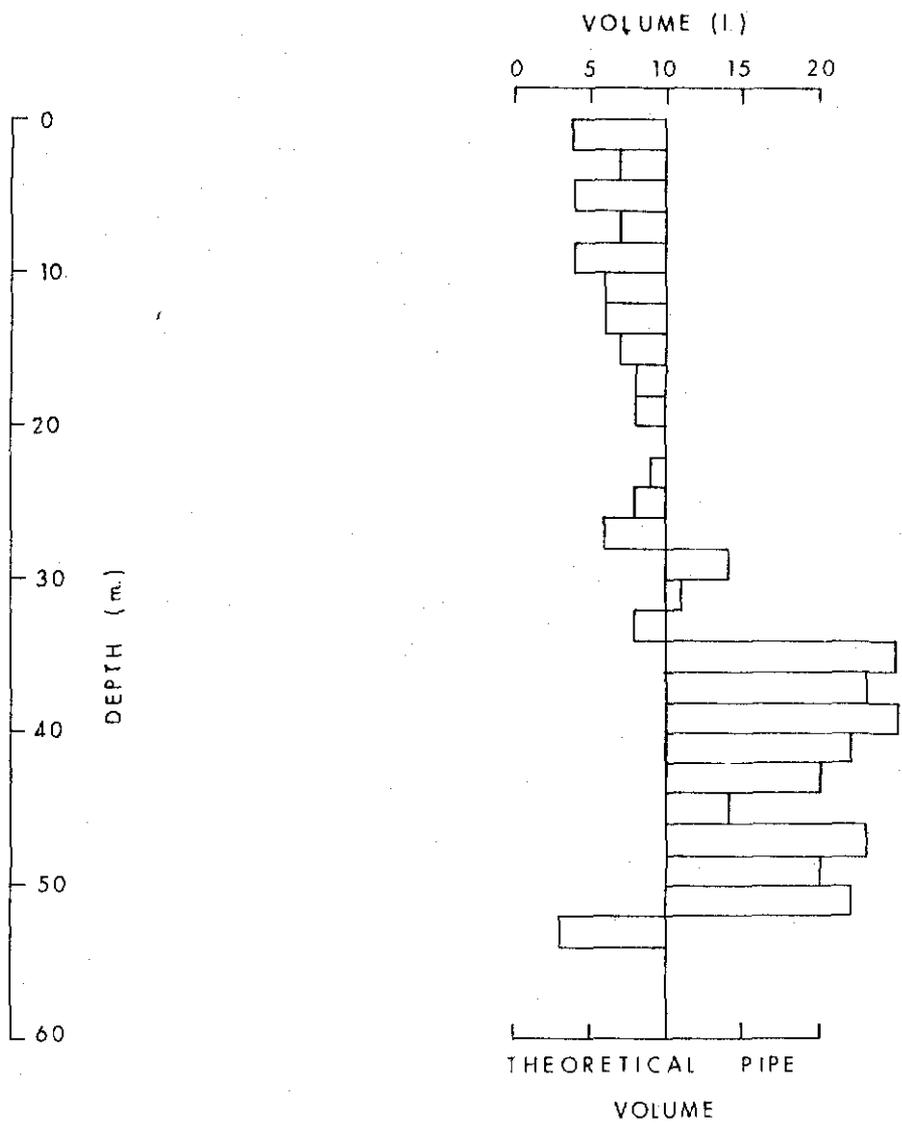
PIONEER, TASMANIA

K 163

RECOVERED VOLUME
HISTOGRAM

Drilling Method: WALLIS

Author: T. J. NEALE	Date: March, 1980	Dwg. No.:	
Drafting: B. G.	Report No.:	Base Plan:	



Amdex Mining Limited

PIONEER, TASMANIA

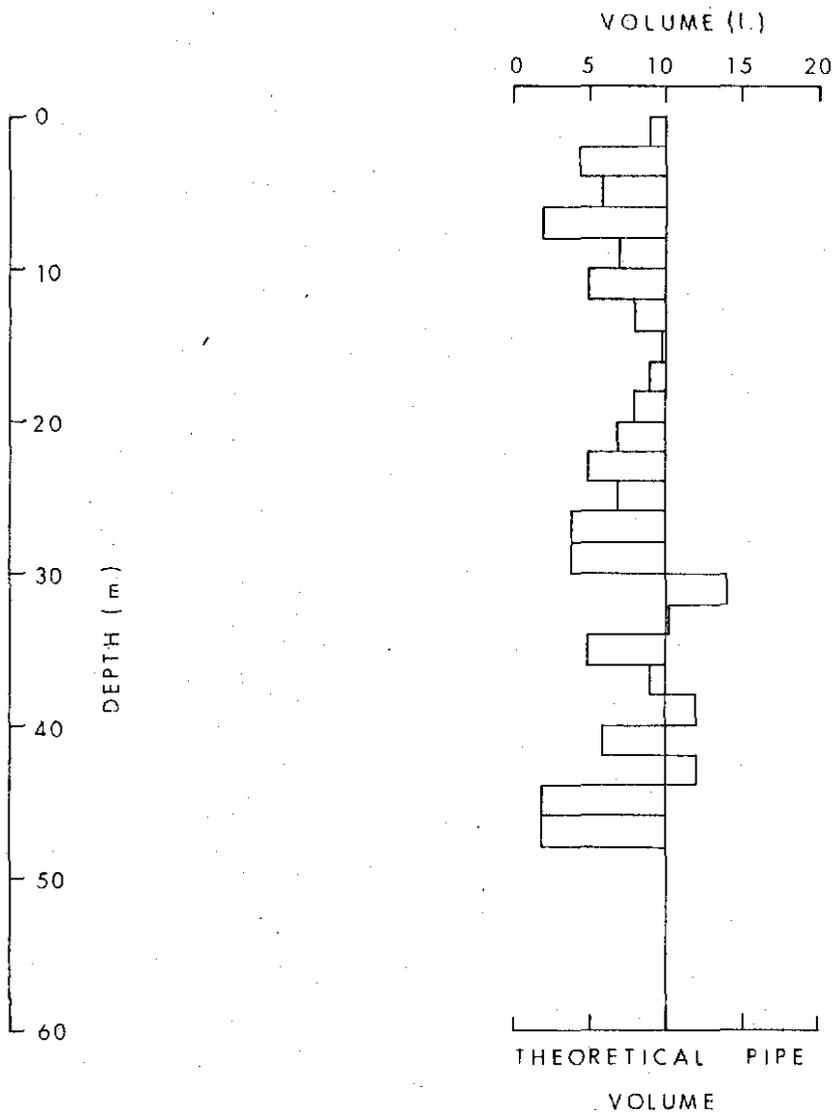
K 164

RECOVERED VOLUME

HISTOGRAM

Drilling Method: WALLIS

Author: T. I. NEALE	Date: March, 1980	Dwg. No.:	
Drafting: B. G.	Report No.:	Base Plan:	



Amdex Mining Limited

PIONEER, TASMANIA

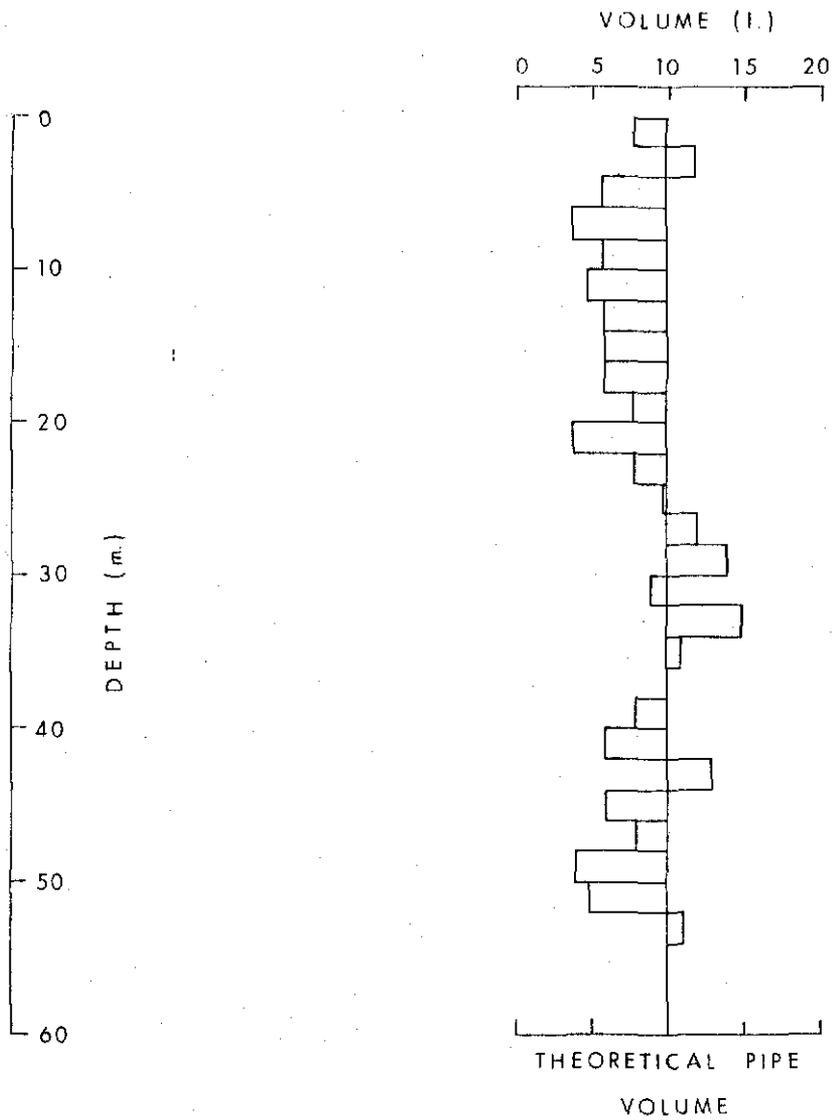
K 165

RECOVERED VOLUME

HISTOGRAM

Drilling Method: WALLIS

Author: T. I. NEALE	Date: March, 1980	Dwg. No.:	
Drafting: B. G.	Report No.:	Base Plan:	



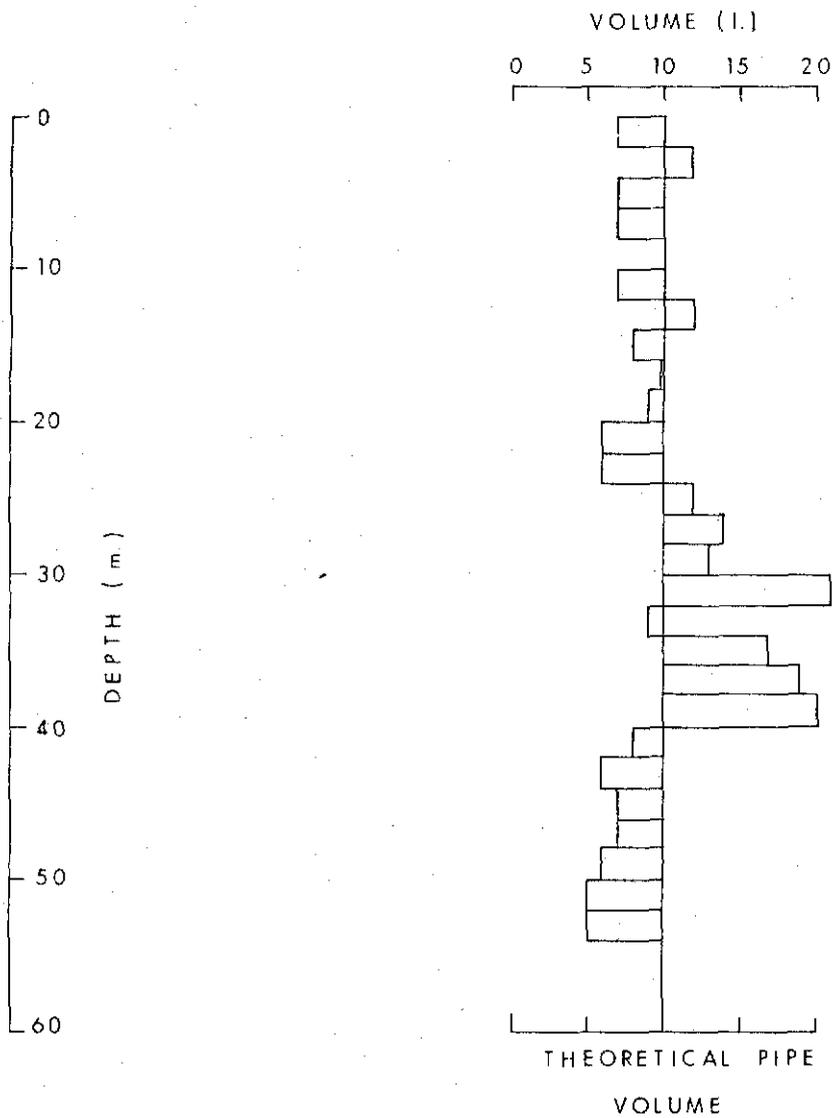
Amdex Mining Limited
 PIONEER, TASMANIA

K 166

**RECOVERED VOLUME
 HISTOGRAM**

Drilling Method: WALLIS

Author: T. J. NEALE	Date: March, 1980	Dwg. No.:	
Drafting: B.G.	Report No.:	Base Plan:	



Amdex Mining Limited

PIONEER, TASMANIA

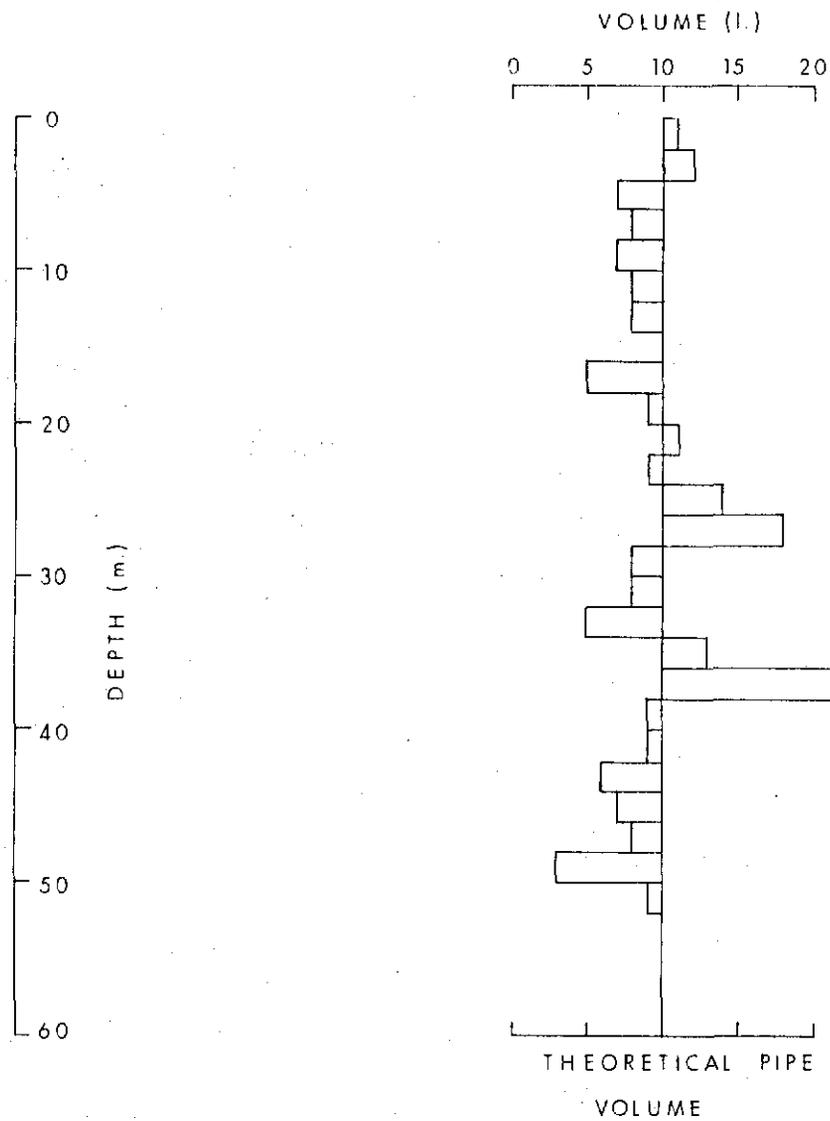
K 167

RECOVERED VOLUME

HISTOGRAM

Drilling Method: WALLIS

Author: T. I. NEALE	Date: March, 1980	Dwg. No.:	
Drafting: B.G.	Report No.:	Base Plan:	



Amdex Mining Limited

PIONEER, TASMANIA

K 168

RECOVERED VOLUME

HISTOGRAM

Drilling Method: WALLIS

Author: T. J. NEALE	Date: March, 1980	Dwg. No.:	
Drafting: B.G.	Report No.:	Base Plan:	

APPENDIX II

Pioneer Test
Drilling - Drill Logs

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: Hole No.: K 81 Collar Co-ordinates: mN mE Drilling Method:

Surface R.L.: m Basement R.L.: m Cutting Shoe / Bit diameter: Theoretical Volume: 40 litres

Date: Driller: Assistant: Sample Washer: Geologist:

Section	Metres	Sample No.	Recovered Volume (l)	Weight Conc. (g)	Conc. Assay (%Sn)	Recovered Tin (gSnO2)	Grade * gSnO2/m ³	Grade + gSnO2/m ³	Description of Sample
From	To								
0	2		30	4.17	8.42		17	11	
2	4		38	14.85	2.11		12	14	
4	6		38)			12	11	
6	8		33)			12	11	
8	10		26)			12	11	
10	12		28)	7 bulked samples		12	11	
12	14		38)	93.47	1.88	2.51	12	11
14	16		33)			12	11	
16	18		19)			12	11	
18	20		22	30.12	0.54	0.23	10	7	
20	22		21	24.56	2.0	0.7	33	22	
22	24		29)			19	19	
24	26		28)			19	19	
26	28		30)			19	19	
28	30		23)			19	19	

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 44.7 m. Grade from surface to inferred basement at m g SnO₂ / m³ *
 Total recovered volume, surface to basement l. at m g SnO₂ / m³ +
 Total recovered tin g SnO₂

047051

050

047052

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: Hole No.: K 81. Collar Co-ordinates: mN mE Drilling Method:

Surface R.L.: m Basement R.L.: m Cutting Shoe / Bit diameter: Theoretical Volume: 40 litres

Date: Driller: Assistant: Sample Washer: Geologist:

Section		Metres	Sample No.	Recovered Volume (l)	Weight Conc (g)	Conc. Assay (%Sn)	Recovered Tin (gSnO ₂)	Grade * gSnO ₂ /m ³	Grade + gSnO ₂ /m ³	Description of Sample
From	To									
30	32		24)				19	19	
32	34		22)				19	19	
34	36		29)	9 bulked samples			19	19	
36	38		32)	210.28	1.8	5.41	19	19	
38	40		26)				19	19	
40	42		18)	57.58	10.0	8.23	457	257	
42	44		22)	223.81	45	143.88	6540	4486	
44	46		30)	193.26	49.1	135.56	4519	4236	
46	48		19)	39.71	31.7	17.98	946	562	
48	50		18)	12.9	11.7	2.16	120	67	
50	51		8)	5.21	6.66	0.49	61	31	
)						
)						
)						
)						

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 44.7 m. Grade from surface to inferred basement at 46 m. 545 g SnO₂ / m³ *
 Total recovered volume, surface to basement 98 l. at 46 m. 432 g SnO₂ / m³ +
 Total recovered tin 318 g SnO₂

051

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

047053

Area: Hole No.: K.110. Collar Co-ordinates: mN mE Drilling Method:

Surface R.L.: m Basement R.L.: m Cutting Shoe / Bit diameter: Theoretical Volume: 50 litres

Date: Driller: Assistant: Sample Washer: Geologist:

Section		Sample No.	Recovered Volume (l)	Weight Conc. (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * (g SnO ₂ / m ³)	Grade + (g SnO ₂ / m ³)	Description of Sample
From	To								
0	2		32	2.68	22.2	0.85	27	21	
2	4		31				10	7	
4	6		20				10	7	
6	8		21				10	7	
8	10		28				10	7	
10	12		40				10	7	
12	14		21				10	7	
14	16		20	57.99	5.28	4.37	10	7	
16	18		29				10	7	
18	20		24				10	7	
20	22		35				10	7	
22	24		28				10	7	
24	26		46				10	7	
26	28		24				10	7	
28	30		35				10	7	

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 41 m. Grade from surface to inferred basement at m g SnO₂ / m³ *
 Total recovered volume, surface to basement l. at m g SnO₂ / m³ +
 Total recovered tin g SnO₂

052

047054

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: Hole No. K 110 Collar Co-ordinates: mN mE Drilling Method:

Surface R.L.: m Basement R.L.: m Cutting Shoe / Bit diameter: Theoretical Volume: 50 litres

Date: Driller: Assistant: Sample Washer: Geologist:

Section		Sample No.	Recovered Volume (l)	Weight Conc (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * g SnO ₂ / m ³	Grade + g SnO ₂ / m ³	Description of Sample
From	To								
30	32		31				10	7	
32	34		25				10	7	
34	36		29	11.02	34.9	5.49	189	137	
36	38		21	20.05	44.5	12.75	607	319	
38	40		22	113.52	53.3	86.44	3929	2161	
40	42		20	57	62.5	50.89	2544	1272	
42	44		11	13.5	34.3	6.62	602	165	
44	46		20	9.38	40.2	5.39	270	134	

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 41 m. Grade from surface to inferred basement at 42 m 384 g SnO₂ / m³ *
 Total recovered volume, surface to basement (inf.) 582l. at 42 m 206 g SnO₂ / m³ +
 Total recovered tin 172.8 g SnO₂

053

047055

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No: K.111 Collar Co-ordinates: mN mE Drilling Method: CABLE TOOL PERCUSSION

Surface R.L.: m Basement R.L.: m Cutting Shoe / Bit diameter: Theoretical Volume: 40 litres

Date: 18.1.80 Driller: Assistant: Sample Washer: Geologist: A. Fleming

Section	Metres	Sample No.	Recovered Volume (l)	Weight Conc. (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * (g SnO ₂ /m ³)	Grade + (g SnO ₂ /m ³)	Description of Sample
From	To								
0	2		25			0.97	39	30	
2	4		41			0.72	18	22	
4	6		26				6	5	
6	8		20			0.29	6	5	
8	10		31				12	9	
10	12		22				12	9	
12	14		22				12	9	
14	16		29			4.51	12	9	
16	18		28				12	9	
18	20		20				12	9	
20	22		27				12	9	
22	24		25				12	9	
24	26		24				12	9	
26	28		13				12	9	
28	30		20				12	9	

* Grade calculated by relating recovered volume to recovered tin. + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 51 m. (assumed) Grade from surface to inferred basement at m g SnO₂ / m³ *
 Total recovered volume, surface to basement l. at m g SnO₂ / m³ +
 Total recovered tin g SnO₂

054

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No: K 111 Collar Co-ordinates: mN mE Drilling Method: CABLE TOOL PERCUSSION

Surface R.L.: m Basement R.L.: m Cutting Shoe / Bit diameter: Theoretical Volume: 40 litres

Date: 18.1.80 Driller: Assistant: Sample Washer: Geologist: A. FLEMING

Section	Metres	Sample No.	Recovered Volume (l)	Weight Conc (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * (g SnO ₂ /m ³)	Grade + (g SnO ₂ /m ³)	Description of Sample
From	To								
30	32		25)	12	9	
32	34		30)	12	9	
34	36		25)	12	9	
36	38		25)	12	9	
38	40		22)	12	9	
40	42		17			0.47	28	15	
42	44		20			1.77	88.37	55	
44	46		19			37.24	1958	1163	
46	48		25			92.06	3686	2877	
48	50		33			108.25	3280	3379	
50	51		12		1431	28.97	2414	1811	
51	52		12		1664	5.4	450	337	
52	53		12			3.03	253	199	
53	54		14			2.54	181	158	

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad F = 80%
 Drillers reported basement at 51 m (assumed) Grade from surface to inferred basement at 52 m 468 g SnO₂ / m³ *
 Total recovered volume, surface to basement 638 l to 52 m at 52 m 365 g SnO₂ / m³ +
 Total recovered tin 277 g SnO₂

047056

055

047057

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No: K 150 Collar Co-ordinates: 52000 mN 77300 mE Drilling Method: REVERSE CIRCULATION

(Check hole at K 111)

WALLIS DRILLING CO.

Surface R.L.: 98.19 m Basement R.L.: 47.19 m Cutting Shoe / Bit diameter: 83 mm Theoretical Volume: 10.8 litres

Date: 18.1.80 Driller: A. Cameron Assistant: T. King Sample Washer: S. Moore Geologist: A. Fleming

Section		Sample No.	Recovered Volume (l)	Weight Conc. (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * g SnO ₂ /m ³	Grade + g SnO ₂ /m ³	Description of Sample
From	To								
0	2	C 9701	6	90.3	0.31	0.40	66.7	46	Coarse & fine sand, heavy drift; tr. fine tin, mon.
2	4	C 9702	7	75.5	0.23	0.25	35	29	Coarse & fine sand, white sandy clay; fine tin, mon.
4	6	C 9703	10	89.9	0.21	0.27	19	31	Coarse & fine sand, yellow clay; ilmenite, monazite
6	8	C 9704	4						" " " " " " " "
8	10	C 9705	10	Bulked 8-40 m, 16 samples		8	13	Coarse & fine sand, white clay; ilmenite	
10	12	C 9706	7	159	0.8	1.82	8	13	White sandy clay; trace tin and ilmenite
12	14	C 9707	10				8	13	Trace tin, ilmenite and monazite; coarse & fine sand, sdy clay, heavy drift
14	16	C 9708	10				8	13	Coarse & fine sand, white clay; ilmenite & monazite
16	18	C 9709	10				8	13	Coarse & fine sand, white clay; ilmenite & monazite
18	20.5	C 9710	11				8	13	Brown clay; monazite & ilmenite
20.5	22	C 9711	4				8	13	Sand, clay, organic silt; monazite & ilmenite
22	24	C 9712	18				8	13	Sand, clay, organic, silt; monazite, ilmenite, pyrite
24	26	C 9713	14				8	13	Sand, clay, organic silt; monazite & ilmenite
26	28	C 9714	16				8	13	Sand, clay; monazite & ilmenite
28	30	C 9715	17				8	13	Sand, brown clay, wood; ilmenite, monazite & pyrite

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad F = 80%
 Drillers reported basement at 51 m. Grade from surface to inferred basement at 52 m 317 g SnO₂ / m³ *
 Total recovered volume, surface to basement l. at m g SnO₂ / m³ +
 Total recovered tin g SnO₂

Dwg. no. : P 136 / 64

056

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No: K 150 Collar Co-ordinates: 52000 mN 77300 mE Drilling Method: REVERSE CIRCULATION
 (Check hole at K 111) WALLIS DRILLING CO.

Surface R.L. 98.19 m Basement R.L. 47.19 m Cutting Shoe / Bit diameter: 83 mm Theoretical Volume: 10.8 litres

Date: 18.1.80 Driller: A. Cameron Assistant: T. King Sample Washer: S. Moore Geologist: A. Fleming

Section	Metres	Sample No.	Recovered Volume (l)	Weight Conc (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * g SnO ₂ /m ³	Grade + g SnO ₂ /m ³	Description of Sample
From	To								
30	32	C 9716	18				8	13	Coarse & fine sand, brown clay, drift; mon., ilmenite
32	34	C 9717	28				8	13	" " " " " " " " "
34	36	C 9718	14				8	13	Coarse & fine sand, org. silt, wood; ilmen., mon.
36	38	C 9719	15				8	13	White clay, no heavy minerals
38	40	C 9720	13				8	13	Brown clay, no heavy minerals
40	42	C 9721	22	94.5	1.46	1.97	90	90	Coarse & fine sand, heavy drift, small wash; tin, ilmenite, monazite
42	44	C 9722	22	113.1	12.72	20.55	934	934	Coarse & fine sand, white clay; tin and ilmenite
44	46	C 9723	24	81.8	2.16	2.52	105	106	Coarse & fine sand, birds eye wash, drift, clay; tin & ilmenite
46	48	C 9724	8	138.1	16.7	32.95	4118	3813	Coarse & fine sand, birds eye wash, drift, clay; abundant tin and ilmenite
48	50	C 9725	15	119.9	17.64	30.21	2014	2014	Coarse & fine sand, birds eye wash, drift, clay; abundant tin and ilmenite
50	52	C 9726	10	120.7	2.76	4.76	475.9	551	Coarse & fine sand, granite; tin & ilmenite
52	54	C 9727	10	117.6	0.85	1.43	142.8	166	Decomposed granite; trace tin & ilmenite
54	56	C 9728	11	95.5	0.73	1.00	90.54	91	" " " " " "

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 51 m. Grade from surface to inferred basement at 52 m 317 g SnO₂/m³ *
 Total recovered volume surface to basement at 52 m 343 l at 52 m 313 g SnO₂/m³ +
 Total recovered tin 98.13 g SnO₂

98.13 g SnO₂ from 343 l = 286 g SnO₂/m³

047058

057

047059

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No.: K 150 Collar Co-ordinates: 52000 mN 77300 mE Drilling Method: REVERSE CIRCULATION
(Redrill) (Check hole at K 111) WALLIS DRILLING CO.

Surface R.L.: 98.19 m Basement R.L.: 47.19 m Cutting Shoe / Bit diameter: 83 mm Theoretical Volume: 10.8 litres

Date: 18.1.80 Driller: A. Cameron Assistant: T. King Sample Washer: B. Shean Geologist: A. Fleming

Section		Sample No.	Recovered Volume (l)	Weight Conc (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * g SnO ₂ / m ³	Grade + g SnO ₂ / m ³	Description of Sample
From	To								
0	2	C 9729	4	119.3	0.26	0.44	111	51	Black soil, coarse & fine sand; fine tin & monazite
2	4	C 9730	7	119.1	0.08	0.19	28	22	Coarse & fine sand, yellow clay; tr. fine tin & mon.
4	6	C 9731	7	98.7	0.14	0.20	18	12	Sand, clay; trace monazite
6	8	C 7932	4						
8	10	C 7933	6				7	8	Sand, silt; ilmenite & monazite
10	12	C 7934	6				7	8	Sand, heavy drift, clay; ilmenite & monazite
12	14	C 7935	6				7	8	Sand; trace ilmenite
14	16	C 7936	6				7	8	Sand, heavy drift; ilmenite & trace monazite
16	18	C 7937	9				7	8	Coarse & fine sand, clay; ilmenite & monazite
18	20	C 7938	8				7	8	Sand, clay, heavy drift; ilmenite & monazite
20	22	C 7939	10				7	8	Sand, brown clay; ilmenite
22	24	C 7940	7				7	8	" " " "
24	26	C 7941	8				7	8	Coarse & fine sand, organic silt; ilmenite, pyrite
26	28	C 7942	12				7	8	Sand, drift, organic silt, clay; ilmenite & monazite
28	30	C 7943	16				7	8	Sand, clay; ilmenite & monazite

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 51 m. Grade from surface to inferred basement at m g SnO₂ / m³ *
 Total recovered volume, surface to basement l. at m g SnO₂ / m³ +
 Total recovered tin g SnO₂

058

047060

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No: K 150 Collar Co-ordinates: 52000 mN 77300 mE Drilling Method: REVERSE CIRCULATION
 (Redrill) (Check hole at K 111) WALLIS DRILLING CO.
 Surface R.L.: 98.19 m Basement R.L.: 47.19 m Cutting Shoe / Bit diameter: 83 mm Theoretical Volume: 10,8 litres
 Date: 18.1.80 Driller: A. Cameron Assistant: T. King Sample Washer: B. Shean Geologist: A. Fleming

Section		Sample No.	Recovered Volume (l)	Weight Conc (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * g SnO ₂ / m ³	Grade + g SnO ₂ / m ³	Description of Sample
From	To								
30	32	C 9744	12				7	8	Sand, clay, drift; ilmenite
32	34	C 9745	13	Bulked 8-40 m			7	8	" " " "
34	36	C 9746	9	157.3	0.47	1.06	7	8	Sand, wood, organic silt; ilmenite & pyrite
36	38	C 9747	14				7	8	Clay, no heavy minerals
38	40	C 9748	8				7	8	" " " "
40	42	C 9749	9	117.9	0.23	0.39	43	45	Sand, clay, heavy drift, birds eye wash; mon. & ilm.
42	44	C 9750	19	90.1	1.1	1.42	83	83	Coarse & fine sand, white clay; trace tin, mon. & ilm.
44	46	C 9751	30	106.1	3.5	5.31	177	177	Sand, birds eye wash; trace tin & ilmenite
46	48	C 9752	12	138.9	37.1	73.62	6134	6134	Sand, clay, birds eye wash, heavy drift; abundant tin & ilmenite
48	50	C 9753	14	121.2	12.05	20.86	1490	1490	Sand, birds eye wash; abundant tin & ilmenite.
50	52	C 9754	5	107.2	0.48	0.74	147	86	Decomposed granite; trace tin & ilmenite
52	54	C 9755	5	140.0	0.20	0.40	80.0	46	" " " " " "

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 51 m. Grade from surface to inferred basement at 52 m 325 g SnO₂ / m³ *
 Total recovered volume, surface to basement at 52 m, 261 l at 52 m 319 g SnO₂ / m³ +
 Total recovered tin 104.63 g SnO₂

104.63 g SnO₂ from 261 l = 401 g SnO₂ / m³

059

047061

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No: K.151 Collar Co-ordinates: 52200 mN 77400 mE Drilling Method: REVERSE CIRCULATION
 (Check hole at K 110) WALLIS DRILLING CO.

Surface R.L.: 92.49 m Basement R.L.: 50.49 m Cutting Shoe / Bit diameter: 83 mm Theoretical Volume: 10.8 litres

Date: 19.1.80 Driller: A. Cameron Assistant: T. King Sample Washer: B. Shean Geologist: A. Fleming

Section		Sample No.	Recovered Volume (l)	Weight Conc (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * g SnO ₂ / m ³	Grade + g SnO ₂ / m ³	Description of Sample
From	To								
0	2	C 9756	4	102.5	0.55	0.8	200	93	Sand, brown cement; trace tin & ilmenite
2	4	C 9757	12	139.5	0.79	1.55	129	129	Sand, clay; trace monazite & ilmenite
4	6	C 9758	11				2	3	" " " " " "
6	8	C 9759	10				2	3	Clay, no heavy minerals
8	10	C 9760	12				2	3	Clay, trace sand, no heavy minerals
10	12	C 9761	10				2	3	Sand, clay; ilmenite, monazite
12	14	C 9762	12				2	3	Clay, sand; trace ilmenite & monazite
14	16	C 9763	8	16 bulked samples			2	3	Sand, clay; monazite & ilmenite
16	18	C 9764	5	Total volume 148 l			2	3	Coarse & fine sand, organic silt; ilmenite & pyrite
18	20	C 9765	8				2	3	Coarse & fine sand, organic silt; ilmenite & pyrite
20	22	C 9766	3				2	3	Sand, heavy drift; pyrite
22	24	C 9767	11				2	3	Sand, white clay, drift; ilmenite & monazite
24	26	C 9768	9				2	3	" " " " " " "
26	28	C 9769	10				2	3	Sand, white clay; ilmenite & monazite
28	30	C 9770	13				2	3	Sand, drift, clay; ilmenite & monazite

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 41 m. Grade from surface to inferred basement at 42 m 1735 g SnO₂ / m³ *
 Total recovered volume, surface to basement l. at m g SnO₂ / m³ +
 Total recovered tin g SnO₂

060

047062

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No: K 151 Collar Co-ordinates: 52200 mN 77400 mE Drilling Method REVERSE CIRCULATION

(Check hole at K 110) WALLIS DRILLING CO.

Surface R.L.: 92.49 m Basement R.L.: 50.49 m Cutting Shoe / Bit diameter: 83 mm Theoretical Volume: 10.8 litres

Date: 19.1.80 Driller: A. Cameron Assistant: T. King Sample Washer: B. Shean Geologist: A. Fleming

Section		Metres	Sample No.	Recovered Volume (l)	Weight Conc (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * (g SnO ₂ /m ³)	Grade + (g SnO ₂ /m ³)	Description of Sample
From	To									
30	32		C 9771	14				2	3	Sand, clay, heavy drift; ilmenite & monazite
32	34		C 9772	12				2	3	" " " " " " "
34	36		C 9773	16	105.3	0.23	0.35	2	3	Sand, peat bed, heavy drift, wash; trace tin & mon.
36	38		C 9774	11	95.3	8.22	11.19	10.7	10.7	Sand, clay, birds eye wash, heavy drift; tin, ilmenite & monazite
38	40		C 9775	12	198.7	40.00	113.5	9458	9458	Sand, heavy drift, birds eye wash, clay; large amount tin, ilmenite & monazite
40	42		C 9776	2)	84.7	50.12	74.56	24858	8630	Sand, clay, birds eye wash; abundant tin, ilmenite, & monazite
42	44		C 9777	1) ³	93.3	10.37				Sand, decomposed granite; trace tin & ilmenite
44	46		C 9778	4	127.5	0.34	0.34	0.62	155	Decomposed granite; trace tin & monazite
46	48		C 9779	4	127.6	0.75	1.39	31.8	161	" " " " " "

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad F = 80%
 Drillers reported basement at 41 m. Grade from surface to inferred basement at 42 m 1735 g SnO₂ / m³ *
 Total recovered volume, surface to basement at 42 m = 206 l at 42 m 936 g SnO₂ / m³ +
 Total recovered tin 203.96 g SnO₂

203.96 g SnO₂ from 206 l = 990 g SnO₂/m³

061

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

047063

Area: PIONEER Hole No: K 153 Collar Co-ordinates: 52550 mN 77000 mE Drilling Method: REVERSE CIRCULATION
 (Check hole at K 81) WALLIS DRILLING CO.

Surface R.L.: 91.06 m Basement R.L.: 46.06 m Cutting Shoe / Bit diameter: 83 mm Theoretical Volume: 10.8 litres

Date: 20.1.80 Driller: A. Cameron Assistant: T. King Sample Washer: B. Shean
S. Moore Geologist: A. Fleming

Section		Sample No.	Recovered Volume (l)	Weight Conc. (g)	Conc. Assay (%Sn)	Recovered Tin (g SnO ₂)	Grade * g SnO ₂ / m ³	Grade + g SnO ₂ / m ³	Description of Sample	
From	To									
0	2	C 9801	6)			6	6	Coarse & fine sand; trace monazite & ilmenite	
2	4	C 9802	6)			6	6	Coarse & fine sand, clay; trace monazite & ilmenite	
4	6	C 9803	8)			6	6	Sand, cement; trace monazite & ilmenite	
6	8	C 9804	5)			6	6	Sand, clay, drift; trace monazite & ilmenite	
8	10	C 9805	5)			6	6	Sand, heavy drift, small wash; trace ilmenite	
10	12	C 9806	6)	65.1	0.68	0.63	6	6	Sand, heavy drift, small wash, clay; trace ilmenite
12	14	C 9807	4)			6	6	Sand, clay; trace ilmenite & monazite	
14	16	C 9808	9)			6	6	Sand, clay; trace ilmenite	
16	18	C 9809	6)			6	6	" " " "	
18	20	C 9810	7)			6	6	Sand, clay, wood; trace ilmenite	
20	22	C 9811	8)			6	6	Sand, organic silt, drift; ilmenite	
22	24	C 9812	9)			6	6	Sand, organic silt, heavy drift, small wash; ilmenite	
24	26	C 9813	13)	109.4	0.33	0.52	40	40	Small-medium wash, clay, sand, pyrite; tr. tin, ilm.
26	28	C 9814	15)			18	18	Sand, small & med wash, clay; tr. fine tin & ilmenite	
28	30	C 9815	16)			18	18	" " " " " " " " " "	

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 45 m. Grade from surface to inferred basement at m g SnO₂ / m³ *
 Total recovered volume, surface to basement l. at m g SnO₂ / m³ +
 Total recovered tin g SnO₂

062

AMDEX MINING LIMITED - NORTH EAST TASMANIA DRILL LOG

Area: PIONEER Hole No: K 153 Collar Co-ordinates: 52550 mN 77000 mE Drilling Method: REVERSE CIRCULATION
 (Check hole at K 81) WALLIS DRILLING CO.

Surface R.L.: 91.06 m Basement R.L.: 46.06 m Cutting Shoe / Bit diameter: 83 mm Theoretical Volume: 10.8 litres

Date: 20.1.80 Driller: A. Cameron Assistant: T. King Sample Washer: B. Shean S. Moore Geologist: A. Fleming

Section		Metres	Sample No.	Recovered Volume (l)	Weight Conc. (g)	Conc. Assay (%Sn)	Recovered Tin (gSnO ₂)	Grade * gSnO ₂ /m ³	Grade + gSnO ₂ /m ³	Description of Sample	
From	To										
30	32		C 9816	12)			18	18	Sand, heavy drift, clay; ilmenite & monazite	
32	34		C 9817	21)	7 bulked samples		18	18	Sand, silty clay, small wash; pyrite & ilmenite	
34	36		C 9818	10)	173.6	0.74	1.84	18	18	Sand, wash, clay; pyrite, ilmenite
36	38		C 9819	21)			18	18	Sand, wash, heavy drift; pyrite, ilmenite	
38	40		C 9820	8)			18	18	Sand, clay, wash; pyrite, ilmenite	
40	42		C 9821	11		119.2	16.26	27.69	2517	2517	Sand, birds eye wash; abundant tin & ilmenite
42	44		C 9822	13		102.1	56.23	82.02	6309	6309	Sand, drift, birds eye wash; abundant tin & ilmenite
44	46		C 9823	4		90.7	6.14	7.96	1990	921	Sand, drift, minor small wash; tin, ilmenite
46	48		C 9824	6		95.9	3.84	5.26	877	651	Decomposed granite; trace tin, ilmenite, pyrite
Check sample-bearing material											
44	45			6		96.3					

* Grade calculated by relating recovered volume to recovered tin + Grade calculated by relating Radford factored theoretical volume to recovered tin Rad.F = 80%
 Drillers reported basement at 45 m Grade from surface to inferred basement at 46 m 338 g SnO₂ / m³ *
 Total recovered volume, surface to basement 223 l at 46 m 465 g SnO₂ / m³ +
 Total recovered tin 125.92 g SnO₂

047064

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